## Supporting Information

# Insights on Foam Transport from a Texture-Implicit Local-Equilibrium Model with an Improved Parameter Estimation Algorithm 

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Table S1: Relative permeability data of Bentheimer sandstone ${ }^{41,46}$

| Parameter | Bentheimer sandstone |
| :---: | :---: |
| $k_{r w}^{o}$ | 0.22 |
| $k_{r g}^{o}$ | 0.94 |
| $S_{w c}$ | 0.10 |
| $S_{g r}$ | 0.05 |
| $n_{w}$ | 4.00 |
| $n_{g}$ | 1.80 |

Derivation for Equation 13 and Equation 14:

According to Darcy's law, the superficial velocity for gas and liquid phases can be expressed as:

Equation S1
$u_{g}=-\frac{k_{\text {rock }} \cdot k_{r g}^{f}}{\mu_{g}} \nabla p=-\frac{k_{\text {rock }} \cdot k_{r g}^{n f} \cdot F M}{\mu_{g}} \nabla p$

Equation S2

$$
u_{w}=-\frac{k_{r o c k} \cdot k_{r w}}{\mu_{w}} \nabla p
$$

According to the definition of apparent viscosity of foam in Equation 1, the $-k_{r o c k} \nabla p$ term can be expressed as:

$$
-k_{\text {rock }} \nabla p=\mu_{a p p} \times\left(u_{g}+u_{w}\right)
$$

Substitute Equation S3 into Equation S2, the relative permeability to aqueous phase can be solved as:

$$
k_{r w}=\frac{\mu_{w} \times u_{w}\left(1-f_{g}\right)}{\mu_{a p p} \times\left(u_{w}+u_{g}\right)}=\frac{\mu_{w} \times\left(1-f_{g}\right)}{\mu_{a p p}}
$$

Equation S4

Further substitute Equation S4 into Equation 11 and water saturation $S_{w}$ can be solved for as in Equation 13.

In addition, $k_{r g}^{n f}$ can be calculated from Equation 11 as:

$$
k_{r g}^{n f}=k_{r g}^{o} \times\left(\frac{S_{g}-S_{g r}}{1-S_{w c}-S_{g r}}\right)^{n_{g}}=k_{r g}^{o} \times\left(\frac{1-S_{w}-S_{g r}}{1-S_{w c}-S_{g r}}\right)^{n_{g}}
$$

Equation S5

Plug Equation S3 and Equation S5 into Equation S1, FM can be solved for accordingly as shown in Equation 14.

