

Energy demand of electrochemical FA production

Table S1: Energy demand for the production of formic acid for different voltages and faradic efficiencies in kJ mol^{-1}

| Faradic efficiency → Voltage / V ↓ | 50% | 60% | 70% | 80% | 90% | 95% | 100% |
|--|--------|-------|-------|-------|-------|-------|-------|
| 1 | 385.9 | 321.6 | 275.7 | 241.2 | 214.4 | 203.1 | 193.0 |
| 1.5 | 578.9 | 482.4 | 413.5 | 361.8 | 321.6 | 304.7 | 289.5 |
| 1.7 | 656.1 | 546.8 | 468.6 | 410.1 | 364.5 | 345.3 | 328.1 |
| 1.8 | 694.7 | 578.9 | 496.2 | 434.2 | 385.9 | 365.6 | 347.3 |
| 1.9 | 733.3 | 611.1 | 523.8 | 458.3 | 407.4 | 385.9 | 366.6 |
| 2 | 771.9 | 643.2 | 551.3 | 482.4 | 428.8 | 406.3 | 385.9 |
| 2.1 | 810.5 | 675.4 | 578.9 | 506.5 | 450.3 | 426.6 | 405.2 |
| 2.2 | 849.1 | 707.6 | 606.5 | 530.7 | 471.7 | 446.9 | 424.5 |
| 2.3 | 887.7 | 739.7 | 634.0 | 554.8 | 493.1 | 467.2 | 443.8 |
| 2.4 | 926.3 | 771.9 | 661.6 | 578.9 | 514.6 | 487.5 | 463.1 |
| 2.5 | 964.9 | 804.0 | 689.2 | 603.0 | 536.0 | 507.8 | 482.4 |
| 2.6 | 1003.4 | 836.2 | 716.7 | 627.2 | 557.5 | 528.1 | 501.7 |
| 2.7 | 1042.0 | 868.4 | 744.3 | 651.3 | 578.9 | 548.4 | 521.0 |
| 2.75 | 1061.3 | 884.4 | 758.1 | 663.3 | 589.6 | 558.6 | 530.7 |

Table S2: Energetic efficiency for the production of formic acid for different voltages and faradic efficiencies in %

| Faradic efficiency → Voltage / V ↓ | 50% | 60% | 70% | 80% | 90% | 95% | 100% |
|--|------|------|------|-------|-------|-------|-------|
| 1 | 62.7 | 75.2 | 87.7 | 100.3 | 112.8 | 119.1 | 125.4 |
| 1.5 | 41.8 | 50.1 | 58.5 | 66.9 | 75.2 | 79.4 | 83.6 |
| 1.7 | 36.9 | 44.2 | 51.6 | 59.0 | 66.4 | 70.1 | 73.7 |
| 1.8 | 34.8 | 41.8 | 48.7 | 55.7 | 62.7 | 66.2 | 69.6 |
| 1.9 | 33.0 | 39.6 | 46.2 | 52.8 | 59.4 | 62.7 | 66.0 |
| 2 | 31.3 | 37.6 | 43.9 | 50.1 | 56.4 | 59.5 | 62.7 |
| 2.1 | 29.8 | 35.8 | 41.8 | 47.8 | 53.7 | 56.7 | 59.7 |
| 2.2 | 28.5 | 34.2 | 39.9 | 45.6 | 51.3 | 54.1 | 57.0 |
| 2.3 | 27.3 | 32.7 | 38.2 | 43.6 | 49.1 | 51.8 | 54.5 |
| 2.4 | 26.1 | 31.3 | 36.6 | 41.8 | 47.0 | 49.6 | 52.2 |
| 2.5 | 25.1 | 30.1 | 35.1 | 40.1 | 45.1 | 47.6 | 50.1 |
| 2.6 | 24.1 | 28.9 | 33.7 | 38.6 | 43.4 | 45.8 | 48.2 |
| 2.7 | 23.2 | 27.9 | 32.5 | 37.1 | 41.8 | 44.1 | 46.4 |
| 2.75 | 22.8 | 27.4 | 31.9 | 36.5 | 41.0 | 43.3 | 45.6 |

Neglected energy demands: heat losses to ambience, energy demand for provision of CO_2 .

Energy demand for the bicarbonate / formate approach

Table S3. Assumptions made for estimating energy demand of the bicarbonate / formate approach

| | | |
|--|------------|--|
| Concentration of formate / bicarbonate | 5 ± 1 M | based on Bi et al., 2014 ¹ |
| Ambient temperature | 20 °C | |
| Reaction temperature - charging | 40 ± 5 °C | based on Bi et al., 2014 ¹ |
| Charging pressure | 40 ± 5 bar | based on Bi et al., 2014 ¹ |
| Efficiency of compressor | 60 ± 5 % | |
| Conversion in hydrogenation reaction | 100 % | <i>Estimate</i> |
| Reaction temperature - discharging | 80 ± 5 °C | based on Papp et al, 2011 ² |
| Discharging pressure | 6 bar | based on Papp et al, 2011 ² |
| Conversion in dehydrogenation reaction | 100 % | <i>Estimate</i> |
| Assumptions for internal heat recovery: | | |
| <ul style="list-style-type: none"> ○ During charging: 50 % of the heat released during H₂ compression can be used for preheating ○ During discharging: the hot bicarbonate solution is used to preheat the cold formate solution entering the reactor; 20 K temperature that cannot be covered by internal heat integration | | |

Neglected energy demands: heat losses to ambience and energy demand for mixing and gas introduction.

Energy demand for catalytic decomposition of FA to H₂ and CO₂

Table S4. Assumptions made for estimating energy demand for catalytic hydrogen release from FA

| | | |
|---|-----------------------|---|
| Concentration of formate / bicarbonate | 4 ± 2 M | based on Fellay et al., 2008 ³ |
| Ambient temperature | 20 °C | |
| Reaction temperature | 80 ± 20 °C | based on Fellay et al., 2008 ³ |
| Share of water / formic acid evaporated | 10 ± 5 % 5 ± 2.5 % | <i>Estimate</i> |
| conversion | 100% | <i>Estimate</i> |
| Assumptions for internal heat recovery: | | |
| <ul style="list-style-type: none"> ○ Cold FA solution is preheated by cooling the hot streams leaving the reactor ○ It is assumed that 20 ± 10 K of the temperature difference must be provided externally, because of limitations in heat transfer | | |

Neglected energy demands: heat losses to ambience.

Energy demand for thermal decomposition of FA to H₂O and CO

Table S5. Assumptions made for estimating energy demand for thermal carbon monoxide release from FA

| | | |
|--|--------------|---|
| Ambient temperature | 20 °C | |
| Reaction temperature | 500 ± 100 °C | Estimate based on Blake et al., 1971 ⁴ |
| conversion | 100% | <i>Estimate</i> |
| Assumptions for internal heat recovery: | | |
| <ul style="list-style-type: none"> ○ Cold FA is preheated by cooling the hot stream leaving the reactor ○ It is assumed that 100 ± 25 K of the temperature difference must be provided externally, because of limitations in heat transfer | | |

Neglected energy demands: heat losses to ambience.

Data on direct formic acid fuel cells

Table S6: Crossover current data reported by Jeong et al.⁵ at 30 °C for a direct formic acid fuel cell membrane

| | no electric current | | electric current $j = 90 \text{ mA cm}^{-2}$ | | | electric current $j = 137 \text{ mA cm}^{-2}$ | | |
|---------------------|---------------------|-------------------------------------|---|-------------------------------------|-----------------------|--|-------------------------------------|-----------------------|
| c(FA) | Crossover current | molar Flux | Crossover current | molar Flux | loss due to crossover | Crossover current | molar Flux | loss due to crossover |
| mol L^{-1} | mA cm^{-2} | $\text{mol cm}^{-2} \text{ s}^{-1}$ | mA cm^{-2} | $\text{mol cm}^{-2} \text{ s}^{-1}$ | % | mA cm^{-2} | $\text{mol cm}^{-2} \text{ s}^{-1}$ | % |
| 2 | 20 | 1.0E-07 | | | | | | |
| 6 | 29 | 1.5E-07 | 13 | 6.7E-08 | 12.6 | | | |
| 10 | 51 | 2.6E-07 | 33 | 1.7E-07 | 26.8 | 35 | 1.8E-07 | 20.3 |
| 12 | 63 | 3.3E-07 | 40 | 2.1E-07 | 30.8 | 50 | 2.6E-07 | 26.7 |
| 15 | 92 | 4.8E-07 | 60 | 3.1E-07 | 40.0 | 60 | 3.1E-07 | 30.5 |

Table S7: Voltages of direct formic acid fuel cell membranes at different current densities reported in literature

| | | Ha et al., 2004 ⁶ | | | | Rice et al., 2002 ⁷ | Larsen et al., 2006 ⁸ | | Ortiz-Ortega et al., 2014 ⁹ | | |
|-----------------|----------------------|------------------------------|------|------|------|--------------------------------|----------------------------------|-------|--|------|------|
| | | maximum | 1.8M | 1.8M | 4.4M | | | | | | |
| Current density | mA cm^{-2} | 250 | 67 | 40 | 36 | | 650 | 290 | 0 | 150 | 200 |
| Power density | mW cm^{-2} | 33 | 17.8 | 16 | 14.2 | | 255 | 160 | 0 | 69 | 68 |
| Voltage | V | 0.13 | 0.27 | 0.40 | 0.39 | 0.72 | 0.39 | 0.55 | 0.89 | 0.46 | 0.34 |
| Electric energy | kJ mol^{-1} | 25.5 | 51.3 | 77.2 | 76.1 | 138.9 | 75.7 | 106.5 | 171.7 | 88.8 | 65.6 |
| Efficiency | % | 10.5 | 21.2 | 31.9 | 31.5 | 57.4 | 31.3 | 44.0 | 71.0 | 36.7 | 27.1 |

Neglected effects that might influence the efficiency of direct formic acid fuel cell:

- If the direct FAFC is fed with an aqueous solution of FA, the solvent water must be transported out of the cell to avoid its accumulation. This water will most likely transport a certain share of the FA out of the system.
- Ohmic losses
- Preheating (might be negligible, since the FAFC is operated near ambient temperature and the heat released by the cell seems to be sufficient).

Producing electricity from FA

Table S8: Assumptions made for estimating efficiency of electricity production from FA

| | | |
|--|--------------------------------|---|
| All assumption concerning the individual release options as described in the respective tables above | | |
| Provision of heat for decomposition | Partial combustion of hydrogen | |
| Energy demand for purification | 21.7 kJ mol ⁻¹ | PSA; based on Liu et al., 2011 ¹⁰ |
| Efficiency of fuel cell | 60 ± 10 % | based on DoE report for status 2015 ¹¹ |
| Efficiency of ICE for repowering CO | 37 ± 2 % | Based on Natkin et al., 2003 ¹² |

Table S9: Energy demand for hydrogen release and efficiency for electricity production from FA assuming electric heating for heat provision to the release step

| | energy demand / kJ mol ⁻¹ | | | | h _{FA→Electricity} / % | | | |
|----------------------------|---|------|-------------------------|------|--|------|-----------------------|------|
| | with heat recovery ± | | without heat recovery ± | | assuming electric heating; not considering purification | | | |
| | with heat recovery | ± | without heat recovery | ± | with heat recovery | ± | without heat recovery | ± |
| Catalytic (aqueous) | 65.69 | 18.9 | 108.10 | 32.8 | 32.8 | 12.7 | 15.3 | 16.8 |
| Catalytic (pure FA) | 20.41 | 1.4 | 24.37 | 2.2 | 51.6 | 10.0 | 49.9 | 10.0 |
| Bicarbonate | 40.54 | 13.6 | 77.00 | 19.1 | 43.2 | 11.5 | 28.2 | 12.7 |
| Biological | ? | ? | ? | ? | ? | ? | ? | ? |
| thermal | 53.73 | 1.7 | 80.30 | 6.3 | 14.8 | 2.1 | 3.8 | 3.0 |
| direct-FAFC | not applicable | | not applicable | | | | 24 | 5 |

Table S10: Efficiency of electricity production from FA assuming partial combustion of hydrogen to cover the energy demand of the release step

| | h _{FA→Electricity} / % | | | | h _{FA→Electricity} / % | | | |
|----------------------------|---|------|-----------------------|------|---|------|-----------------------|------|
| | assuming partial combustion of the gas; not considering purification | | | | assuming partial combustion of the gas; considering purification (PSA) | | | |
| | with heat recovery | ± | without heat recovery | ± | with heat recovery | ± | without heat recovery | ± |
| Catalytic (aqueous) | 43.7 | 10.7 | 33.2 | 14.6 | 34.7 | 11.4 | 24.2 | 15.2 |
| Catalytic (pure FA) | 54.9 | 9.2 | 54.0 | 9.0 | 46.0 | 10.1 | 45.0 | 9.9 |
| Bicarbonate | 49.9 | 10.0 | 40.9 | 10.4 | 49.9 | 10.0 | 40.9 | 10.4 |
| Biological | ? | ? | ? | ? | ? | ? | ? | ? |
| thermal | 30.0 | 1.7 | 26.5 | 2.9 | 30.0 | 1.7 | 26.5 | 2.9 |
| direct-FAFC | | | 24 | 5 | | | 24 | 5 |

Sensitivity analysis: Bicarbonate / Formate approach

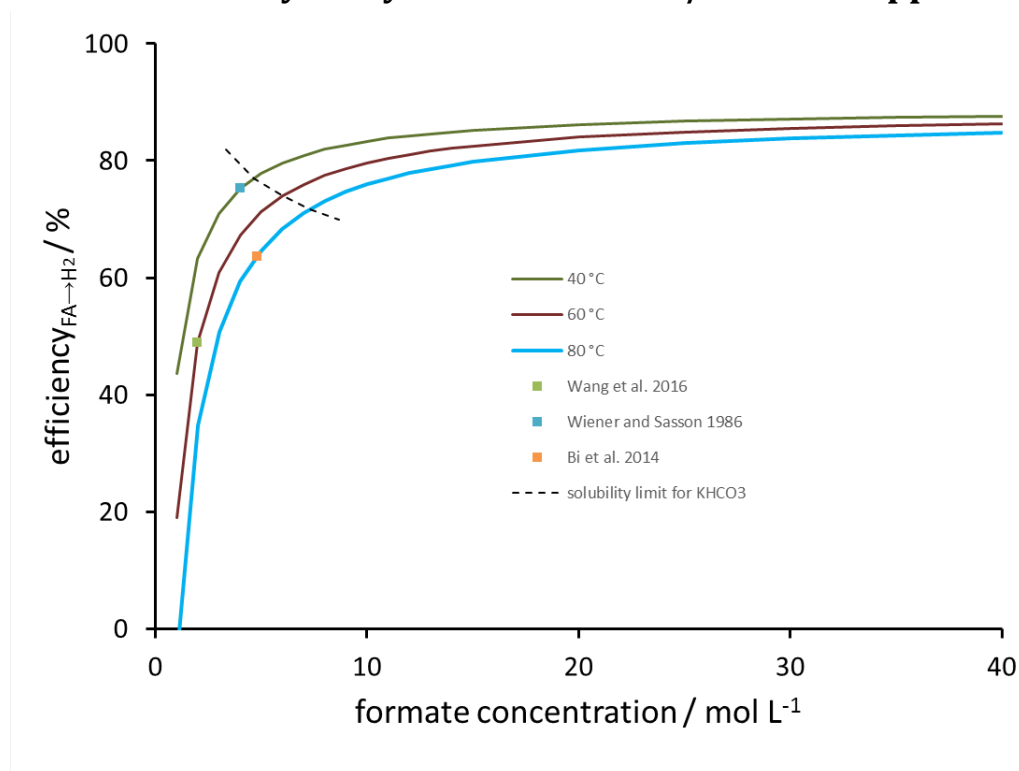


Figure S1: Efficiency of H_2 release from an aqueous solution of a formate salt as a function of concentration for different temperatures; added are three examples for concentrations/temperatures found in literature and the solubility limit for potassium bicarbonate

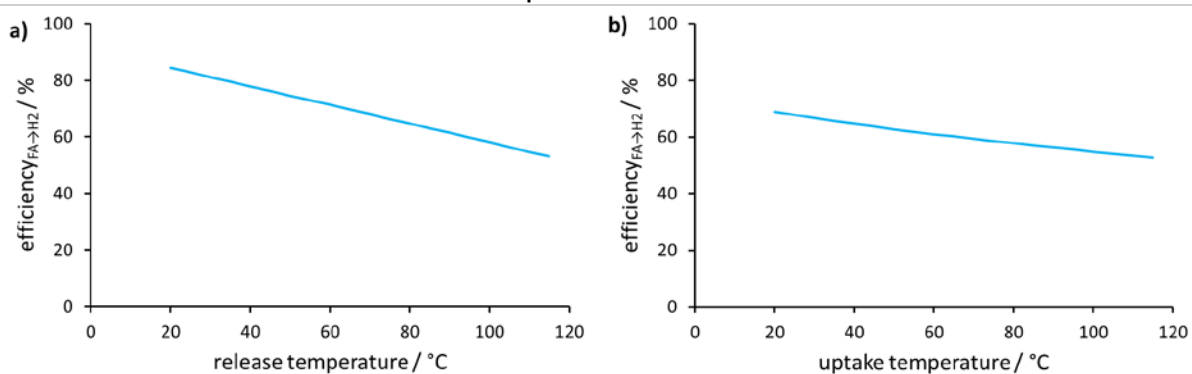


Figure S2: Efficiency of H_2 release from an aqueous solution of a formate salt as a function of a) temperature of hydrogen release and b) temperature of hydrogen uptake

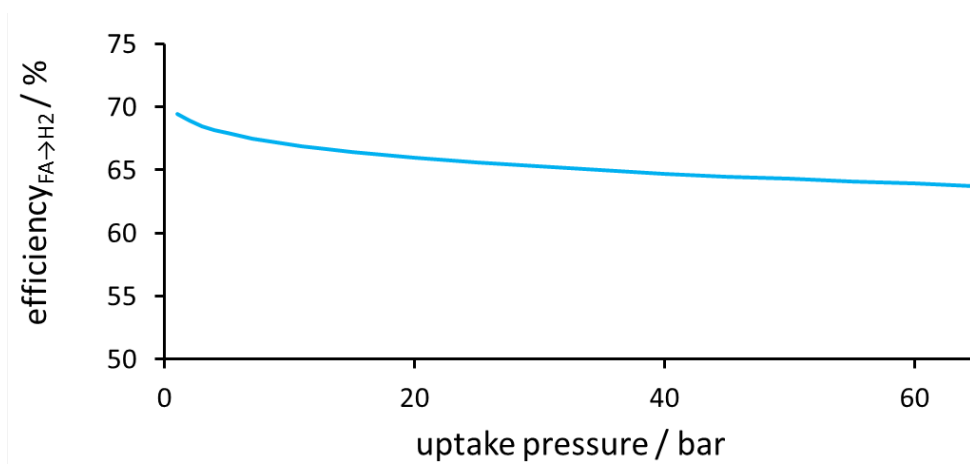


Figure S3 : Efficiency of H₂ release from an aqueous solution of a formate salt as a function of hydrogen pressure for the hydrogenation reaction of Bicarbonate to Formate

Sensitivity analysis: Catalytic decomposition of FA to H₂ and CO₂

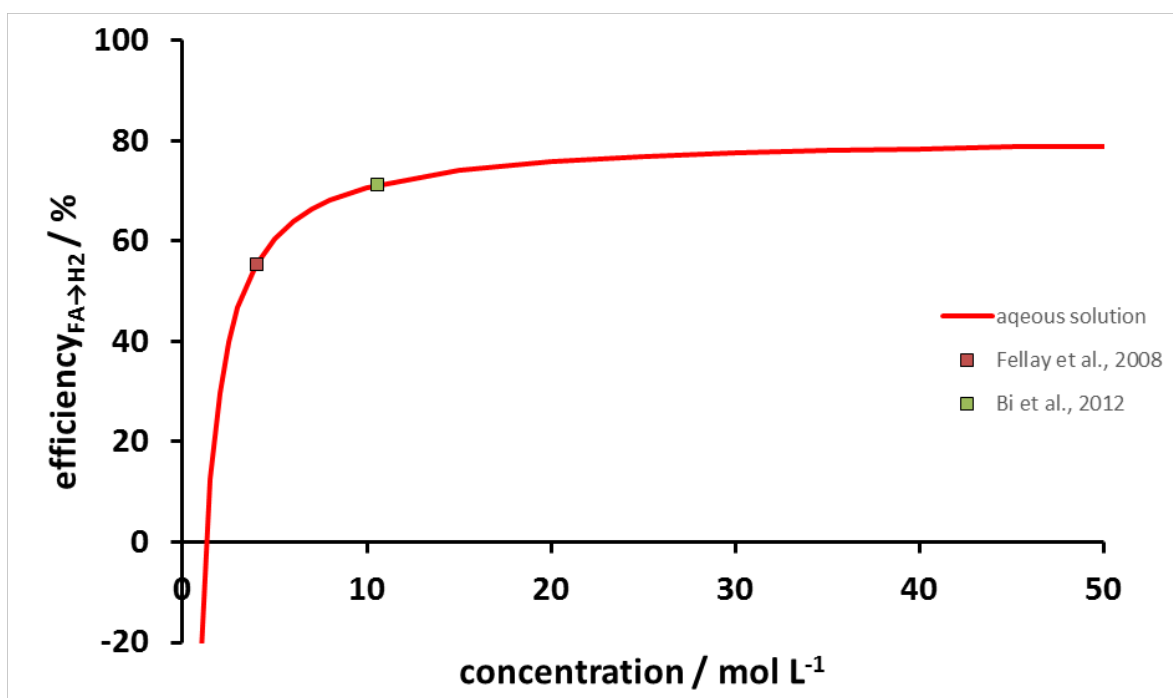


Figure S4: Efficiency of catalytic H₂ release from FA at 80 °C as a function concentration; added are two examples for concentrations found in literature

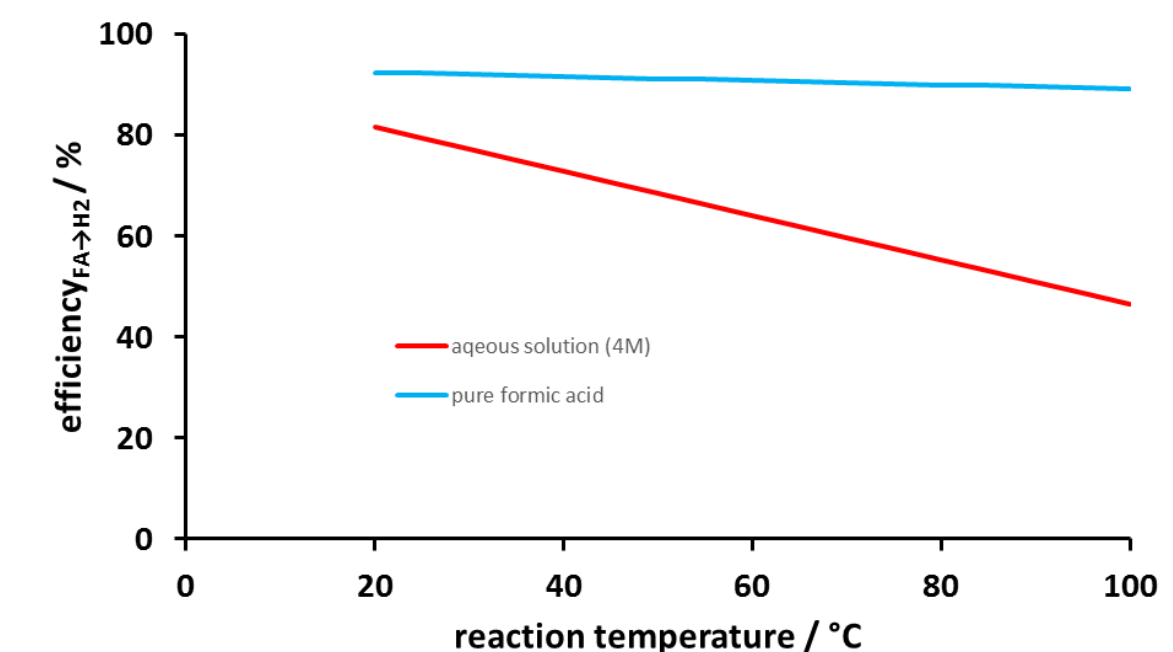


Figure S5: Efficiency of catalytic H₂ release from FC as function of reaction temperature

References for the supporting information

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