

Supporting Information  
 Synthesis, Structure and Bonding of  $\text{Sc}_6\text{MTe}_2$  ( $\text{M}=\text{Ag, Cu, Cd}$ ): Heterometal Induced Polymerization of Metal Chains in  $\text{Sc}_2\text{Te}$

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Table S1. Single crystal X-ray data collection and structure refinement parameters for  $\text{Sc}_6\text{MTe}_2$  ( $\text{M} = \text{Ag, Cu}$ )

formula, Z	$\text{Sc}_6\text{AgTe}_2$	$\text{Sc}_6\text{Cu}_{0.80(2)}\text{Te}_{2.20(2)}$
temperature	293(2) K	293(2) K
crystal system, space group, Z	orthorhombic, $Pnma$ , 4	orthorhombic, $Pnma$ , 4
lattice parameters <sup>a</sup> (Å, Å <sup>3</sup> )	$a = 20.094$ (9) $b = 3.913$ (1) $c = 10.688$ (2) $V = 840.4$ (5)	$a = 19.853$ (4) $b = 3.914$ (1) $c = 10.644$ (2) $V = 827.1$ (3)
$d_{\text{calc}}$ , (g/cm <sup>3</sup> )	5.002	4.726
crystal size (mm)	0.11 x 0.1 x 0.04	0.08 x 0.08 x 0.04
diffractometer	SMART CCD	SMART CCD
absorption coefficient (mm <sup>-1</sup> )	13.537	13.957
index range	$-12 \leq h \leq 26$ , $-5 \leq k \leq 2$ , $-12 \leq l \leq 12$	$-11 \leq h \leq 25$ , $-2 \leq k \leq 5$ , $-14 \leq l \leq 8$
reflections collected	3241	3149
independent reflections	1042 [ $R(\text{int}) = 0.0273$ ]	1120 [ $R(\text{int}) = 0.0506$ ]
absorption correction	SADABS	SADABS
goodness -of-fit on $F^2$	1.123	1.016
$R1$ , $wR2^b$ for $I > 2\sigma(F_o^2)$	$R1 = 0.0239$ , $Rw = 0.0574$	$R1 = 0.0276$ , $Rw = 0.0623$
$R1$ , $wR2$ for all data	$R1 = 0.0265$ , $Rw = 0.0583$	$R1 = 0.0345$ , $Rw = 0.0643$
largest diff. peak and hole	0.977 and -1.875 e/Å <sup>3</sup>	1.633 and -0.997 e/Å <sup>3</sup>

<sup>a</sup> Guinier data.

<sup>b</sup>  $R1 = \sum || F_o | - | F_c || / \sum | F_o |$ ;  $wR2 = \{\sum [w(F_o^2 - F_c^2)^2] / \sum [w(F_o^2)^2]\}^{1/2}$ .  
 in  $\text{Sc}_6\text{AgTe}_2$ :  $w^{-1} = [\sigma^2(F_o^2) + (0.0327p)^2 + 1.3898p]$ , where  $p = (F_o^2 + 2F_c^2)/3$   
 in  $\text{Sc}_6\text{Cu}_{0.80(2)}\text{Te}_{2.20(2)}$ :  $w^{-1} = [\sigma^2(F_o^2) + (0.0310p)^2]$ , where  $p = (F_o^2 + 2F_c^2)/3$ .

**Table S2.** Anisotropic displacement parameters ( $\text{\AA}^2 \times 103$ ) for  $\text{Sc}_6\text{AgTe}_2$  and  $\text{Sc}_6\text{Cu}_{0.80(2)}\text{Te}_{2.20(2)}$ .  
The anisotropic displacement factor exponent takes the form:  $-2p^2[h^2 a^*2U11 + \dots + 2h k a^* b^* U12]$

$\text{Sc}_6\text{AgTe}_2$	U11	U22	U33	U23	U13	U12
Ag1	12(1)	10(1)	11(1)	0	2(1)	0
Te2	12(1)	10(1)	10(1)	0	1(1)	0
Te3	12(1)	9(1)	11(1)	0	0(1)	0
Sc1	12(1)	20(1)	13(1)	0	2(1)	0
Sc2	14(1)	16(1)	9(1)	0	0(1)	0
Sc3	13(1)	12(1)	10(1)	0	0(1)	0
Sc4	16(1)	15(1)	15(1)	0	-4(1)	0
Sc5	17(1)	10(1)	11(1)	0	0(1)	0
Sc6	13(1)	23(1)	15(1)	0	1(1)	0

  

$\text{Sc}_6\text{Cu}_{0.80(2)}\text{Te}_{2.20(2)}$	U11	U22	U33	U23	U13	U12
Cu1	11(1)	9(1)	10(1)	0	3(1)	0
Te2	12(1)	11(1)	8(1)	0	1(1)	0
Te3	11(1)	9(1)	10(1)	0	0(1)	0
Sc1	10(1)	24(1)	12(1)	0	1(1)	0
Sc2	14(1)	26(1)	8(1)	0	0(1)	0
Sc3	13(1)	13(1)	10(1)	0	0(1)	0
Sc4	17(1)	23(1)	16(1)	0	6(1)	0
Sc5	13(1)	10(1)	10(1)	0	0(1)	0
Sc6	12(1)	18(1)	15(1)	0	2(1)	0