

**Supporting information for:**

**Regulatory Control of Amine Scrubbing for CO<sub>2</sub>**

**Capture from Power Plants**

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## Power Plant Model Parameters

Table S1: Power plant operating conditions

	Value
$P_{boiler}$	24.1 MPa
$T_{boiler}$	593°C
$Q_{boiler}$ (full-load)	1410 MW
$Q_{RH}$ (full-load)	357 MW
$\hat{H}_{feedwater}$	1250 kJ/kg
$P_{condenser}$	6.89 kPa
$C_v$ (extraction valve)	0.248 m <sup>2</sup>

Table S2: Flow constants ( $\text{Pa}^2 \cdot \text{s}^2 / \text{K} \cdot \text{kg}^2$ ) for uncontrolled extractions to the next turbine stage ( $\phi_{Di}$ ) and to the feedwater heater ( $\phi_{Dxi}$ )

Turbine	Stage ( $i$ )	$\phi_{Di}$	$\phi_{Dxi}$
HP	1	$1.71 \times 10^6$	$4.86 \times 10^8$
	2	$1.98 \times 10^5$	$8.03 \times 10^6$
IP	3	$1.06 \times 10^5$	$1.89 \times 10^7$
	4	$3.82 \times 10^5$	$2.66 \times 10^7$
LP	5	$8.52 \times 10^3$	$4.24 \times 10^6$
	6	$1.55 \times 10^3$	$9.68 \times 10^5$
	7	295	$3.93 \times 10^5$
	8	44.8	$9.51 \times 10^4$
	9	13.4	—

## Controller Parameters

The discrete-time PI control law is given in Equation S.1. A one second sampling time ( $t_s$ ) was assumed. The parameters for the controllers used in this work are listed in Table S3.

$$u = \bar{u} + K_P(x_{SP} - x_k) + K_I t_s \sum_{k=-\infty}^n (x_{SP} - x_k) \quad (\text{S.1})$$

Table S3: P and PI controller parameters

$u$	$\bar{u}$	$x$	$x_{SP}$	$K_P$	$K_I$
$F_{FT}$	99.3 kmol/s	$l_{FT}$	9.8 m	-540 kmol/m·s	–
$F_{IC}$	102 kmol/s	$l_{CT}$	1.0 m	-1950 kmol/m·s	–
$F_{SU}$	103 kmol/s	$l_{SU}$	2.6 m	-1950 kmol/m·s	–
$F_{WW1}$	32.1 kmol/s	$l_{WT}$	1.0 m	-590 kmol/m·s	–
$F_{WW2}$	30.9 kmol/s	$T_{WW}^V$	315.2 K	65 kmol/K·s	0.477 kmol/K·s <sup>2</sup>
$q_v$	1	$T_{SH}$	426.0 K	0.0500 1/K	0.0220 1/K·s
$F_{CO_2}$	2.50 kmol/s	$\begin{cases} T_{SH} & 426.0 \text{ K} \\ Rem & 90\% \\ P_{ST} & 6.01 \text{ bar} \end{cases}$	$\begin{cases} -2.00 \text{ kmol/K·s} \\ 0.0160 \text{ kmol/s} \\ -0.0120 \text{ kmol/bar·s} \end{cases}$	$\begin{cases} -0.0733 \text{ kmol/K·s}^2 \\ 4.88 \times 10^{-5} \text{ kmol/s}^2 \\ -5.30 \times 10^{-3} \text{ kmol/bar·s}^2 \end{cases}$	

# Notation

## Greek

$\phi_{Di}$	flow constant for uncontrolled steam extraction to next stage
$\phi_{Dxi}$	flow constant for uncontrolled steam extraction to feedwater heater

## Roman

$C_v$	steam extraction valve flow coefficient
$F_{CO_2}$	CO <sub>2</sub> flowrate through multi-stage compressor
$F_{FT}$	flash tank effluent flowrate
$F_{IC}$	absorber chimney tray effluent flowrate
$F_{SU}$	absorber sump effluent flowrate
$F_{WW1}$	water tank effluent flowrate
$F_{WW2}$	water wash chimney tray effluent flowrate
$\hat{H}_{feedwater}$	specific enthalpy of boiler feedwater
$K_I$	integral gain
$K_P$	proportional gain
$l_{CT}$	absorber chimney tray level
$l_{FT}$	flash tank level
$l_{SU}$	absorber sump level
$l_{WT}$	water tank level
$P_{boiler}$	supercritical boiler pressure

$P_{condenser}$	LP steam condenser
$P_{ST}$	stripper pressure
$Q_{boiler}$	duty applied to boiler feedwater
$Q_{RH}$	reheating duty applied to steam exiting HP turbine
$q_V$	steam extraction valve stem position
$Rem$	$\text{CO}_2$ removal rate from the flue gas
$T_{boiler}$	supercritical boiler temperature
$t_s$	sampling time
$T_{SH}$	steam heater outlet temperature
$T_{WW}^V$	water wash outlet vapor temperature
$u$	manipulated variable
$\bar{u}$	nominal value for manipulated variable
$x$	controlled variable
$x_{SP}$	set point for controlled variable