

Crystal Data and Structure Refinement for (C₅Me₅)₂Sr(THF)₂ (2) and (C₅Me₅)₂Ba(THF)₂ (3)

parameter	(2)	(3)
empirical formula	C ₂₈ H ₄₆ O ₂ Sr	C ₂₈ H ₄₆ O ₂ Ba
formula weight	502.27	551.99
temp, K	193	193
λ (Mo K α), Å	0.71073	0.71073
crystal system	monoclinic	monoclinic
space group	C2/c (No. 15)	C2/c (No 15)
<i>a</i> , Å	21.931(4)	22.054(4)
<i>b</i> , Å	20.688(4)	20.556(4)
<i>c</i> , Å	15.877(3)	16.087(3)
α , deg	90	90
β , deg	130.17(3)	129.45(3)
γ , deg	90	90
<i>V</i> (Å ³), <i>Z</i>	5505(2), 8	5631(2), 8
<i>d</i> calc, g/cm ³	1.212	1.302
μ , mm ⁻¹	1.979	1.430
<i>F</i> (000)	2144	2288
Crystal Size, mm	0.35 × 0.35 × 0.27	0.50 × 0.50 × 0.40
θ range, deg	2.58-24.98	2.55-24.04
limiting indices	0 ≤ <i>h</i> ≤ 26 0 ≤ <i>k</i> ≤ 24 -18 ≤ <i>l</i> ≤ 14	0 ≤ <i>h</i> ≤ 25 0 ≤ <i>k</i> ≤ 23 -18 ≤ <i>l</i> ≤ 14
reflections collected	4231	4220
independent reflections	4010	4133
no. of reflections [<i>F</i> ₀ > 4 σ (<i>F</i>)]	2919	3724
refinement method	full-matrix least-squares on <i>F</i> ²	
data/parameters	4010/299	4133/298
goodness-of-fit on <i>F</i> ²	1.033	1.031
final <i>R</i> indices [<i>I</i> > 2 σ (<i>I</i>)] ^a	<i>R</i> _I =0.0686, <i>wR</i> ₂ =0.1584	<i>R</i> _I =0.0409, <i>wR</i> ₂ =0.1042
<i>R</i> indices (all data)	<i>R</i> _I =0.1054, <i>wR</i> ₂ =0.1720	<i>R</i> _I =0.0471, <i>wR</i> ₂ =0.1076
extinction coefficient	0.0014(3)	none
max/min diff peak, e Å ⁻³	1.365/-1.75	1.012/-1.587

$$^a R_I = 3 \left| |F_o| - |F_c| \right| / 3 |F_o|, wR_2 = \{3[w(F_o^2 - F_c^2)^2] / 3[w(F_o^2)^2]\}^{1/2}$$

Using Cyclopentadienyl Precursors by J. Ihanus et al.

Complex (2)

US0111130

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data_srl

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_chemical_name_common ?
 _chemical_formula_moiety ?
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'C28 H46 O2 Sr'

_chemical_formula_weight 502.27

loop

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 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
 'O' 'O' 0.0106 0.0060
 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
 'Sr' 'Sr' -1.5307 3.2498
 'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

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 'x+1/2, y+1/2, z'
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 '-x, -y, -z'
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 'x+1/2, -y+1/2, z-1/2'

_cell_length_a 21.931(4)
 _cell_length_b 20.688(4)
 _cell_length_c 15.877(3)
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 _cell_angle_gamma 90.00
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_exptl_absorpt_process_details  'North etal. (1968). Acta Cryst. A24,
351-359'
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_diffraction_radiation_monochromator graphite
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_diffraction_measurement_method    'omega-2theta'
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_computing_cell_refinement         'Rigaku AFC-7S software'
_computing_data_reduction         'Texsan (1993)'
_computing_structure_solution     'SHELXS-97 (Sheldrick, 1990)'
_computing_structure_refinement   'SHELXL-97 (Sheldrick, 1997)'
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_computing_publication_material   'SHELXL-97 (Sheldrick, 1997)'

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_refine_special_details

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Refinement of F^2 against ALL reflections. The weighted R-factor wR and goodness of fit S are based on F^2 , conventional R-factors R are based on F, with F set to zero for negative F^2 . The threshold expression of $F^2 > 2\sigma(F^2)$ is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on F^2 are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

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loop

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_atom_site_calc_flag
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Sr1 Sr 0.22579(3) 0.63326(3) 0.74950(5) 0.0318(2) Uani 1 d . . .
C1 C 0.1373(4) 0.7202(4) 0.5642(5) 0.0365(17) Uani 1 d . . .
C2 C 0.1196(4) 0.7428(3) 0.6288(5) 0.0342(16) Uani 1 d . . .
C3 C 0.0736(4) 0.6950(3) 0.6301(5) 0.0345(16) Uani 1 d . . .
C4 C 0.0619(4) 0.6433(3) 0.5622(6) 0.0426(18) Uani 1 d . . .
C5 C 0.1014(4) 0.6584(4) 0.5230(5) 0.046(2) Uani 1 d . . .
C6 C 0.1760(5) 0.7606(5) 0.5299(7) 0.062(3) Uani 1 d . . .

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H6A H 0.1352 0.7746 0.4533 0.094 Uiso 1 calc R . .
H6B H 0.2163 0.7345 0.5364 0.094 Uiso 1 calc R . .
H6C H 0.2016 0.7985 0.5779 0.094 Uiso 1 calc R . .
C7 C 0.1335(5) 0.8097(3) 0.6782(7) 0.057(2) Uani 1 d . . .
H7A H 0.0834 0.8264 0.6566 0.085 Uiso 1 calc R . .
H7B H 0.1528 0.8388 0.6511 0.085 Uiso 1 calc R . .
H7C H 0.1734 0.8069 0.7587 0.085 Uiso 1 calc R . .
C8 C 0.0352(5) 0.7026(5) 0.6813(7) 0.062(2) Uani 1 d . . .
H8A H -0.0165 0.7241 0.6289 0.093 Uiso 1 calc R . .
H8B H 0.0698 0.7287 0.7484 0.093 Uiso 1 calc R . .
H8C H 0.0274 0.6599 0.6997 0.093 Uiso 1 calc R . .
C9 C 0.0126(5) 0.5841(4) 0.5335(7) 0.082(3) Uani 1 d . . .
H9A H -0.0309 0.5824 0.4535 0.123 Uiso 1 calc R . .
H9B H -0.0098 0.5856 0.5706 0.123 Uiso 1 calc R . .
H9C H 0.0461 0.5456 0.5575 0.123 Uiso 1 calc R . .
C10 C 0.0976(6) 0.6195(5) 0.4387(7) 0.090(4) Uani 1 d . . .
H10A H 0.0453 0.6254 0.3656 0.135 Uiso 1 calc R . .
H10B H 0.1056 0.5736 0.4586 0.135 Uiso 1 calc R . .
H10C H 0.1395 0.6342 0.4374 0.135 Uiso 1 calc R . .
C11 C 0.1970(4) 0.5558(3) 0.8714(5) 0.0376(17) Uani 1 d . . .
C12 C 0.2473(4) 0.5179(3) 0.8669(6) 0.0412(18) Uani 1 d . . .
C13 C 0.3229(4) 0.5480(4) 0.9327(5) 0.0414(18) Uani 1 d . . .
C14 C 0.3190(4) 0.6040(4) 0.9775(6) 0.0416(17) Uani 1 d . . .
C15 C 0.2398(4) 0.6087(4) 0.9392(6) 0.0451(18) Uani 1 d . . .
C16 C 0.1144(5) 0.5374(4) 0.8249(7) 0.060(2) Uani 1 d . . .
H16A H 0.1131 0.5324 0.8851 0.090 Uiso 1 calc R . .
H16B H 0.0994 0.4964 0.7849 0.090 Uiso 1 calc R . .
H16C H 0.0768 0.5712 0.7744 0.090 Uiso 1 calc R . .
C17 C 0.2247(6) 0.4518(4) 0.8106(7) 0.068(3) Uani 1 d . . .
H17A H 0.2011 0.4251 0.8342 0.102 Uiso 1 calc R . .
H17B H 0.2725 0.4305 0.8312 0.102 Uiso 1 calc R . .
H17C H 0.1859 0.4575 0.7305 0.102 Uiso 1 calc R . .
C18 C 0.3984(5) 0.5212(4) 0.9587(7) 0.064(3) Uani 1 d . . .
H18A H 0.4430 0.5238 1.0382 0.096 Uiso 1 calc R . .
H18B H 0.4110 0.5466 0.9195 0.096 Uiso 1 calc R . .
H18C H 0.3897 0.4760 0.9349 0.096 Uiso 1 calc R . .
C19 C 0.3862(5) 0.6491(4) 1.0593(6) 0.063(3) Uani 1 d . . .
H19A H 0.3983 0.6455 1.1303 0.094 Uiso 1 calc R . .
H19B H 0.3705 0.6936 1.0322 0.094 Uiso 1 calc R . .
H19C H 0.4336 0.6376 1.0687 0.094 Uiso 1 calc R . .
C20 C 0.2122(6) 0.6584(4) 0.9792(7) 0.065(2) Uani 1 d . . .
H20A H 0.2545 0.6654 1.0586 0.097 Uiso 1 calc R . .
H20B H 0.1641 0.6425 0.9648 0.097 Uiso 1 calc R . .
H20C H 0.2002 0.6993 0.9400 0.097 Uiso 1 calc R . .
O1 O 0.2829(3) 0.5733(3) 0.6687(4) 0.0523(14) Uani 1 d . . .
C21 C 0.3005(7) 0.5059(5) 0.6665(8) 0.095(4) Uani 1 d . . .
H21A H 0.261(3) 0.4876(15) 0.598(5) 0.114 Uiso 1 calc R . .
H21B H 0.3052(7) 0.4822(19) 0.720(4) 0.114 Uiso 1 calc R . .
C22 C 0.3793(7) 0.5093(7) 0.6903(9) 0.106(5) Uani 1 d . . .
H22A H 0.418(4) 0.5066(8) 0.760(6) 0.127 Uiso 1 calc R . .
H22B H 0.3830(8) 0.478(3) 0.658(3) 0.127 Uiso 1 calc R . .
C23 C 0.3792(6) 0.5735(7) 0.6468(9) 0.099(5) Uani 1 d . . .
H23A H 0.3766(6) 0.5690(7) 0.593(5) 0.118 Uiso 1 calc R . .
H23B H 0.420(4) 0.594(2) 0.694(4) 0.118 Uiso 1 calc R . .
C24 C 0.3064(5) 0.6065(5) 0.6150(7) 0.066(3) Uani 1 d . . .
H24A H 0.3174(8) 0.649(3) 0.6367(15) 0.080 Uiso 1 calc R . .

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H24B H 0.266(3) 0.6051(5) 0.540(5) 0.080 Uiso 1 calc R . .
 O2 O 0.3464(3) 0.7070(3) 0.8274(4) 0.0529(14) Uani 1 d . . .
 C25 C 0.3517(5) 0.7767(4) 0.8345(7) 0.061(2) Uani 1 d . . .
 H25A H 0.3783(16) 0.7901(9) 0.905(4) 0.074 Uiso 1 calc R . .
 H25B H 0.302(3) 0.7949(12) 0.790(3) 0.074 Uiso 1 calc R . .
 C26 C 0.3970(5) 0.7944(5) 0.7960(7) 0.068(3) Uani 1 d . . .
 H26A H 0.361(2) 0.8046(8) 0.718(5) 0.081 Uiso 1 calc R . .
 H26B H 0.431(2) 0.831(2) 0.836(2) 0.081 Uiso 1 calc R . .
 C27 C 0.4453(5) 0.7357(5) 0.8187(7) 0.066(3) Uani 1 d . . .
 H27A H 0.497(3) 0.7448(7) 0.866(3) 0.079 Uiso 1 calc R . .
 H27B H 0.4327(9) 0.7205(11) 0.756(4) 0.079 Uiso 1 calc R . .
 C28 C 0.4247(4) 0.6866(5) 0.8679(7) 0.064(3) Uani 1 d . . .
 H28A H 0.4228(5) 0.645(3) 0.8443(15) 0.077 Uiso 1 calc R . .
 H28B H 0.461(2) 0.6876(5) 0.944(5) 0.077 Uiso 1 calc R . .

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Sr1 0.0238(3) 0.0313(3) 0.0298(3) -0.0003(3) 0.0126(3) 0.0006(3)
 C1 0.028(4) 0.053(5) 0.028(3) 0.009(3) 0.018(3) 0.005(3)
 C2 0.031(4) 0.027(4) 0.031(4) 0.002(3) 0.014(3) 0.001(3)
 C3 0.028(4) 0.034(4) 0.036(4) 0.007(3) 0.019(3) 0.004(3)
 C4 0.027(3) 0.026(4) 0.045(4) -0.001(3) 0.009(3) -0.004(3)
 C5 0.029(4) 0.052(5) 0.027(4) -0.010(3) 0.004(3) 0.013(3)
 C6 0.039(4) 0.098(7) 0.051(5) 0.016(5) 0.029(4) -0.003(5)
 C7 0.042(4) 0.032(4) 0.062(5) -0.005(4) 0.018(4) -0.003(4)
 C8 0.040(4) 0.084(7) 0.070(6) 0.028(5) 0.039(5) 0.016(5)
 C9 0.058(6) 0.044(5) 0.069(6) 0.008(5) 0.008(5) -0.017(5)
 C10 0.066(6) 0.108(9) 0.045(5) -0.025(5) 0.012(5) 0.031(6)
 C11 0.034(4) 0.031(4) 0.033(4) 0.007(3) 0.015(3) 0.003(3)
 C12 0.043(4) 0.024(4) 0.037(4) 0.002(3) 0.017(4) -0.001(3)
 C13 0.033(4) 0.044(4) 0.029(4) 0.009(3) 0.012(3) 0.012(3)
 C14 0.037(4) 0.042(4) 0.034(4) -0.002(3) 0.017(3) 0.000(4)
 C15 0.045(4) 0.035(4) 0.048(4) 0.003(3) 0.027(4) 0.002(4)
 C16 0.043(5) 0.056(5) 0.063(5) 0.018(4) 0.026(4) -0.006(4)
 C17 0.081(7) 0.035(5) 0.062(6) -0.002(4) 0.035(5) 0.002(5)
 C18 0.057(5) 0.079(7) 0.060(5) 0.022(5) 0.039(5) 0.036(5)
 C19 0.055(5) 0.078(7) 0.036(4) -0.011(4) 0.021(4) -0.020(5)
 C20 0.078(6) 0.055(5) 0.073(6) 0.001(5) 0.054(6) 0.004(5)
 O1 0.045(3) 0.056(4) 0.050(3) -0.013(3) 0.028(3) 0.005(3)
 C21 0.121(10) 0.071(7) 0.054(6) -0.018(5) 0.040(6) 0.025(7)
 C22 0.090(9) 0.143(13) 0.064(7) -0.004(7) 0.041(6) 0.070(9)
 C23 0.053(6) 0.149(13) 0.086(8) -0.039(8) 0.042(6) 0.008(7)
 C24 0.059(5) 0.090(7) 0.060(5) -0.014(5) 0.043(5) 0.002(5)
 O2 0.039(3) 0.066(4) 0.048(3) -0.004(3) 0.025(3) -0.014(3)
 C25 0.042(5) 0.060(6) 0.066(6) -0.014(4) 0.027(5) -0.006(4)
 C26 0.057(6) 0.065(6) 0.064(6) -0.009(5) 0.031(5) -0.028(5)
 C27 0.042(5) 0.091(8) 0.061(5) -0.025(5) 0.031(5) -0.029(5)
 C28 0.034(4) 0.084(7) 0.048(5) -0.003(5) 0.015(4) 0.004(5)

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All esds (except the esd in the dihedral angle between two l.s. planes)
are estimated using the full covariance matrix. The cell esds are taken
into account individually in the estimation of esds in distances, angles
and torsion angles; correlations between esds in cell parameters are only
used when they are defined by crystal symmetry. An approximate (isotropic)
treatment of cell esds is used for estimating esds involving l.s. planes.
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Sr1 O1 2.612(5) . ?
Sr1 C5 2.827(7) . ?
Sr1 C4 2.832(7) . ?
Sr1 C13 2.848(7) . ?
Sr1 C14 2.847(7) . ?
Sr1 C3 2.864(6) . ?
Sr1 C15 2.869(7) . ?
Sr1 C12 2.873(7) . ?
Sr1 C11 2.878(7) . ?
Sr1 C1 2.880(6) . ?
Sr1 C2 2.912(6) . ?
C1 C2 1.390(9) . ?
C1 C5 1.420(10) . ?
C1 C6 1.521(10) . ?
C2 C3 1.422(9) . ?
C2 C7 1.520(9) . ?
C3 C4 1.420(10) . ?
C3 C8 1.508(10) . ?
C4 C5 1.392(11) . ?
C4 C9 1.496(10) . ?
C5 C10 1.518(11) . ?
C6 H6A 0.9800 . ?
C6 H6B 0.9800 . ?
C6 H6C 0.9800 . ?
C7 H7A 0.9800 . ?
C7 H7B 0.9800 . ?
C7 H7C 0.9800 . ?
C8 H8A 0.9800 . ?
C8 H8B 0.9800 . ?
C8 H8C 0.9800 . ?
C9 H9A 0.9800 . ?
C9 H9B 0.9800 . ?
C9 H9C 0.9800 . ?
C10 H10A 0.9800 . ?
C10 H10B 0.9800 . ?
C10 H10C 0.9800 . ?
C11 C15 1.391(10) . ?
C11 C12 1.393(10) . ?
C11 C16 1.499(10) . ?
C12 C13 1.412(10) . ?

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C12 C17 1.531(10) . ?
C13 C14 1.390(10) . ?
C13 C18 1.530(10) . ?
C14 C15 1.426(10) . ?
C14 C19 1.504(11) . ?
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C16 H16A 0.9800 . ?
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C22 H22B 0.8571 . ?
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C24 H24B 0.9142 . ?
O2 C28 1.454(9) . ?
O2 C25 1.446(10) . ?
C25 C26 1.509(11) . ?
C25 H25A 0.9070 . ?
C25 H25B 0.9070 . ?
C26 C27 1.495(12) . ?
C26 H26A 0.9702 . ?
C26 H26B 0.9702 . ?
C27 C28 1.516(12) . ?
C27 H27A 0.8946 . ?
C27 H27B 0.8946 . ?
C28 H28A 0.9210 . ?
C28 H28B 0.9210 . ?

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O2 Sr1 O1 81.27(17) . . ?
O2 Sr1 C5 110.5(2) . . ?
O1 Sr1 C5 80.65(19) . . ?
O2 Sr1 C4 132.53(19) . . ?
O1 Sr1 C4 101.8(2) . . ?
C5 Sr1 C4 28.5(2) . . ?
O2 Sr1 C13 90.9(2) . . ?
O1 Sr1 C13 85.85(19) . . ?
C5 Sr1 C13 152.3(2) . . ?
C4 Sr1 C13 136.4(2) . . ?
O2 Sr1 C14 80.96(19) . . ?
O1 Sr1 C14 110.18(19) . . ?
C5 Sr1 C14 165.7(2) . . ?
C4 Sr1 C14 137.3(2) . . ?
C13 Sr1 C14 28.3(2) . . ?
O2 Sr1 C3 116.80(19) . . ?
O1 Sr1 C3 127.58(18) . . ?
C5 Sr1 C3 47.1(2) . . ?
C4 Sr1 C3 28.86(19) . . ?
C13 Sr1 C3 137.5(2) . . ?
C14 Sr1 C3 120.7(2) . . ?
O2 Sr1 C15 102.67(19) . . ?
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C5 Sr1 C12 126.8(2) . . ?
C4 Sr1 C12 107.9(2) . . ?
C13 Sr1 C12 28.6(2) . . ?
C14 Sr1 C12 46.8(2) . . ?
C3 Sr1 C12 115.7(2) . . ?
C15 Sr1 C12 46.4(2) . . ?
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C14 Sr1 C11 46.8(2) . . ?
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C12 Sr1 C11 28.0(2) . . ?
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O1 Sr1 C1 90.91(18) . . ?
C5 Sr1 C1 28.8(2) . . ?
C4 Sr1 C1 47.1(2) . . ?
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C14 Sr1 C1 152.9(2) . . ?
C3 Sr1 C1 46.79(18) . . ?
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C11 Sr1 C1 137.64(19) . . ?
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C14 Sr1 C2 128.0(2) . . ?
C3 Sr1 C2 28.50(18) . . ?
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C12 Sr1 C2 143.2(2) . . ?
C11 Sr1 C2 116.54(19) . . ?
C1 Sr1 C2 27.77(19) . . ?
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C2 C1 C6 124.4(7) . . ?
C5 C1 C6 126.9(7) . . ?
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C5 C1 Sr1 73.5(4) . . ?
C6 C1 Sr1 123.0(4) . . ?
C1 C2 C3 108.3(6) . . ?
C1 C2 C7 128.9(7) . . ?
C3 C2 C7 122.2(6) . . ?
C1 C2 Sr1 74.8(4) . . ?
C3 C2 Sr1 73.9(4) . . ?
C7 C2 Sr1 124.0(4) . . ?
C4 C3 C2 107.2(6) . . ?
C4 C3 C8 126.6(7) . . ?
C2 C3 C8 125.7(7) . . ?
C4 C3 Sr1 74.3(4) . . ?
C2 C3 Sr1 77.6(4) . . ?
C8 C3 Sr1 120.5(4) . . ?
C5 C4 C3 108.0(6) . . ?
C5 C4 C9 125.8(8) . . ?
C3 C4 C9 126.2(8) . . ?
C5 C4 Sr1 75.6(4) . . ?
C3 C4 Sr1 76.8(4) . . ?
C9 C4 Sr1 116.0(5) . . ?
C4 C5 C1 108.5(6) . . ?
C4 C5 C10 125.4(8) . . ?
C1 C5 C10 125.7(8) . . ?
C4 C5 Sr1 76.0(4) . . ?
C1 C5 Sr1 77.7(4) . . ?
C10 C5 Sr1 118.9(5) . . ?
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C1 C6 H6B 109.5 . . ?
H6A C6 H6B 109.5 . . ?
C1 C6 H6C 109.5 . . ?
H6A C6 H6C 109.5 . . ?
H6B C6 H6C 109.5 . . ?
C2 C7 H7A 109.5 . . ?
C2 C7 H7B 109.5 . . ?
H7A C7 H7B 109.5 . . ?
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C5 C10 H10B 109.5 . . ?
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C5 C10 H10C 109.5 . . ?
H10A C10 H10C 109.5 . . ?
H10B C10 H10C 109.5 . . ?
C15 C11 C12 108.8(6) . . ?
C15 C11 C16 125.3(7) . . ?
C12 C11 C16 125.3(7) . . ?
C15 C11 Sr1 75.6(4) . . ?
C12 C11 Sr1 75.8(4) . . ?
C16 C11 Sr1 122.0(5) . . ?
C11 C12 C13 107.7(6) . . ?
C11 C12 C17 124.3(7) . . ?
C13 C12 C17 127.6(7) . . ?
C11 C12 Sr1 76.2(4) . . ?
C13 C12 Sr1 74.7(4) . . ?
C17 C12 Sr1 120.5(5) . . ?
C14 C13 C12 108.4(6) . . ?
C14 C13 C18 125.3(7) . . ?
C12 C13 C18 126.1(7) . . ?
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C12 C13 Sr1 76.7(4) . . ?
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C13 C14 C15 107.4(7) . . ?
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C15 C14 Sr1 76.4(4) . . ?
C19 C14 Sr1 117.8(5) . . ?
C11 C15 C14 107.7(7) . . ?
C11 C15 C20 127.1(7) . . ?
C14 C15 C20 124.8(7) . . ?
C11 C15 Sr1 76.3(4) . . ?
C14 C15 Sr1 74.7(4) . . ?
C20 C15 Sr1 121.1(5) . . ?
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C11 C16 H16C 109.5 . . ?
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C12 C17 H17A 109.5 . . ?
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H20A C20 H20B 109.5 . . ?
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H20A C20 H20C 109.5 . . ?
H20B C20 H20C 109.5 . . ?
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C24 O1 Sr1 122.5(5) . . ?
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O1 C21 H21B 111.1 . . ?
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C22 C23 H23B 110.9 . . ?
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C25 O2 Sr1 129.4(5) . . ?
O2 C25 C26 104.6(7) . . ?
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O2 C25 H25B 110.8 . . ?
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C27 C26 C25 104.7(7) . . ?
C27 C26 H26A 110.8 . . ?

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C25 C26 H26A 110.8 . . ?
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C25 C26 H26B 110.8 . . ?
H26A C26 H26B 108.9 . . ?
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C26 C27 H27B 110.6 . . ?
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H27A C27 H27B 108.8 . . ?
O2 C28 C27 103.7(7) . . ?
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