

# Supporting Information

## A Scalable Synthesis of 2-(1,2,4-Oxadiazol-3-yl)propan-2-amine Hydrobromide using a Process Safety-Driven Protecting Group Strategy

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### Contents

**DynoChem<sup>®</sup> studies.....S2**

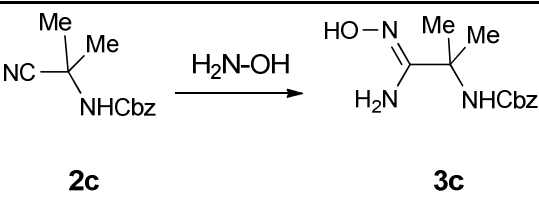
**Impact and Friction tests.....S6**

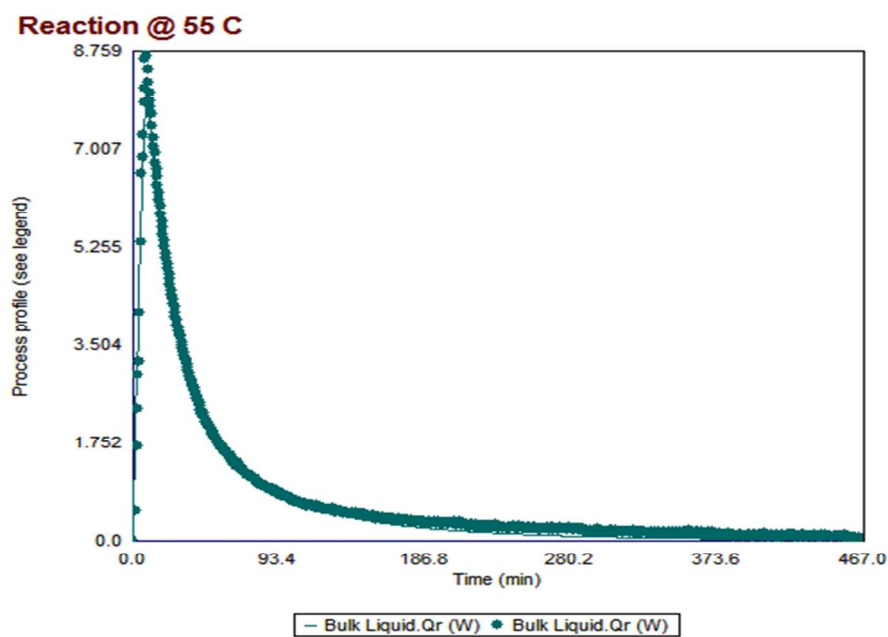
### DynoChem<sup>®</sup> studies.

In the RC1e experiment, 10.6 g (1.4 equiv) of 50% aqueous hydroxylamine (dosing rate: 1.5 mL/min) was added to **2c** (25 g; 114.6 mmol) in 2-propanol (120 mL) at 55 °C. We realized that the heat data from reaction calorimeter obtained at two different temperatures could be used to fit the kinetics in DynoChem<sup>®</sup> software to find the optimum dosing time and reaction temperature. Thus in a separate experiment in RC1e, the hydroxylamine solution was added at faster rate (10.5 mL/min) at 35 °C and the heat data was recorded over a period 15-16 h. The heat data obtained from experiments done at two different temperatures was exported to the DynoChem<sup>®</sup> software for fitting the kinetics. In this case, the heat evolution rate ( $q_r$ ) data corrected for baseline heat signal ( $q_r - q_b$ ) was used for fitting the rate parameters.

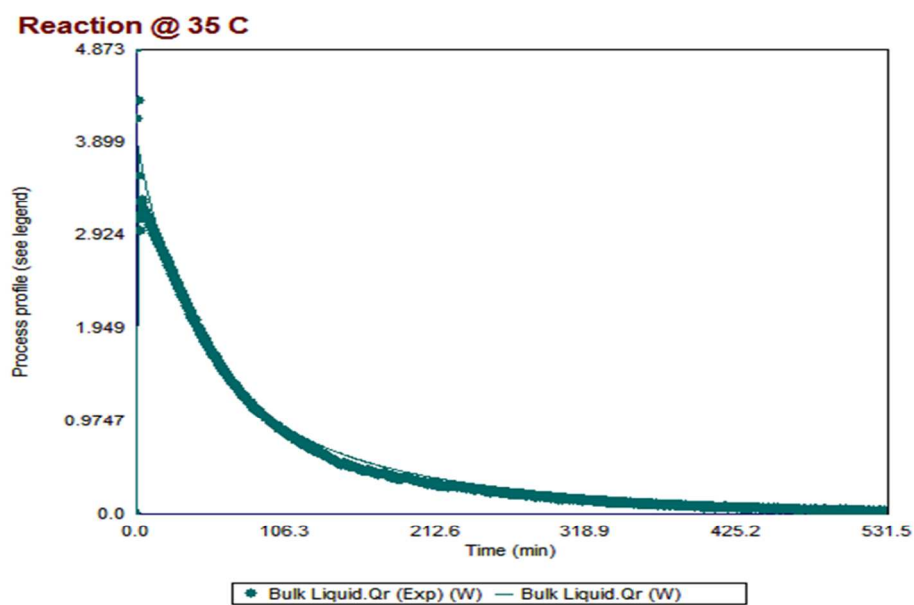
Initially the rate constant,  $k$  at reference temperature ( $T_{ref}$ ) was fitted for the heat data obtained at near isothermal reaction temperature of 35 °C and then the activation energy ( $E_a$ ) was fitted for the other run carried out at 55 °C. As seen from the Figures S1 and S2, a good fit of experimental and predicted heat data was obtained and the reaction was determined to be first order in **2c** and hydroxylamine as initially assumed in the model (Table S1)

**Table S1.** Rate equations used for kinetic fitting in DynoChem<sup>®</sup> Software

Reaction	$T_{ref}$	Order
 <b>2c</b> → <b>3c</b>	35 °C	First order in <b>2c</b> and hydroxylamine



**Figure S1.** Fitting of  $q_r$  data for the RC1e run done at 55 °C



**Figure S2.** Fitting of  $q_r$  data for the RC1e run done at 35 °C

As seen from Table S2, the formation of **3c** is not very sensitive to temperature ( $E_a = 38.3$  kJ/mol).

**Table S2.** Fitted kinetic parameters from DynoChem<sup>®</sup>

Parameter	value	confidence intervals (%)	Unit
$k$	$1.96 \times 10^{-4}$	$\pm 1.5$	L/mol.s
$E_a$	38.3	$\pm 1.8$	kJ/mol
$\Delta H_r$	-175.05	$\pm 0.8$	kJ/mol

Maximum accumulation is a function of both the reaction temperature and dosing time, which requires two dimensional optimization. A response surface plot of dosing time, reaction temperature and Maximum Heat Accumulation was generated using the feed time and the temperature as a variable in the model.<sup>1</sup> Temperature was used as a variable to calculate the reaction temperature based on the cooling capacity of the reactor which is a function of the overall heat transfer (UA) and the temperature difference [ $\Delta T$ , where  $\Delta T$  = reaction temperature ( $T_r$ ) - jacket temperature ( $T_j$ )], as shown in Eq.1. The temperature profile in the reactor is obtained by integrating Eq.1. A simple controller was also used in the model to calculate the  $T_j$  based on the deviation from the set temperature ( $T_{set}$ ) and the proportional gain ( $K_p$ ) as shown in Eq.2. This was more realistic, as a variation of  $T_r$  may have an impact on the required feed time.

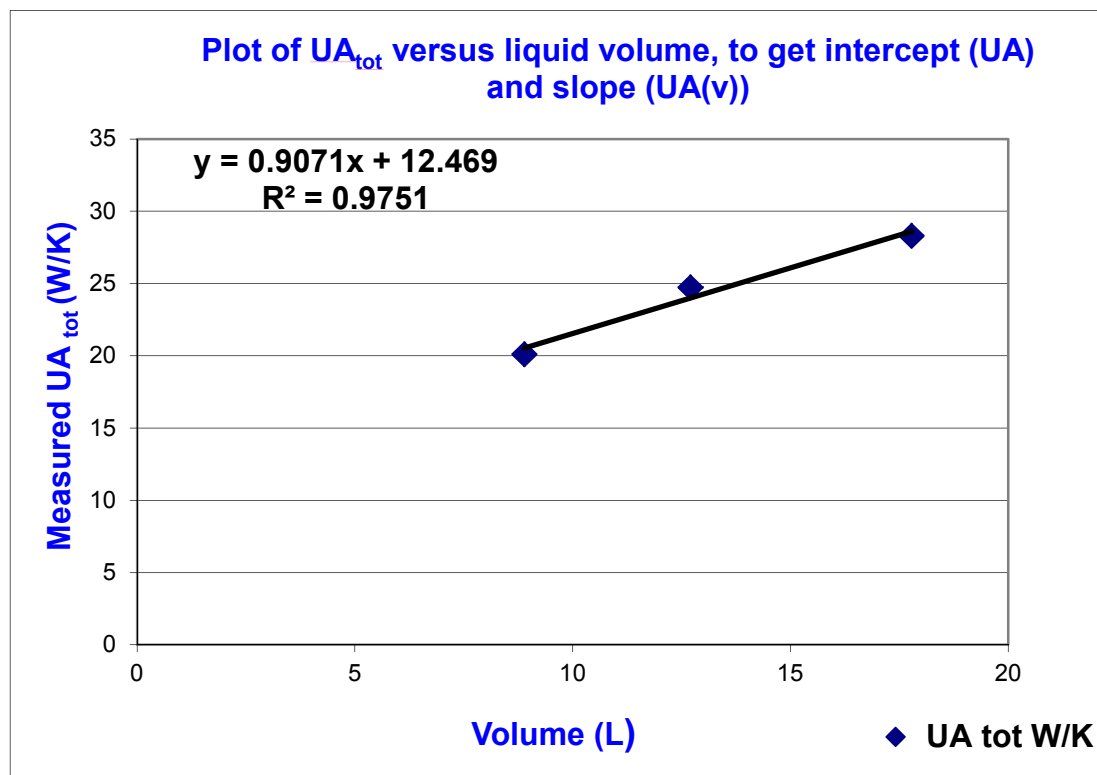
$$\frac{dT}{dt} = \frac{q_r}{mC_p} - \frac{UA}{mC_p} \Delta T \quad \text{Eq. 1}$$

$$T_j = T_{set} - K_p * (T_r - T_{set}) \quad \text{Eq. 2}$$

As shown in Figure S3, the variation of UA with liquid volume (V) was incorporated in the model (Eq 3) by doing solvent tests in a 30 L glass reactor.

$$UA_{tot} = UA + UA(V) * Volume \quad \text{Eq. 3}$$

**Figure S3.** Variation of UA with volume for a 30 L glass reactor



A two dimensional surface plot was generated in DynoChem<sup>®</sup>, by varying the feed time from 30 to 600 min in 21 levels and the temperature from 50 to 80 °C in two steps (16 levels). In all 336 (21\* 16) scenarios were generated and used for generating the plot in Excel.

### **Impact and Friction sensitivity tests**

BAM falling hammer impact sensitivity test was conducted with a Type MP-3 Falling Hammer from the Swiss Institute for Promotion of Safety and Security following a published procedure.<sup>2</sup> Negative results were observed in six trials at impact energy of 60 J. As a result, the material is not considered to be impact sensitive.

BAM friction sensitivity test was conducted with a HAAKE model 002-5792-9300 friction tester following a published procedure.<sup>3</sup> Negative results were observed in six trials at a friction force of 360 N. As a result, the material is not considered to be friction sensitive.

### **References:**

- (1) Applications of DynoChem in Thermal Process Safety – Optimization of Accumulation and Time to Maximum Rate by Bernhard Berger can be found at <https://dcresources.scale-up.com>
- (2) UN Transport of Dangerous Goods: Classification Procedures, Test Methods and Criteria Relating to Explosives of Class 1, section 13.4.2
- (3) UN Transport of Dangerous Goods: Classification Procedures, Test Methods and Criteria Relating to Explosives of Class 1, section 13.5.1