

**Development and Scope of the Arene-Fused Michael/Mannich/N-Alkylation Reaction:  
Application to the Total Syntheses of *Aspidosperma* Alkaloids (*-*)-Aspidospermidine, (*-*)-  
Tabersonine, and (*-*)-Vincadiformine**

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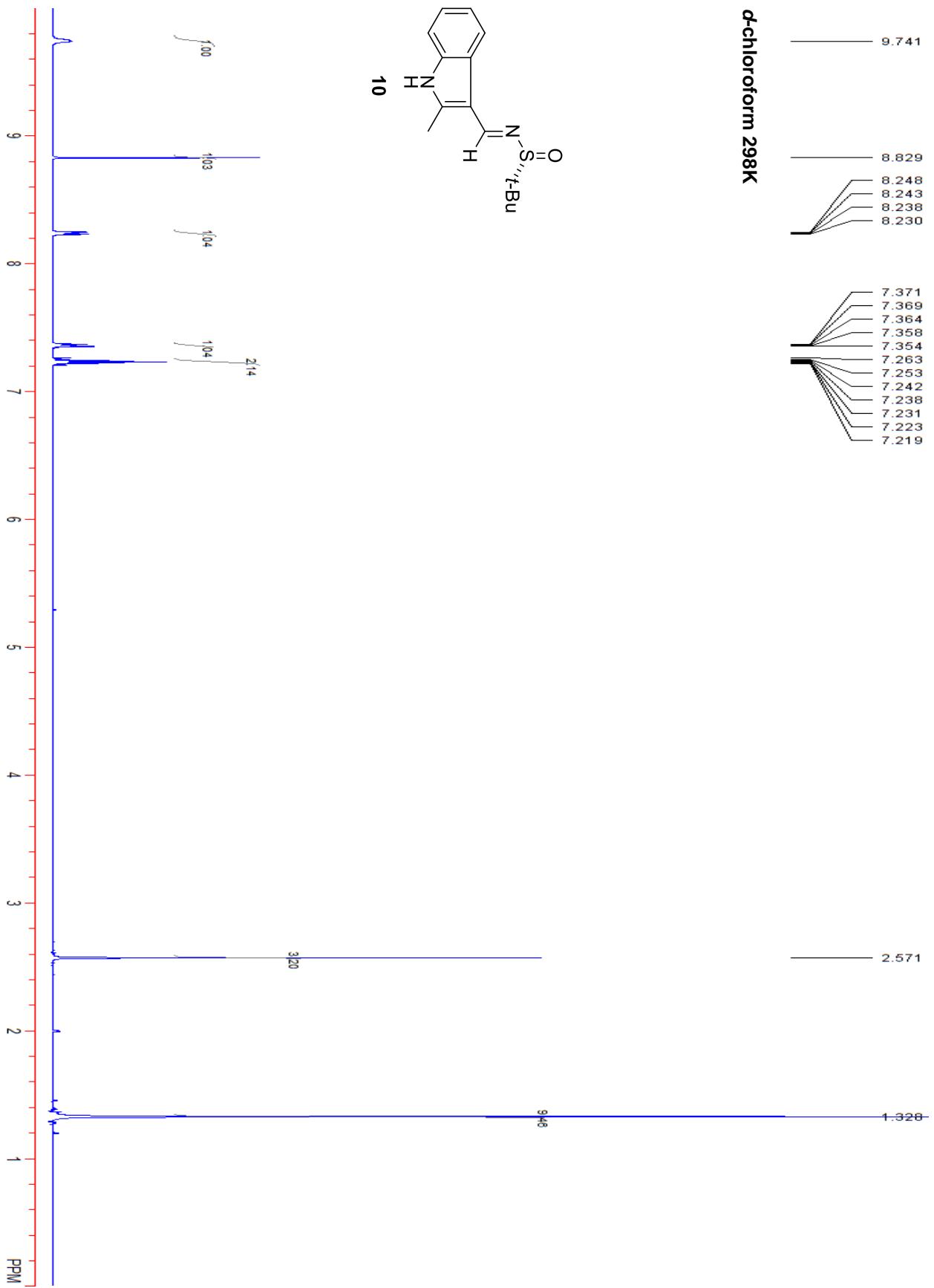
**SUPPORTING INFORMATION**

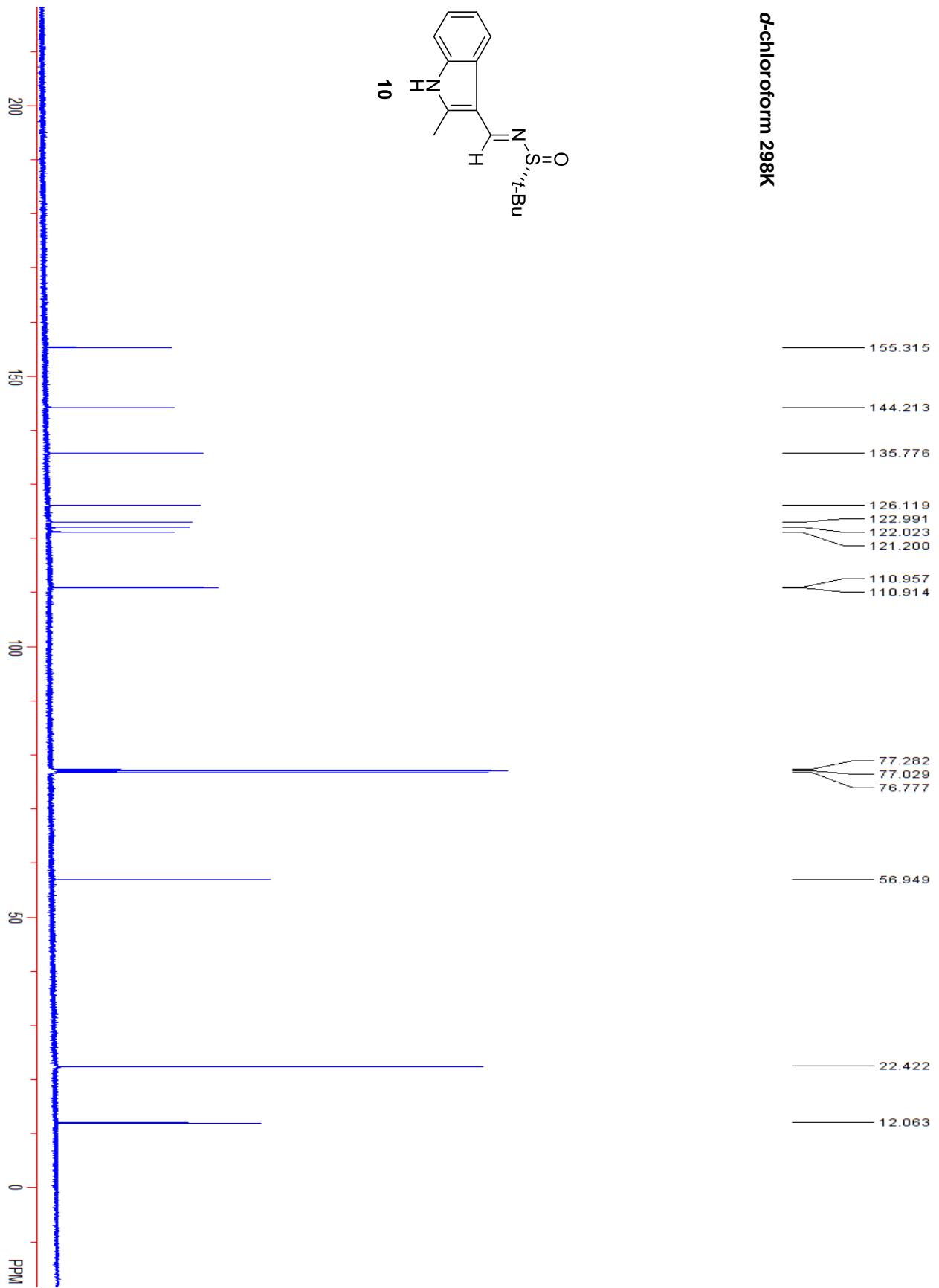
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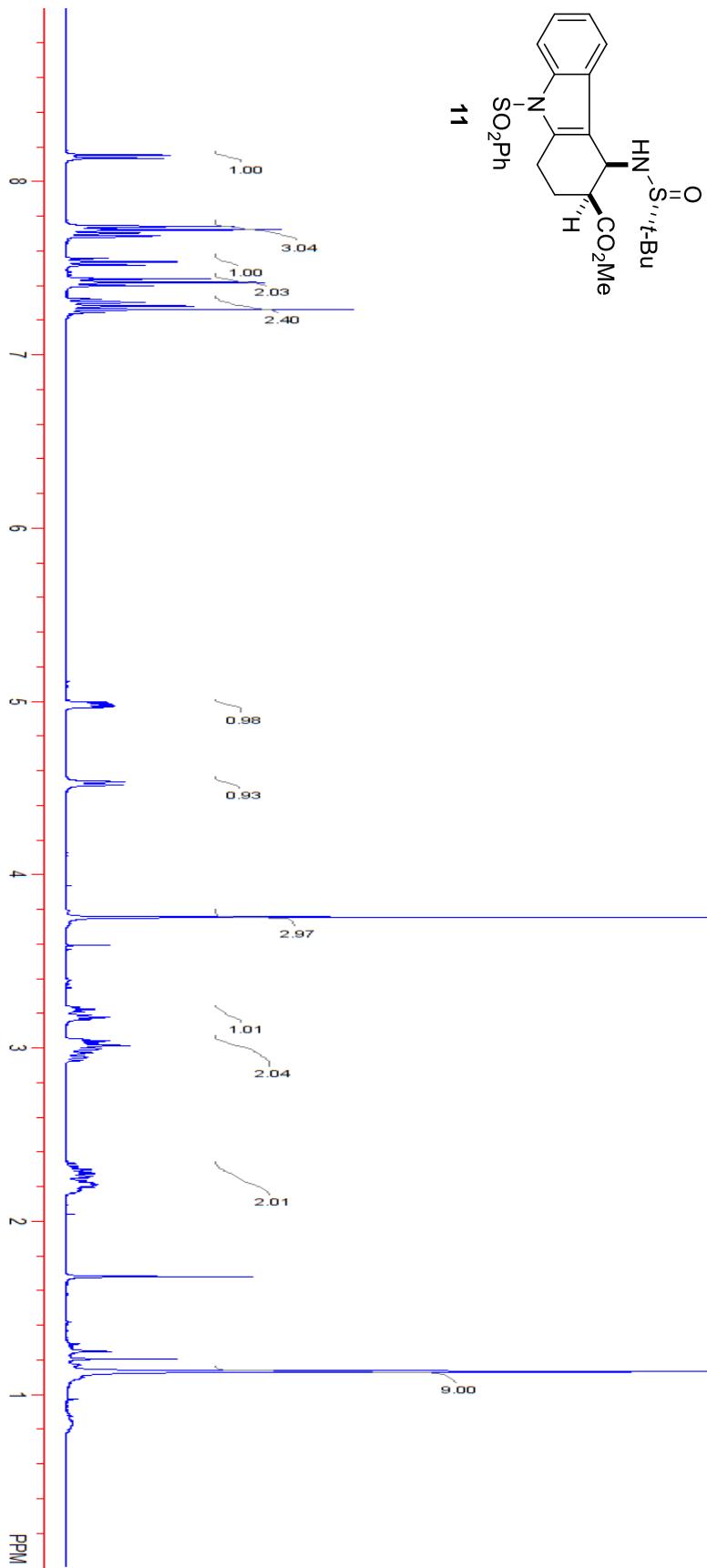
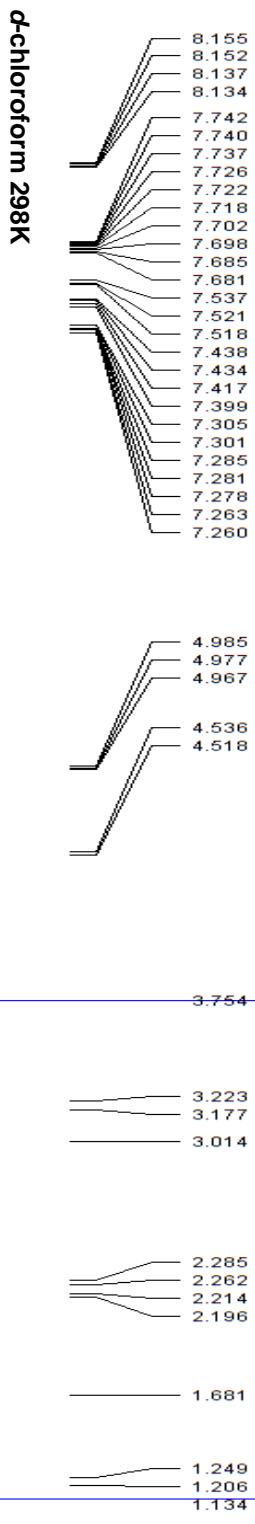
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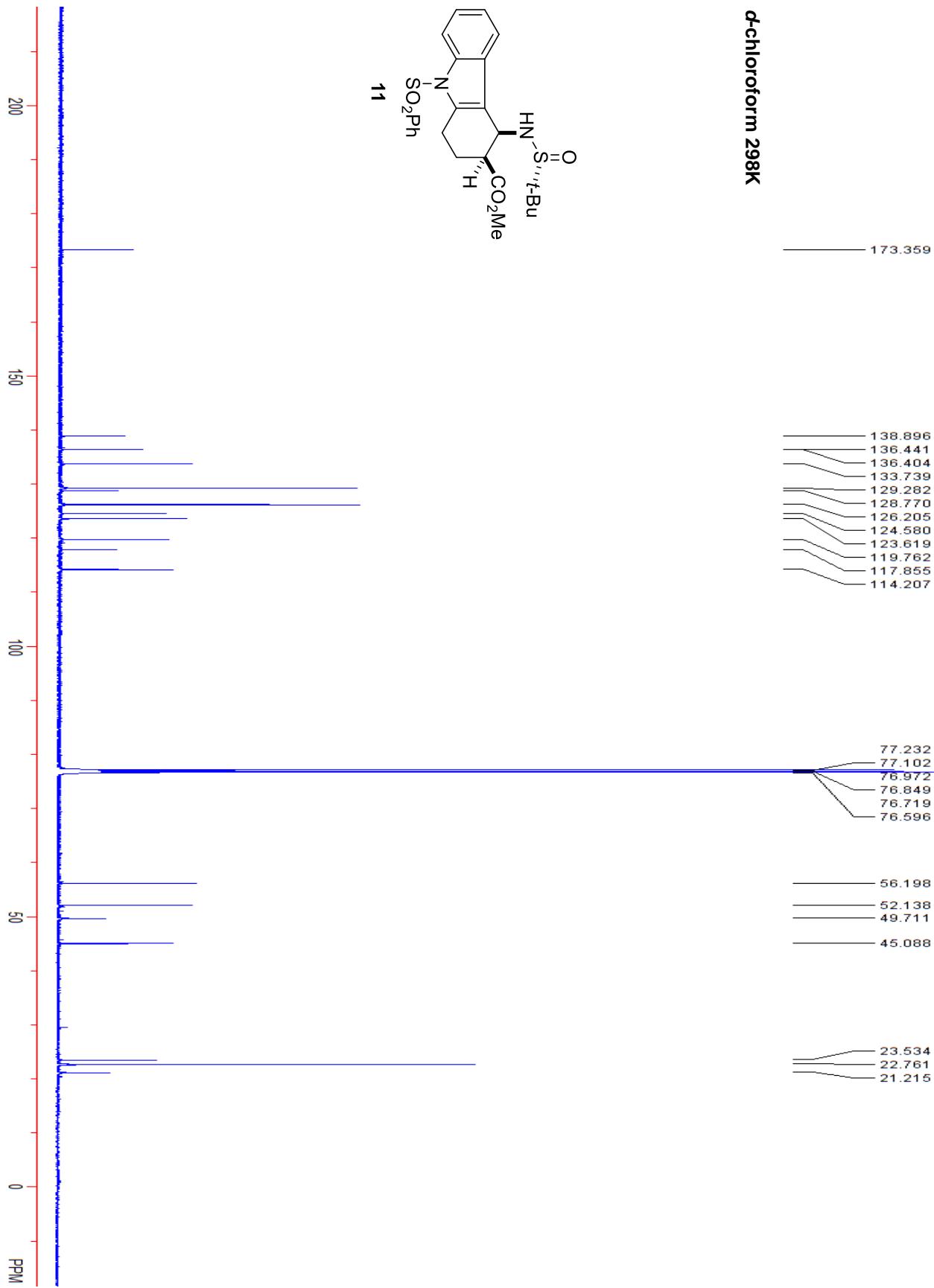
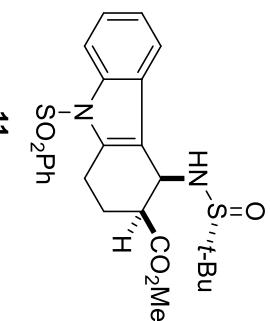
***General Information.*** Single crystal X-ray diffraction was performed with a Mo K $\alpha$  radiation obtained from a sealed molybdenum tube with a monochromator. The structure was solved using direct methods and refined using full-matrix least squares (SHELXTL). Additional experimental and sample details are given in the crystallographic tables.

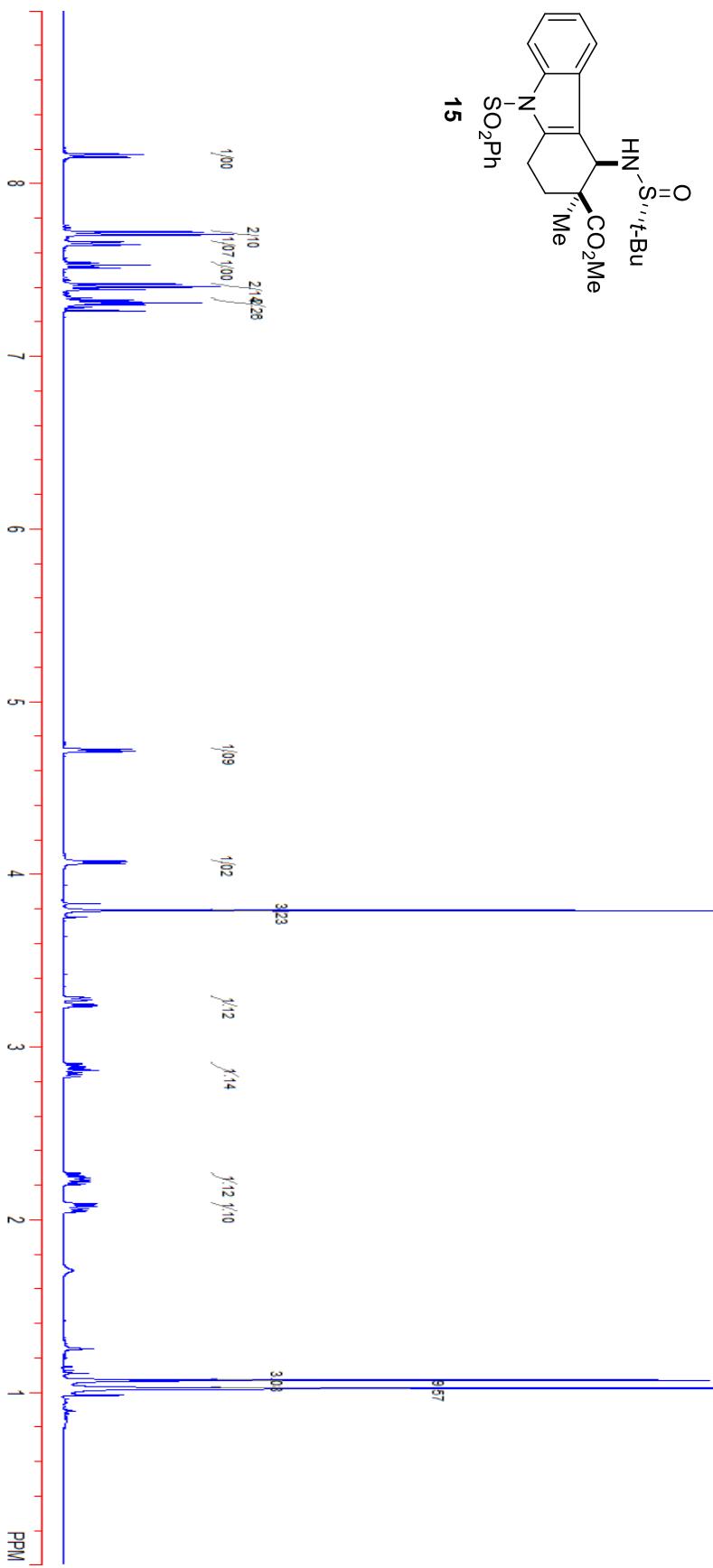
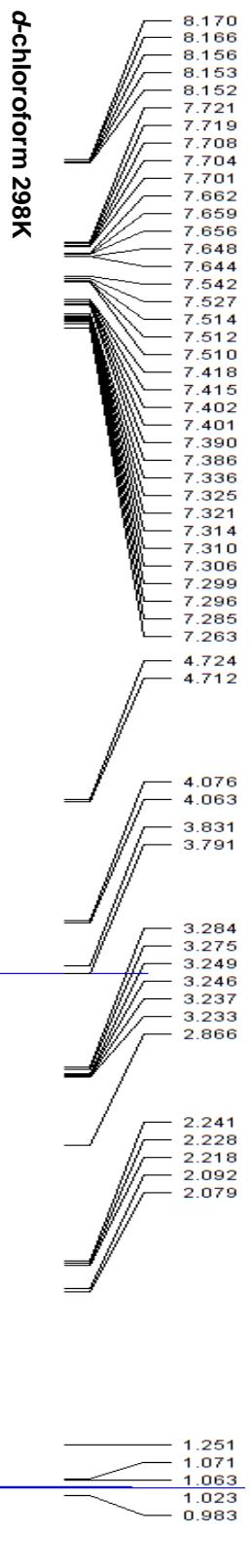




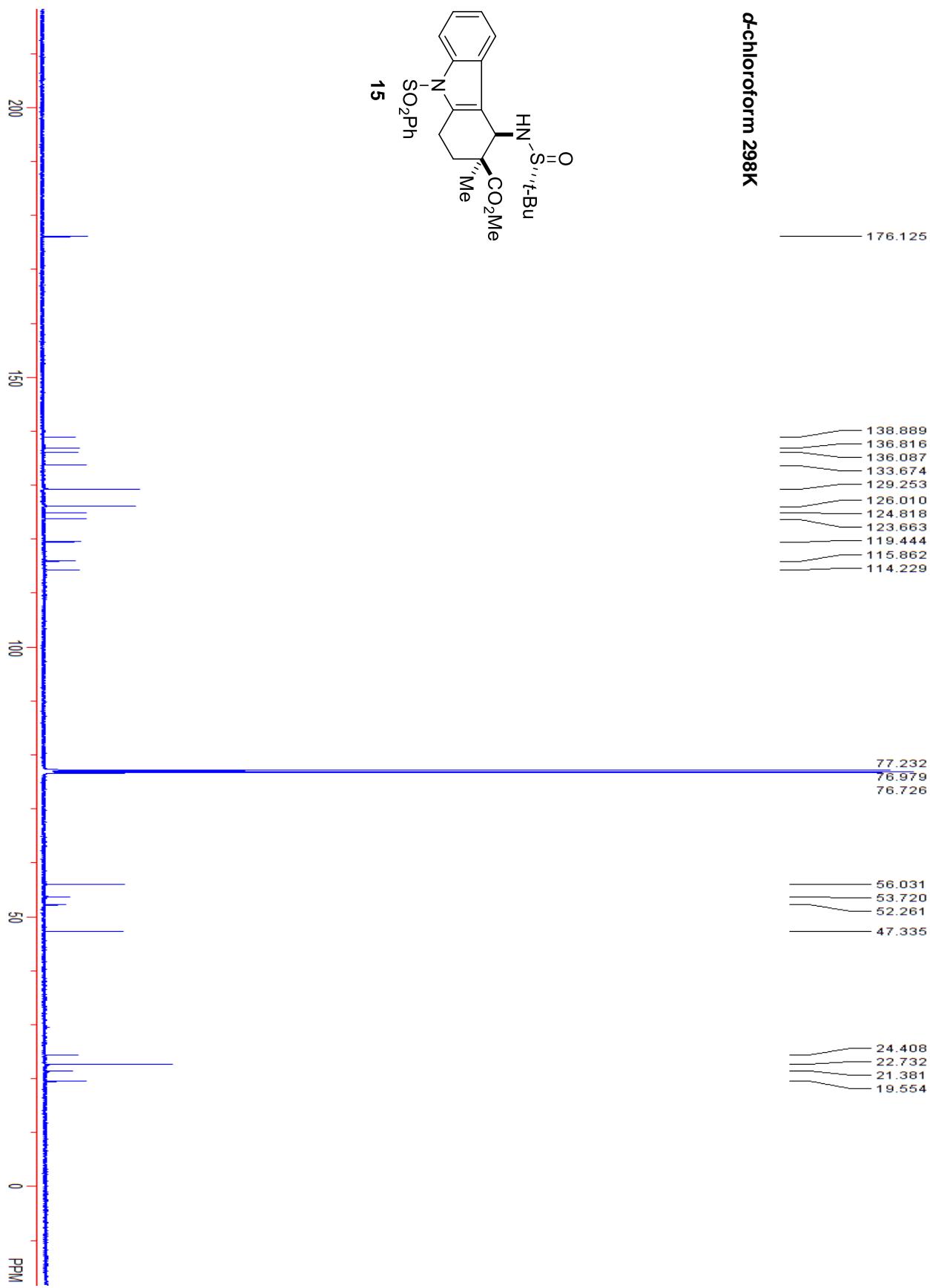


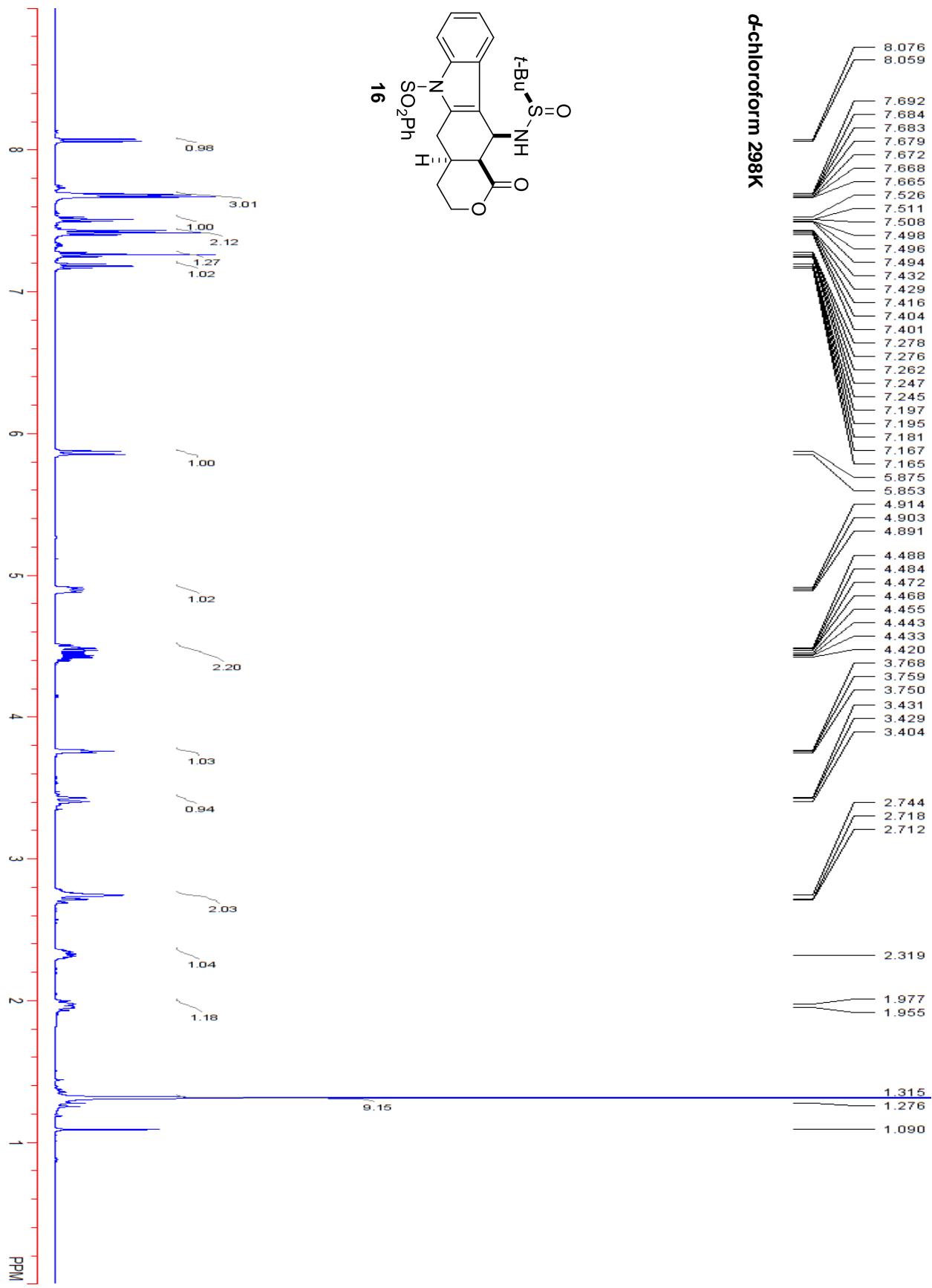
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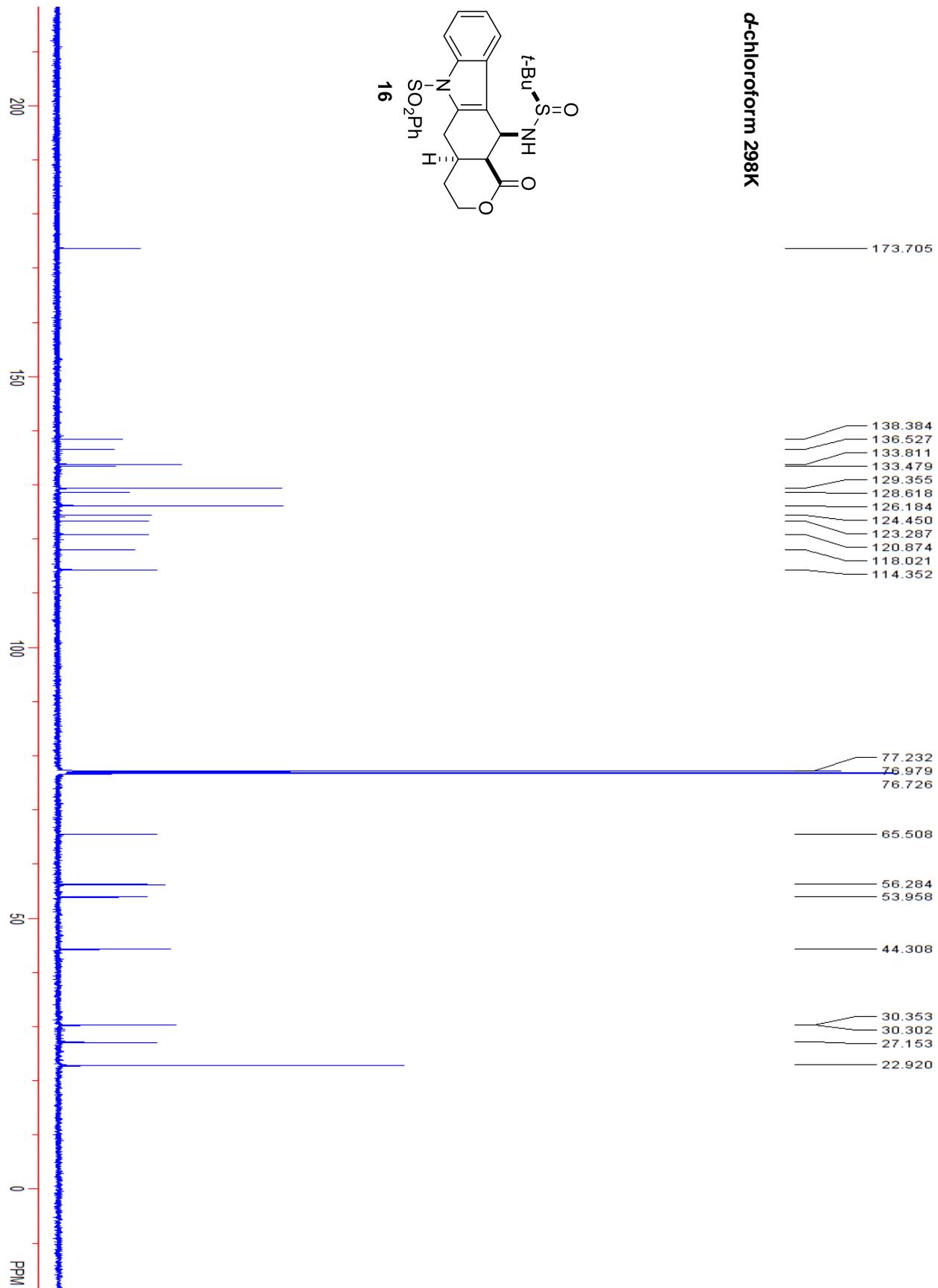


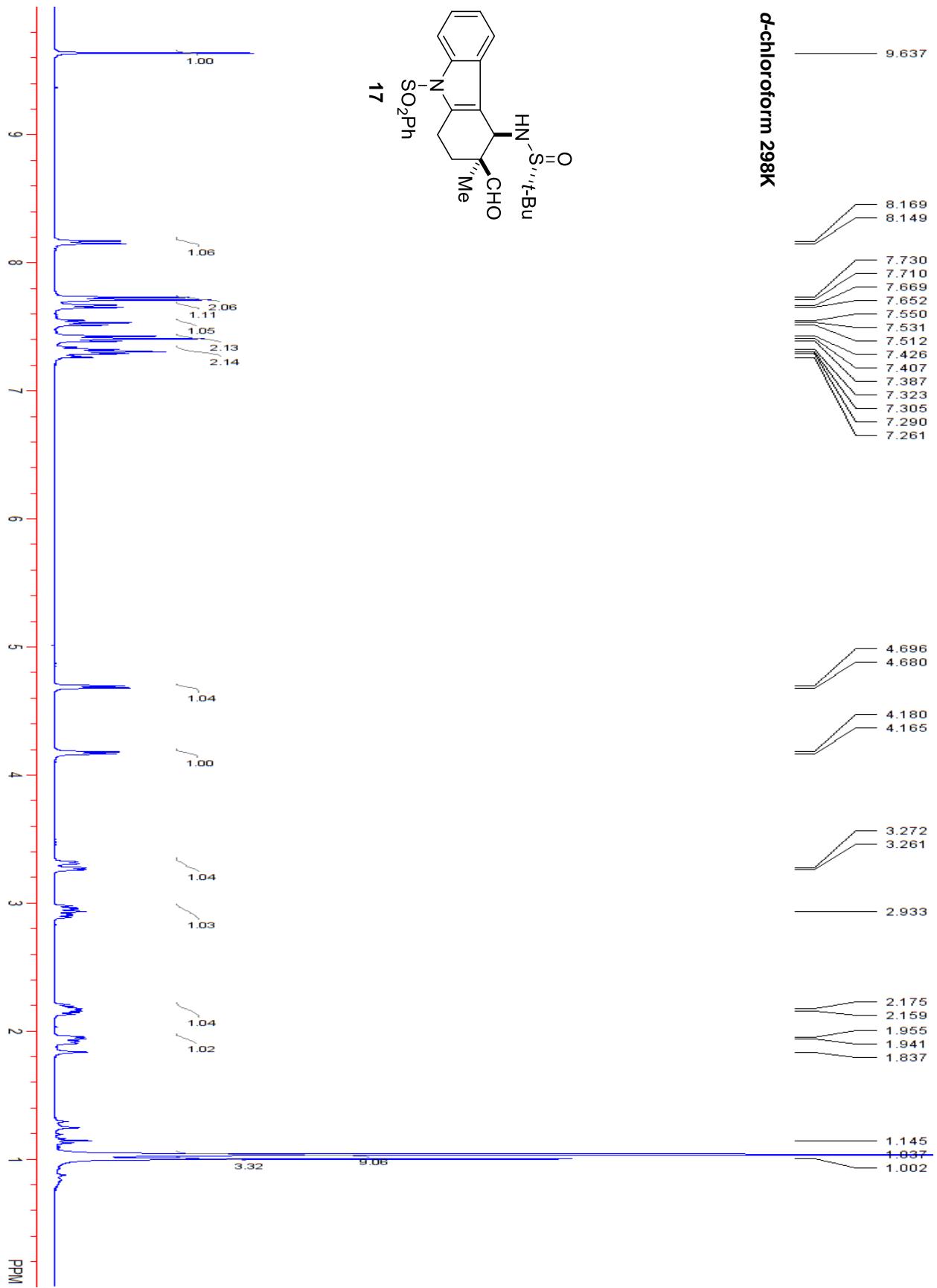


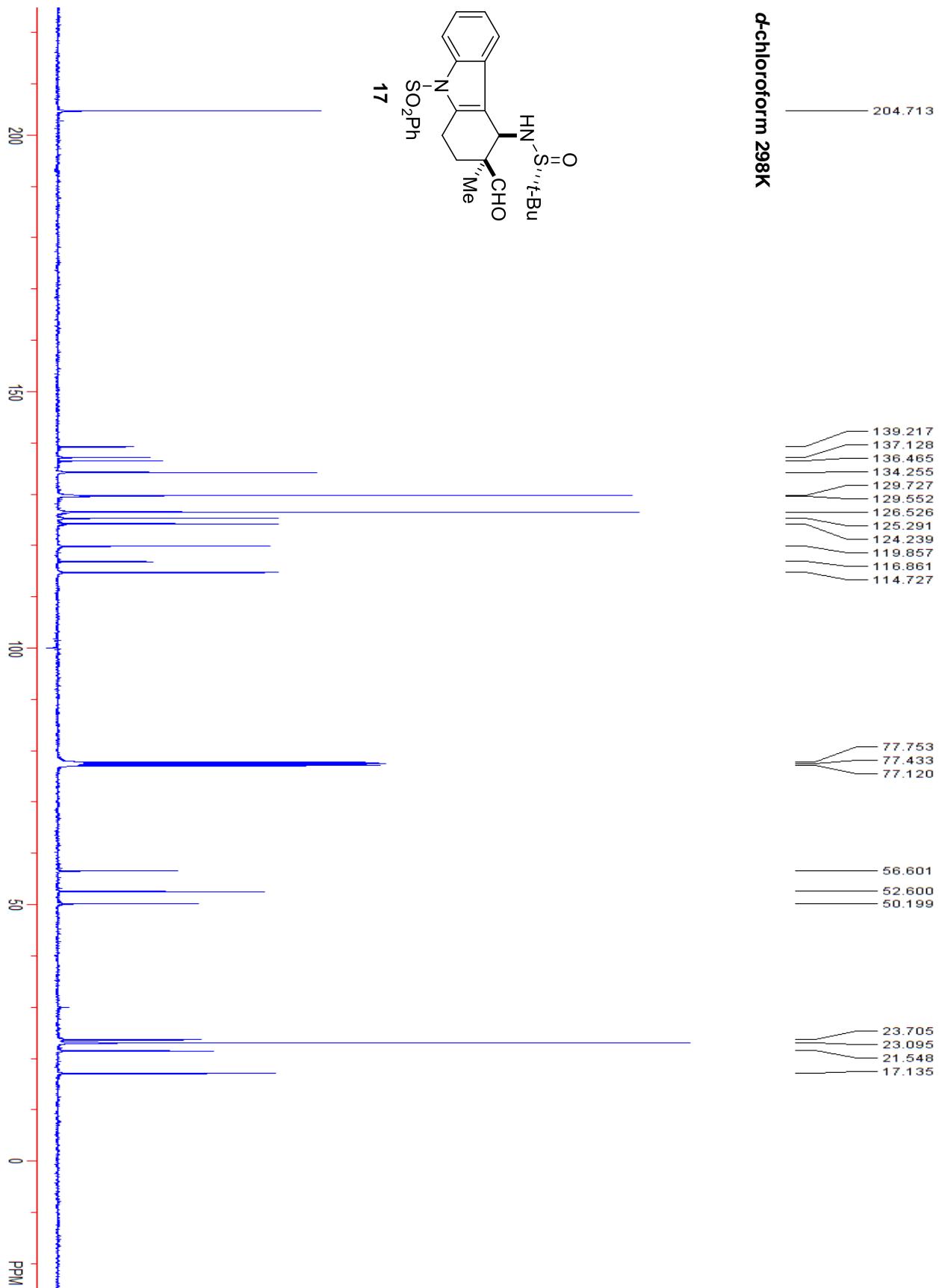
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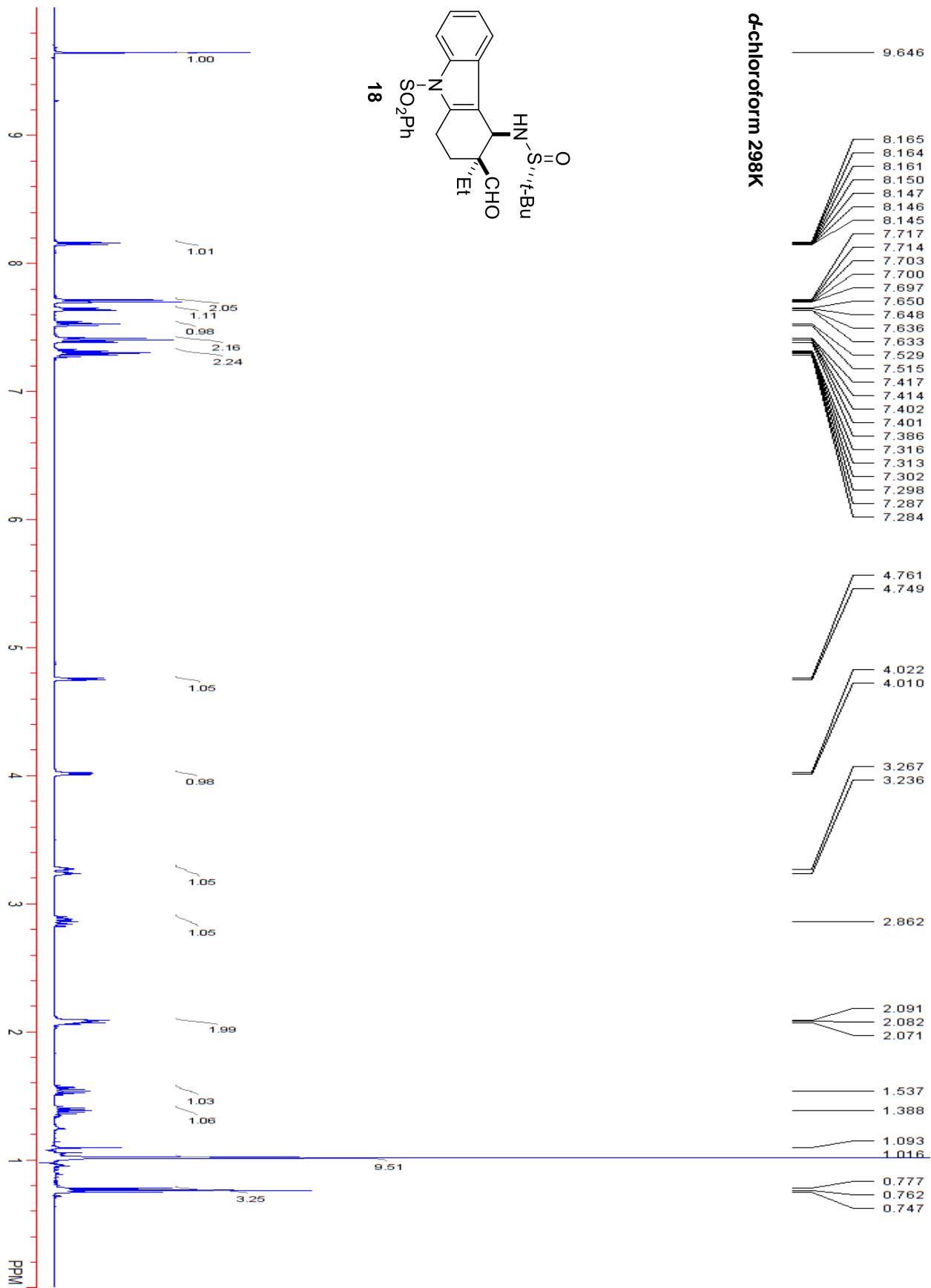


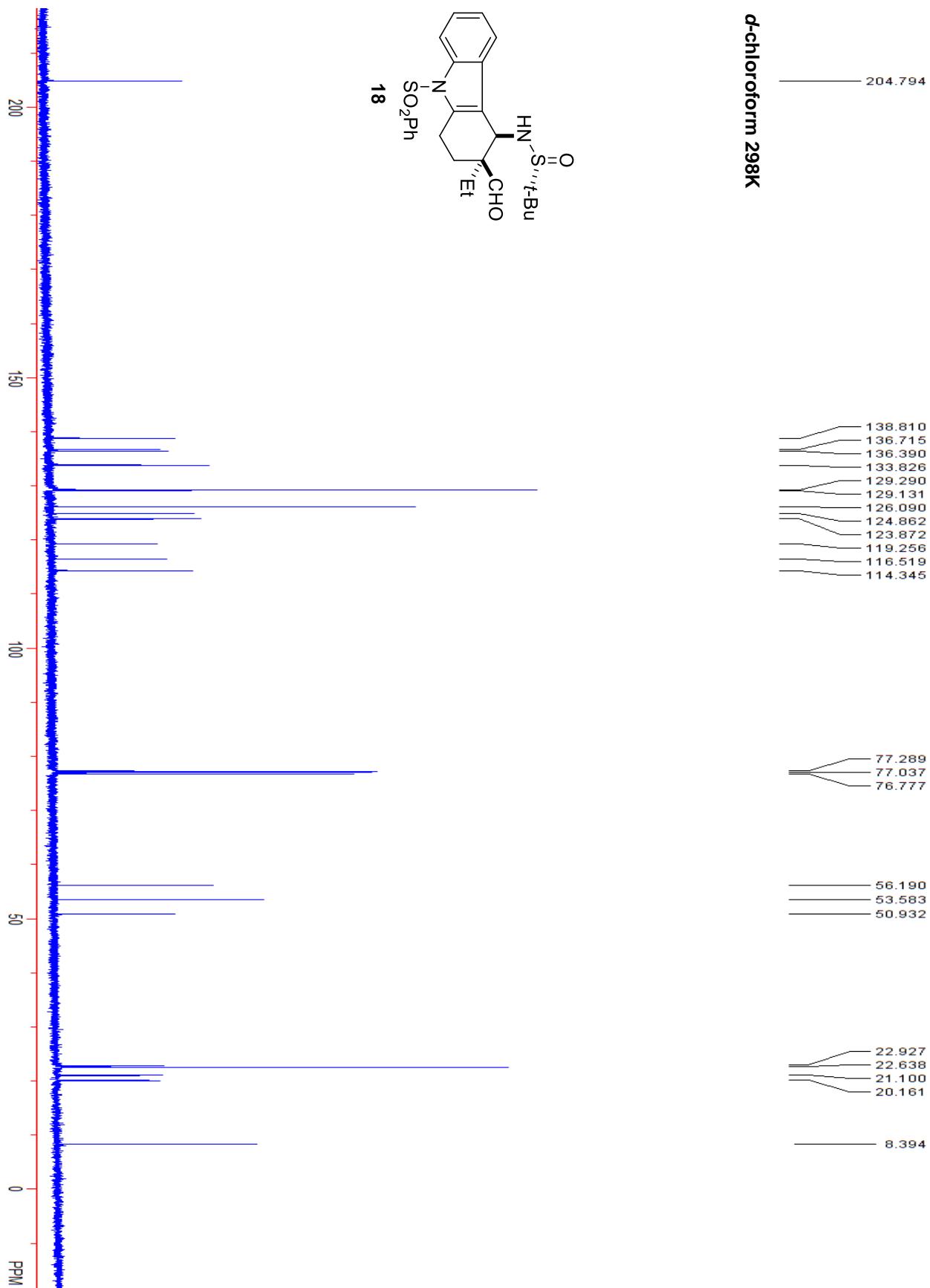


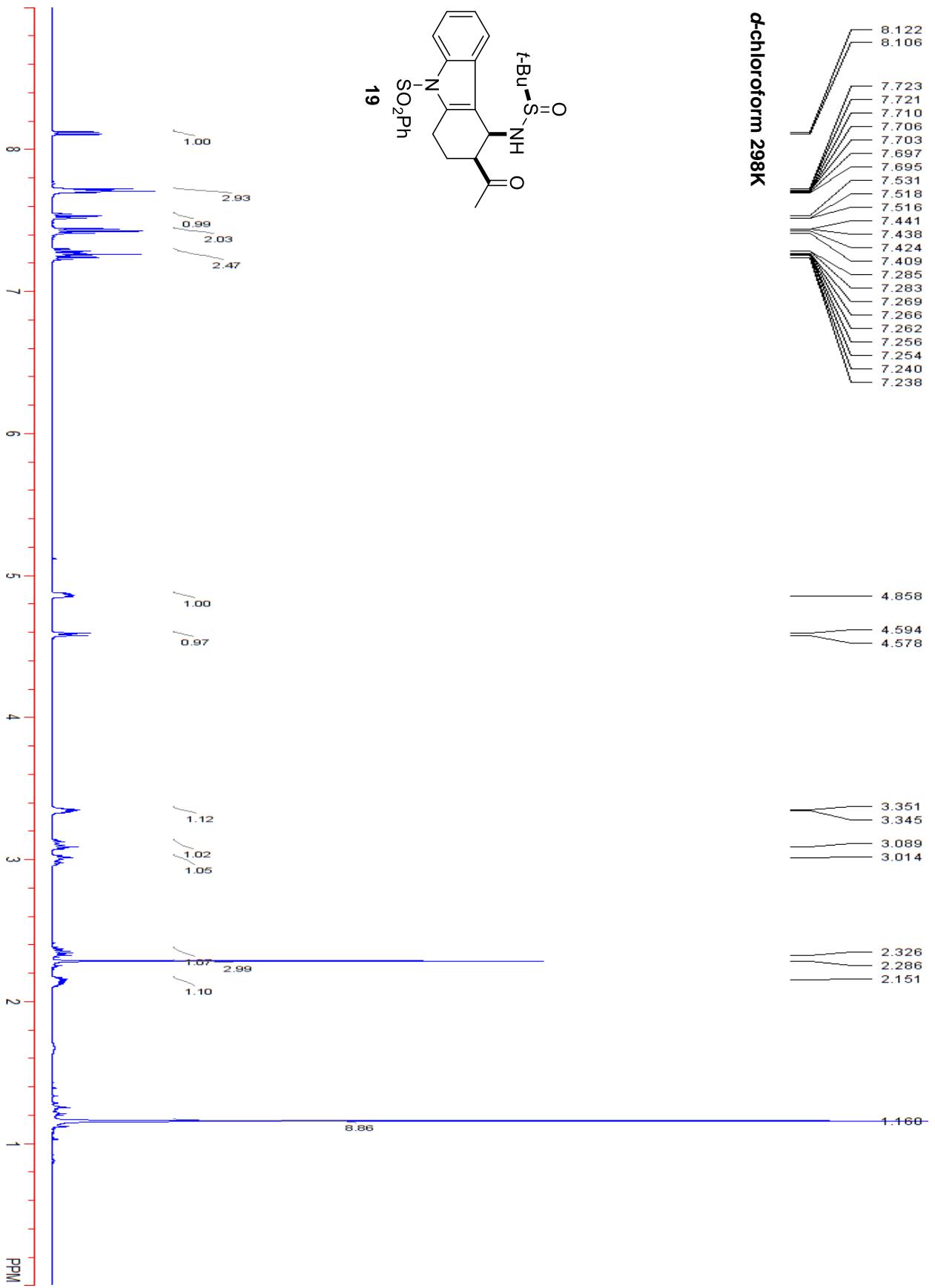


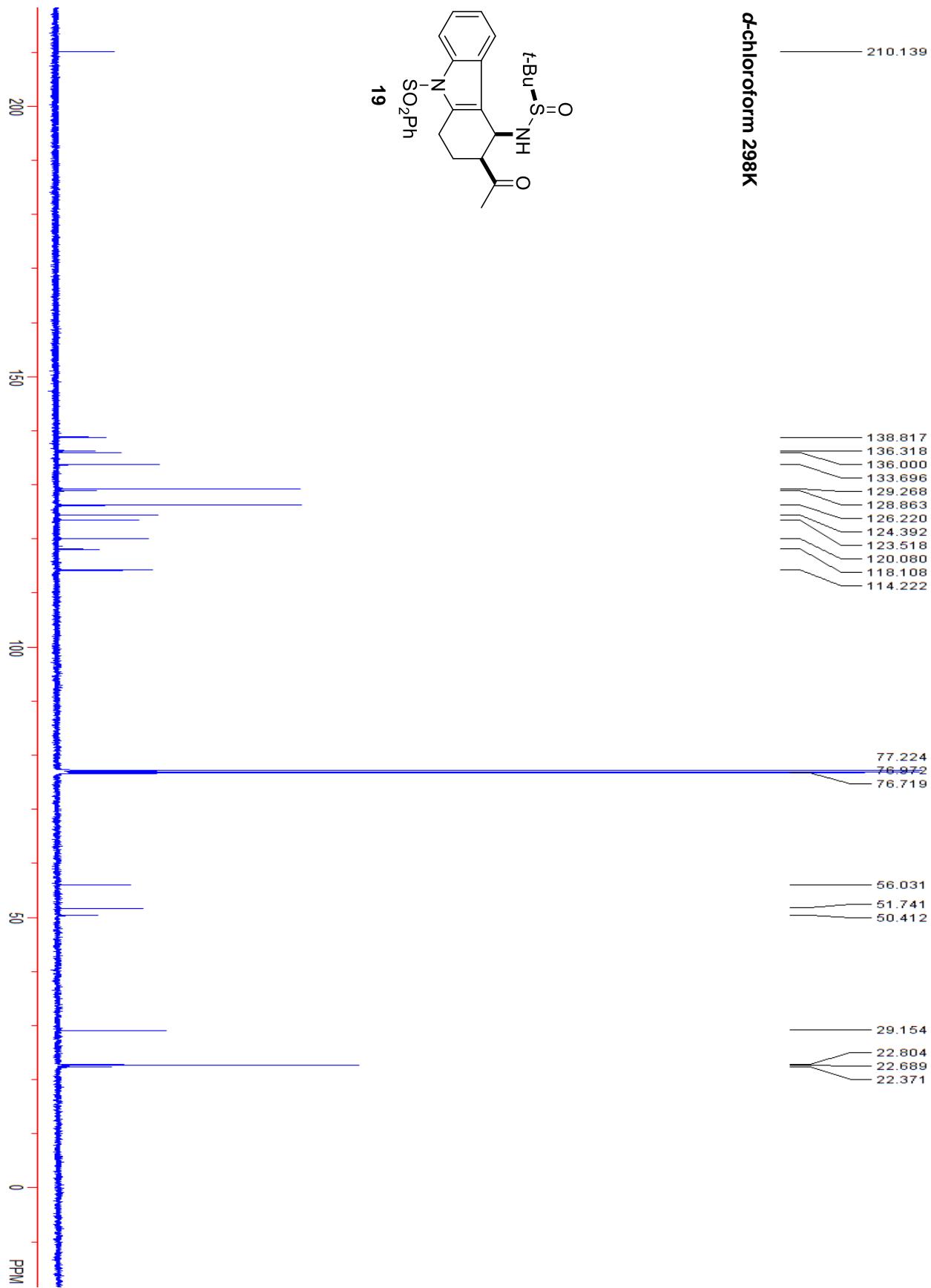


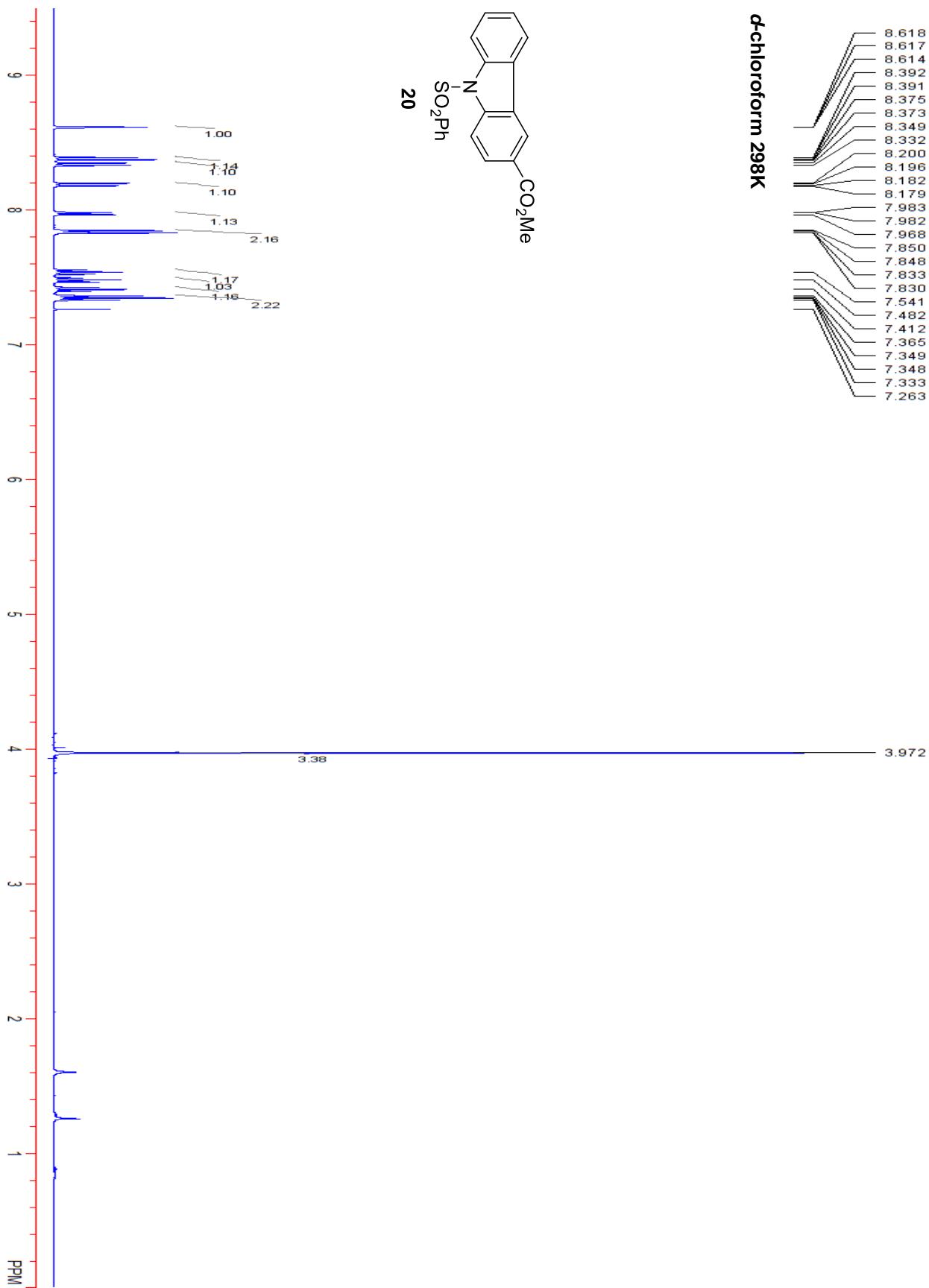


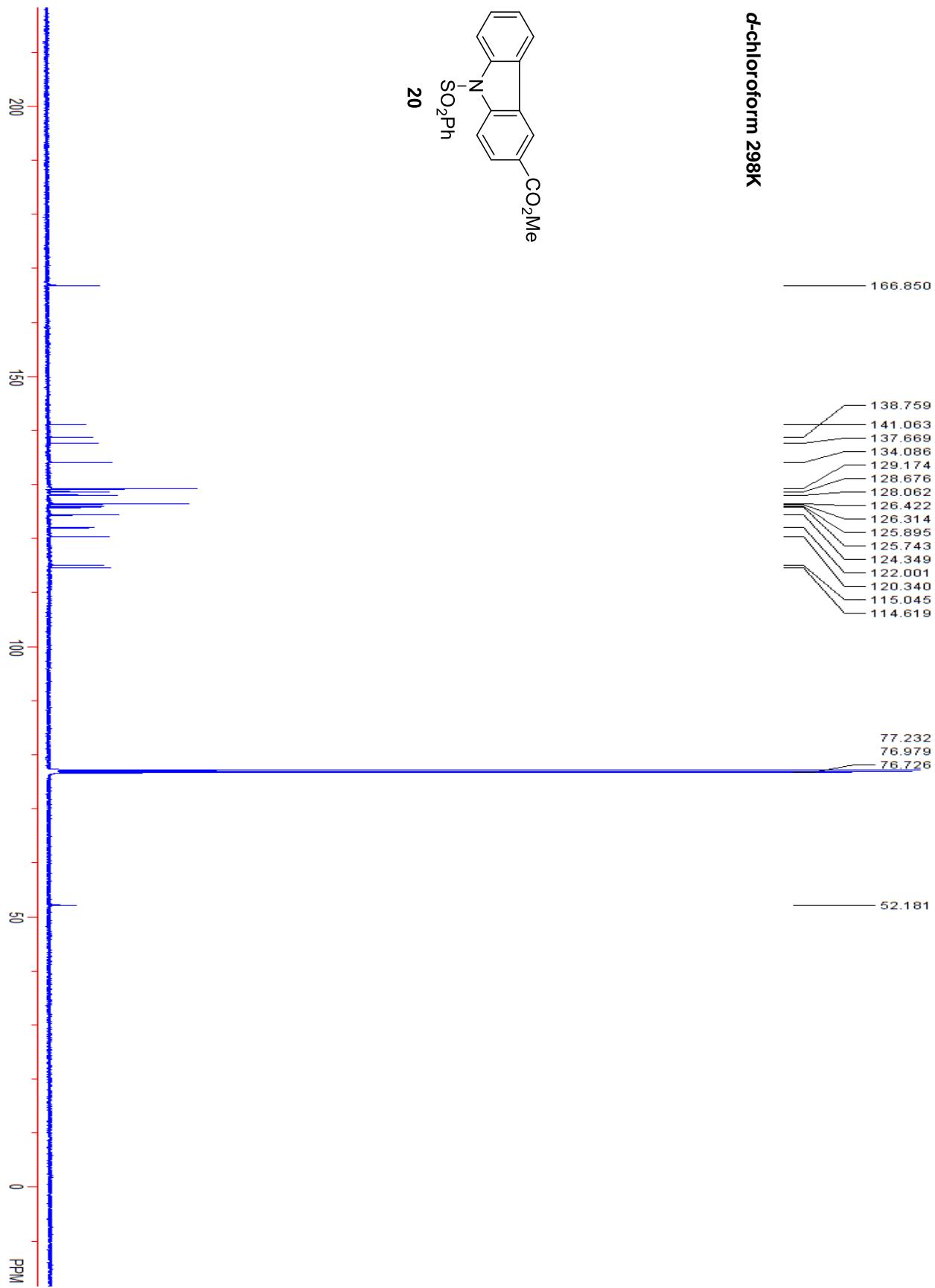


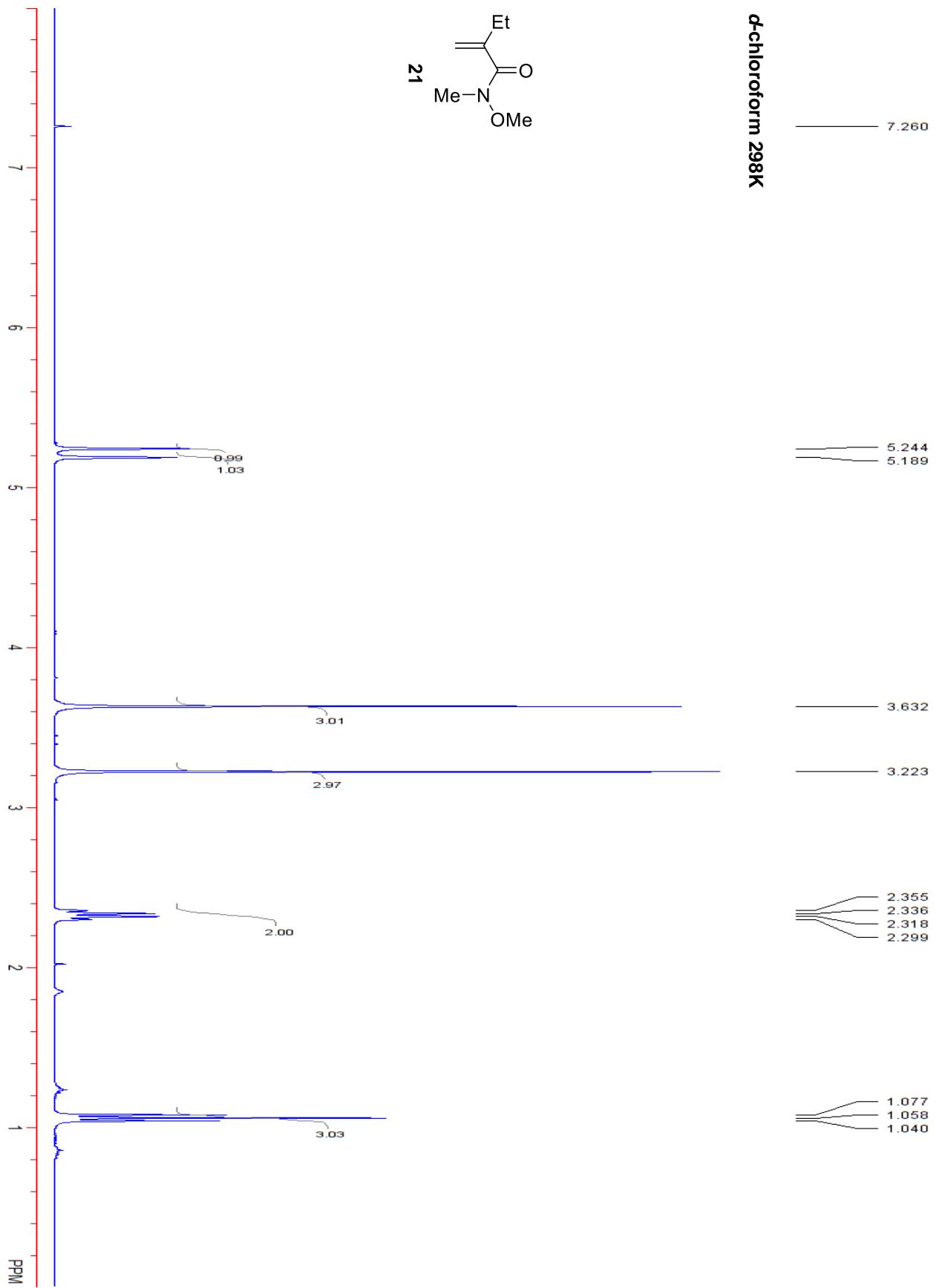


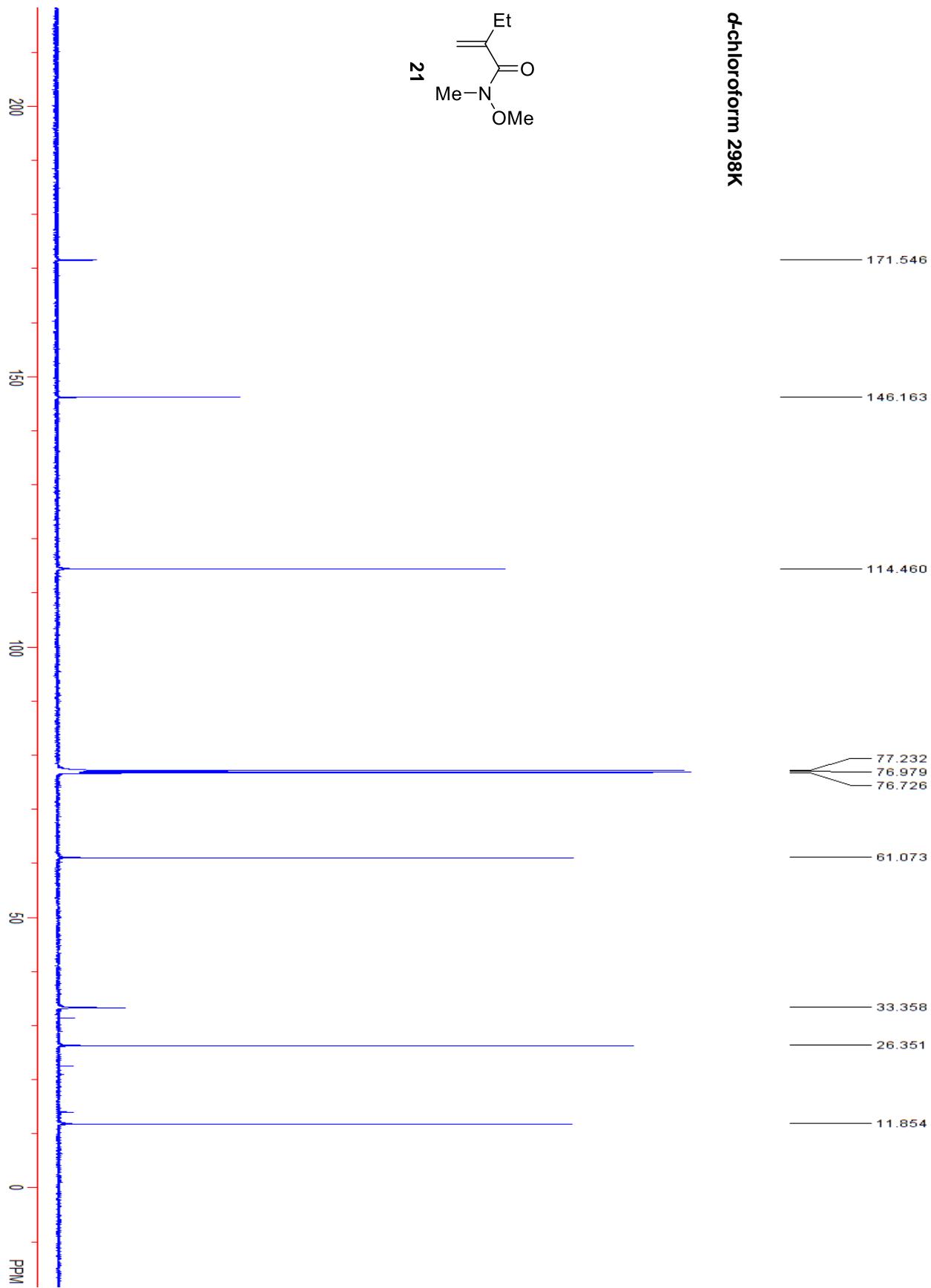


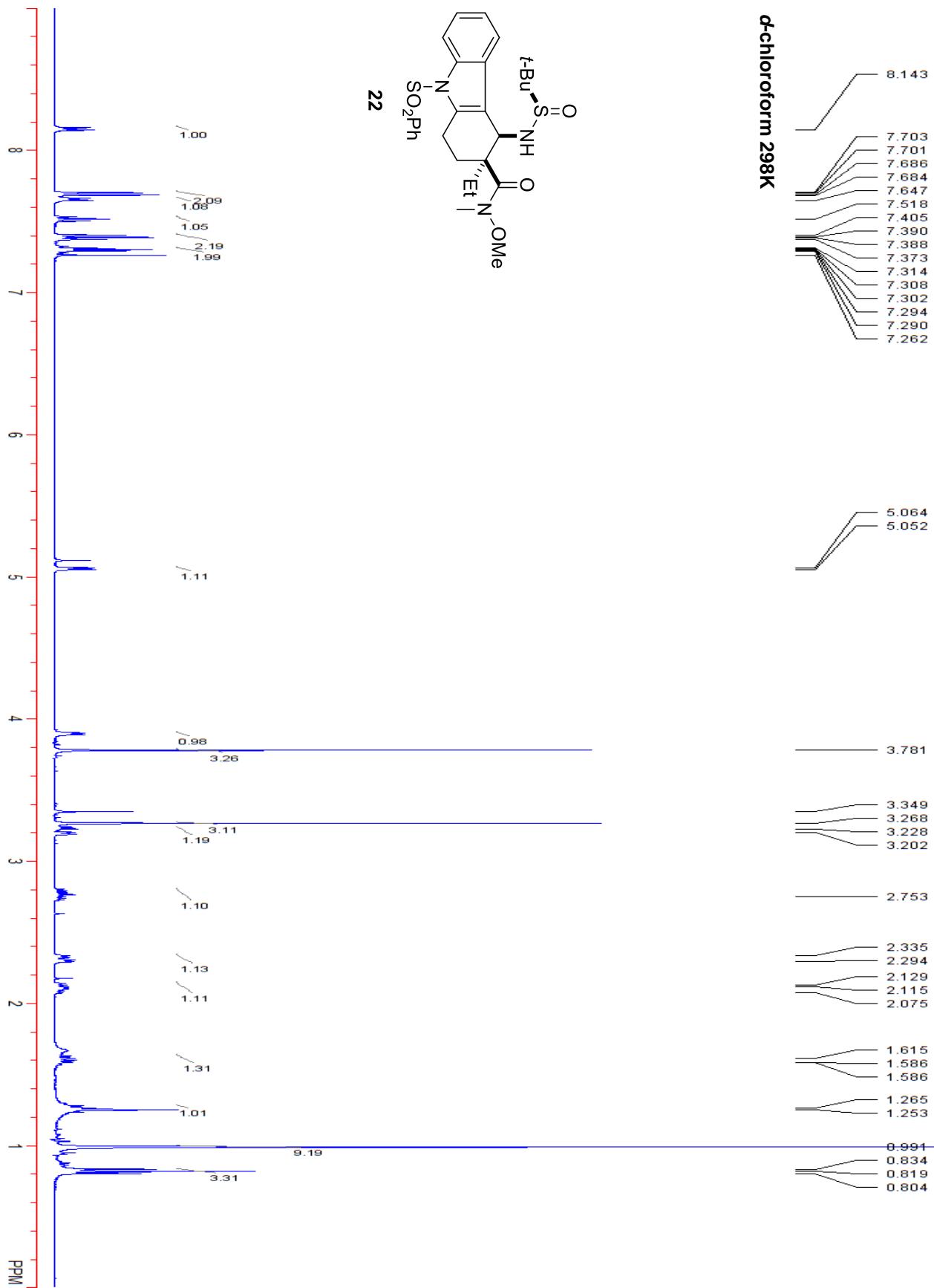


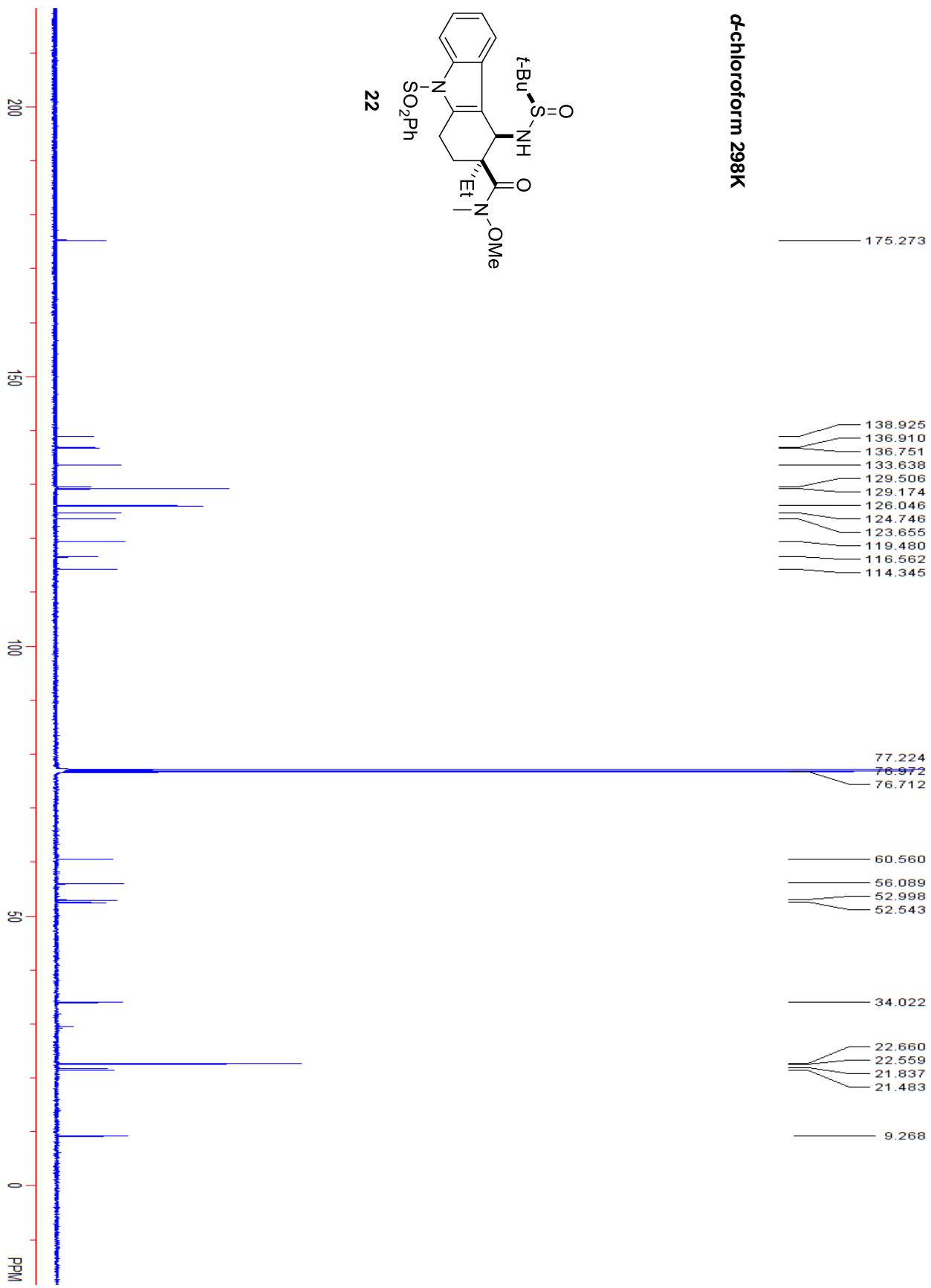


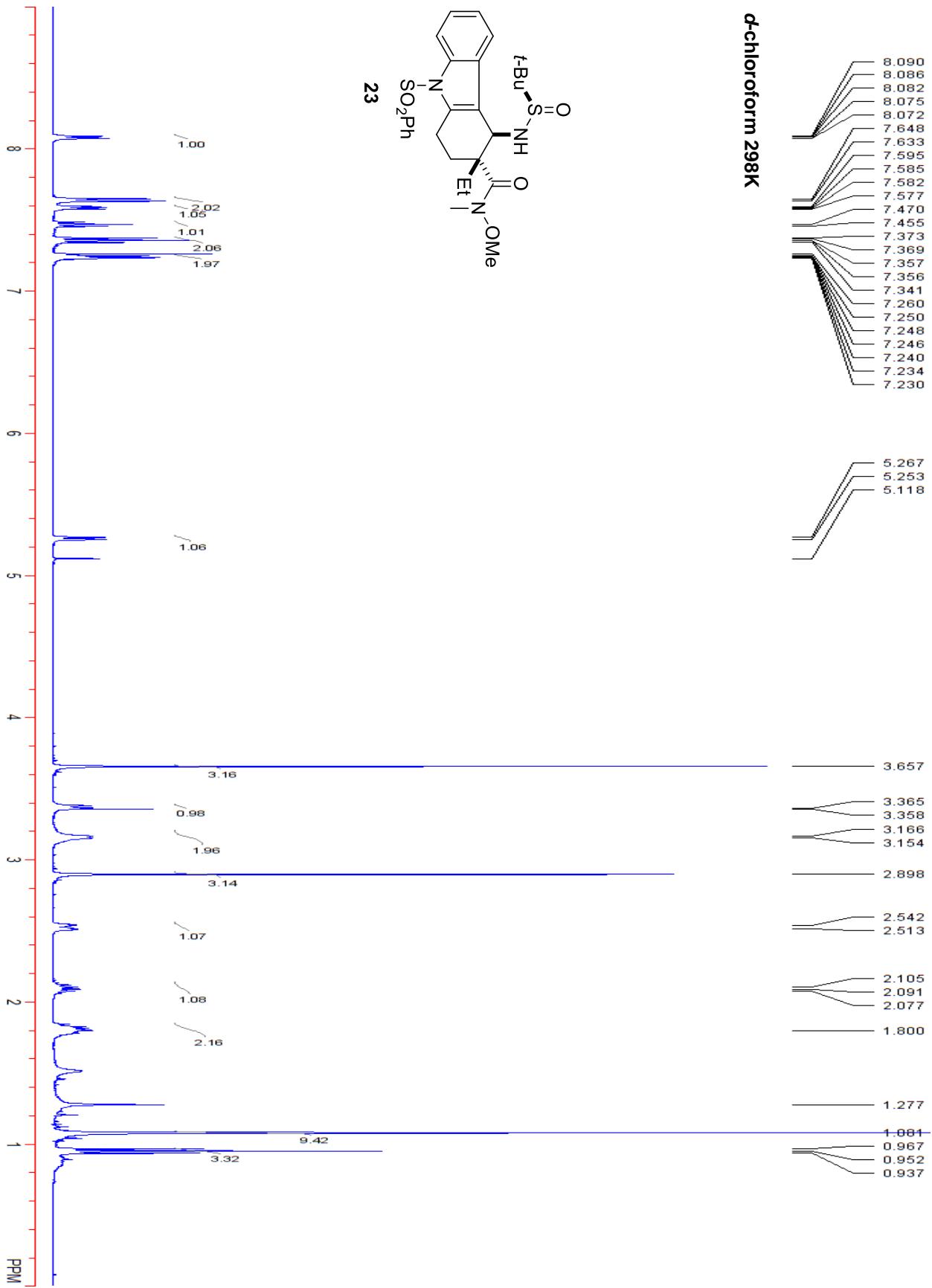




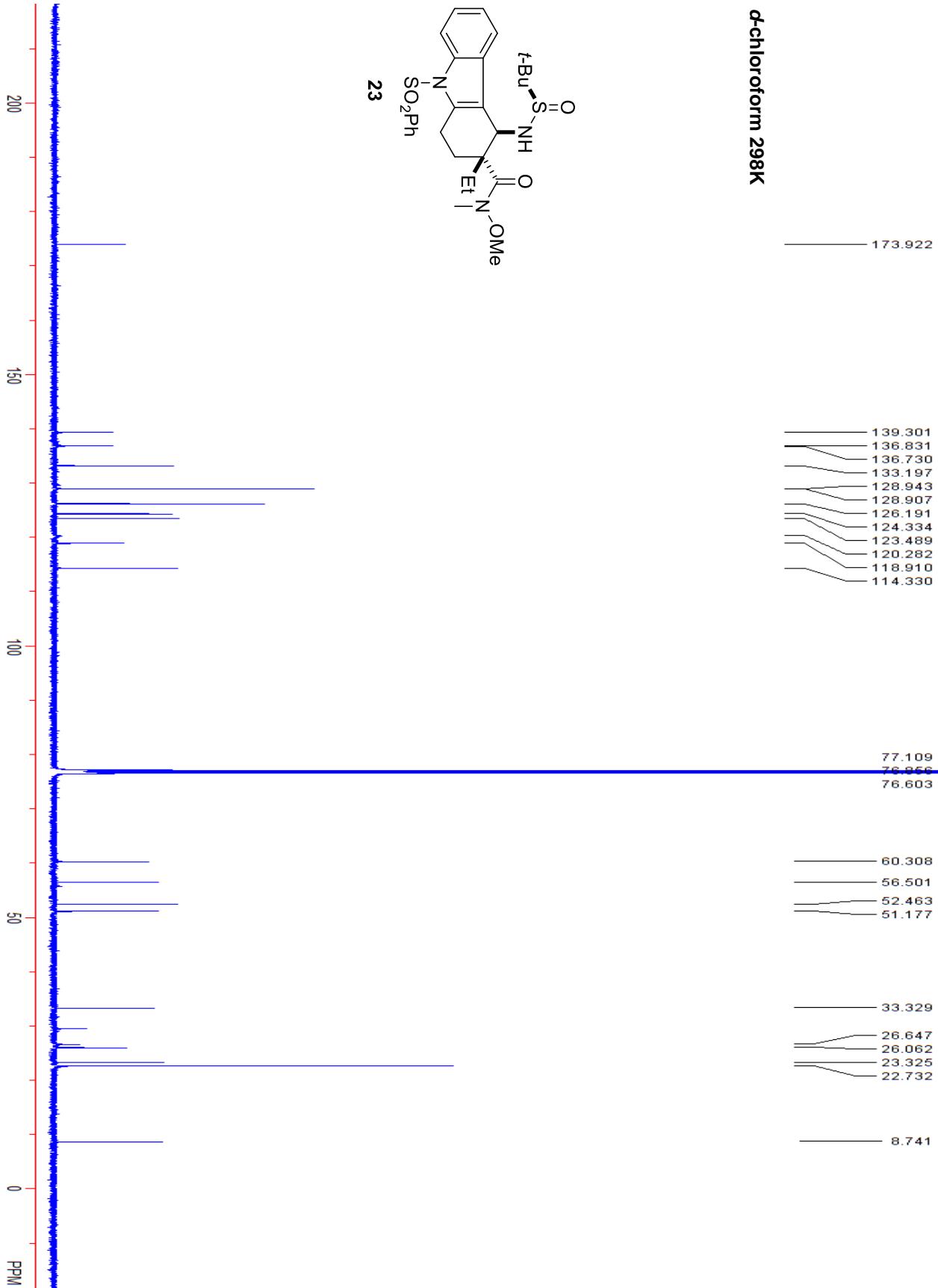
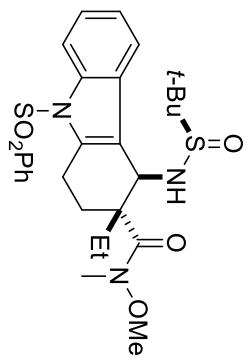


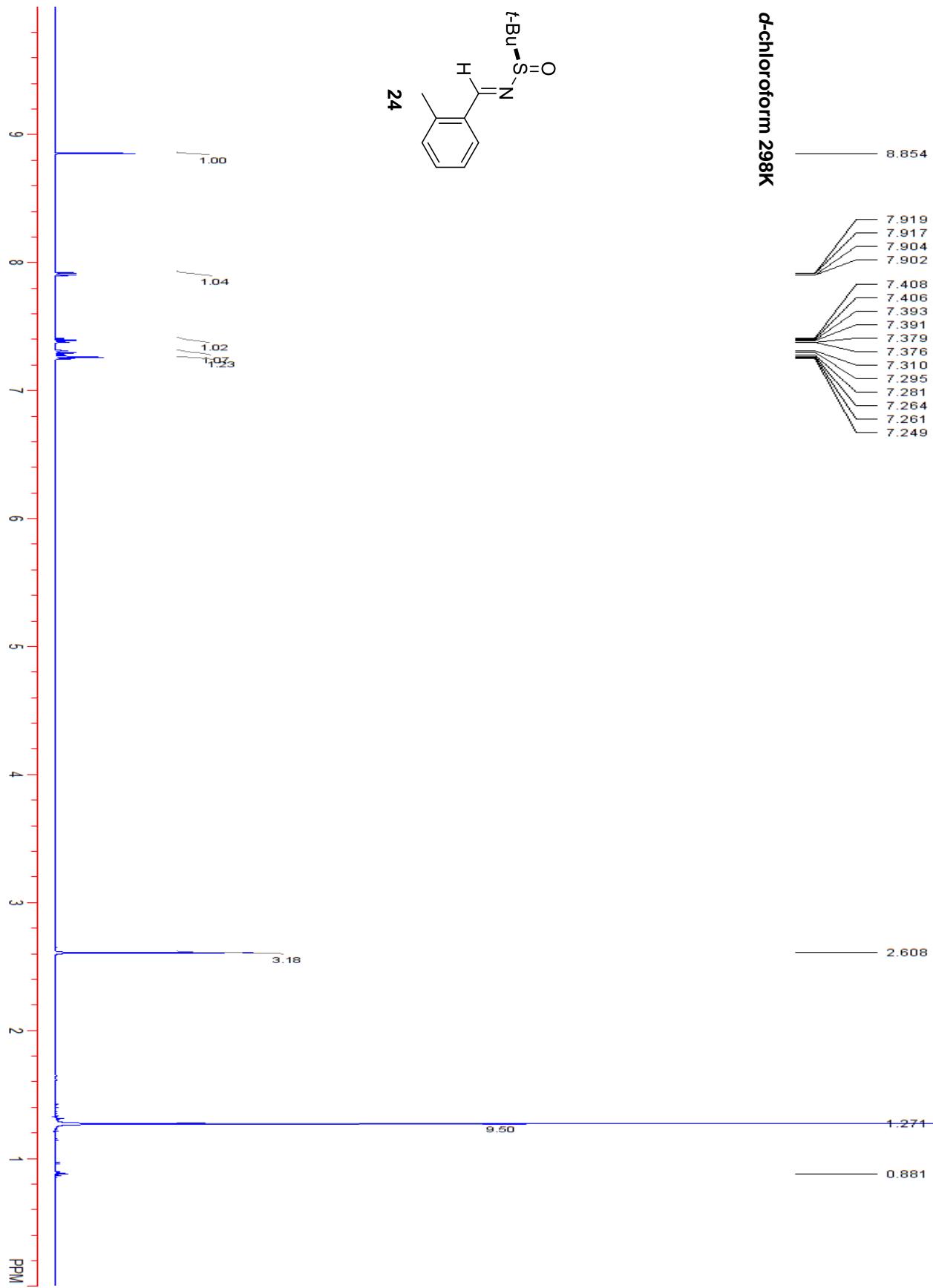


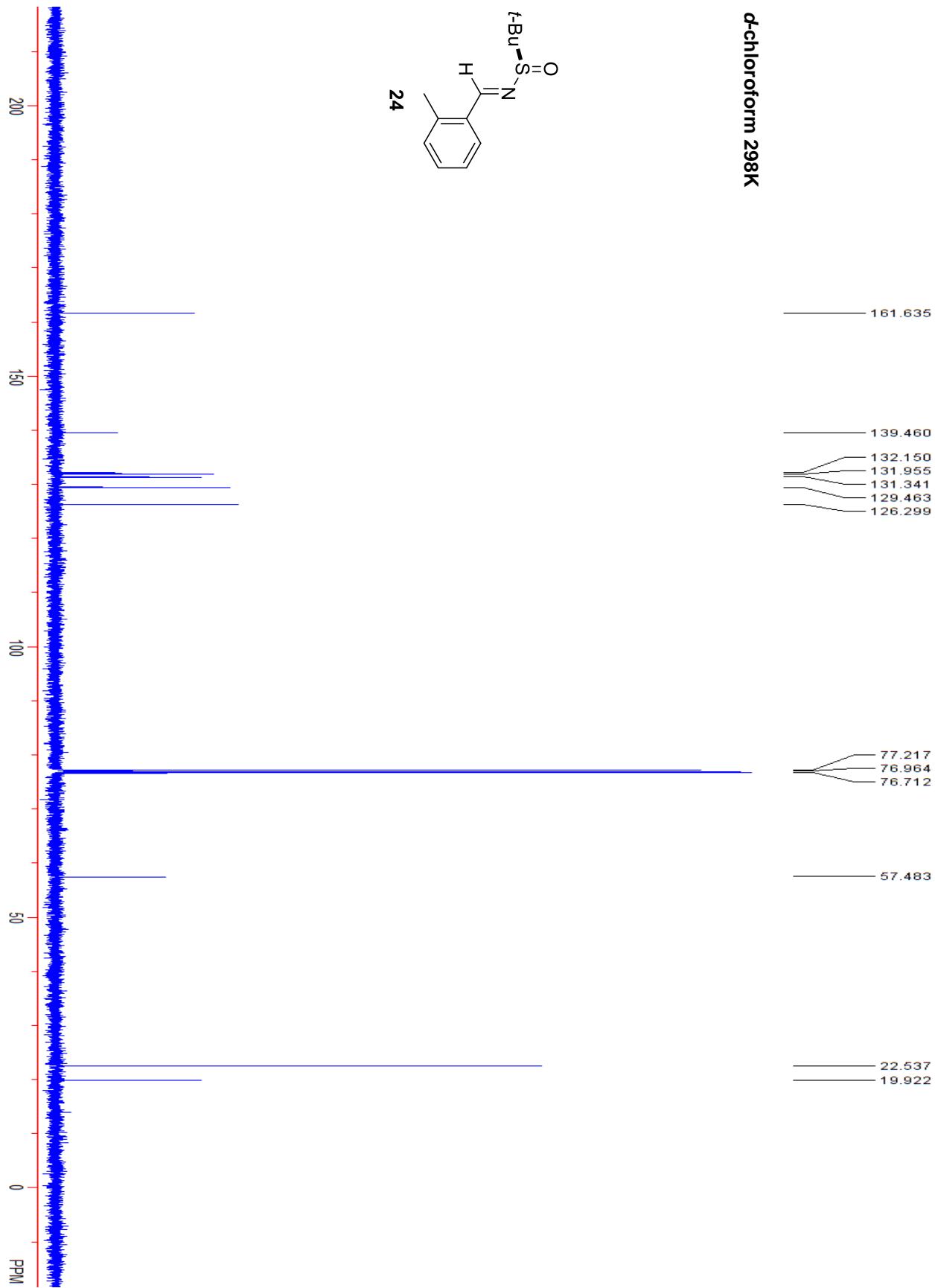


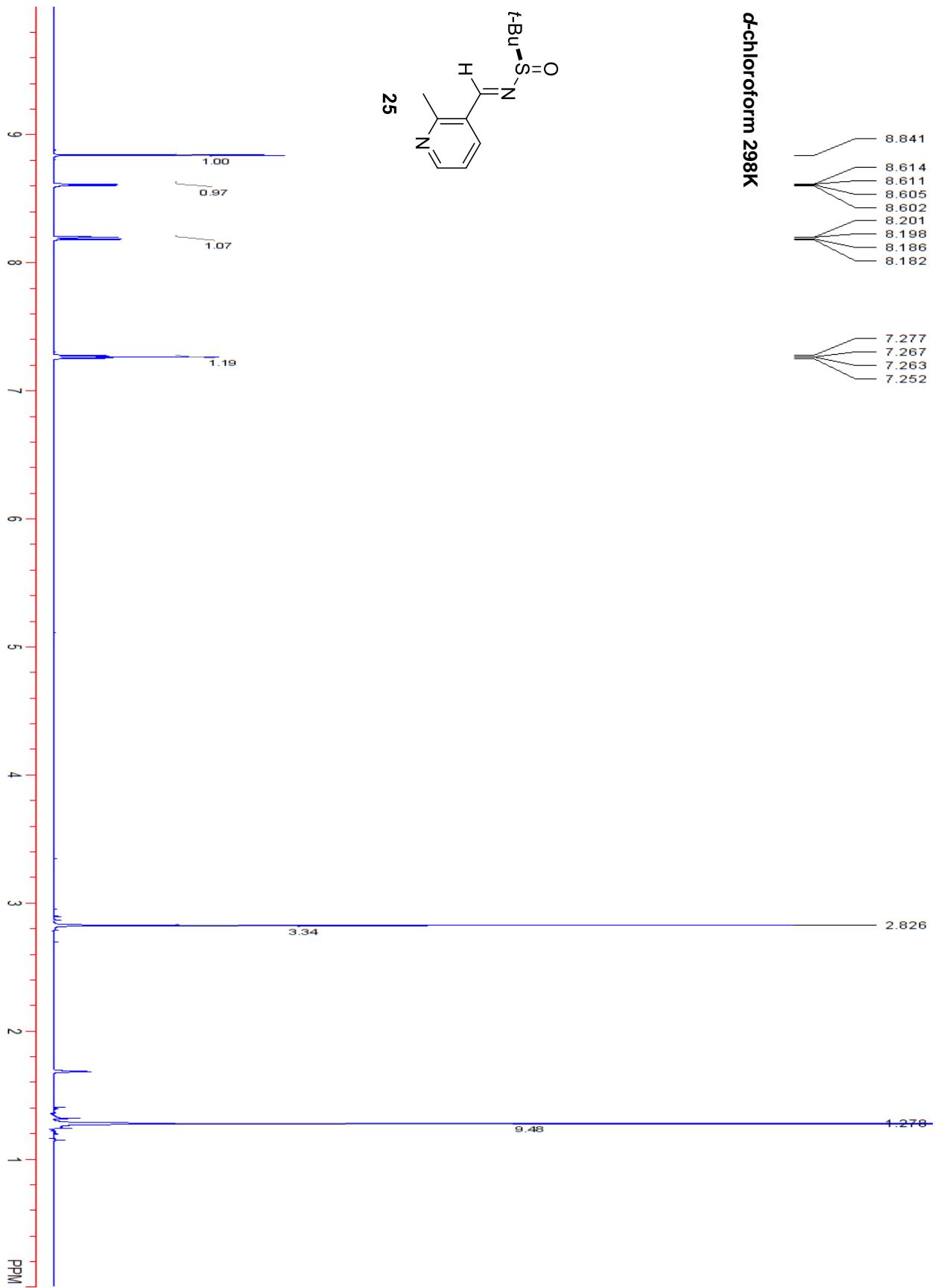


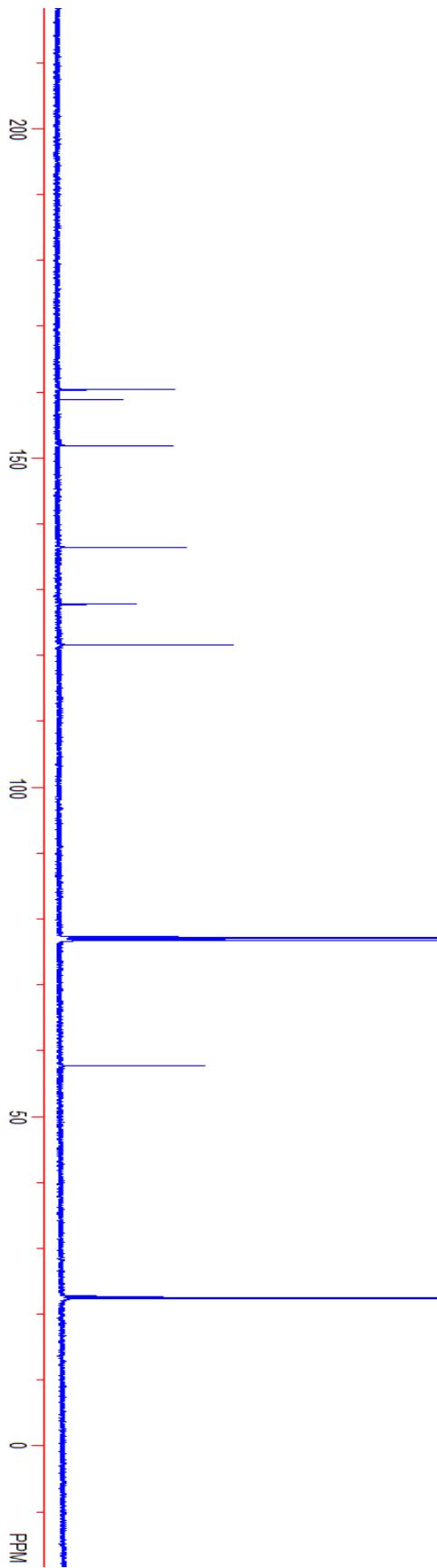
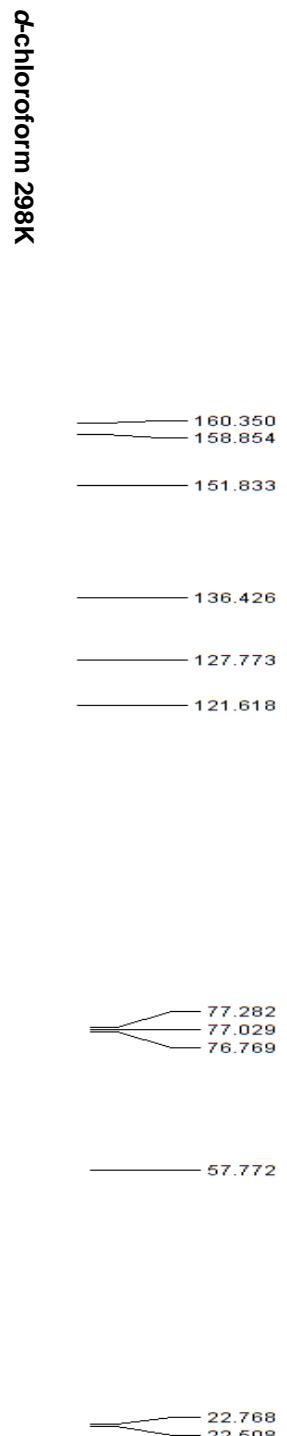
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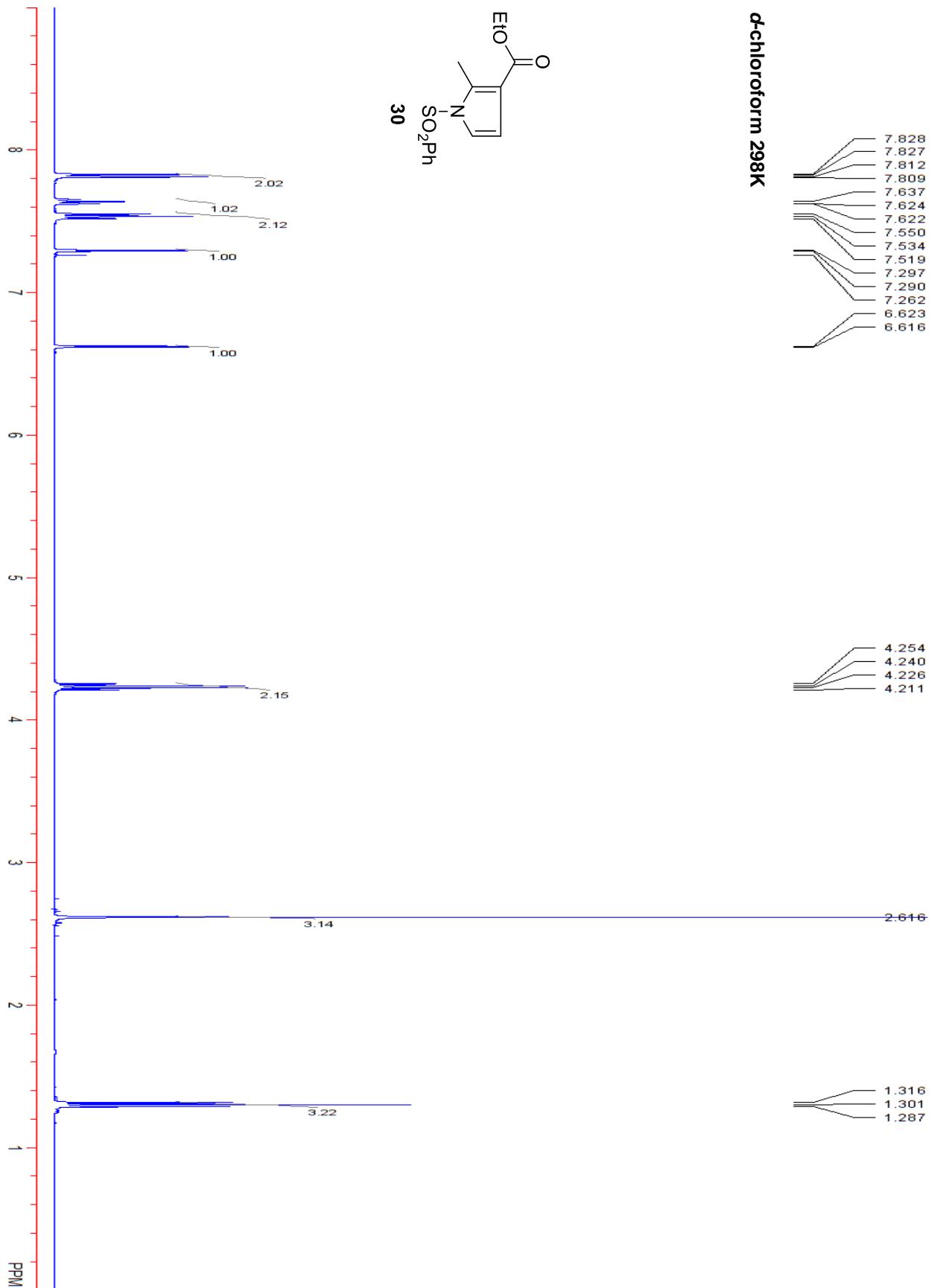




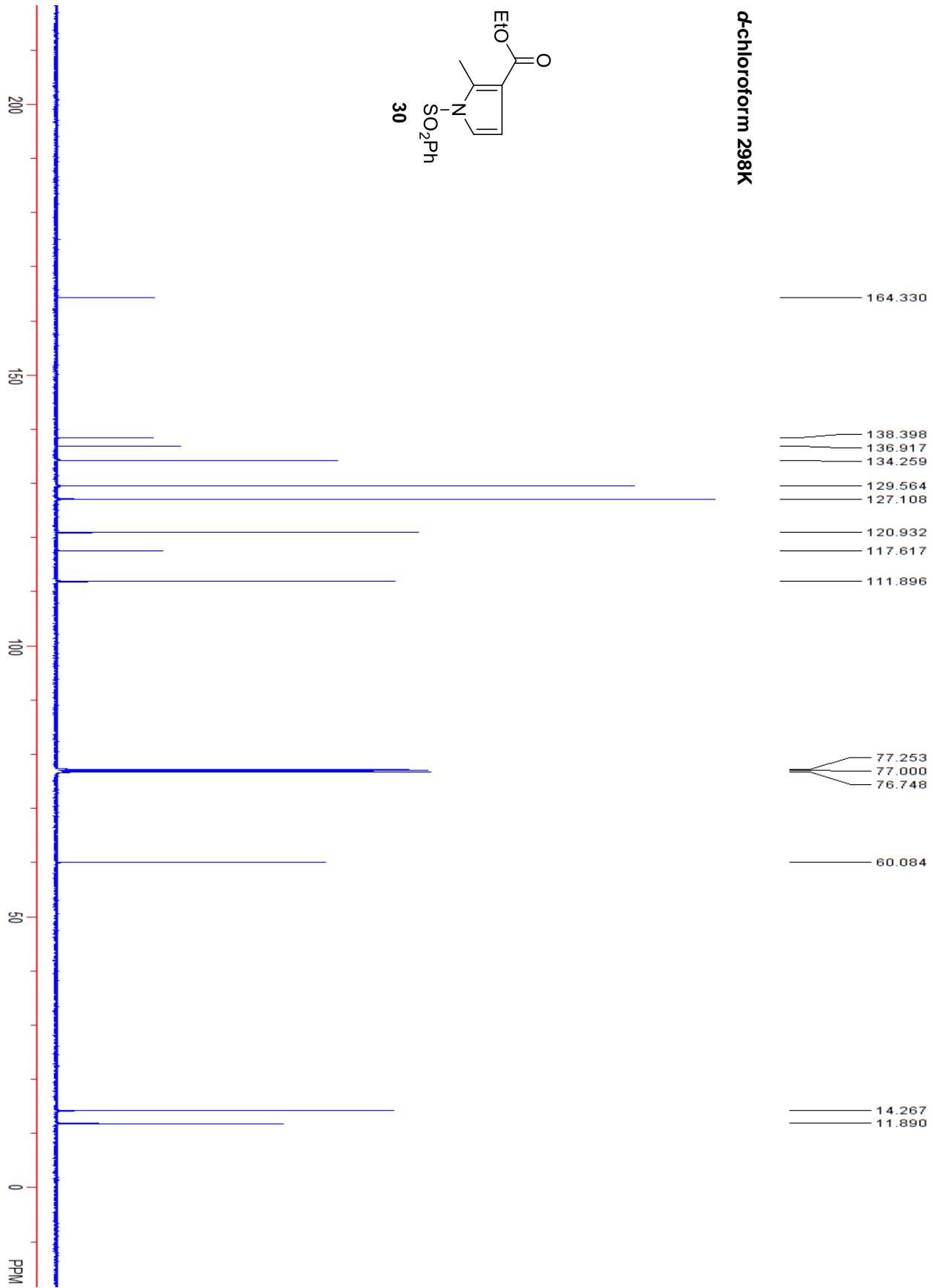
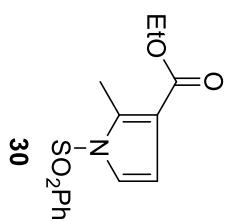


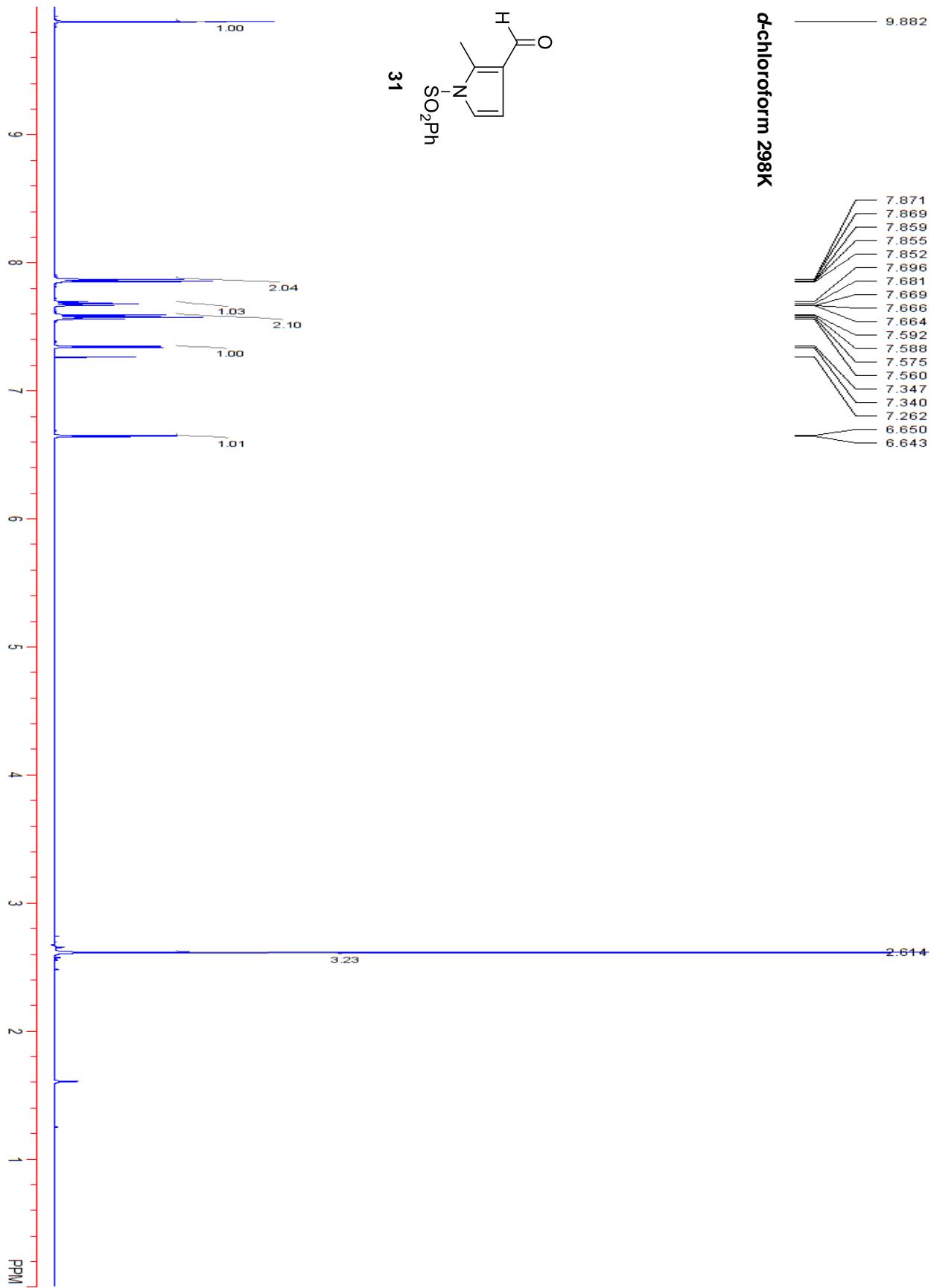




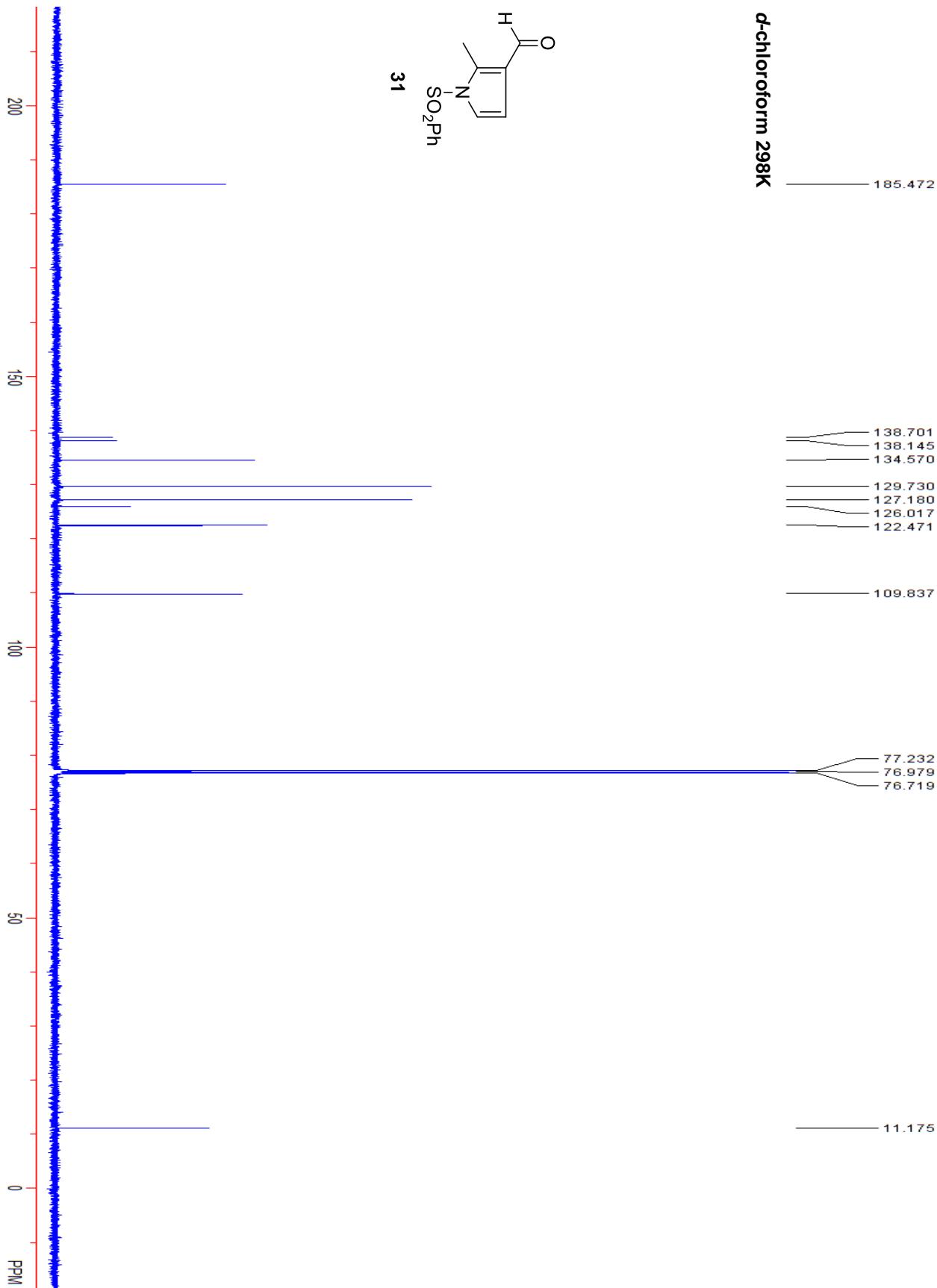
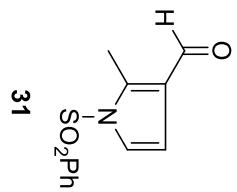


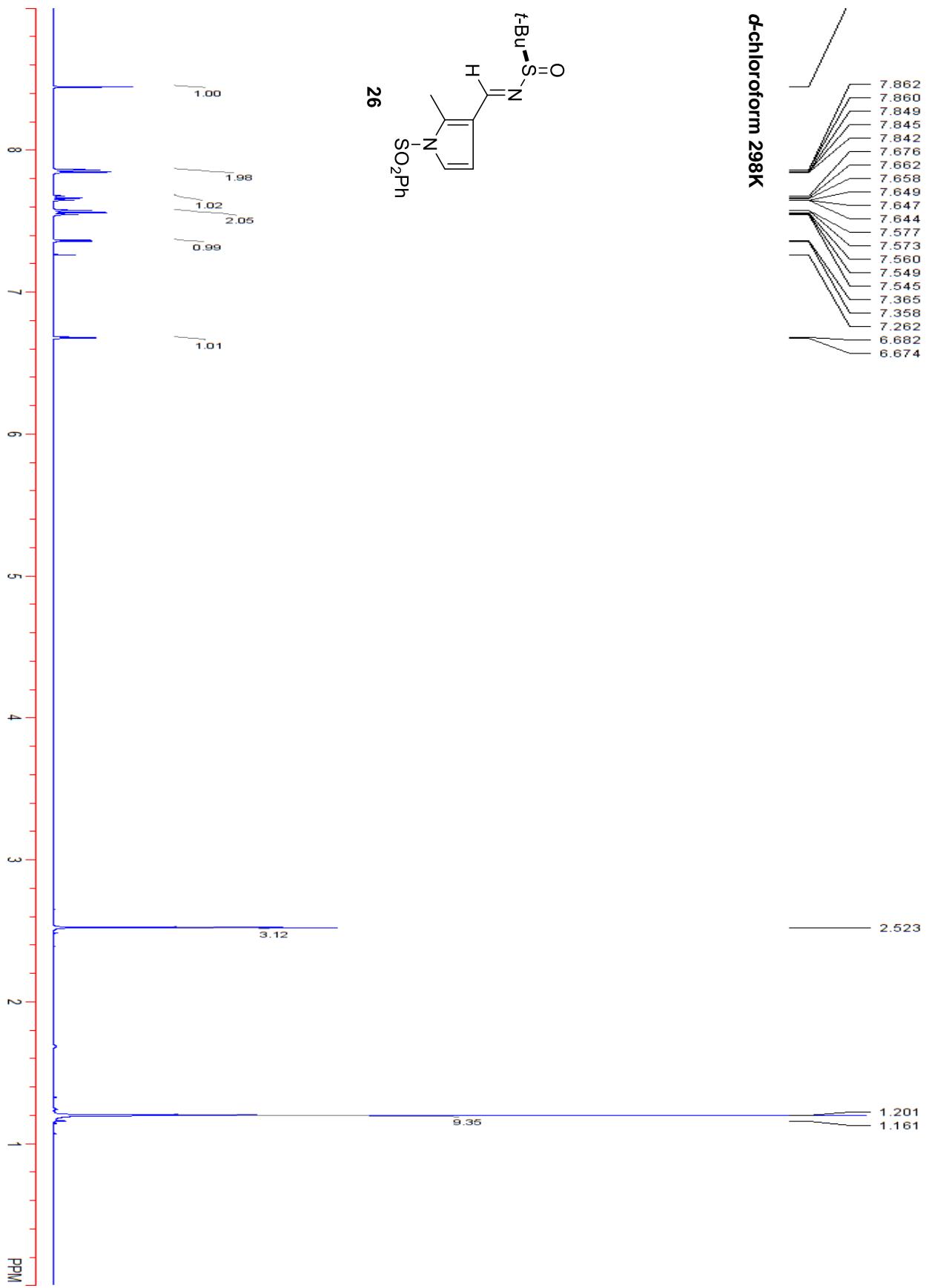
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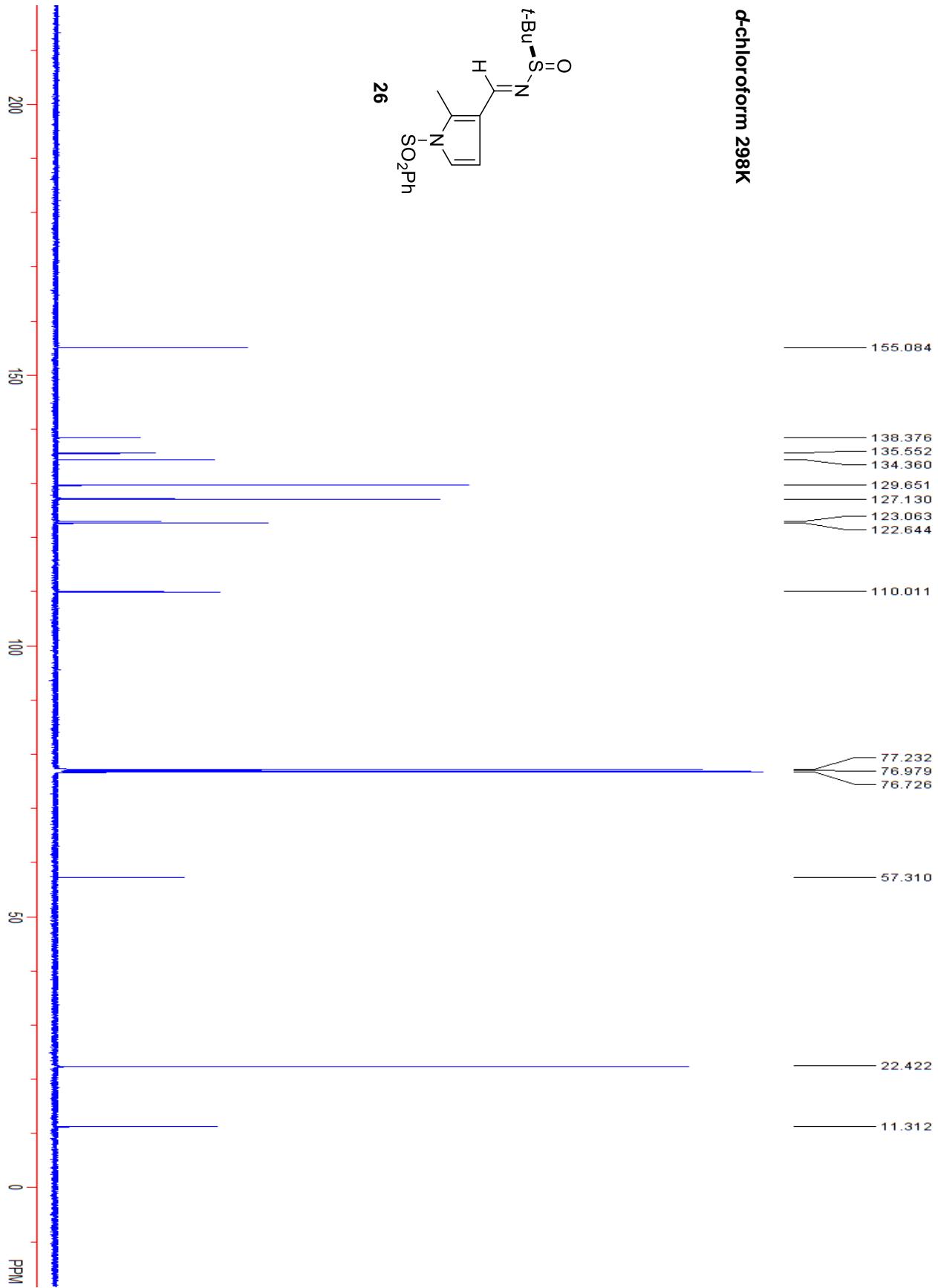
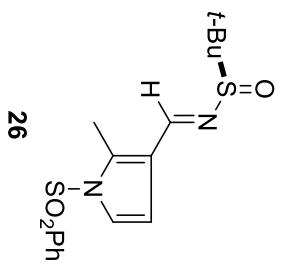


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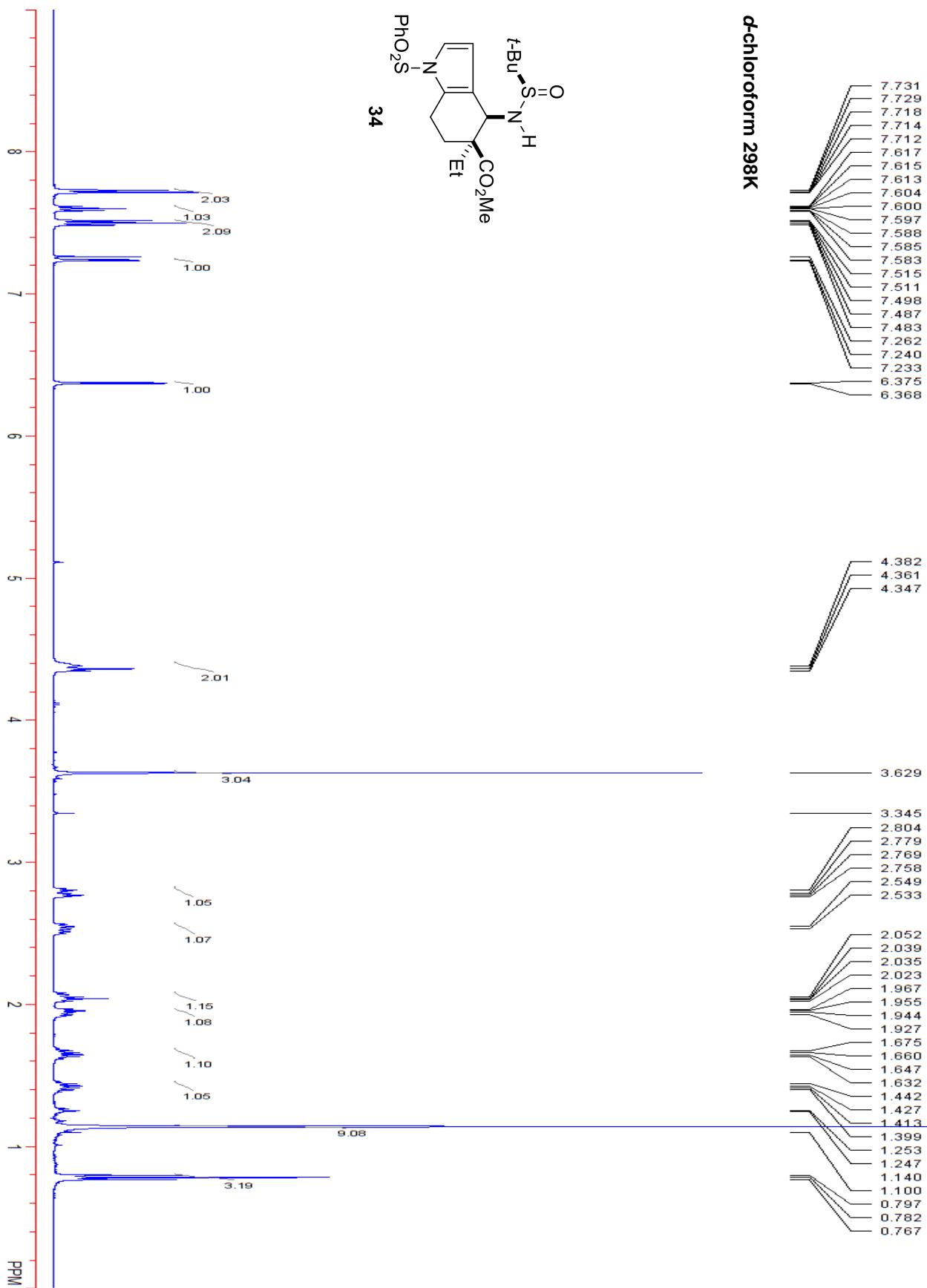


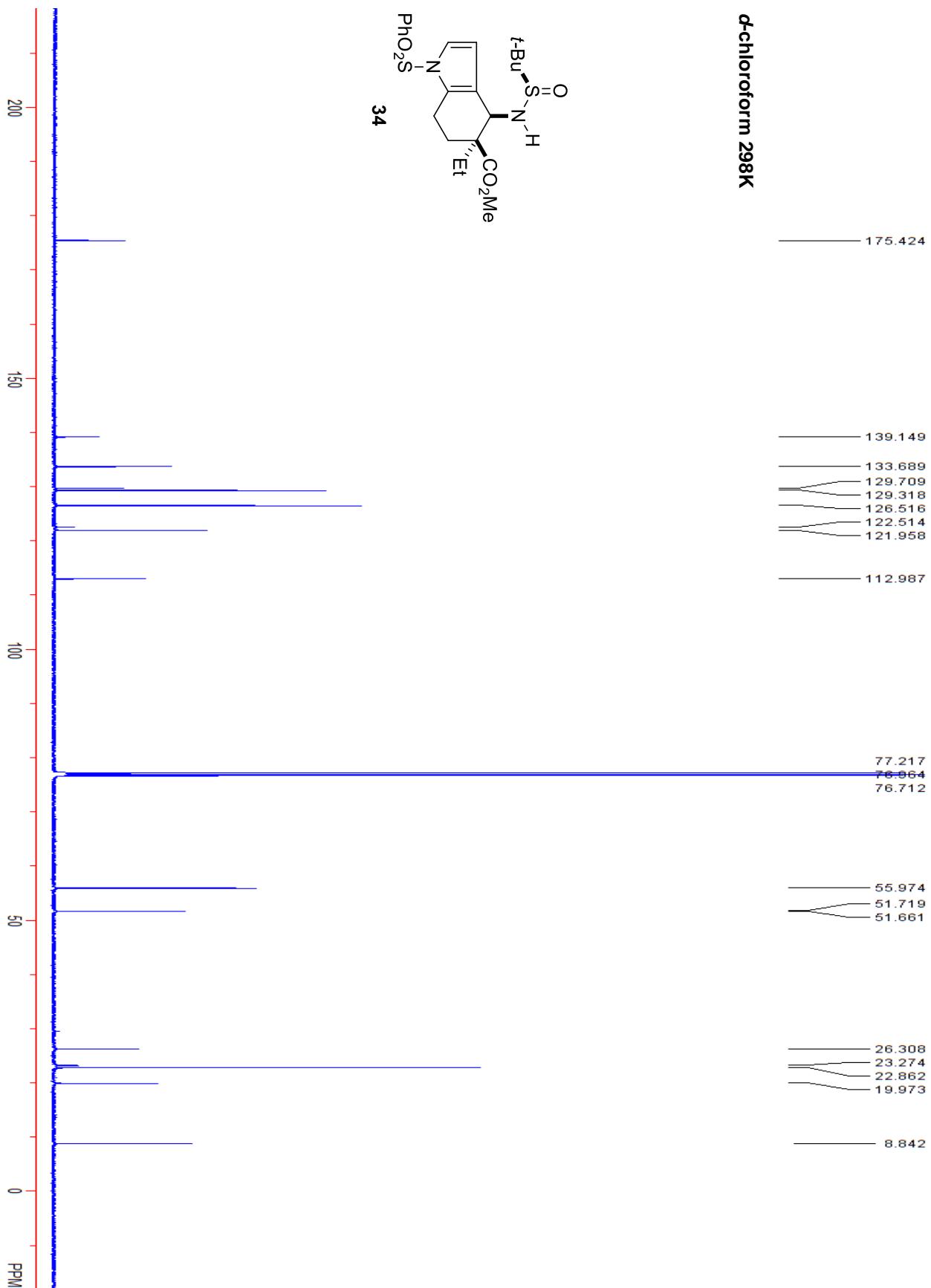


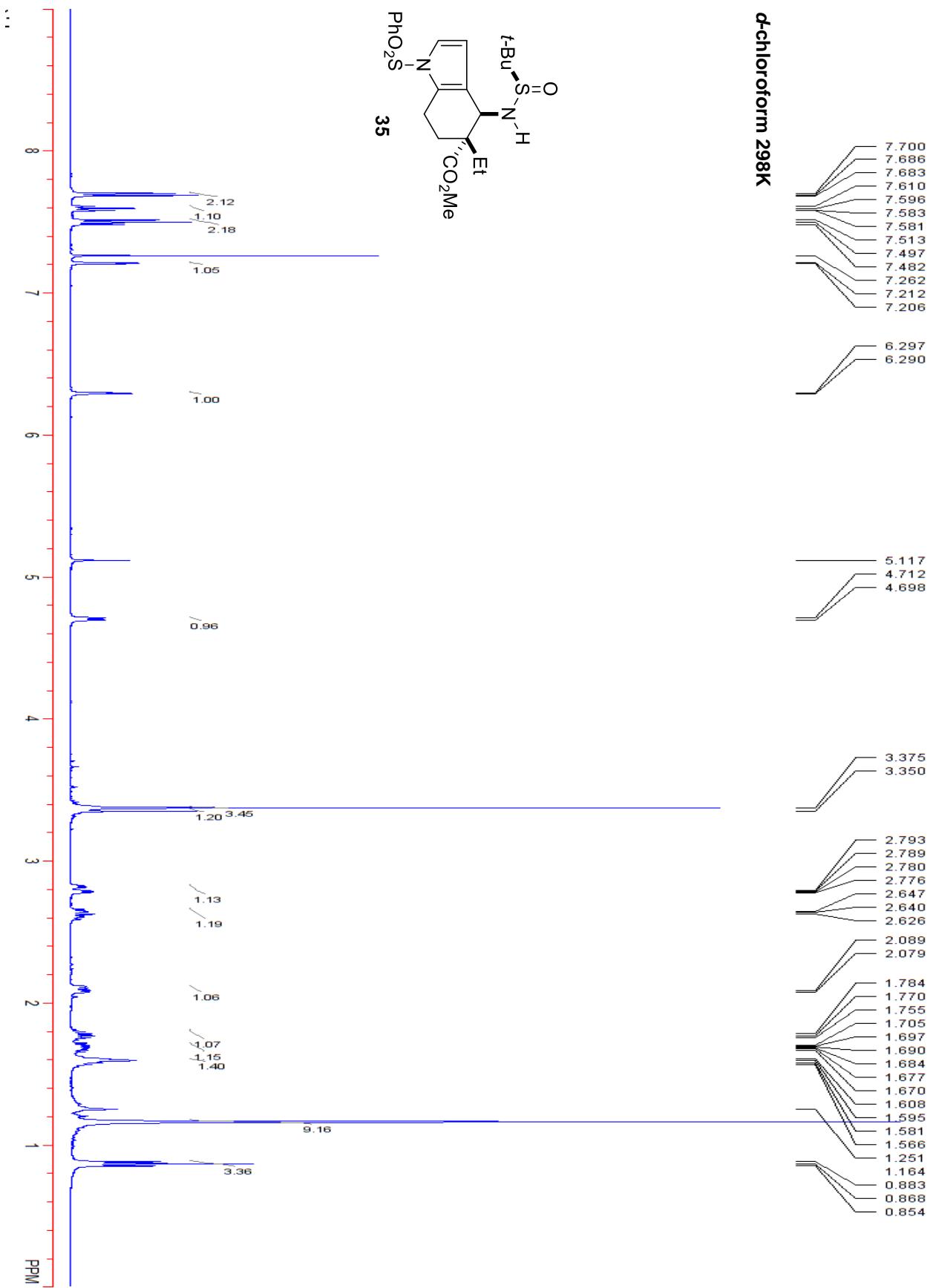
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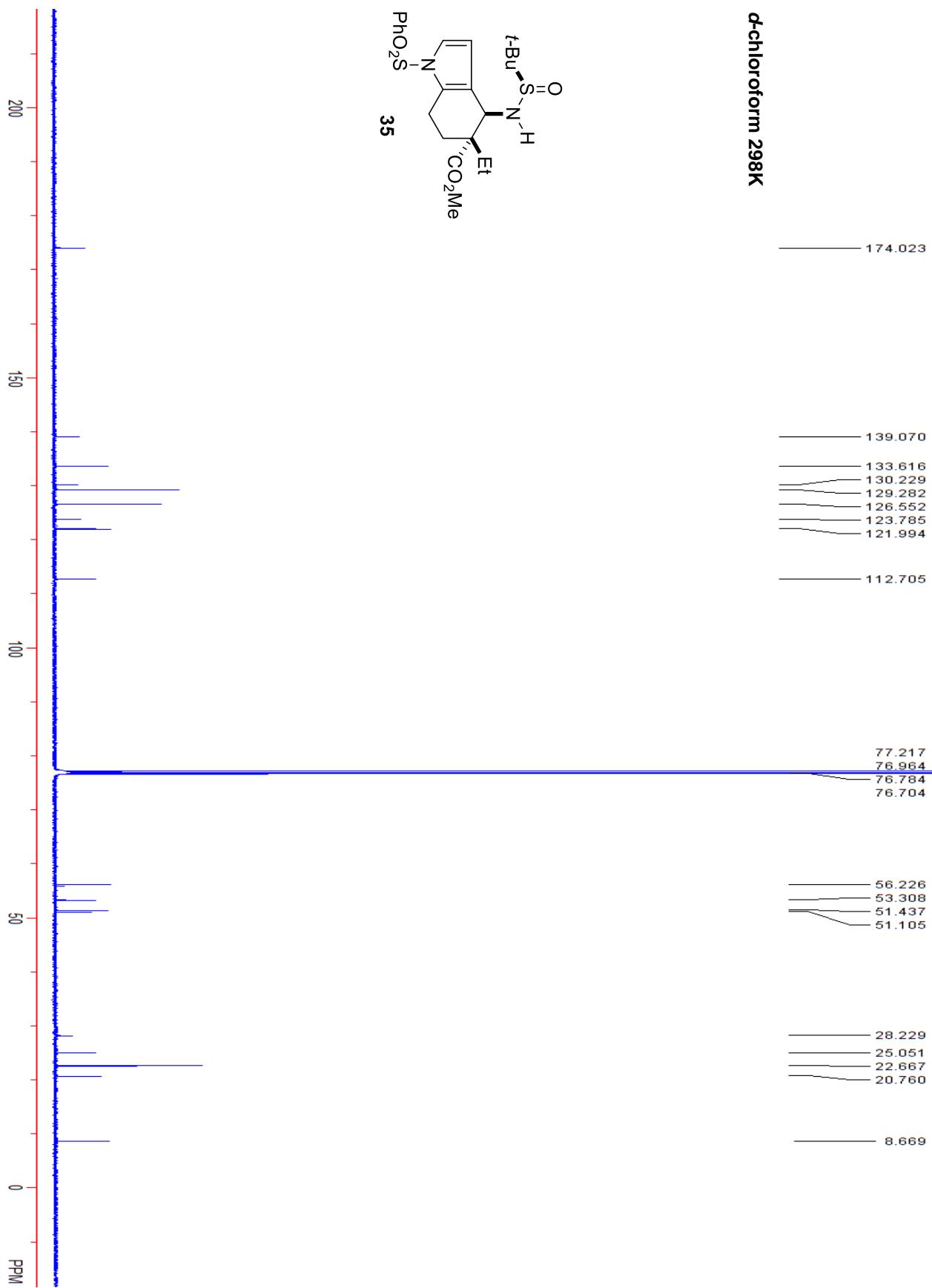
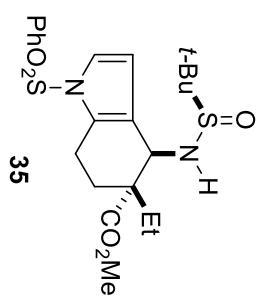
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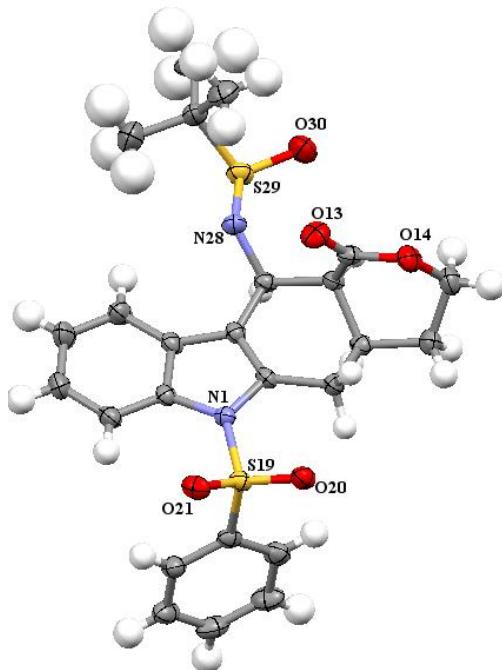


# Crystal Structure Report 16

A specimen of  $C_{25}H_{27}N_2O_5S_2$ , approximate dimensions 0.046 mm x 0.164 mm x 0.622 mm, was used for the X-ray crystallographic analysis. The X-ray intensity data were measured.

The total exposure time was 9.75 hours. The frames were integrated with the Bruker SAINT software package using a narrow-frame algorithm. The integration of the data using an orthorhombic unit cell yielded a total of 11005 reflections to a maximum  $\theta$  angle of  $27.86^\circ$  ( $0.76\text{ \AA}$  resolution), of which 5677 were independent (average redundancy 1.939, completeness = 98.5%,  $R_{\text{int}} = 3.17\%$ ) and 4354 (76.70%) were greater than  $2\sigma(F^2)$ . The final cell constants of  $a = 16.865(7)\text{ \AA}$ ,  $b = 24.087(10)\text{ \AA}$ ,  $c = 6.115(3)\text{ \AA}$ , volume =  $2484.1(18)\text{ \AA}^3$ , are based upon the refinement of the XYZ-centroids of 4100 reflections above  $20\sigma(I)$  with  $5.111^\circ < 2\theta < 55.43^\circ$ . Data were corrected for absorption effects using the multi-scan method (SADABS). The ratio of minimum to maximum apparent transmission was 0.764. The calculated minimum and maximum transmission coefficients (based on crystal size) are 0.7637 and 1.0000.

The structure was solved and refined using the Bruker SHELXTL Software Package, using the space group P 21 21 2, with  $Z = 4$  for the formula unit,  $C_{25}H_{27}N_2O_5S_2$ . The final anisotropic full-matrix least-squares refinement on  $F^2$  with 307 variables converged at  $R1 = 4.50\%$ , for the observed data and  $wR2 = 11.60\%$  for all data. The goodness-of-fit was 1.059. The largest peak in the final difference electron density synthesis was  $0.419\text{ e}^-/\text{\AA}^3$  and the largest hole was  $-0.548\text{ e}^-/\text{\AA}^3$  with an RMS deviation of  $0.068\text{ e}^-/\text{\AA}^3$ . On the basis of the final model, the calculated density was  $1.336\text{ g/cm}^3$  and  $F(000)$ , 1052  $\text{e}^-$ .



**Ellipsoid contour percent probability level for Compound 16 = 50%**

**Table 1.** Sample and crystal data.

<b>Chemical formula</b>	C <sub>25</sub> H <sub>27</sub> N <sub>2</sub> O <sub>5</sub> S <sub>2</sub>		
<b>Formula weight</b>	499.60		
<b>Temperature</b>	173(2) K		
<b>Wavelength</b>	0.71073 Å		
<b>Crystal size</b>	0.046 x 0.164 x 0.622 mm		
<b>Crystal system</b>	orthorhombic		
<b>Space group</b>	P 21 21 2		
<b>Unit cell dimensions</b>	a = 16.865(7) Å	α = 90°	
	b = 24.087(10) Å	β = 90°	
	c = 6.115(3) Å	γ = 90°	
<b>Volume</b>	2484.1(18) Å <sup>3</sup>		
<b>Z</b>	4		
<b>Density (calculated)</b>	1.336 g/cm <sup>3</sup>		
<b>Absorption coefficient</b>	0.253 mm <sup>-1</sup>		
<b>F(000)</b>	1052		

**Table 2. Data collection and structure refinement.**

<b>Theta range for data collection</b>	1.69 to 27.86°
<b>Index ranges</b>	-18<=h<=22, -31<=k<=28, -8<=l<=8
<b>Reflections collected</b>	11005
<b>Independent reflections</b>	5677 [R(int) = 0.0317]
<b>Coverage of independent reflections</b>	98.5%
<b>Absorption correction</b>	multi-scan
<b>Max. and min. transmission</b>	1.0000 and 0.7637
<b>Structure solution technique</b>	direct methods
<b>Structure solution program</b>	SHELXL-2013 (Sheldrick, 2013)
<b>Refinement method</b>	Full-matrix least-squares on $F^2$
<b>Refinement program</b>	SHELXL-2013 (Sheldrick, 2013)
<b>Function minimized</b>	$\Sigma w(F_o^2 - F_c^2)^2$
<b>Data / restraints / parameters</b>	5677 / 0 / 307
<b>Goodness-of-fit on <math>F^2</math></b>	1.059
$\Delta/\sigma_{\text{max}}$	0.001
<b>Final R indices</b>	4354 data; $I>2\sigma(I)$ $R_1 = 0.0450$ , $wR_2 = 0.1004$ all data $R_1 = 0.0742$ , $wR_2 = 0.1160$
<b>Weighting scheme</b>	$w=1/[\sigma^2(F_o^2)+(0.0483P)^2+0.9848P]$ where $P=(F_o^2+2F_c^2)/3$
<b>Absolute structure parameter</b>	-0.0(0)
<b>Largest diff. peak and hole</b>	0.419 and -0.548 eÅ <sup>-3</sup>
<b>R.M.S. deviation from mean</b>	0.068 eÅ <sup>-3</sup>

**Table 3. Atomic coordinates and equivalent isotropic atomic displacement parameters ( $\text{\AA}^2$ ).**

$U(\text{eq})$  is defined as one third of the trace of the orthogonalized  $U_{ij}$  tensor.

	x/a	y/b	z/c	$U(\text{eq})$
C2	0.3238(2)	0.74807(14)	0.2689(7)	0.0231(8)
C3	0.3513(2)	0.80094(14)	0.2903(7)	0.0245(8)
C4	0.4128(2)	0.80987(15)	0.1290(8)	0.0286(9)
C5	0.4634(2)	0.85483(16)	0.0816(9)	0.0377(11)
C6	0.5168(2)	0.84977(18)	0.9098(10)	0.0450(12)
C7	0.5206(2)	0.80155(17)	0.7854(9)	0.0384(11)
C8	0.4722(2)	0.75600(16)	0.8287(8)	0.0320(9)
C9	0.41907(19)	0.76079(13)	0.0018(8)	0.0252(8)
C10	0.3208(2)	0.84099(13)	0.4606(7)	0.0261(8)
C11	0.2428(2)	0.81934(14)	0.5637(7)	0.0249(8)
C12	0.1701(2)	0.82542(14)	0.4196(7)	0.0270(9)
C15	0.1072(2)	0.77826(18)	0.7209(9)	0.0407(11)
C16	0.1752(2)	0.73689(16)	0.7452(8)	0.0349(10)
C17	0.2495(2)	0.75642(15)	0.6179(7)	0.0265(8)
C18	0.2610(2)	0.72189(15)	0.4106(7)	0.0271(8)
C22	0.4323(2)	0.62006(14)	0.1341(7)	0.0273(9)
C23	0.5034(2)	0.61287(14)	0.0226(9)	0.0326(10)
C24	0.5649(2)	0.58421(16)	0.1266(10)	0.0415(12)
C25	0.5541(3)	0.56406(16)	0.3376(10)	0.0430(12)
C26	0.4829(3)	0.57148(17)	0.4459(9)	0.0438(12)
C27	0.4208(3)	0.59950(16)	0.3451(8)	0.0354(10)
C31	0.3111(3)	0.00739(16)	0.3527(9)	0.0404(11)
C32	0.3192(4)	0.05939(17)	0.4966(13)	0.0734(19)
C33	0.2300(3)	0.00632(19)	0.2410(10)	0.0528(14)
C34	0.3772(3)	0.0052(2)	0.1807(12)	0.0693(19)
N1	0.36269(18)	0.72243(11)	0.0884(6)	0.0241(7)
N28	0.31357(19)	0.89746(12)	0.3644(6)	0.0298(8)
O13	0.16761(16)	0.84661(12)	0.2410(6)	0.0387(7)
O14	0.10335(14)	0.80164(11)	0.5011(6)	0.0366(7)
O20	0.27938(15)	0.63700(11)	0.0913(5)	0.0328(7)
O30	0.25070(19)	0.95174(13)	0.6937(6)	0.0481(9)
S19	0.35392(5)	0.65606(3)	0.00720(18)	0.0258(2)
S29	0.32166(6)	0.94906(4)	0.5474(2)	0.0353(3)

	<b>x/a</b>	<b>y/b</b>	<b>z/c</b>	<b>U(eq)</b>
O21	0.36812(16)	0.65612(11)	0.7759(5)	0.0330(6)

**Table 4. Bond lengths (Å).**

C2-C3	1.362(5)	C2-N1	1.425(5)
C2-C18	1.506(5)	C3-C4	1.448(6)
C3-C10	1.510(5)	C4-C5	1.409(5)
C4-C9	1.419(5)	C5-C6	1.389(7)
C5-H5A	0.95	C6-C7	1.390(6)
C6-H6A	0.95	C7-C8	1.393(6)
C7-H7A	0.95	C8-C9	1.391(6)
C8-H8A	0.95	C9-N1	1.428(5)
C10-N28	1.487(5)	C10-C11	1.550(5)
C10-H10A	1.0	C11-C12	1.518(5)
C11-C17	1.555(5)	C11-H11A	1.0
C12-O13	1.206(5)	C12-O14	1.358(5)
C15-O14	1.458(6)	C15-C16	1.526(6)
C15-H15A	0.99	C15-H15B	0.99
C16-C17	1.548(5)	C16-H16A	0.99
C16-H16B	0.99	C17-C18	1.528(6)
C17-H17A	1.0	C18-H18A	0.99
C18-H18B	0.99	C22-C23	1.391(6)
C22-C27	1.395(6)	C22-S19	1.761(4)
C23-C24	1.398(6)	C23-H23A	0.95
C24-C25	1.390(8)	C24-H24A	0.95
C25-C26	1.384(7)	C25-H25A	0.95
C26-C27	1.391(6)	C26-H26A	0.95
C27-H27A	0.95	C31-C33	1.529(7)
C31-C34	1.534(7)	C31-C32	1.537(7)
C31-S29	1.850(5)	C32-H32A	0.98
C32-H32B	0.98	C32-H32C	0.98
C33-H33A	0.98	C33-H33B	0.98
C33-H33C	0.98	C34-H34A	0.98
C34-H34B	0.98	C34-H34C	0.98
N1-S19	1.680(3)	N28-S29	1.678(3)
O20-S19	1.434(3)	O30-S29	1.496(3)
S19-O21	1.434(3)		

**Table 5. Bond angles (°).**

C3-C2-N1	108.8(3)	C3-C2-C18	125.2(3)
N1-C2-C18	126.0(3)	C2-C3-C4	108.6(3)
C2-C3-C10	123.2(3)	C4-C3-C10	128.2(3)
C5-C4-C9	118.9(4)	C5-C4-C3	133.5(4)
C9-C4-C3	107.6(3)	C6-C5-C4	118.7(4)
C6-C5-H5A	120.6	C4-C5-H5A	120.6
C5-C6-C7	121.2(4)	C5-C6-H6A	119.4
C7-C6-H6A	119.4	C6-C7-C8	121.8(4)
C6-C7-H7A	119.1	C8-C7-H7A	119.1
C9-C8-C7	117.2(4)	C9-C8-H8A	121.4
C7-C8-H8A	121.4	C8-C9-C4	122.2(3)
C8-C9-N1	131.1(3)	C4-C9-N1	106.6(3)
N28-C10-C3	109.9(3)	N28-C10-C11	113.5(3)
C3-C10-C11	110.8(3)	N28-C10-H10A	107.5
C3-C10-H10A	107.5	C11-C10-H10A	107.5
C12-C11-C10	114.7(3)	C12-C11-C17	106.0(3)
C10-C11-C17	110.7(3)	C12-C11-H11A	108.4
C10-C11-H11A	108.4	C17-C11-H11A	108.4
O13-C12-O14	118.9(3)	O13-C12-C11	126.5(4)
O14-C12-C11	114.6(4)	O14-C15-C16	112.1(4)
O14-C15-H15A	109.2	C16-C15-H15A	109.2
O14-C15-H15B	109.2	C16-C15-H15B	109.2
H15A-C15-H15B	107.9	C15-C16-C17	111.1(3)
C15-C16-H16A	109.4	C17-C16-H16A	109.4
C15-C16-H16B	109.4	C17-C16-H16B	109.4
H16A-C16-H16B	108.0	C18-C17-C16	110.8(3)
C18-C17-C11	111.3(3)	C16-C17-C11	110.2(3)
C18-C17-H17A	108.2	C16-C17-H17A	108.2
C11-C17-H17A	108.2	C2-C18-C17	109.8(3)
C2-C18-H18A	109.7	C17-C18-H18A	109.7
C2-C18-H18B	109.7	C17-C18-H18B	109.7
H18A-C18-H18B	108.2	C23-C22-C27	121.9(4)
C23-C22-S19	119.5(3)	C27-C22-S19	118.6(3)
C22-C23-C24	118.6(5)	C22-C23-H23A	120.7
C24-C23-H23A	120.7	C25-C24-C23	119.8(4)

C25-C24-H24A	120.1	C23-C24-H24A	120.1
C26-C25-C24	120.8(4)	C26-C25-H25A	119.6
C24-C25-H25A	119.6	C25-C26-C27	120.3(5)
C25-C26-H26A	119.8	C27-C26-H26A	119.8
C26-C27-C22	118.5(4)	C26-C27-H27A	120.7
C22-C27-H27A	120.7	C33-C31-C34	110.1(5)
C33-C31-C32	110.4(4)	C34-C31-C32	110.9(4)
C33-C31-S29	111.2(3)	C34-C31-S29	110.2(3)
C32-C31-S29	104.0(4)	C31-C32-H32A	109.5
C31-C32-H32B	109.5	H32A-C32-H32B	109.5
C31-C32-H32C	109.5	H32A-C32-H32C	109.5
H32B-C32-H32C	109.5	C31-C33-H33A	109.5
C31-C33-H33B	109.5	H33A-C33-H33B	109.5
C31-C33-H33C	109.5	H33A-C33-H33C	109.5
H33B-C33-H33C	109.5	C31-C34-H34A	109.5
C31-C34-H34B	109.5	H34A-C34-H34B	109.5
C31-C34-H34C	109.5	H34A-C34-H34C	109.5
H34B-C34-H34C	109.5	C2-N1-C9	108.3(3)
C2-N1-S19	126.9(3)	C9-N1-S19	124.4(3)
C10-N28-S29	114.0(3)	C12-O14-C15	117.7(3)
O20-S19-O21	120.03(18)	O20-S19-N1	106.01(16)
O21-S19-N1	106.01(17)	O20-S19-C22	110.00(19)
O21-S19-C22	108.05(19)	N1-S19-C22	105.79(16)
O30-S29-N28	111.47(18)	O30-S29-C31	105.9(2)
N28-S29-C31	97.2(2)		

**Table 6. Torsion angles (°).**

N1-C2-C3-C4	-3.1(4)	C18-C2-C3-C4	178.2(4)
N1-C2-C3-C10	177.8(3)	C18-C2-C3-C10	-0.9(6)
C2-C3-C4-C5	-177.1(5)	C10-C3-C4-C5	1.9(7)
C2-C3-C4-C9	2.6(4)	C10-C3-C4-C9	-178.4(4)
C9-C4-C5-C6	0.9(7)	C3-C4-C5-C6	-179.5(5)
C4-C5-C6-C7	0.2(7)	C5-C6-C7-C8	-0.9(8)
C6-C7-C8-C9	0.4(7)	C7-C8-C9-C4	0.8(6)
C7-C8-C9-N1	-179.5(4)	C5-C4-C9-C8	-1.4(6)
C3-C4-C9-C8	178.8(4)	C5-C4-C9-N1	178.8(4)
C3-C4-C9-N1	-0.9(4)	C2-C3-C10-N28	-140.0(4)

C4-C3-C10-N28	41.1(5)	C2-C3-C10-C11	-13.8(5)
C4-C3-C10-C11	167.3(4)	N28-C10-C11-C12	48.6(4)
C3-C10-C11-C12	-75.6(4)	N28-C10-C11-C17	168.5(3)
C3-C10-C11-C17	44.3(4)	C10-C11-C12-O13	-2.6(5)
C17-C11-C12-O13	-125.0(4)	C10-C11-C12-O14	173.9(3)
C17-C11-C12-O14	51.5(4)	O14-C15-C16-C17	38.1(5)
C15-C16-C17-C18	-106.1(4)	C15-C16-C17-C11	17.5(5)
C12-C11-C17-C18	61.6(4)	C10-C11-C17-C18	-63.4(4)
C12-C11-C17-C16	-61.7(4)	C10-C11-C17-C16	173.3(3)
C3-C2-C18-C17	-15.8(5)	N1-C2-C18-C17	165.7(3)
C16-C17-C18-C2	169.5(3)	C11-C17-C18-C2	46.6(4)
C27-C22-C23-C24	-0.1(6)	S19-C22-C23-C24	179.9(3)
C22-C23-C24-C25	-0.5(6)	C23-C24-C25-C26	0.7(6)
C24-C25-C26-C27	-0.2(7)	C25-C26-C27-C22	-0.4(6)
C23-C22-C27-C26	0.6(6)	S19-C22-C27-C26	-179.5(3)
C3-C2-N1-C9	2.6(4)	C18-C2-N1-C9	-178.8(3)
C3-C2-N1-S19	175.3(3)	C18-C2-N1-S19	-6.1(5)
C8-C9-N1-C2	179.3(4)	C4-C9-N1-C2	-0.9(4)
C8-C9-N1-S19	6.4(6)	C4-C9-N1-S19	-173.8(3)
C3-C10-N28-S29	-153.3(2)	C11-C10-N28-S29	82.1(3)
O13-C12-O14-C15	-177.7(4)	C11-C12-O14-C15	5.6(5)
C16-C15-O14-C12	-53.7(5)	C2-N1-S19-O20	22.8(4)
C9-N1-S19-O20	-165.6(3)	C2-N1-S19-O21	151.4(3)
C9-N1-S19-O21	-37.0(3)	C2-N1-S19-C22	-94.0(3)
C9-N1-S19-C22	77.6(3)	C23-C22-S19-O20	152.3(3)
C27-C22-S19-O20	-27.7(4)	C23-C22-S19-O21	19.5(3)
C27-C22-S19-O21	-160.4(3)	C23-C22-S19-N1	-93.6(3)
C27-C22-S19-N1	86.4(3)	C10-N28-S29-O30	-70.8(3)
C10-N28-S29-C31	178.9(3)	C33-C31-S29-O30	-52.4(4)
C34-C31-S29-O30	-174.7(4)	C32-C31-S29-O30	66.4(4)
C33-C31-S29-N28	62.4(4)	C34-C31-S29-N28	-59.9(4)
C32-C31-S29-N28	-178.7(3)		

**Table 7. Anisotropic atomic displacement parameters ( $\text{\AA}^2$ ).**

The anisotropic atomic displacement factor exponent takes the form:  $-2\pi^2 [ h^2 a^{*2} U_{11} + \dots + 2 h k a^* b^* U_{12} ]$

	<b>U<sub>11</sub></b>	<b>U<sub>22</sub></b>	<b>U<sub>33</sub></b>	<b>U<sub>23</sub></b>	<b>U<sub>13</sub></b>	<b>U<sub>12</sub></b>
C2	0.0189(15)	0.0266(16)	0.024(2)	-0.0031(15)	0.0009(16)	0.0040(14)

	<b>U<sub>11</sub></b>	<b>U<sub>22</sub></b>	<b>U<sub>33</sub></b>	<b>U<sub>23</sub></b>	<b>U<sub>13</sub></b>	<b>U<sub>12</sub></b>
C3	0.0188(15)	0.0262(17)	0.029(2)	0.0000(15)	-0.0003(17)	0.0017(14)
C4	0.0191(17)	0.0300(18)	0.037(3)	-0.0020(18)	0.0007(17)	0.0029(14)
C5	0.031(2)	0.0274(19)	0.055(3)	-0.007(2)	0.007(2)	-0.0052(15)
C6	0.032(2)	0.039(2)	0.064(4)	-0.005(2)	0.016(2)	-0.0071(18)
C7	0.030(2)	0.040(2)	0.046(3)	0.003(2)	0.012(2)	0.0017(17)
C8	0.0277(19)	0.0324(19)	0.036(3)	-0.0031(19)	0.0039(19)	0.0048(16)
C9	0.0199(15)	0.0259(16)	0.030(2)	0.0005(18)	-0.0007(18)	0.0015(12)
C10	0.0212(15)	0.0231(15)	0.034(2)	-0.0039(17)	-0.0020(17)	0.0013(13)
C11	0.0230(17)	0.0235(16)	0.028(2)	-0.0020(16)	0.0000(16)	0.0032(13)
C12	0.0244(18)	0.0229(16)	0.034(3)	-0.0030(16)	-0.0058(17)	0.0029(13)
C15	0.031(2)	0.043(2)	0.049(3)	-0.002(2)	0.012(2)	-0.0019(18)
C16	0.038(2)	0.033(2)	0.033(3)	0.0037(19)	0.008(2)	-0.0001(17)
C17	0.0247(18)	0.0263(17)	0.028(2)	0.0006(16)	-0.0007(16)	0.0033(14)
C18	0.0249(18)	0.0243(16)	0.032(2)	-0.0002(16)	0.0010(17)	-0.0004(13)
C22	0.0274(18)	0.0198(16)	0.035(3)	-0.0046(16)	-0.0032(18)	-0.0008(14)
C23	0.0291(18)	0.0253(17)	0.043(3)	0.0017(19)	0.000(2)	0.0010(14)
C24	0.026(2)	0.030(2)	0.068(4)	0.004(2)	-0.001(2)	0.0017(16)
C25	0.041(2)	0.0270(19)	0.061(4)	0.004(2)	-0.016(2)	0.0027(17)
C26	0.058(3)	0.036(2)	0.037(3)	0.003(2)	-0.011(2)	0.0080(19)
C27	0.042(2)	0.031(2)	0.034(3)	-0.0048(19)	0.003(2)	0.0053(17)
C31	0.040(2)	0.0241(18)	0.058(3)	-0.004(2)	0.011(2)	-0.0021(17)
C32	0.098(4)	0.024(2)	0.099(5)	-0.016(3)	0.009(5)	-0.005(2)
C33	0.057(3)	0.040(2)	0.061(4)	0.015(3)	0.003(3)	0.005(2)
C34	0.066(3)	0.046(3)	0.096(6)	0.010(3)	0.034(4)	-0.006(2)
N1	0.0245(15)	0.0218(13)	0.0259(18)	-0.0012(13)	0.0008(14)	0.0016(11)
N28	0.0341(17)	0.0215(14)	0.034(2)	-0.0052(14)	0.0030(16)	-0.0002(13)
O13	0.0363(15)	0.0394(15)	0.040(2)	0.0073(15)	-0.0109(14)	0.0005(12)
O14	0.0210(12)	0.0398(14)	0.049(2)	-0.0008(16)	-0.0025(15)	-0.0003(10)
O20	0.0279(13)	0.0275(12)	0.043(2)	-0.0067(13)	0.0009(13)	-0.0018(10)
O30	0.056(2)	0.0441(17)	0.045(2)	-0.0101(17)	0.0162(17)	0.0039(15)
S19	0.0250(4)	0.0226(4)	0.0297(5)	-0.0043(4)	-0.0021(4)	0.0014(3)
S29	0.0328(5)	0.0266(4)	0.0465(8)	-0.0104(5)	0.0004(5)	-0.0011(4)
O21	0.0405(15)	0.0353(14)	0.0231(16)	-0.0055(13)	-0.0047(13)	0.0067(12)