Supporting Information:

Confronting Workplace Exposure to Chemicals with LCA: The Examples of Trichloroethylene and Perchloroethylene in Metal Degreasing and Dry Cleaning

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Machine technology description

Types I and II are open top, cold-cleaners, with solvent baths and a vapor bath. To prevent vapors escaping to the workplace they have a capturing device at the rim of the baths. In Type II machines the rim also has an electro-cooling apparatus that further enhances vapor capture. Type III machines operate on the same principle, but in this case the baths are all enclosed to prevent solvent evaporation and loss. The Type IV apparatus is a closed system with a refrigerated recirculation system, which recycles the solvent. Type V machines release no exhaust air to the environment. The entire cleaning process takes place in a closed, looped drying and recycling system, including an activated carbon filter to ensure solvent capture. The cleaning chamber opens only after concentrations have reached less than 1 g/m^3 .

In the dry-cleaning industry there are five different machine generations. First generation "transfer machines" have a separate washer and dryer. In some countries, such as

Germany, transfer machines are no longer used (1), but in many countries they are still in use, e.g. in the U.S. (2,3). The next four generations are all "dry-to-dry" machines, which eliminate the need for manual transfer of solvent-covered clothing. Second generation machines have a water-cooling system for solvent-laden air. Exhaust air is then vented directly to the atmosphere. Third generation machines have a water-cooling or refrigeration unit incorporated to facilitate vapor recovery. Fourth generation machines are non-vented and have a closed system. The solvent-concentrated air is recovered by passing through a condenser and an activated carbon filter. Even though the same nomenclature is used for the various machines types, in the U.S. and Germany for instance, there are small differences in the technology for the machines between 2nd to 4th generation. However, the differences are minor and are not considered to affect the outcome. Fifth generation machines are broadly used in Germany but not in the U.S. (2,3). In addition to the refrigerated cooling device and the carbon adsorber, the fifth generation also includes an interlocking system, allowing the chamber door to open only after the concentration has reached a specified level.

Data tables

| THEE ST. Muchine Sizes and batch times | | | | | |
|--|---------------|-------------|------------|--|--|
| Machine | Capacity (kg) | Machine | Batch-time | | |
| size | | generation | (min) | | |
| | Dry- cl | eaning | | | |
| 1 | 12 | First | 20-30 | | |
| 2 | 16 | Second | 40-55 | | |
| 3 | 22 | Third | 40-55 | | |
| 4 | 28 | Fourth | 45-65 | | |
| 5 | 32 | Fifth | 50-70 | | |
| | Metal-de | greasing | | | |
| 1 | 40- | 50 | 4.8-7.2 | | |
| 2 | 50-0 | 60 | 6-10.2 | | |
| 3 | 120- | 150 | 8.4-12 | | |
| 4 | Approx | Approx. 600 | | | |
| 5 | Approx | . 1000 | 30-60 | | |

TABLE S1: Machine sizes and batch-times

| TCE emission factors for metal- | | | | | |
|-------------------------------------|------------------|------------|------------|------------|------------|
| degreasing | Туре І | Type II | Type III | Type IV | Type V |
| E _{diff} min ^a | 0.30 | 0.17 | 0.05 | 0.01 | 0.00 |
| E _{diff} avg ^a | 0.91 | 0.52 | 0.13 | 0.04 | 0.01 |
| E _{diff} max ^a | 7.4 | 4.2 | 0.84 | 0.20 | 0.12 |
| E _{rc} min ^a | 0.98 | 0.98 | 0.12 | 0.03 | 0.02 |
| E _{rc} avg ^a | 5.9 | 5.9 | 1.9 | 0.03 | 0.02 |
| E _{rc} max ^a | 11 | 11 | 3.6 | 0.03 | 0.02 |
| E _{rep} min ^a | 0.39 | 0.23 | 0.19 | 0.02 | 0.00 |
| E _{rep} avg ^{b,c} | 1.4 | 0.83 | 0.68 | 0.11 | 0.00 |
| E _{rep} max ^c | 11 | 7,0 | 5.8 | 1.3 | 0.02 |
| PCE emission factors for metal- | | | | | |
| degreasing | Type I | Type II | Type III | Type IV | Type V |
| E _{diff} min ^a | 0.10 | 0.06 | 0.02 | 0.01 | 0.00 |
| E _{diff} avg ^a | 0.31 | 0.17 | 0.04 | 0.04 | 0.01 |
| E _{diff} max ^a | 2.5 | 1.4 | 0.28 | 0.20 | 0.12 |
| E _{rc} min ^a | 3.3 | 3.3 | 0.41 | 0.10 | 0.05 |
| E _{rc} avg ^a | 19 | 19 | 6.2 | 0.11 | 0.05 |
| E _{rc} max ^a | 36 | 36 | 12 | 0.11 | 0.06 |
| E _{rep} min ^a | 0.15 | 0.08 | 0.06 | 0.01 | 0.00 |
| E _{rep} avg ^a | 0.57 | 0.33 | 0.25 | 0.05 | 0.00 |
| E _{rep} max ^a | 4.9 | 2.9 | 2.2 | 0.77 | 0.02 |
| PCE emission factors for dry- | First | Second | Third | Fourth | Fifth |
| cleaning | generation | generation | generation | generation | generation |
| E _{diff} min | | 3.4 | 3.4 | 1.7 | 0.20 |
| E _{diff} a∨g [▷] | | 4.6 | 4.6 | 1.9 | 0.30 |
| E _{diff} max | | 5.7 | 5.7 | 2.1 | 0.40 |
| E _{rc} min | | 0.46 | 0.38 | 0.26 | 0.12 |
| E _{rc} avg ^b | | 1.7 | 1.40 | 0.96 | 0.35 |
| E _{rc} max | | 6.6 | 5.5 | 3.8 | 1.3 |
| E _{rep} min ^c | <10 [°] | 1.9 | 0.32 | 0.33 | 0.03 |
| E _{rep} avg ^{b,c} | | 2.5 | 0.42 | 0.48 | 0.04 |
| E _{rep} max ^c | <15 ^ª | 3.0 | 0.53 | 0.63 | 0.05 |

TABLE S2: Emissions of dry-cleaning emission (g per kg garment) and metal-degreasing (g per m^2 surface area) for various machine generations and types (data taken or calculated from (1)).

^b Minimum and maximum emissions of machines with and without vapor degreasing and of plate and sphere shaped metal parts. The average was calculated as the average between minimum and maximum value of size 3 machines (Table S1), as this is the machine size used most (1). ^b Minimum and maximum values are empiric values. Average values are calculated as the

average between min and max, except for E_{rc} , for which empiric information was available. [°] Emissions were calculated by multiplying the concentrations measured in the cylinder (1) to the cylinder volume and division by the load (79% of the capacity (1)). With respect to second and third generation machines, 50% of this emission amount is emitted to the workplace and the other 50% directly to the environment due to ventilation devices.

^d In EPA 1995 (4), the total for 'miscellaneous emissions' including losses from opening and closing dryers is given as 10-15 g/kg.

| | average | | | | | | |
|------------|-------------------|--------------|---|----------------------|--------------|--------------|--------------|
| Machine | load size (ka) | | Type I | | Type III | | Type V |
| | ions from m | otal day | rype i | İypen İ | туретт | турети | Type v |
| | | | 122 Jieasing (g/n), | 102 | 20.2 | 4.60 | 0.024 |
| Size 1 | 45 | IVIII Mov | 132 | 102 | 20.3 | 4.00 | 0.034 |
| SIZE I | 40 | Min | 203 | 210 | 20.1 20.6 | 12.3 | 3.07 |
| Sizo2 | 55 | Mox | 107 | 124 | 30.0 | 0.00 | 0.090 |
| SIZEZ | 55 | Min | 307 | 240 | 70.7 | 17.2 | 4.30 |
| Si-02 | 105 | IVIII Mov | 204 | 107 | 100 | 10.2 | 1.10 E 01 |
| Sizes | 135 | Min | 450 | 348 | 122 | 29.0 | 5.81 |
| Size 4 | 600 | IVIII Mov | 472 | 317 | 147 | 17.Z | 1.34 |
| 51264 | 600 | Min | 040 | 021 | 200 | 30.0 40.0 | 1.92 |
| SizeE | 1000 | IVIIN | 1100 | 000 | 398 | 42.9 | 1.43 |
| Sizes | 1000 | max | 2340 | 1520 | 873 | 192 | 15.5 |
| PCE emiss | ions from m | etal-de | greasing (g/h), | , E _{A,PCE} | | | |
| _ | | Min | 204.6 | 190.7 | 29.1 | 7.3 | 2.7 |
| Size 1 | 45 | Max | 566.0 | 550.7 | 67.7 | 19.8 | 8.5 |
| | | Min | 228.8 | 208.7 | 33.7 | 8.5 | 2.9 |
| Size2 | 55 | Max | 583.7 | 559.5 | 75.1 | 23.1 | 9.0 |
| | | Min | 307.5 | 273.4 | 51.1 | 11.5 | 3.7 |
| Size 3 | 135 | Max | 760.2 | 718.3 | 106.8 | 26.2 | 11.6 |
| | | Min | 451.9 | 383.7 | 83.9 | 15.7 | 4.8 |
| Size4 | 600 | Max | 1215.3 | 1125.8 | 188.7 | 58.3 | 17.3 |
| | | Min | 637.0 | 455.8 | 161.7 | 24.3 | 3.8 |
| Size5 | 1000 | max | 1934.6 | 1614.5 | 439.9 | 147.9 | 26.1 |
| Machine | Load | | First | Second | Third | Fourth | Fifth |
| generation | size (kg) | | generation | generation | generation | generation | generation |
| PCE emiss | ions from dr | y-clean | ing (g/h), $\dot{\mathrm{E}}_{\mathrm{A},\mathrm{P}}$ | CE | | | |
| | | Min | 263 | 72.3 | 55.1 | 23.1 | 3.17 |
| Size 1 | 12 | Max | 776 | 195 | 144 | 76.2 | 17.7 |
| | | Min | 350 | 96.4 | 73.5 | 30.8 | 4.23 |
| Size2 | 16 | Max | 1040 | 261 | 192 | 102 | 22.7 |
| | | Min | 482 | 133 | 101 | 42.4 | 5.82 |
| Size3 | 22 | Max | 1420 | 357 | 264 | 140 | 32.5 |
| | | Min | 613 | 169 | 129 | 53.8 | 7.40 |
| Size4 | 28 | Max | 1810 | 456 | 337 | 178 | 41.4 |
| | | Min | 701 | 193 | 147 | 61.6 | 8.46 |
| Size5 | 32 | max | 2070 | 520 | 384 | 203 | 47.3 |

TABLE S3: Emission flows $\dot{E}_{A,x}$ (g/h) of TCE and PCE to workplace air for different machine generations (Type I-V) and sizes. The three components of $\dot{E}_{A,x}$ (Equation 6) were calculated from (1,5). For machine sizes and batch times see Table S1.

| , | | 6 | 1 () / |
|---------------------------------|------------------|-------------------------------------|------------------------------|
| Parameter | Unit | Metal-degreasing | Dry-cleaning |
| Volume of inner box | m³ | 100 ^a | 100 ^a |
| (near-field), V _A | | | |
| Volume of outer box | m³ | 300–500 ^a | 300–500 ^a |
| (far-field), V _B | | | |
| Air exchange rate | h⁻¹ | 6–6.5 for type I and II machines | 6–10 |
| with the environment, | | 5.5–6 for type III–V | |
| k _L | 4 | | |
| Air exchange rate | h ⁻ ' | 7–7.5 for type I and II machines | 8–12 |
| between box A and B, | | 6–6.5 for type III–V | |
| k _A ^b | | | |
| Number of workers | - | Near-field: 1.5-3 (average 2.25) | Near-field: 1-1.5 (average |
| exposed ('n _{pop} ' in | | for type I and II machines, and | 1.25) |
| Equation 4) | | 1–1.6 (average 1.3) for type III to | Far-field: 4-5 (average 4.5) |
| | | V | |
| | | Far-field: 3-10 (average 6.5) for | |
| | | type I and II machines, and 2-8 | |
| | | (average 5) for type III to V | |

TABLE S4: Volume, air exchange rates and number of workers exposed (1,5).

 $^{\rm a}$ The total room volume is the sum of $V_{\rm A}$ and $V_{\rm B}.$

^b $k_B = k_A \cdot V_A / V_B$

TABLE S5: PCE and TCE concentrations^a, (g/m^3) , for various machine types, in both near- and far-field. Bold values surpass the MAK value.

| Concentration / | | | | | | |
|------------------------------|-------------|------------|------------|------------|------------|------------|
| machine Type | | Type I | Type II | Type III | Type IV | Type V |
| TCE Concentrations from | metal-degre | easing | | | | |
| Near-Field | Min | 0.24 | 0.19 | 0.06 | 0.01 | 0.002 |
| Concentration. C_{A} | Average | 1.21 | 0.84 | 0.45 | 0.08 | 0.009 |
| (g/m ³) | Max | 4.63 | 3.02 | 1.98 | 0.43 | 0.04 |
| Far-field | | | | | | |
| Concentration, C_B | Min | 0.07 | 0.05 | 0.02 | 0.03 | 0.0005 |
| (g/m ³) | Average | 0.34 | 0.23 | 0.12 | 0.02 | 0.003 |
| | Max | 1.30 | 0.85 | 0.52 | 0.11 | 0.01 |
| PCE Concentrations from | metal-degre | easing | | | | |
| Near-Field | Min | 0.38 | 0.85 | 0.06 | 0.02 | 0.006 |
| Concentration, C_{Λ} | Average | 1.23 | 1.08 | 0.27 | 0.07 | 0.02 |
| (g/m ³) | Max | 3.84 | 3.20 | 1.00 | 0.34 | 0.06 |
| Far-field | Min | 0.11 | 0.10 | 0.02 | 0.004 | 0.002 |
| Concentration. C_{B} | Average | 0.34 | 0.30 | 0.07 | 0.02 | 0.006 |
| (g/m ³) | Max | 1.07 | 0.90 | 0.26 | 0.09 | 0.04 |
| Concentration / | | First | Second | Third | Fourth | Fifth |
| machine generation | | generation | generation | generation | generation | generation |
| PCE emissions from drv-c | leaning | | | | | |
| Near-Field | Min | 0.33 | 0.09 | 0.07 | 0.03 | 0.004 |
| Concentration, C_{A} | Average | 1.46 | 0.38 | 0.28 | 0.14 | 0.03 |
| (g/m ³) | Max | 3.74 | 0.94 | 0.69 | 0.37 | 0.09 |
| Far-field | Min | 0.11 | 0.03 | 0.02 | 0.01 | 0.001 |
| Concentration, C_B | Average | 0.46 | 0.12 | 0.09 | 0.04 | 0.009 |
| (g/m ³) | Max | 1.15 | 0.29 | 0.21 | 0.11 | 0.03 |

^a Calculated according to Equation 2.



Figure S1: Near- and far-field concentrations for PCE in dry-cleaning (various machine generations and sizes).

| Industrial Sector | Germany (1999) | | United Kingdom (2002-2004) |
|---|-----------------|--------------------------|------------------------------|
| | | | Majority are open-topped |
| Motol | 100 |)% Type V | vapor degreasers (i.e. Types |
| | 301 T | ype V (TCE) ^a | I and II) ^c |
| Degreasing | 1351 T | ype V (PCE) ^b | ~6,000 hot-vapor degreasers |
| | | | in the UK ^d |
| | Generatio | Germany (2001) | U.S. (1995) ^f |
| | n | Cermany (2001) | 0.0. (1999) |
| | 1 st | - | 34% |
| | 2 nd | - | 32% |
| Dry Cleaning | 3 rd | - | |
| | 4 th | - | 34% |
| | 5 th | 100% (4700) ^e | Less than 1% (2002) |
| a. Ref. (6) b. Ref. (7) c. Ref. (8) d. Ref. <i>(9)</i> | | | |

TABLE S6: Machine Distribution

e. Ref. (10) f. Ref. (4)

| (mm/max). | | | | | |
|--|------------------|------------------|------------------|------------------|------------------|
| TCE | Type I | Type II | Type III | Type IV | Type V |
| Net consumption of fresh TCE ^a Mass of waste solvent mixture per m ² | 70 | 70 | 50 | 39 | 39 |
| (solvent and pollutants) | 702 | 702 | 702 | 702 | 702 |
| Waste solvent mass in distillation ^a | 700 | 700 | 700 | 700 | 700 |
| Pollutants ^b Solvent losses from distillation ^a (this | 2 | 2 | 2 | 2 | 2 |
| amount of waste solvent is incinerated) | 38 | 38 | 39 | 39 [°] | 39 ^c |
| Recovered solvent | 662 | 662 | 661 | 661 | 661 |
| Recovery rate | 94% | 94% | 94% | 94% | 94% |
| PCE | Type I | Type II | Type III | Type IV | Type V |
| Net consumption of fresh PCE ^a Mass of waste solvent mixture per m ² going into distillation | 90 | 90 | 57 | 44 | 44 |
| (solvent and pollutants) Waste solvent mass in distillation ^a (this | 776 | 776 | 776 | 776 | 776 |
| amount of waste solvent is incinerated) | 774 | 774 | 774 | 774 | 774 |
| Pollutants ^b | 2 | 2 | 2 | 2 | 2 |
| Solvent losses from distillation ^a | 42 | 42 | 44 | 44 ^c | 44 ^c |
| Recovered solvent | 732 | 732 | 730 | 730 | 730 |
| Recovery rate | 94% | 94% | 94% | 94% | 94% |
| Amounts (g per kg garment) / | First | Second | Third | Fourth | Fifth |
| Machine generation | generation | generation | generation | generation | generation |
| Total consumption of fresh PCE | e e ed | 0 | 0 | 0 | |
| Min | 300 ^d | 100° | 40° | 20° | 0 |
| Max | 500° | 150° | 80° | 40° | 10° |
| PCE into distillation | aaaf | 2009 | ana | aaaf | |
| | 320 | 200° | 200° | 230 | 170 ^e |
| Avg Max | 320 ^f | 280 ^g | 280 ^g | 240 ^f | 170 |
| Waste PCE into incineration | | | | | |
| Min | 10 ^h | 14 | 14 | 12 ^e | |
| Avg | h | | | | 8.3 ^e |
| Max | 160'' | 14 | 14 | 12 ^e | |

TABLE S7: Net solvent consumption and amounts of waste solvents generated in g per m² metal surface and kg garment for various machine types/generations (two significant figures). The indicated data sources either provided average values (avg) or data ranges (min/max)

^a Ref. (11)

^b 4.8 g/l according to Mannheim et al. (11). The densities of TCE and PCE are 1,465 g/cm3 and 1,62 g/cm³, respectively. ^c Assumption: Same as Type III machines.

^d Ref. *(12)*. ^e Ref. *(13)*.

^f From these amounts, 94-95% are recovered in case of fourth and fifth generation machines (13). Values for first generation machines calculated as the difference of total consumption and total emissions to air.

⁹ Assumption: Average between first and fourth generation machines (only distillation residues). ^h Ref. (4). From this amount, approximately 16 g/kg account for distillation residues (and the remaining

fraction for filter residues).

| TABLE S8: In | ventory data for the distillation of 1 | kg PCE or T | CE containing waste- |
|-----------------|--|-------------|----------------------|
| solvent mixture | e (calculated with (14)). | | |
| Inventory flow | Name of corresponding data set in (15) | Unit | Amount |

| Inventory flow | Name of corresponding data set in (15) | Unit | | Amount |
|-------------------------|---|-----------------|---------|--------------|
| Electricity | electricity, medium voltage, production | kWh | Min | 0.004 |
| | UCTE, at grid | | Average | 0.033 |
| | | | Max | 0.110 |
| Cooling water | | m ³ | Min | 0.004 |
| | | | Average | 0.027 |
| | | | Max | 0.070 |
| Steam | heat, heavy fuel oil, at industrial furnace | MJ | Min | 1.2 |
| | | | Average | 3.4 |
| | | | Max | 7.5 |
| Nitrogen | Nitrogen, liquid, at plant | kg | Min | 0.0000012 |
| | | | Average | 0.0003 |
| | | | Max | 0.0011 |
| Outlet air ^a | | Nm ³ | Min | 0.024 |
| | | | Average | 0.062 |
| | | | Max | 0.151 |
| a The early and | content is between 10s and 20 s contains | A Mine 3 | | according of |

^a The carbon content is between 10g and 20 g carbon per Nm³. Assumption: consisting of emissions of PCE or TCE, depending on the solvent distilled.

| (16), two significant figures). | | | | |
|---------------------------------|---|-----------------|-----------|----------|
| Inventory flow | Name of corresponding data set in <i>(15)</i> | unit | TCE | PCE |
| Use of heating oil | Heavy fuel oil, at regional | kg | | 0.42 |
| | storage | - | 0.38 | |
| Use of heating gas | Natural gas, at long-distance | Nm ³ | | 0.0017 |
| | pipeline | | 0.0017 | |
| Use of drinking water | tap water, at user | kg | 8.7 | 8.7 |
| Use of NaOH | sodium hydroxide, 50% in H2O, | kg | | 2.5 |
| | production mix, at plant | | 2.3 | |
| Use of HCI | hydrochloric acid, 30% in H2O, | kg | | 0.0078 |
| | at plant | | 0.0078 | |
| Use of NH₄OH | chemicals inorganic, at plant | kg | 0.0030 | 0.0030 |
| Steam production | heat, heavy fuel oil, at industrial | MJ | | 17 |
| | furnace 1MW | | 17 | |
| Electricity (net production) | electricity, medium voltage, | kWh | | 0.060 |
| | production UCTE, at grid | | 0.060 | |
| CO ₂ | | kg | 1.9 | 1.9 |
| NO_x as NO_2 | | kg | 0.00026 | 0.00026 |
| NMVOC | | kg | 0.0000030 | 0.000003 |
| particles | | kg | 0.000038 | 0.000038 |
| NH ₃ | | kg | 0.000011 | 0.000011 |
| CO | | kg | 0.000022 | 0.000022 |
| CI as HCI (air) | | kg | 0.00025 | 0.00026 |
| Cl ⁻ to water | | kg | 0.81 | 0.85 |

TABLE S9: Inventory data for the incineration of 1 kg of PCE and TCE (calculated with (16), two significant figures).

TABLE S10: Number of workers and population number per scale, used as weighting factors $n_{pop,x}$ (Equation 4).

| Scale | Number of persons exposed |
|------------------------|--|
| Near-field workplace | Dry-cleaning: 1-1.5 (average 1.25) |
| (1) | Metal degreasing: 1.5-3 (average 2.25) for type I and II machines, and 1- |
| | 1.6 (average 1.3) for type III to V |
| Far-field workplace | Dry-cleaning: 4-5 (average 4.5) |
| (1) | Metal degreasing: 3-10 (average 6.5) for type I and II machines, and 2-8 (average 5) for type III to V |
| Continental scale (17) | 367,000,000 |
| Global scale (17) | Moderate zone: 2,120,000,000 |
| | Tropical zone: 2,290,000,000 |
| | Arctic zone: 99,100,000 |

| Later transfer to outdoor air is not considered here. | | | | | |
|---|---------|---------|---------|--|--|
| | Min | Average | Max | | |
| weightedRCR (A) MAK based | 1.2E+05 | 1.9E+05 | 3.2E+05 | | |
| weightedRCR (B) MAK based | 9.4E+04 | 1.7E+05 | 3.3E+05 | | |
| weightedRCR (total) MAK based | 2.2E+05 | 3.6E+05 | 6.5E+05 | | |
| weightedRCR (A) TLV based | 2.5E+05 | 4.0E+05 | 6.6E+05 | | |
| weightedRCR (B) TLV based | 2.0E+05 | 3.4E+05 | 6.8E+05 | | |
| weightedRCR (total) TLV based | 4.5E+05 | 7.5E+05 | 1.3E+06 | | |
| weightedRCR (A) HLV Uses based (8h) | 4.1E+07 | 6.5E+07 | 1.1E+08 | | |
| weightedRCR (B) HLV Uses based (8h) | 3.2E+07 | 5.6E+07 | 1.1E+08 | | |
| weightedRCR (total) HLV Uses based (8h) | 7.3E+07 | 1.2E+08 | 2.2E+08 | | |

TABLE S11: Weighted Risk Characterization Ratios (*weightedRCR*) for dry-cleaning. The numbers refer to a fictitious emission flow of 1000 tonnes/day to workplace air. Later transfer to outdoor air is not considered here.

TABLE S12: Characterization factors (CF, Equation 5) for workplace emissions and outdoor emissions.

| | | Workplace | Environment | | | | | |
|---|-----|-------------------|-------------------|----------|-----|--|--|--|
| | | (emission to indo | (emission to | | | | | |
| | | considering also | ambient air) (17) | | | | | |
| | | Metal | Metal | Dry | | | | |
| | | degreasing type | degreasing | cleaning | | | | |
| | | I and II | type III to V | | | | | |
| MAK based | | | | | | | | |
| | Min | 35 | 35 | - | | | | |
| TCE | Max | 35 | 35 | - | 34 | | | |
| | Min | 6 | 6 | 5.7 | | | | |
| PCE | Max | 6 | 6 | 5.9 | 5.5 | | | |
| TLV based | | | | | | | | |
| | Min | 35 | 35 | - | | | | |
| TCE | Max | 36 | 36 | - | 34 | | | |
| | Min | 6 | 6 | 5.77 | | | | |
| PCE | Max | 7 | 7 | 6.24 | 5.5 | | | |
| Environmental HLV based (adjusted to 40h exposure/week) | | | | | | | | |
| | Min | 3400 | 2600 | - | | | | |
| TCE | Max | 12000 | 8600 | - | 34 | | | |
| | Min | 79 | 61 | 46 | | | | |
| PCE | Max | 260 | 190 | 130 | 5.5 | | | |



Figure S2: Human Toxicity Potential on the basis of characterization factors (in 1,4dichlorobenzene-equivalents, $HTP_{workplace,CF}$ in Equation 6) from the use of PCE (left) and TCE (right) in the degreasing of 1 m² metal surface (top) as well as from the use of PCE in the dry-cleaning of 1 kg of garments (bottom). The uncertainty ranges show the range of minimum and maximum emissions (see Tables 2-4 and S8). In contrast to Figure 3, the bars for workplace include the direct effects of workplace emissions as well as the potential subsequent outdoor effects (emissions released at the workplace will eventually reach the environment through ventilation).

TABLE S13: Contribution of solvent emissions to the total human health potential considering the complete life cycle of TCE and PCE use in metal-degreasing and dry-cleaning. Emissions were weighted with the *weightedRCR* (two significant figures).

| <u> </u> | | 0 | 0 | <u> </u> | | | | | |
|--|--------------|------------|------------|------------|------------|--|--|--|--|
| TCE in metal-degreasing – MAK based | Type I | Type II | Type III | Type IV | Type V | | | | |
| Fraction of impact from TCE outdoor emissions of total impact | 83% | 83% | 68% | 37% | 37% | | | | |
| Fraction of impact from TCE emissions at the workplace of total impact | 0.31% | 0.27% | 0.15% | 0.021% | 0.0036% | | | | |
| Remaining emissions from production and disposal | 17% | 17% | 32% | 63% | 63% | | | | |
| TCE in metal-degreasing - environmental H | ILV based | | | | | | | | |
| Fraction of impact from TCE outdoor emissions of total impact | 2.2% | 2.5% | 3.5% | 11% | 26% | | | | |
| Fraction of impact from TCE emissions at the workplace of total impact | 97% | 97% | 95% | 72% | 30% | | | | |
| Remaining emissions from production and disposal | 0.44% | 0.49% | 1.7% | 18% | 44% | | | | |
| PCE in metal-degreasing – MAK based | | | | | | | | | |
| Fraction of impact from PCE outdoor emissions of total impact | 54% | 54% | 30% | 11% | 11% | | | | |
| Fraction of impact from PCE emissions at the workplace of total impact | 1.6% | 1.6% | 0.60% | 0.025% | 0.0087% | | | | |
| Remaining emissions from production and disposal | 45% | 45% | 69% | 89% | 89% | | | | |
| PCE in metal-degreasing – environmental HLV based | | | | | | | | | |
| Fraction of impact from PCE outdoor emissions of total impact | 8.5% | 8.6% | 10% | 10% | 11% | | | | |
| Fraction of impact from PCE emissions at the workplace of total impact | 85% | 84% | 67% | 7.7% | 2.8% | | | | |
| Remaining emissions from production and disposal | 7.0% | 7.1% | 23% | 82% | 87% | | | | |
| | First | Second | Third | Fourth | Fifth | | | | |
| PCE in dry-cleaning – MAK based | generation | generation | generation | generation | generation | | | | |
| Fraction of impact from PCE outdoor emissions of total impact | 52% | 71% | 58% | 61% | 18% | | | | |
| Fraction of impact from PCE emissions at the workplace of total impact | 0.58% | 0.43% | 0.61% | 0.41% | 0.30% | | | | |
| Remaining emissions from production and disposal | 47% | 28% | 42% | 39% | 81% | | | | |
| PCE in metal-degreasing – e | nvironmental | HLV based | | | | | | | |
| Fraction of impact from PCE outdoor emissions of total impact | 18% | 29% | 19% | 26% | 9% | | | | |
| Fraction of impact from PCE emissions at the workplace of total impact | 66% | 59% | 68% | 58% | 50% | | | | |
| Remaining emissions from production and disposal | 16% | 12% | 14% | 16% | 41% | | | | |

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