

1 **Supporting Information for:**
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3 **Toxic Byproduct Formation during Electrochemical Treatment**
4 **of Latrine Wastewater**

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11 18 pages
12 9 figures
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41 **Analytical Methods.** HAAs and THMs were quantified by GC/MS (HP 6890 GC/HP
42 5973 MS). Disinfection by-products were separated by a Phenomenex Zebron ZB-WAX column
43 (30 m x 0.25 mm x 0.25 μ m df) using He at 1 mL min⁻¹ (6 psi). The injector was held at 200 °C
44 and a sample volume of 3 μ L (splitless) was used. For THMs, the oven was set at 30 °C (hold
45 for 2 min) and then ramped as follows: 5 °C min⁻¹ to 50 °C (hold 2 min); 35 °C min⁻¹ to 150 °C
46 (hold 5 min); 25 °C min⁻¹ to 185 °C (hold 5 min). For HAAs, the oven was set at 35 °C (hold for
47 10 min) and then ramped as follows: 5 °C min⁻¹ to 75 °C (hold 15 min); 40 °C min⁻¹ to 185 °C
48 (hold 5 min). Disinfection by-products were measured in single ion monitoring (SIM) mode at
49 the following mass to charge ratios and dwell times: chloroform (83; 100 ms);
50 bromodichloromethane (83; 100 ms); dibromochloromethane (129; 100 ms); bromoform (173;
51 100 ms); monochloroacetic acid (MCAA; 59; 250 ms), dichloroacetic acid (DCAA; 59; 250 ms),
52 and trichloroacetic acid (TCAA; 59; 250 ms).

53 **Average Number of Treatment Cycles before Discharge Calculation.** In off-the-grid
54 electrochemical wastewater treatment systems, treated wastewater can be used as flushing water
55 to reduce or eliminate water requirements. This design will result in parcels of water being
56 treated multiple times after flushing, potentially increasing electrochemical byproduct
57 concentrations prior to discharge. The average number of treatment cycles a parcel of water will
58 go through prior to discharge can be calculated according to:

59 cycles = $\frac{V_{\text{treated}}}{V_{\text{input}}} = \frac{V_{\text{input}} + V_{\text{flush}}}{V_{\text{input}}} \approx \frac{0.3 \text{ L} + 3 \text{ L}}{0.3 \text{ L}} = 11$ (S1)

60 where V_{treated} is the volume of water to be treated per use, which is the input volume of urine per
61 use (V_{input}) plus the volume of treated water used for flushing (V_{flush}). Typical values of 0.3 L of
62 urine per user and 3 L of treated water per flush were assumed.

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Table SI 1. Health guidelines for electrochemically produced by-products in drinking water measured in this study.

Contaminant	US EPA (μM)	WHO (μM)
Chlorate	2.5 ^{(1)a}	8.4 ^{(2)b}
Perchlorate	0.15 ^{(3)c}	0.7 ^{(4)d}
Nitrate	700 ^{(5)e}	3500 ^{(6)f}
Bromate	0.08 ^{(5)e}	0.08 ^{(7)b}
Contaminant	US EPA (mg L^{-1})	WHO (μM)
THMs ^g	0.08 ^{(8)e}	no guideline
Chloroform	no guideline	3 ^{(9)f}
Bromodichloromethane	no guideline	0.4 ^{(9)f}
Dibromochloromethane	no guideline	0.5 ^{(9)f}
Bromoform	no guideline	0.4 ^{(9)f}
HAA ₅ ^h	0.06 ^{(8)e}	no guideline
MCAA	no guideline	0.2 ^{(10)f}
DCAA	no guideline	0.4 ^{(11)d}
TCAA	no guideline	1 ^{(12)f}

65 ^aHealth reference level. ^bProvisional guideline. ^cHealth advisory. ^dDraft guideline. ^eMaximum
66 contaminant level. ^fGuideline. ^gSum of chloroform, bromodichloromethane, dibromochloromethane,
67 and bromoform. ^hSum of mono-, di-, and trichloroacetic acids and mono- and dibromoacetic acids.

Table SI 2. Summary of Electrochemical Byproduct Formation in Previous Studies.

Water Treated	Anode	Current Density (mA cm^{-2})	Membrane	$[\text{COD}]_{\text{init}}$ (mg L^{-1})	$[\text{Cl}]_{\text{init}}$ (mM)	$[\text{NH}_4^+]_{\text{init}}$ (mM)	$[\text{THM}]$ (mg L^{-1})	$[\text{HAA}]$ (mg L^{-1})	AOCl (μM)	$[\text{ClO}_3^-]$ (mM)	$[\text{ClO}_4^-]$ (mM)	$[\text{NO}_3^-]$ (mM)	Ref.	
RO ^a	BDD ^b	12.5	cation exchange	140	40	0.4	1.3 (1.3) ^c	3.8 (3.8) ^c	800 (250) ^c	-- ^d	--	--	13	
RO	BDD	12.5	cation exchange	150	4	--	1.1	8.8	--	--	--	--	14	
RO	BDD	12.5	cation exch., none	140	40	--	--	--	560 (200) ^c	--	--	--	15	
RO	BDD	2-20	none	130	20	8	0.2 (0.1) ^{c,e}	--	--	3.6 (1.8) ^{c,e}	--	2 (2) ^{c,e}	16	
RO	BDD	17	none	160	20	3	--	--	--	4 (4) ^c	--	--	17	
RO	BDD	10-30	none	180	20	3	--	--	--	4.2 (4.2) ^c	--	--	18	
RO	RuO_2^f	10-30	none	180	20	3	--	--	--	0.9	--	--	18	
RO	$\text{Ir}, \text{SnO}_2^g$	12.5	cation exchange	150	4	--	0.7	3.9	--	--	--	--	14	
RO	RuIrO_2^h	10	cation exchange	170	30	0.6	0.3 (0.1) ^e	2.8 (0.8) ^e	--	0.8 (0.2) ^e	0	--	19	
Domestic ⁱ	BDD	10, 20	cation exchange	--	10	--	--	--	20 (8) ^c	1.5 (0.1) ^c	1 (0.4) ^c	--	20	
Domestic	BDD	2.5-120	none	--	3	--	--	--	30 (0.4) ^j	0	0	--	21	
Landfill ^k	BDD	120-260	none	3400	70	90	2.1	--	--	--	--	--	4	22
Landfill	PbO_2^l	3.0	cation exchange	2800	130	2	--	--	560	--	--	--	23	
Latrine ^m	TiO_2^n	1.25	none	--	20	5	0.4	0.7	--	--	--	--	24	
Latrine	SbSn^o	25	none	250	30-60	10	--	--	--	10 (3) ^{c,e}	6 (6) ^{c,e}	5 (1) ^{c,e}	25	
OO leach. ^p	BDD	0.1, 0.3	none	1000	0.1	20	3.5 (2) ^c	--	--	--	--	--	26	
Drinking ^q	BDD	10-30	none	--	1	--	--	--	--	--	1	--	27	
Surface ^r	IrO_2^s	0-8	none	10	3	--	0.05 (0.03) ^j	0.1 (0.04) ^j	--	0	0	--	28	
GW ^t	RuIrO_2	11	none	30	2	--	--	--	70	--	--	--	29	
Urine	BDD	10-20	none	1710	35	133	3 (2) ^{c,u}	--	280	20 (20) ^c	30 (10) ^c	--	30	
Urine	TDIROF ^v	10-20	none	1710	35	133	1.3 ^u	--	370	28	28	--	30	

^aReverse osmosis retentate. ^bBoron-doped diamond. ^cMax conc. (conc. upon COD removal). ^dNot measured. ^eMax conc. (conc. upon NH_4^+ removal). ^f RuO_2/Ti . ^gPt-IrO₂/Ti or SnO₂-Sb/Ti. ^hRuIrO₂/Ti. ⁱDomestic wastewater. ^jMax conc. (conc. upon disinfection). ^kLandfill leachate. ^l PbO_2/Ti . ^mLatrine wastewater. ⁿ $\text{TiO}_2/\text{IrO}_2/\text{Ti}$. ^oSb-SnO₂/Co-TiO₂/IrO₂/Ti. ^pOlive oil leachate. ^qDrinking water. ^rSurface water. ^s IrO_2/Ti . ^tGroundwater. ^uOnly chloroform was measured. ^vThermally decomposed iridium oxide film.

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75**Table SI 3. Chemical Oxygen Demand (COD), Total Organic Carbon (TOC), and Total Inorganic Carbon (TIC) Concentrations during Electrolysis.**

Conditions	COD (mg O₂ L⁻¹)	TOC (mg C L⁻¹)	TIC (mM)
TiO ₂ /IrO ₂ ^a 2.5 A L ⁻¹ 30 mM Cl ⁻	0 h: 510	0 h: 142	0 h: 50
	6 h: 440		
	12.5 h: 370	12.5 h: 112	12.5 h: 6
TiO ₂ /IrO ₂ ^a 5.0 A L ⁻¹ 30 mM Cl ⁻	0 h: 510	0 h: 142	0 h: 50
	3 h: 400		
	9 h: 360	9 h: 82	9 h: 3
TiO ₂ /IrO ₂ ^a 7.5 A L ⁻¹ 30 mM Cl ⁻	0 h: 610	0 h: 142	0 h: 51
	6 h: 296	6 h: 86	6 h: 2
TiO ₂ /IrO ₂ ^b 7.5 A L ⁻¹ 65 mM Cl ⁻	0 h: 610	0 h: 152	0 h: 51
	6 h: 164	6 h: 83	6 h: 4
TiO ₂ /IrO ₂ ^b 7.5 A L ⁻¹ 100 mM Cl ⁻	0 h: 432	0 h: 178	0 h: 52
	4 h: 184	4 h: 128	4 h: 4
	12 h: <LOD ^c	12 h: 122	12 h: 4
BDD ^d 4 A L ⁻¹ 30 mM Cl ⁻	0 h: 437	0 h: 149	0 h: 55
	1 h: 120		
	2 h: <LOD ^c		
	4 h: <LOD ^c		
	6 h: <LOD ^c	6 h: 12	6 h: 1
NaOCl addition ^e	0 h: 510	0 h: 147	0 h: 54
	2 h: 410		
	4 h: 270		
	6 h: 110	6 h: 117	6 h: 19

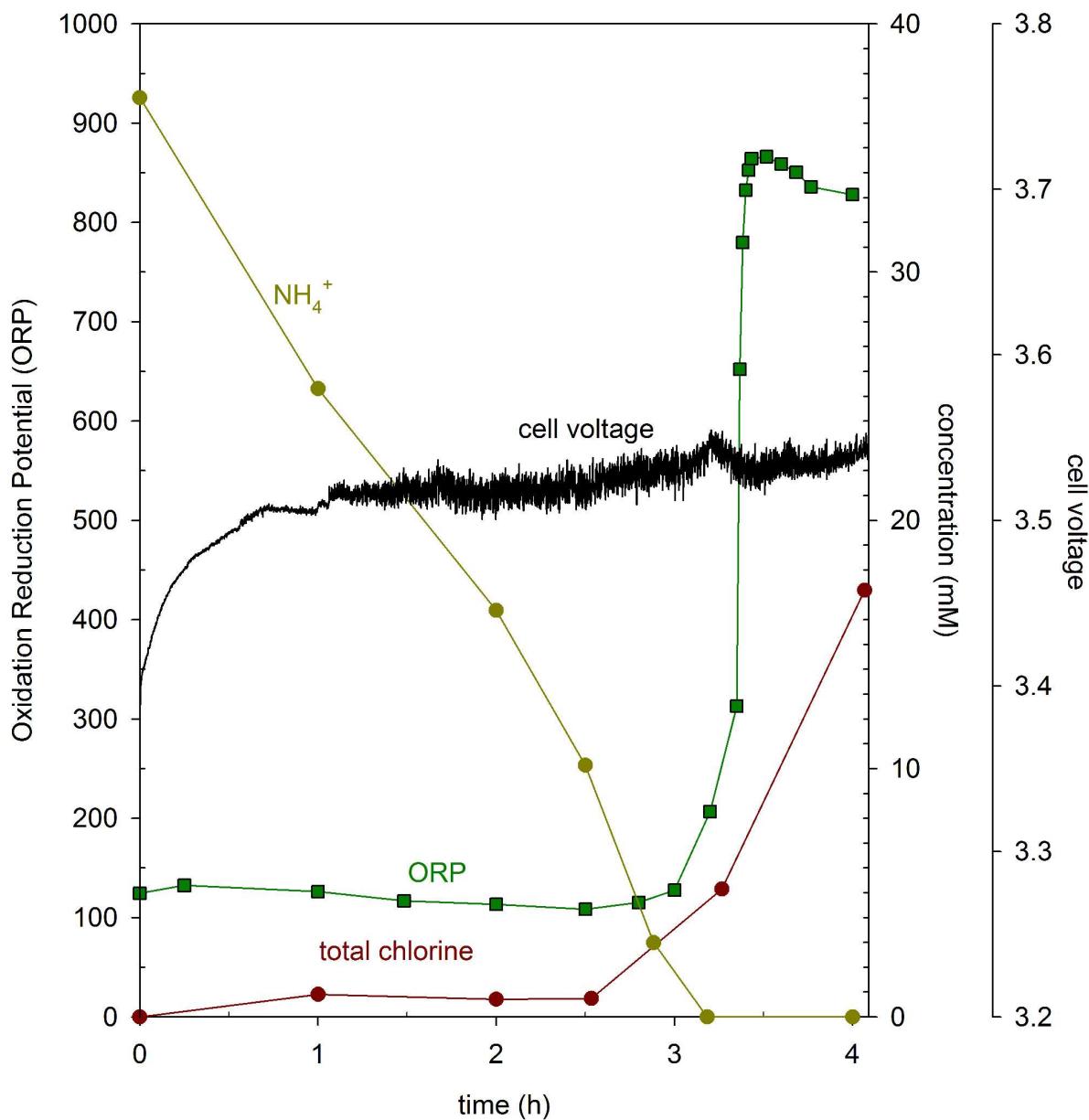
76 ^a See Figure 2 of main manuscript and Figure SI 4 for concentrations of other species. ^c See Figure 3 of
77 main manuscript and Figure SI 5 for concentrations of other species. ^c Limit of detection (LOD) was 30
78 ppm O₂. ^d See Figure 4 of main manuscript for concentrations of other species. ^e See Figure 6 of main
79 manuscript for concentrations of other species.
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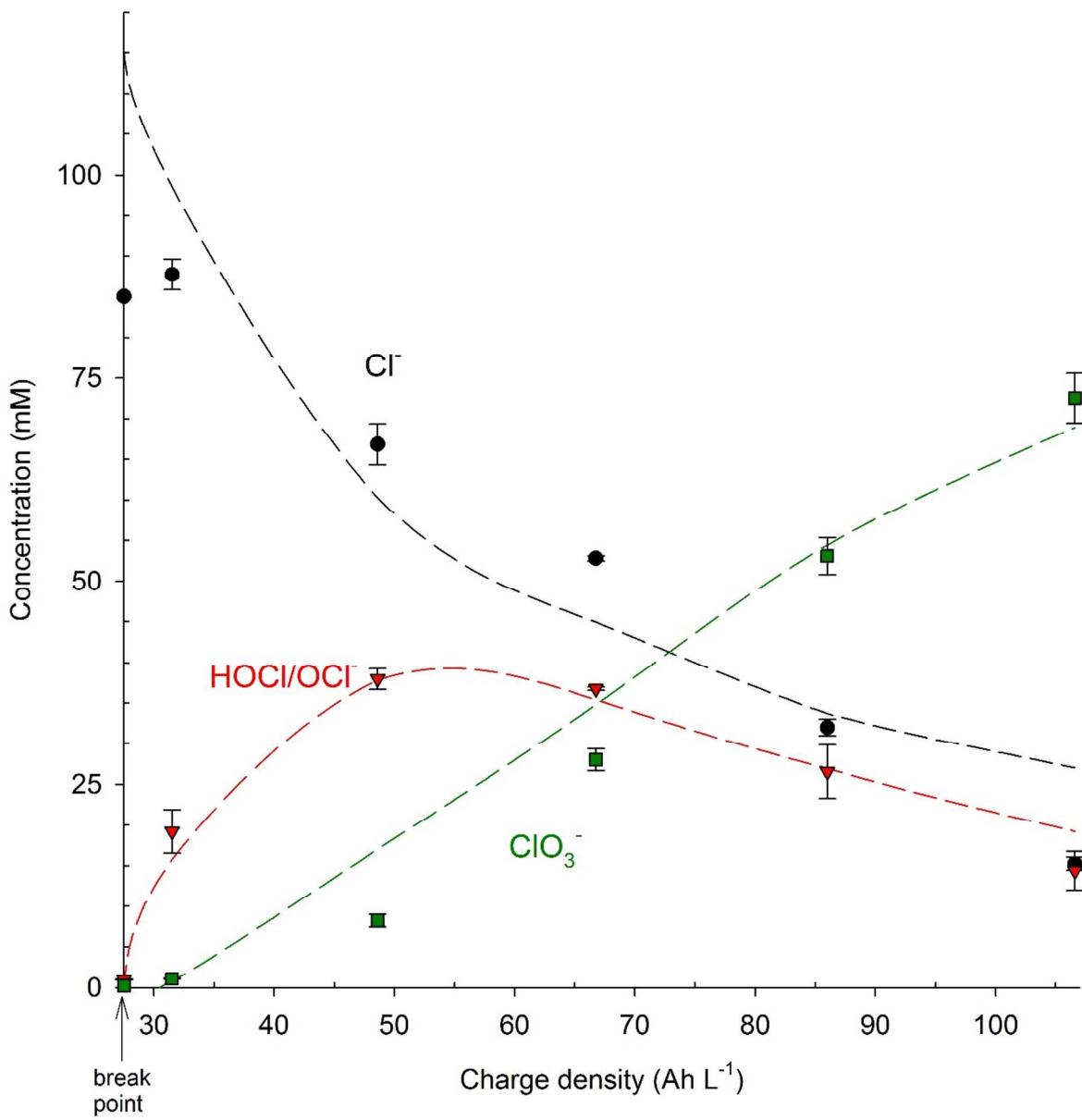
Table SI 4. Measured HAA Electrolysis Rates on BDD Anodes.^a

HAA	$k_{\text{borate}}^{\text{b}} (\text{Ah L}^{-1})$	$k_{\text{latrine}}^{\text{c}} (\text{Ah L}^{-1})$	$k_{\text{borate}}^{\text{b}} (\text{s}^{-1})$	$k_{\text{latrine}}^{\text{c}} (\text{s}^{-1})$
MCAA	$12.7 \pm 0.4 \times 10^{-2}$	$26 \pm 1 \times 10^{-2}$	$1.9 \pm 0.1 \times 10^{-4}$	$2.0 \pm 0.2 \times 10^{-4}$
DCAA	$8.2 \pm 1.0 \times 10^{-2}$	$25 \pm 1 \times 10^{-2}$	$2.2 \pm 0.1 \times 10^{-4}$	$1.3 \pm 0.1 \times 10^{-4}$
TCAA	$8.4 \pm 2.5 \times 10^{-2}$	$35 \pm 1 \times 10^{-2}$	$2.2 \pm 0.1 \times 10^{-4}$	$1.4 \pm 0.3 \times 10^{-4}$

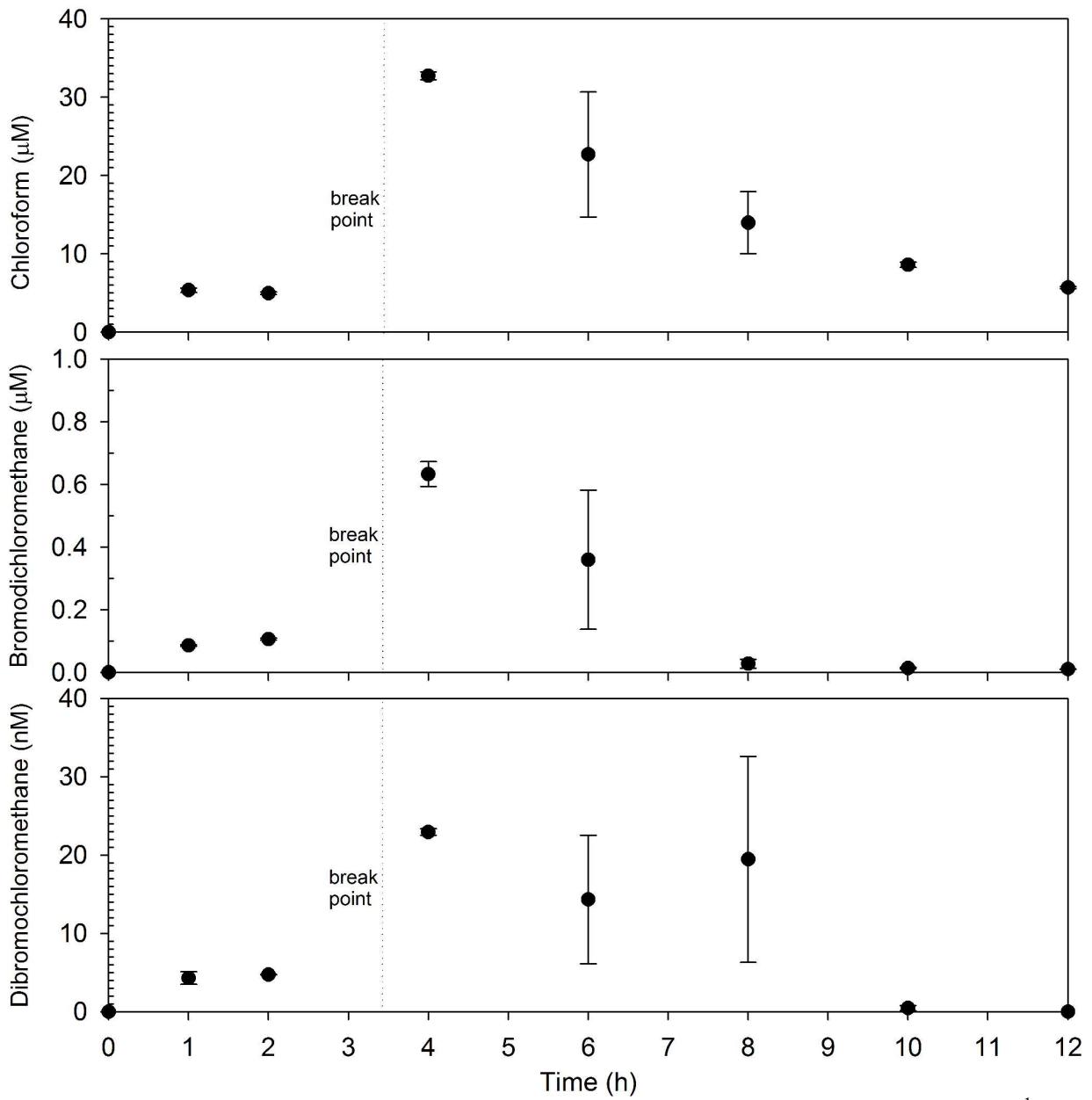
82 ^aHAA concentrations are shown in Figure 5 of main manuscript. ^bBorate buffer solution. ^cLatrine
 83 wastewater.



85
86 Figure SI 1. Oxidation reduction potential (ORP), total chlorine concentration, cell voltage, and
87 ammonium concentration during electrolysis of latrine wastewater amended with sodium
88 chloride ($\text{TiO}_2/\text{IrO}_2$ anodes; 7.5 A L^{-1} ; $[\text{Cl}^-]_{\text{initial}}=100 \text{ mM}$). Near the breakpoint (complete
89 ammonium removal; $\sim 3.2 \text{ h}$), total chlorine concentrations and ORP spiked. At the same point,
90 cell voltage showed a distinct peak. Lines added for clarity.
91

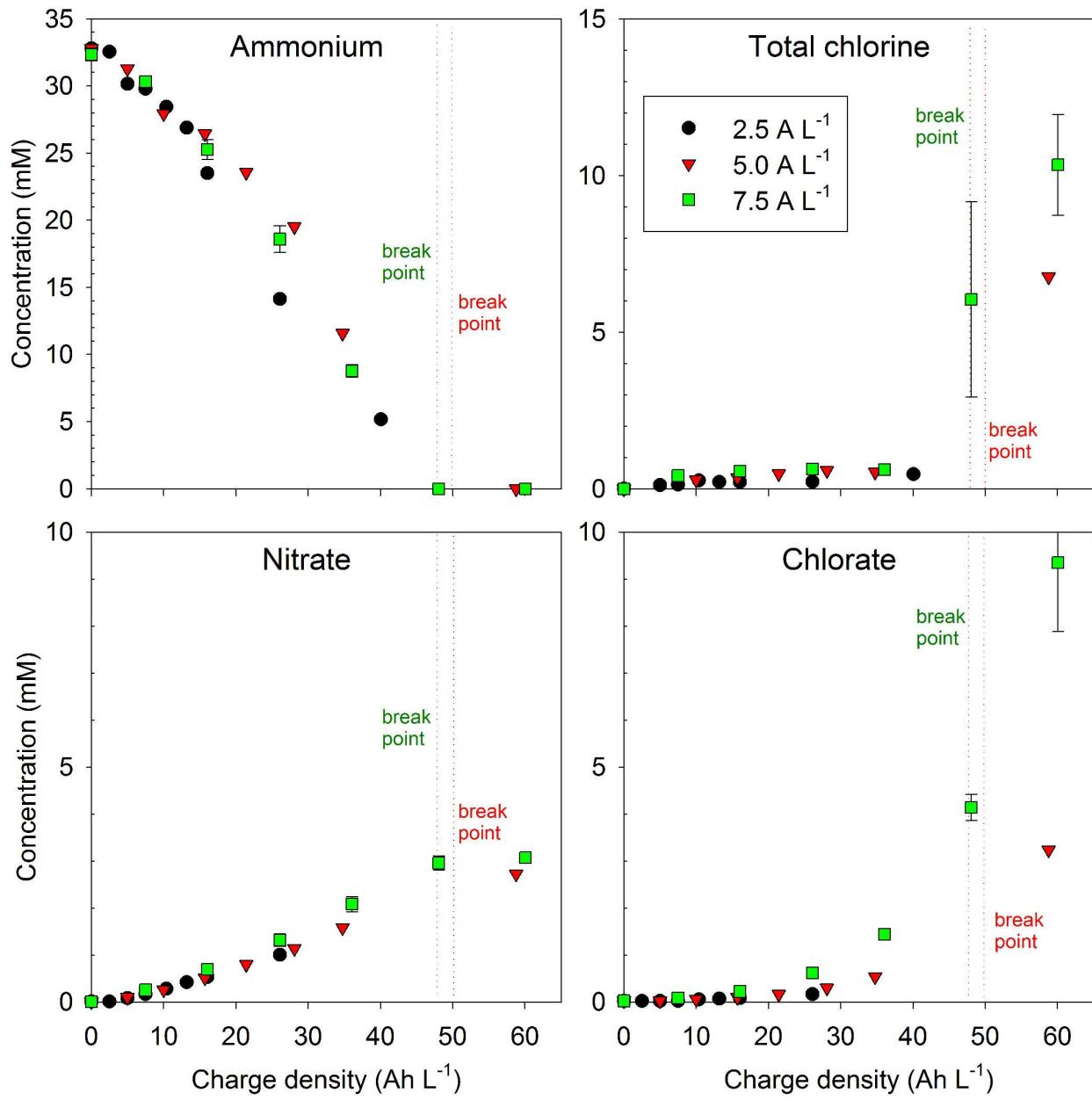


92
 93 Figure SI 2. Concentrations of measured (symbols) and modeled (dashed lines) chlorine species
 94 following the breakpoint during electrolysis of latrine wastewater on $\text{TiO}_2/\text{IrO}_2$ anodes at
 95 7.5 A L^{-1} . Reaction rate constants were obtained by fitting reactions
 96 $(2\text{Cl}^- + \text{H}_2\text{O} \xrightarrow{k_1} \text{OCl}^- + \text{Cl}^- + 2\text{H}^+ + 2\text{e}^-; \text{OCl}^- + 2\text{H}_2\text{O} \xrightarrow{k_2} \text{ClO}_3^- + 4\text{H}^+ + 4\text{e}^-)^{25}$ to the
 97 experimental data ($k_1 = 0.35 \text{ M}^{-1} (\text{Ah L}^{-1})^{-1}$; $k_2 = 0.030 (\text{Ah L}^{-1})^{-1}$). See Figure 1 of main
 98 manuscript for concentrations of other species.
 99



100
101 Figure SI 3. Trihalomethane concentrations during electrolysis ($\text{TiO}_2/\text{IrO}_2$ anodes; 7.5 A L^{-1} ;
102 3.8 V) of latrine wastewater amended with sodium chloride ($[\text{Cl}^-]=100 \text{ mM}$). Bromoform was
103 not detected. Dotted lines indicate where the chlorination breakpoint was reached (i.e., complete
104 ammonium removal).

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106

107 Figure SI 4. Ion and inorganic byproduct concentrations during electrolysis of latrine wastewater
 108 at various current densities with TiO₂/IrO₂ anodes. Average cell voltages: 2.5 A L⁻¹: 3.6 V;
 109 5.0 A L⁻¹: 4.0 V; 7.5 A L⁻¹: 4.4 V. Dotted lines indicate where the chlorination breakpoint was
 110 reached (i.e., complete ammonium removal).

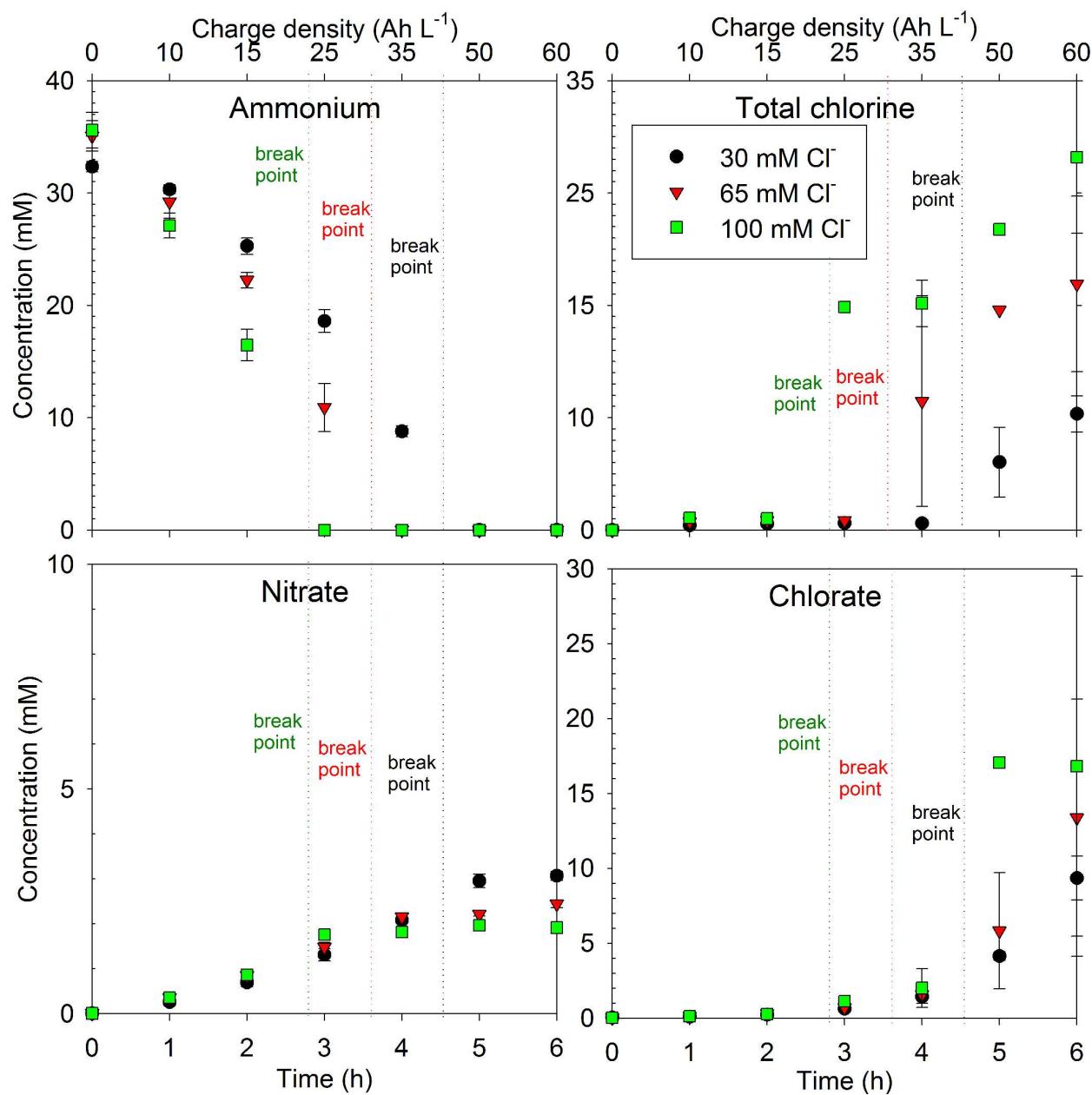
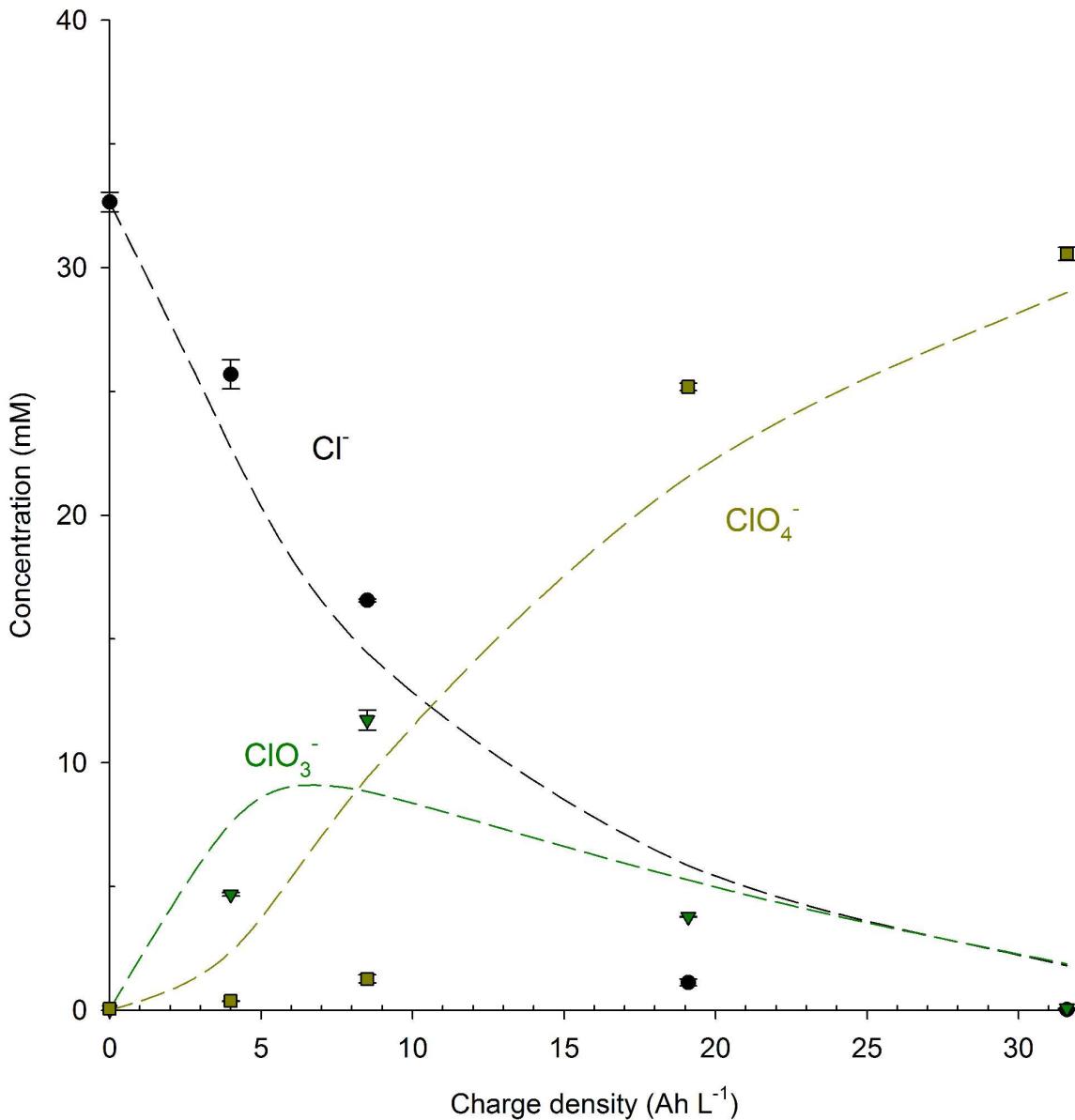


Figure SI 5. Ion and inorganic byproduct concentrations during electrolysis of latrine wastewater at various chloride concentrations with TiO₂/IrO₂ anodes at 7.5 A L⁻¹. Average cell voltages: 30 mM Cl⁻: 4.4 V; 65 mM Cl⁻: 4.0 V; 100 mM Cl⁻: 3.9 V. Dotted lines indicate when the chlorination break point was reached (i.e., complete ammonium removal).

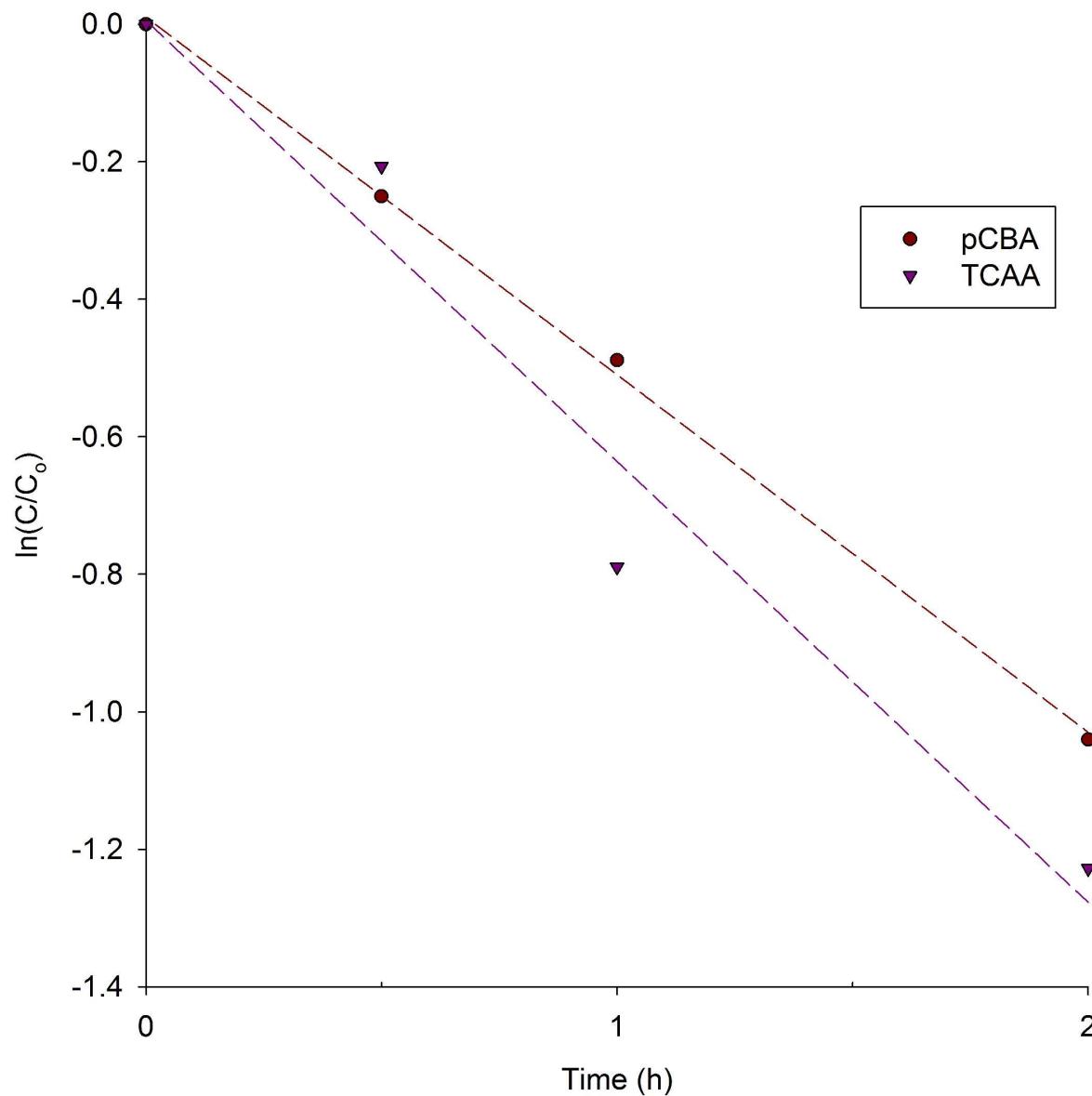


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119 Figure SI 6. Concentrations of measured (symbols) and modeled (dashed lines) chlorine species
 120 during electrolysis of latrine wastewater on BDD anodes at 4.0 A L^{-1} . First-order reaction rate
 121 constants were obtained by fitting the model

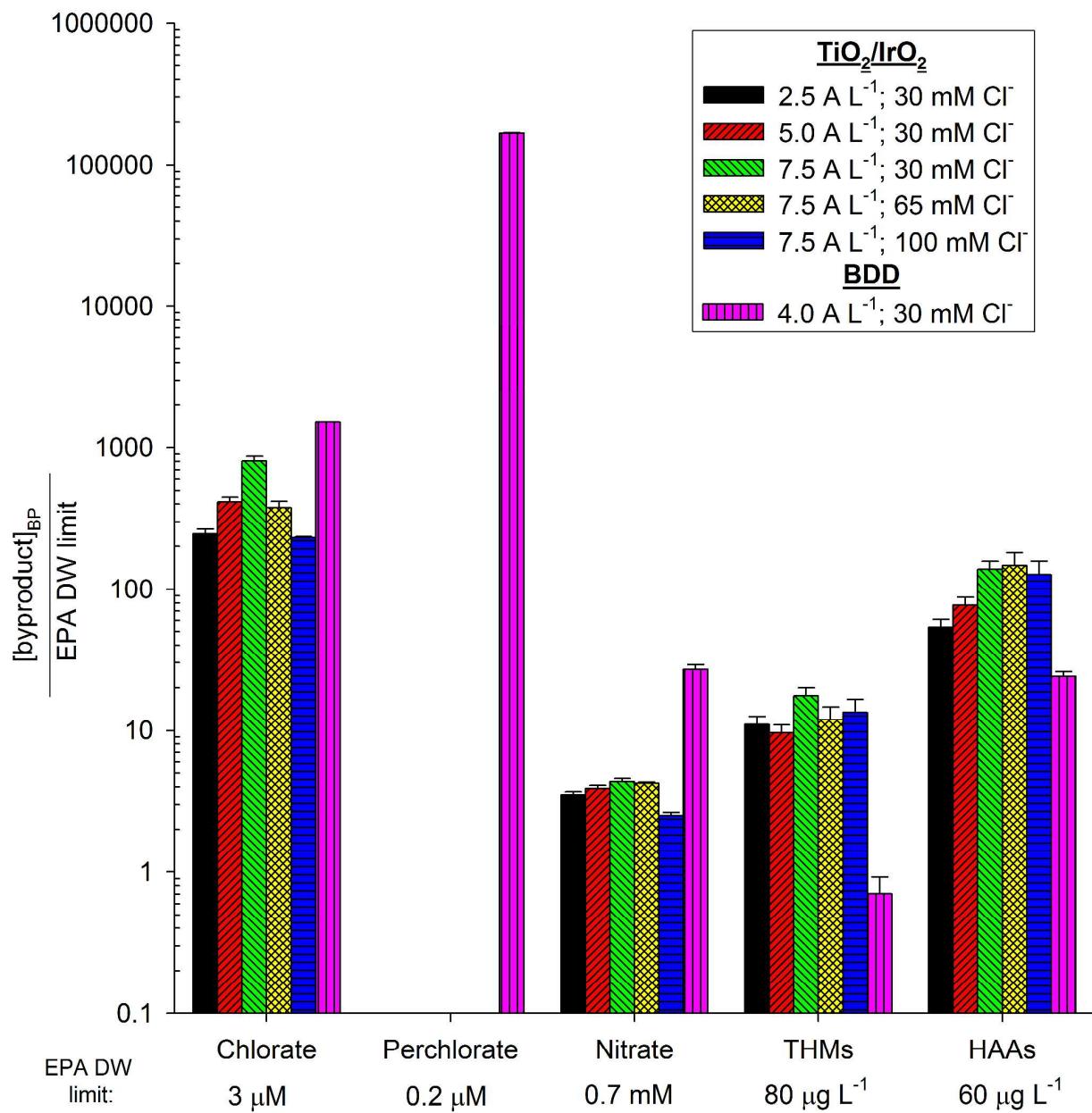
122 $(\text{Cl}^- + 3\text{H}_2\text{O} \xrightarrow{k_3} \text{ClO}_3^- + 6\text{H}^+ + 6\text{e}^-; \text{ClO}_3^- + \text{H}_2\text{O} \xrightarrow{k_4} \text{ClO}_4^- + 2\text{H}^+ + 2\text{e}^-)$ to the experimental
 123 data ($k_3 = 0.17 (\text{Ah L}^{-1})^{-1}$; $k_4 = 0.087 (\text{Ah L}^{-1})^{-1}$). See Figure 4 of main manuscript for
 124 concentrations of other species.

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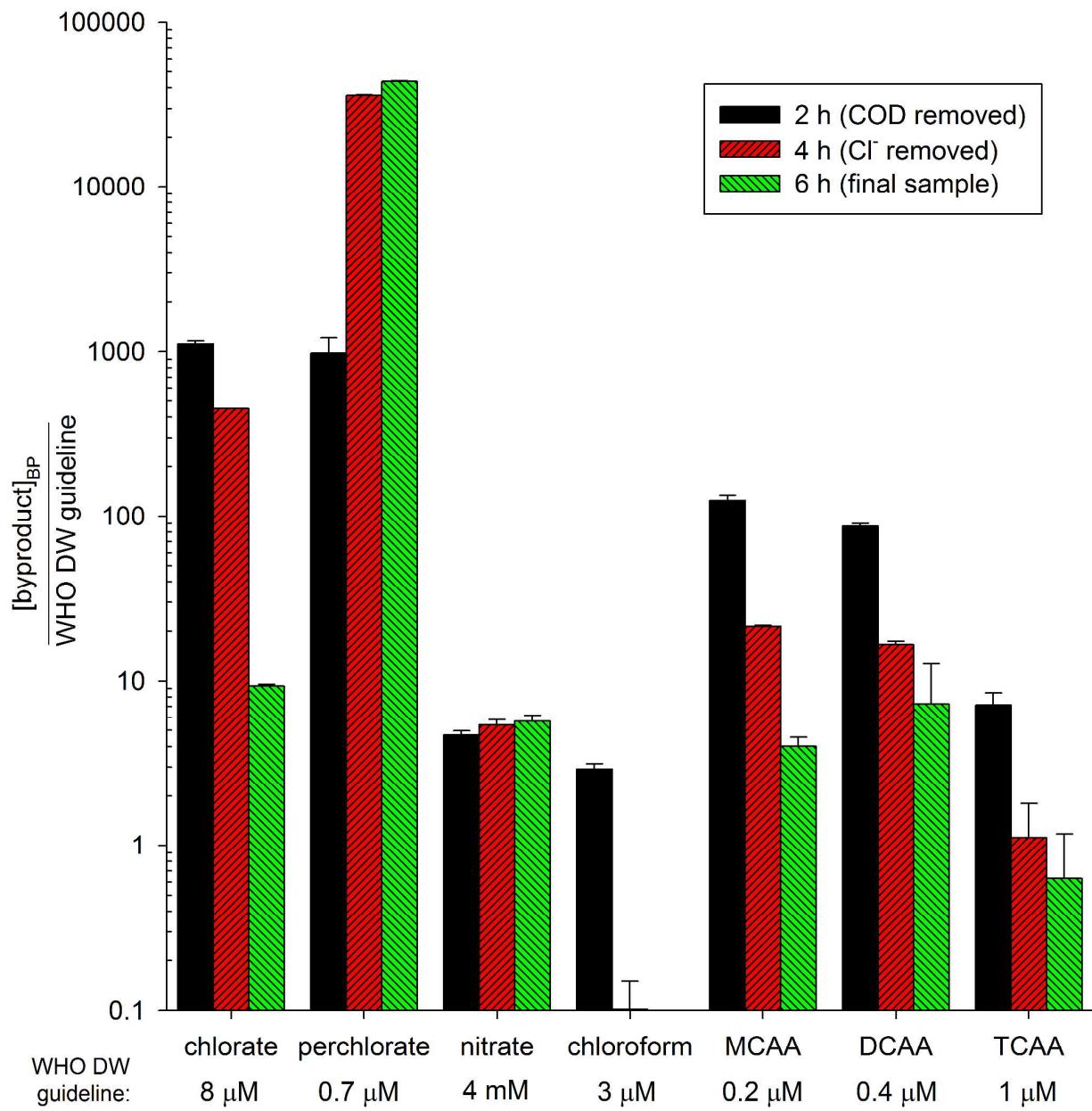
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127 Figure SI 7. Natural log of normalized TCAA and pCBA concentrations during electrolysis in
128 borate buffer on BDD anodes (30 mM; pH 8.7).



130 EPA DW limit: 3 μM 0.2 μM 0.7 mM 80 $\mu\text{g L}^{-1}$ 60 $\mu\text{g L}^{-1}$

131 Figure SI 8. Factors that byproduct concentrations near the chlorination breakpoint
132 ([byproduct]_{BP}) exceeded US Environmental Protection Agency (EPA) drinking water (DW)
133 advisories and limits after one treatment cycle with different anodes, current densities, and
134 chloride concentrations. For treatment with BDD anodes, the point that chloride was removed
135 was used instead of the breakpoint, because complete ammonium removal was not achieved.



137 WHO DW guideline: 8 μM 0.7 μM 4 mM 3 μM 0.2 μM 0.4 μM 1 μM
138 Figure SI 9. Factors that byproduct concentrations near the chlorination breakpoint
139 ([byproduct]_{BP}) exceeded World Health Organization (WHO) drinking water (DW) regulations
140 throughout one treatment cycle of latrine water electrolysis with BDD anodes. 4.0 A L⁻¹;
141 30 mM Cl⁻ initially.

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