

## **SUPPORTING INFORMATION**

### **A Classic, Azo-Dye Agglomeration System: Evidence for Slow, Continuous Nucleation, Autocatalytic Agglomerative Growth, Plus the Effects of Dust-Removal by Microfiltration on the Kinetics**

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## S1 Derivation of the Kinetic Equations Employed in the Main Text

The kinetics derivation which follows refers back to Scheme 3 of the main text. The relevant kinetic equations, derived based on the mechanism provided in Scheme 3, are the following:

$$-\frac{d[A]}{dt} = \frac{d[B]}{dt} = \frac{1}{1/n} \frac{d[B_n]}{dt} = k_1[A] + k_2[A][B] \quad (S1)$$

Since the concentration of water does practically not change during the reaction the constant  $[H_2O]$  is absorbed into the apparent rate constants  $k_1$  and  $k_2$ .

What is actually monitored is the absorbance at 475 nm,  $A_{475}$ , assigned in the original 1978 publication<sup>1</sup> to the agglomerated dye,  $B_n$ . By Beer's law we can write the following equations: What we need are expressions for  $[A]_t$ ,  $[B]_t$ , and  $[B]_\infty$  in terms of  $A_{475}$  measurable.

$$A_{475} = \epsilon_{475} b [B_n], \text{ but since } [B] = 1/n [B_n], \text{ that is, } [B_n] = n [B] \quad (S2a)$$

$$A_{475} = \epsilon_{475} b n [B], \text{ or} \quad (S2b)$$

$$[B]_t = \frac{1}{nb\epsilon_{475}} (A_{475})_t \quad (S2c)$$

and since  $n[B]_\infty = [B_n]_\infty$  and for a reaction with single product by mass balance in eq 5 of Scheme 3 in the main text,  $[B]_\infty = [A]_o$

$$[A]_o = [B]_\infty = \frac{1}{nb\epsilon_{475}} (A_{475})_\infty \quad (S2d)$$

Next we need expressions for  $[A]_o$  and  $[A]_t$  in terms of  $A_{475}$  measurable. Our mass balance and initial reactant,  $[A]_o$ , vs final product,  $[B]_\infty$ , equations give us the needed results:

$$[A]_o = [A]_t + [B]_t \quad (S3a)$$

$$[A]_o = [B]_\infty \text{ so} \quad (S3b)$$

$$[A]_t = [B]_\infty - [B]_t \quad (\text{S3c})$$

Now combining eqs (S8c), (S7c) and (S7d) yields eq (S4):

$$[A]_t = \frac{1}{nb\epsilon_{475}} ((A_{475})_\infty - (A_{475})_t) \quad (\text{S4})$$

We can now combine eq (S4) with eq (S1) to yield eqs (S5)

$$\frac{d[B]}{dt} = \frac{1}{nb\epsilon_{475}} \frac{d(A_{475})}{dt} = \frac{1}{nb\epsilon_{475}} k_1 [(A_{475})_\infty - (A_{475})_t] + \left(\frac{1}{nb\epsilon_{475}}\right)^2 k_2 (A_{475})_t [(A_{475})_\infty - (A_{475})_t] \quad (\text{S5a})$$

Eq (S5a) simplifies to eq (S5b) by substituting  $(A_{475})$  for  $(A_{475})_t$

$$\frac{d(A_{475})}{dt} = k_1 [(A_{475})_\infty - (A_{475})] + \frac{1}{nb\epsilon_{475}} k_2 (A_{475})_t [(A_{475})_\infty - (A_{475})] \quad (\text{S5b})$$

or to eq (S5c) by substituting  $k'_2 = k_2/nb\epsilon_{475}$

$$\frac{d(A_{475})}{dt} = k_1 [(A_{475})_\infty - (A_{475})] + k'_2 (A_{475})_t [(A_{475})_\infty - (A_{475})] \quad (\text{S5c})$$

$$\text{where } k'_2 = k_2 \left(\frac{1}{nb\epsilon_{475}}\right) = k_2 \frac{1}{C_1}$$

$$C_1 = \text{constant} = nb\epsilon_{475} \text{ or } k_2 = (nb\epsilon_{475}) k'_2 = C_1 k'_2$$

Eq (S5c) looks exactly like the  $\frac{d[B]}{dt}$  form of eq (S1), repeated below, for which the integrated rate equation is eq (S6)

$$\frac{d[B]}{dt} = k_1[A] + k_2[A][B] \quad (\text{S1})$$

$$[B]_t = [A]_o \left(1 - \frac{k_1 + k_2[A]_o}{k_2[A]_o + k_1 e^{(k_1 + k_2[A]_o)t}}\right) \quad (\text{S6})$$

By analogy, the integrated rate equation for eq (S5b) is given eqs (S7a), (S7b), (S7c), and (S8):

$$[B]_t = \left( \frac{1}{nb\varepsilon_{475}} \right) (A_{475})_t = \frac{1}{C_1} (A_{475})_t \quad (S7a)$$

$$[A]_t = \frac{1}{nb\varepsilon_{475}} ((A_{475})_\infty - (A_{475})_t) = \frac{1}{C_1} ((A_{475})_\infty - (A_{475})_t) \quad (S7b)$$

$$[A]_0 = [B]_\infty = \frac{1}{nb\varepsilon_{475}} (A_{475})_\infty = \frac{1}{C_1} (A_{475})_\infty \quad (S7c)$$

The integration of eq (S5c) yields eq (S8):

$$(A_{475})_t = (A_{475})_\infty \left( 1 - \frac{k_1 + k'_2 (A_{475})_\infty}{k'_2 (A_{475})_\infty + k_1 e^{(k_1 + k'_2 (A_{475})_\infty)t}} \right) \quad (S8)$$

Comparing of eq (S8) to eq (S6) reveals that using the integrated rate equation (S8) for the product formation in terms of absorbance yields  $k'_2$  instead of  $k_2$  in the normal integrated rate equation (S6).

## References:

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<sup>1</sup> Reeves, R. L.; Harkaway, S. A.; Klingbiel, R. T. Phase transition autocatalysis of the hydrolysis of some esters of azo dyes, *J. Am. Chem. Soc.* **1978**, 100, 3879-3881.