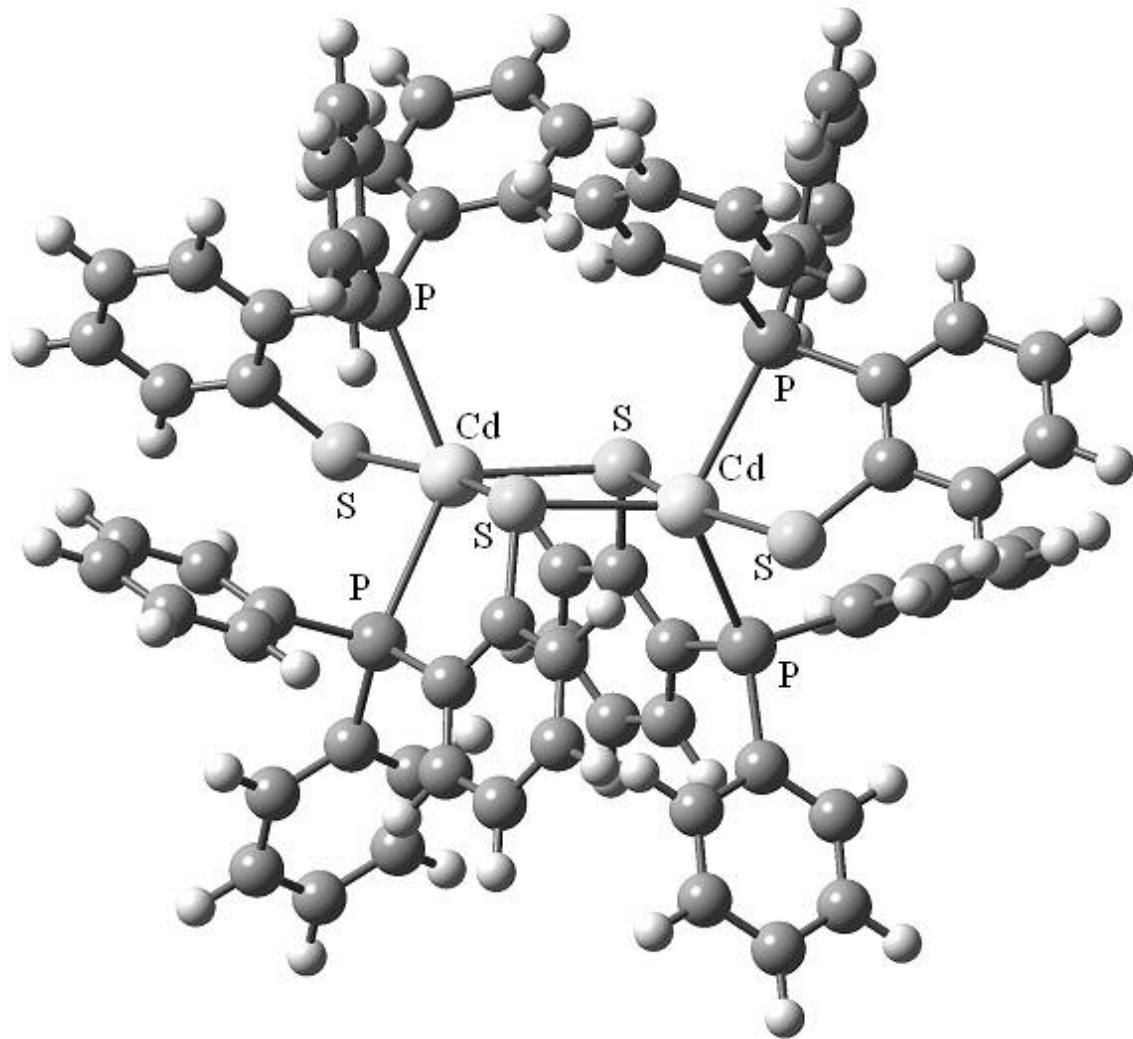
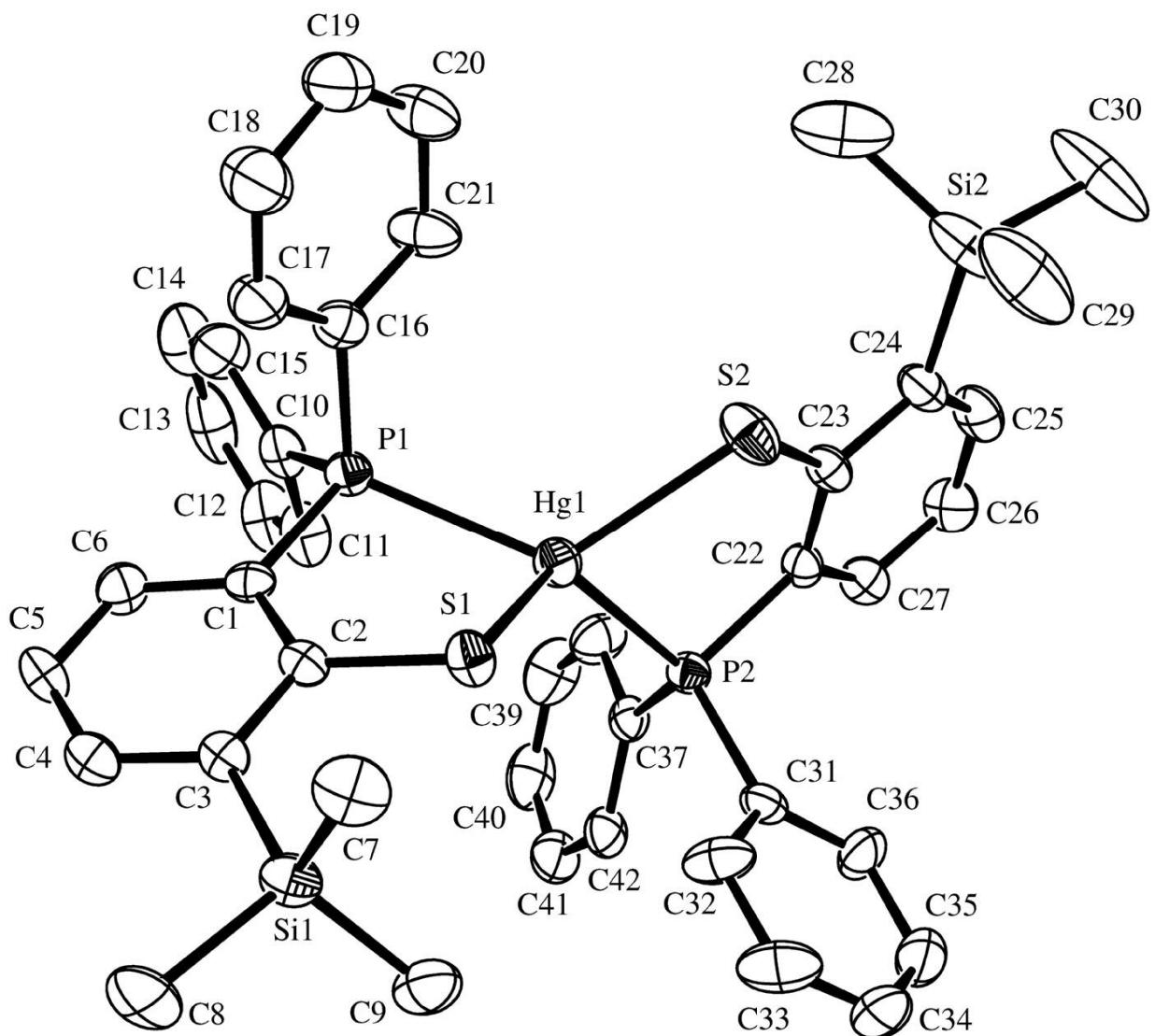
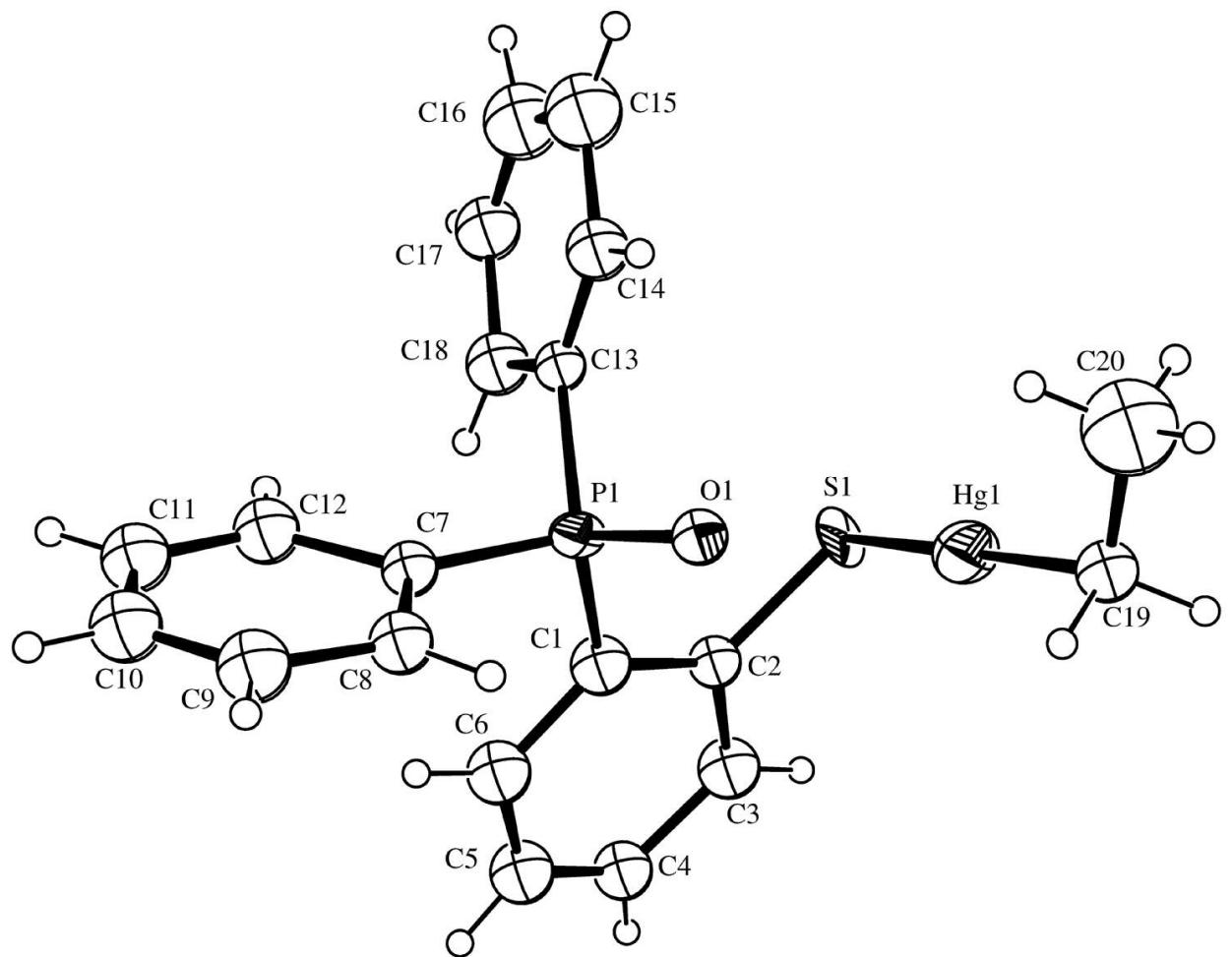


The optimized structure of **1**

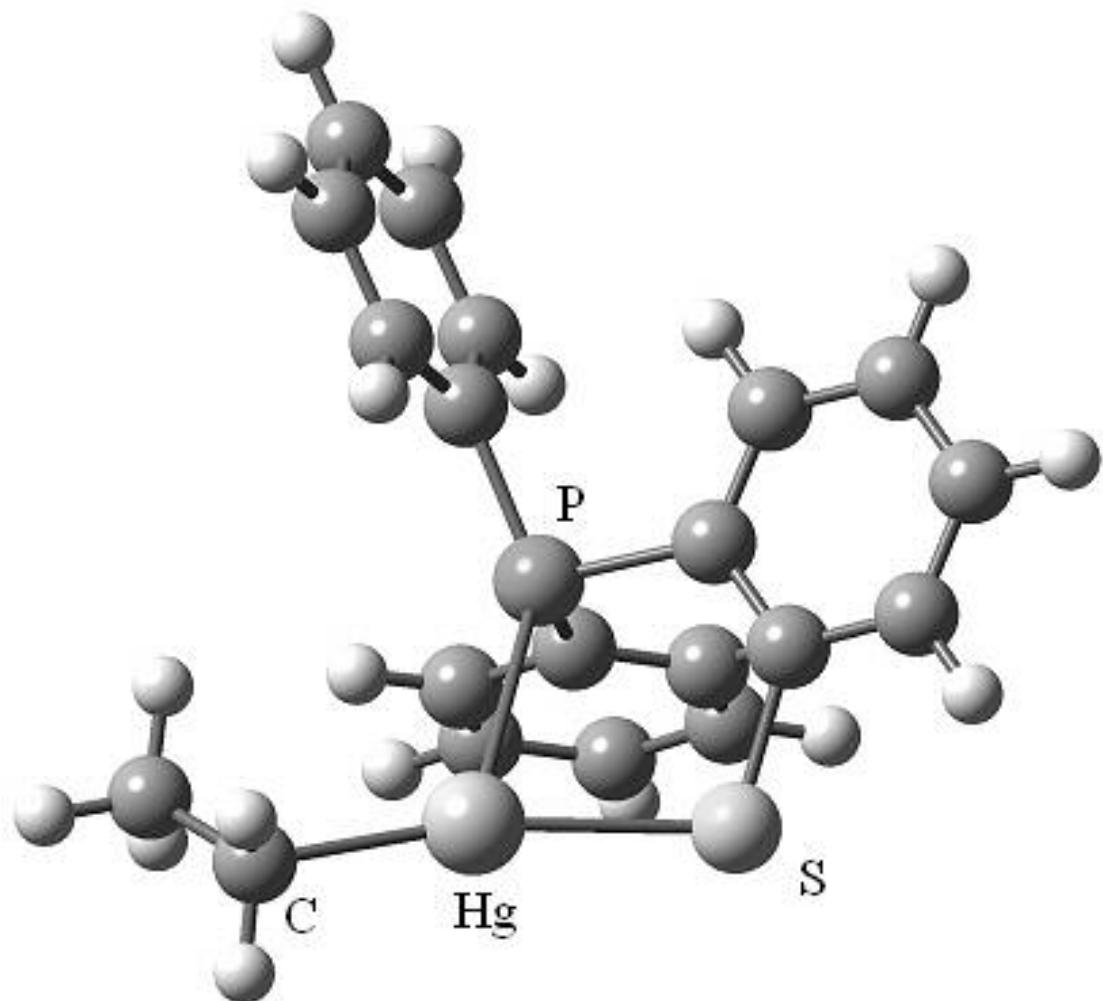


The optimized structure of **2**

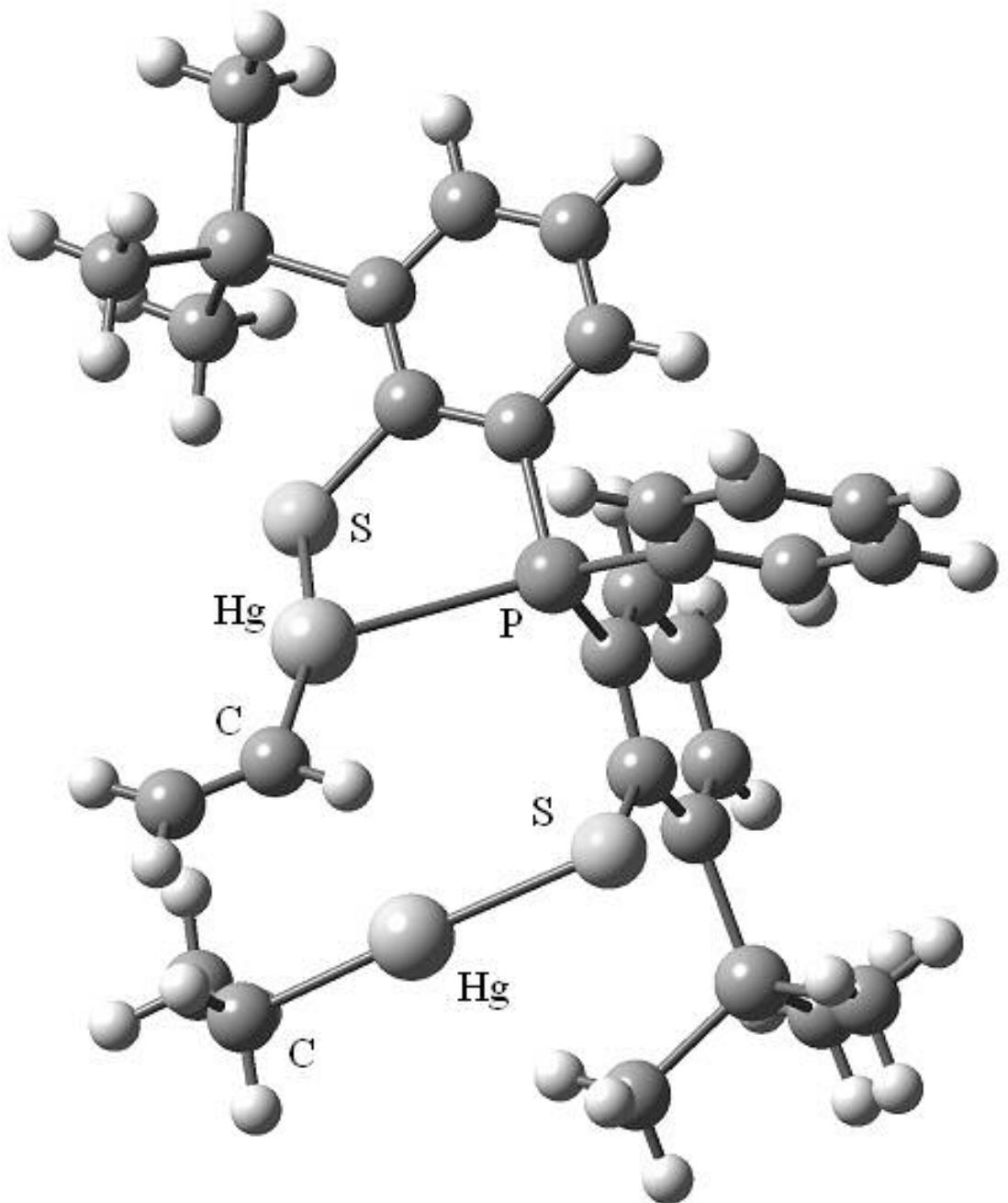




ORTEP diagram of the molecular structure of  $7^*$ , with 50% thermal ellipsoid probability



The optimized structure of **7**



## Compound (1\*)

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?
;
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'H'   'H'   0.0000  0.0000
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'O'   'O'   0.0106  0.0060
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
'P'   'P'   0.1023  0.0942
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'S'   'S'   0.1246  0.1234
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'Zn'   'Zn'   0.2839  1.4301
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_symmetry_space_group_name_H-M    'P -1'

loop_
_symmetry_equiv_pos_as_xyz
'x, y, z'
'-x, -y, -z'

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_cell_length_c                  20.05(2)
_cell_angle_alpha                109.455(15)
_cell_angle_beta                 97.335(16)
_cell_angle_gamma                99.492(16)
_cell_volume                     2938(5)
_cell_formula_units_Z            2
_cell_measurement_temperature     150(2)
_cell_measurement_reflns_used    1016
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_exptl_absorpt_process_details ?  

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;  

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_computing_molecular_graphics ?
_computing_publication_material ?  

_refine_special_details  

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  Refinement of F^2 against ALL reflections. The weighted R-factor wR  

and  

  goodness of fit S are based on F^2, conventional R-factors R are  

based  

  on F, with F set to zero for negative F^2. The threshold expression  

of  

  F^2 > 2sigma(F^2) is used only for calculating R-factors(gt) etc.  

and is

```

not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on  $F$ , and R-factors based on ALL data will be even larger.  
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<u>_refine_ls_structure_factor_coef</u>	Fsqd
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<u>_atom_sites_solution_primary</u>	direct
<u>_atom_sites_solution_secondary</u>	difmap
<u>_atom_sites_solution_hydrogens</u>	geom
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<u>_refine_ls_extinction_method</u>	none
<u>_refine_ls_extinction_coeff</u>	?
<u>_refine_ls_number_reflns</u>	11882
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<u>_refine_ls_R_factor_all</u>	0.0443
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loop\_

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Zn2 Zn 0.37468(3)	0.13150(2)	0.289586(14)	0.02884(8)	Uani	1	1	d	.	.	.
Zn3 Zn 0.20977(3)	0.27390(2)	0.175341(15)	0.02922(8)	Uani	1	1	d	.	.	.
S1 S -0.05879(5)	0.05873(5)	0.33337(3)	0.02807(13)	Uani	1	1	d	.	.	.
S2 S 0.45817(5)	0.17636(5)	0.40625(3)	0.02782(13)	Uani	1	1	d	.	.	.
S3 S 0.38265(6)	0.27569(5)	0.24969(3)	0.02865(13)	Uani	1	1	d	.	.	.
S4 S 0.19809(5)	-0.00018(4)	0.23247(3)	0.02742(13)	Uani	1	1	d	.	.	.
S5 S 0.01511(5)	0.18747(4)	0.18670(3)	0.02522(12)	Uani	1	1	d	.	.	.
S6 S 0.20827(8)	0.27209(6)	0.06132(4)	0.04731(19)	Uani	1	1	d	.	.	.
P1 P 0.19020(5)	0.24297(4)	0.42757(3)	0.02085(12)	Uani	1	1	d	.	.	.
P2 P 0.45323(6)	0.06389(5)	0.17967(3)	0.02875(14)	Uani	1	1	d	.	.	.
P3 P 0.12387(6)	0.41921(5)	0.20518(3)	0.03123(15)	Uani	1	1	d	.	.	.
O1 O 0.19520(13)	0.22966(12)	0.34960(8)	0.0235(3)	Uani	1	1	d	.	.	.
C1 C 0.0371(2)	0.25000(18)	0.44429(12)	0.0243(5)	Uani	1	1	d	.	.	.
C2 C -0.0649(2)	0.17227(18)	0.40279(12)	0.0244(5)	Uani	1	1	d	.	.	.
C3 C -0.1808(2)	0.1826(2)	0.41902(13)	0.0290(5)	Uani	1	1	d	.	.	.

H3 H -0.2508 0.1300 0.3921 0.035 Uiso 1 1 calc R . .
 C4 C -0.1946(2) 0.2669(2) 0.47274(14) 0.0370(6) Uani 1 1 d . .
 H4 H -0.2735 0.2713 0.4835 0.044 Uiso 1 1 calc R . .
 C5 C -0.0951(2) 0.3456(2) 0.51143(15) 0.0414(7) Uani 1 1 d . .
 H5 H -0.1057 0.4051 0.5475 0.050 Uiso 1 1 calc R . .
 C6 C 0.0206(2) 0.3373(2) 0.49734(14) 0.0342(6) Uani 1 1 d . .
 H6 H 0.0892 0.3915 0.5239 0.041 Uiso 1 1 calc R . .
 C7 C 0.2350(2) 0.14229(17) 0.45346(12) 0.0245(5) Uani 1 1 d . .
 C8 C 0.3445(2) 0.11134(18) 0.43917(12) 0.0248(5) Uani 1 1 d . .
 C9 C 0.3699(2) 0.0288(2) 0.45624(15) 0.0359(6) Uani 1 1 d . .
 H9 H 0.4415 0.0050 0.4452 0.043 Uiso 1 1 calc R . .
 C10 C 0.2923(3) -0.0194(2) 0.48906(17) 0.0446(7) Uani 1 1 d . .
 H10 H 0.3114 -0.0756 0.5004 0.054 Uiso 1 1 calc R . .
 C11 C 0.1879(3) 0.0134(2) 0.50543(16) 0.0402(6) Uani 1 1 d . .
 H11 H 0.1361 -0.0189 0.5290 0.048 Uiso 1 1 calc R . .
 C12 C 0.1590(2) 0.09355(19) 0.48742(13) 0.0300(5) Uani 1 1 d . .
 H12 H 0.0865 0.1158 0.4983 0.036 Uiso 1 1 calc R . .
 C13 C 0.2879(2) 0.36249(17) 0.48607(12) 0.0246(5) Uani 1 1 d . .
 C14 C 0.2990(2) 0.44343(18) 0.46171(14) 0.0310(5) Uani 1 1 d . .
 H14 H 0.2605 0.4332 0.4141 0.037 Uiso 1 1 calc R . .
 C15 C 0.3662(2) 0.53914(19) 0.50700(15) 0.0363(6) Uani 1 1 d . .
 H15 H 0.3747 0.5946 0.4903 0.044 Uiso 1 1 calc R . .
 C16 C 0.4211(2) 0.5540(2) 0.57676(15) 0.0386(6) Uani 1 1 d . .
 H16 H 0.4667 0.6198 0.6079 0.046 Uiso 1 1 calc R . .
 C17 C 0.4102(2) 0.4742(2) 0.60108(14) 0.0370(6) Uani 1 1 d . .
 H17 H 0.4481 0.4852 0.6490 0.044 Uiso 1 1 calc R . .
 C18 C 0.3436(2) 0.3773(2) 0.55595(13) 0.0314(5) Uani 1 1 d . .
 H18 H 0.3364 0.3219 0.5727 0.038 Uiso 1 1 calc R . .
 C19 C 0.5282(2) 0.1725(2) 0.16156(12) 0.0291(5) Uani 1 1 d . .
 C20 C 0.4937(2) 0.2658(2) 0.19248(12) 0.0291(5) Uani 1 1 d . .
 C21 C 0.5471(2) 0.3512(2) 0.18062(15) 0.0378(6) Uani 1 1 d . .
 H21 H 0.5228 0.4137 0.2011 0.045 Uiso 1 1 calc R . .
 C22 C 0.6371(3) 0.3463(2) 0.13854(15) 0.0428(7) Uani 1 1 d . .
 H22 H 0.6731 0.4054 0.1300 0.051 Uiso 1 1 calc R . .
 C23 C 0.6741(2) 0.2558(2) 0.10930(14) 0.0413(7) Uani 1 1 d . .
 H23 H 0.7367 0.2531 0.0817 0.050 Uiso 1 1 calc R . .
 C24 C 0.6198(2) 0.1695(2) 0.12034(13) 0.0357(6) Uani 1 1 d . .
 H24 H 0.6447 0.1072 0.0998 0.043 Uiso 1 1 calc R . .
 C25 C 0.3058(2) 0.01944(18) 0.11808(12) 0.0282(5) Uani 1 1 d . .
 C26 C 0.1996(2) -0.01208(17) 0.14097(13) 0.0272(5) Uani 1 1 d . .
 C27 C 0.0898(2) -0.05653(19) 0.09062(15) 0.0351(6) Uani 1 1 d . .
 H27 H 0.0174 -0.0787 0.1058 0.042 Uiso 1 1 calc R . .
 C28 C 0.0857(2) -0.0685(2) 0.01903(14) 0.0378(6) Uani 1 1 d . .
 H28 H 0.0116 -0.1023 -0.0151 0.045 Uiso 1 1 calc R . .
 C29 C 0.1889(2) -0.0317(2) -0.00334(14) 0.0378(6) Uani 1 1 d . .
 H29 H 0.1845 -0.0363 -0.0520 0.045 Uiso 1 1 calc R . .
 C30 C 0.2981(2) 0.0118(2) 0.04577(13) 0.0358(6) Uani 1 1 d . .
 H30 H 0.3690 0.0370 0.0306 0.043 Uiso 1 1 calc R . .
 C31 C 0.5375(2) -0.0349(2) 0.14817(13) 0.0327(6) Uani 1 1 d . .
 C32 C 0.6496(3) -0.0254(2) 0.19043(17) 0.0499(8) Uani 1 1 d . .
 H32 H 0.6778 0.0300 0.2352 0.060 Uiso 1 1 calc R . .
 C33 C 0.7198(3) -0.0955(3) 0.16798(19) 0.0600(9) Uani 1 1 d . .
 H33 H 0.7973 -0.0872 0.1966 0.072 Uiso 1 1 calc R . .
 C34 C 0.6791(3) -0.1772(3) 0.10466(18) 0.0614(10) Uani 1 1 d . .
 H34 H 0.7276 -0.2261 0.0898 0.074 Uiso 1 1 calc R . .
 C35 C 0.5685(3) -0.1884(3) 0.06264(17) 0.0672(11) Uani 1 1 d . .
 H35 H 0.5405 -0.2451 0.0185 0.081 Uiso 1 1 calc R . .
 C36 C 0.4976(3) -0.1180(3) 0.08408(15) 0.0514(8) Uani 1 1 d . .
 H36 H 0.4208 -0.1265 0.0547 0.062 Uiso 1 1 calc R . .
 C37 C -0.0001(2) 0.39186(19) 0.24948(13) 0.0303(5) Uani 1 1 d . .
 C38 C -0.0437(2) 0.29042(18) 0.24160(12) 0.0266(5) Uani 1 1 d . .

C39 C -0.1416(2) 0.2664(2) 0.27359(13) 0.0312(5) Uani 1 1 d . . .
 H39 H -0.1726 0.1975 0.2682 0.037 Uiso 1 1 calc R . .
 C40 C -0.1936(3) 0.3431(2) 0.31319(14) 0.0385(6) Uani 1 1 d . . .
 H40 H -0.2597 0.3263 0.3351 0.046 Uiso 1 1 calc R . .
 C41 C -0.1506(3) 0.4433(2) 0.32124(15) 0.0415(7) Uani 1 1 d . . .
 H41 H -0.1871 0.4953 0.3483 0.050 Uiso 1 1 calc R . .
 C42 C -0.0540(3) 0.4678(2) 0.28964(15) 0.0390(6) Uani 1 1 d . . .
 H42 H -0.0241 0.5370 0.2953 0.047 Uiso 1 1 calc R . .
 C43 C 0.0479(3) 0.3997(2) 0.11431(14) 0.0381(6) Uani 1 1 d . . .
 C44 C 0.0869(3) 0.3362(2) 0.05555(15) 0.0424(7) Uani 1 1 d . . .
 C45 C 0.0232(3) 0.3196(3) -0.01400(17) 0.0577(9) Uani 1 1 d . . .
 H45 H 0.0487 0.2782 -0.0551 0.069 Uiso 1 1 calc R . .
 C46 C -0.0751(4) 0.3624(3) -0.0233(2) 0.0692(11) Uani 1 1 d . . .
 H46 H -0.1174 0.3493 -0.0707 0.083 Uiso 1 1 calc R . .
 C47 C -0.1135(3) 0.4243(3) 0.0353(2) 0.0633(10) Uani 1 1 d . . .
 H47 H -0.1812 0.4540 0.0283 0.076 Uiso 1 1 calc R . .
 C48 C -0.0524(3) 0.4423(2) 0.10389(18) 0.0498(8) Uani 1 1 d . . .
 H48 H -0.0789 0.4842 0.1444 0.060 Uiso 1 1 calc R . .
 C49 C 0.1994(3) 0.5527(2) 0.25049(16) 0.0409(6) Uani 1 1 d . . .
 C50 C 0.1898(5) 0.6241(3) 0.2199(3) 0.1003(18) Uani 1 1 d . . .
 H50 H 0.1405 0.6057 0.1735 0.120 Uiso 1 1 calc R . .
 C51 C 0.2548(6) 0.7264(3) 0.2587(4) 0.132(2) Uani 1 1 d . . .
 H51 H 0.2460 0.7774 0.2388 0.158 Uiso 1 1 calc R . .
 C52 C 0.3293(5) 0.7526(3) 0.3238(3) 0.0957(16) Uani 1 1 d . . .
 H52 H 0.3725 0.8214 0.3491 0.115 Uiso 1 1 calc R . .
 C53 C 0.3416(4) 0.6809(3) 0.3524(2) 0.0704(11) Uani 1 1 d . . .
 H53 H 0.3942 0.6989 0.3977 0.085 Uiso 1 1 calc R . .
 C54 C 0.2782(3) 0.5814(3) 0.31605(18) 0.0586(9) Uani 1 1 d . . .
 H54 H 0.2889 0.5312 0.3365 0.070 Uiso 1 1 calc R . .

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 0.00300(11)
 Zn2 0.02778(15) 0.03096(16) 0.02351(14) 0.00690(12) 0.00595(11)
 0.00056(12)
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 0.00395(12)
 S1 0.0245(3) 0.0289(3) 0.0268(3) 0.0077(2) 0.0067(2) -0.0011(2)
 S2 0.0184(3) 0.0370(3) 0.0278(3) 0.0135(3) 0.0035(2) 0.0026(2)
 S3 0.0279(3) 0.0310(3) 0.0219(3) 0.0056(2) 0.0069(2) -0.0002(2)
 S4 0.0274(3) 0.0233(3) 0.0303(3) 0.0072(2) 0.0104(2) 0.0040(2)
 S5 0.0264(3) 0.0274(3) 0.0184(3) 0.0056(2) 0.0039(2) 0.0027(2)
 S6 0.0569(5) 0.0565(5) 0.0280(3) 0.0136(3) 0.0190(3) 0.0068(4)
 P1 0.0170(3) 0.0236(3) 0.0201(3) 0.0064(2) 0.0030(2) 0.0031(2)
 P2 0.0256(3) 0.0347(3) 0.0183(3) 0.0035(3) 0.0033(2) -0.0006(3)
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 O1 0.0189(8) 0.0278(8) 0.0220(8) 0.0082(7) 0.0039(6) 0.0021(6)
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 C2 0.0215(11) 0.0314(13) 0.0238(11) 0.0141(10) 0.0048(9) 0.0063(10)
 C3 0.0213(12) 0.0387(14) 0.0314(13) 0.0173(11) 0.0077(10) 0.0065(10)
 C4 0.0247(13) 0.0516(17) 0.0405(15) 0.0183(13) 0.0129(11) 0.0157(12)
 C5 0.0341(15) 0.0444(16) 0.0412(15) 0.0036(13) 0.0123(12) 0.0175(13)
 C6 0.0267(13) 0.0383(15) 0.0318(13) 0.0051(11) 0.0059(10) 0.0077(11)
 C7 0.0231(12) 0.0248(12) 0.0239(11) 0.0083(10) 0.0033(9) 0.0027(9)

C8	0.0208(11)	0.0284(12)	0.0234(11)	0.0087(10)	0.0018(9)	0.0035(9)
C9	0.0327(14)	0.0404(15)	0.0436(15)	0.0211(13)	0.0135(12)	0.0155(12)
C10	0.0440(17)	0.0452(17)	0.0620(19)	0.0360(15)	0.0162(14)	0.0173(14)
C11	0.0375(15)	0.0444(16)	0.0514(17)	0.0312(14)	0.0161(13)	0.0081(12)
C12	0.0239(12)	0.0354(14)	0.0324(13)	0.0146(11)	0.0060(10)	0.0056(10)
C13	0.0184(11)	0.0251(12)	0.0260(12)	0.0039(10)	0.0054(9)	0.0043(9)
C14	0.0258(13)	0.0270(13)	0.0357(14)	0.0067(11)	0.0020(10)	0.0063(10)
C15	0.0326(14)	0.0228(13)	0.0481(16)	0.0059(11)	0.0096(12)	0.0053(11)
C16	0.0288(14)	0.0293(14)	0.0432(16)	-0.0044(12)	0.0103(12)	0.0019(11)
C17	0.0268(13)	0.0457(16)	0.0245(12)	-0.0014(11)	0.0022(10)	0.0023(12)
C18	0.0264(13)	0.0349(14)	0.0299(13)	0.0090(11)	0.0064(10)	0.0035(11)
C19	0.0217(12)	0.0400(14)	0.0176(11)	0.0058(10)	0.0011(9)	-0.0024(10)
C20	0.0210(12)	0.0418(14)	0.0198(11)	0.0095(11)	0.0025(9)	-0.0008(10)
C21	0.0329(14)	0.0439(16)	0.0360(14)	0.0168(12)	0.0085(11)	0.0004(12)
C22	0.0351(15)	0.0557(18)	0.0396(15)	0.0253(14)	0.0091(12)	-0.0029(13)
C23	0.0287(14)	0.066(2)	0.0279(13)	0.0189(13)	0.0077(11)	0.0013(13)
C24	0.0284(13)	0.0501(16)	0.0213(12)	0.0073(11)	0.0049(10)	0.0012(12)
C25	0.0236(12)	0.0295(13)	0.0245(12)	0.0022(10)	0.0048(9)	0.0029(10)
C26	0.0291(13)	0.0190(11)	0.0279(12)	0.0008(9)	0.0080(10)	0.0045(10)
C27	0.0261(13)	0.0296(13)	0.0401(15)	0.0017(11)	0.0070(11)	0.0032(10)
C28	0.0300(14)	0.0374(15)	0.0301(14)	-0.0051(11)	-0.0041(11)	
	0.0091(12)					
C29	0.0353(15)	0.0469(16)	0.0224(12)	0.0015(11)	0.0035(11)	0.0105(12)
C30	0.0313(14)	0.0456(16)	0.0223(12)	0.0026(11)	0.0063(10)	0.0058(12)
C31	0.0274(13)	0.0416(15)	0.0264(12)	0.0101(11)	0.0047(10)	0.0056(11)
C32	0.0418(17)	0.0480(18)	0.0446(17)	0.0043(14)	-0.0092(13)	0.0086(14)
C33	0.0445(18)	0.068(2)	0.058(2)	0.0124(18)	-0.0070(15)	0.0222(17)
C34	0.060(2)	0.081(3)	0.0442(18)	0.0117(18)	0.0080(16)	0.042(2)
C35	0.072(2)	0.081(3)	0.0301(16)	-0.0090(16)	-0.0056(15)	0.042(2)
C36	0.0451(17)	0.066(2)	0.0300(15)	-0.0015(14)	-0.0050(12)	0.0262(16)
C37	0.0324(13)	0.0345(14)	0.0248(12)	0.0105(11)	0.0059(10)	0.0101(11)
C38	0.0289(12)	0.0314(13)	0.0193(11)	0.0087(10)	0.0029(9)	0.0082(10)
C39	0.0262(13)	0.0430(15)	0.0292(13)	0.0185(11)	0.0055(10)	0.0092(11)
C40	0.0336(14)	0.0591(18)	0.0302(13)	0.0196(13)	0.0114(11)	0.0192(13)
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C42	0.0454(16)	0.0333(14)	0.0372(15)	0.0089(12)	0.0085(12)	0.0136(12)
C43	0.0426(16)	0.0360(14)	0.0343(14)	0.0188(12)	0.0026(12)	-0.0042(12)
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C49	0.0442(16)	0.0306(14)	0.0460(16)	0.0113(12)	0.0127(13)	0.0054(12)
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All esds (except the esd in the dihedral angle between two l.s.
planes)
are estimated using the full covariance matrix. The cell esds are
taken
into account individually in the estimation of esds in distances,
angles
and torsion angles; correlations between esds in cell parameters are
only
used when they are defined by crystal symmetry. An approximate
(isotropic)

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treatment of cell esds is used for estimating esds involving l.s.  
planes.  
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C23	C22	C21	120.2(3)	. . . ?
C24	C23	C22	119.8(3)	. . . ?
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C26	C25	C30	119.1(2)	. . . ?
C26	C25	P2	120.44(19)	. . . ?
C30	C25	P2	120.36(19)	. . . ?
C25	C26	C27	119.3(2)	. . . ?
C25	C26	S4	122.70(19)	. . . ?
C27	C26	S4	118.0(2)	. . . ?
C28	C27	C26	120.6(3)	. . . ?
C27	C28	C29	120.5(2)	. . . ?
C30	C29	C28	119.4(3)	. . . ?
C29	C30	C25	120.9(3)	. . . ?
C36	C31	C32	118.3(3)	. . . ?
C36	C31	P2	123.8(2)	. . . ?
C32	C31	P2	117.8(2)	. . . ?
C33	C32	C31	120.5(3)	. . . ?
C34	C33	C32	120.5(3)	. . . ?
C33	C34	C35	119.9(3)	. . . ?
C34	C35	C36	120.2(3)	. . . ?
C35	C36	C31	120.5(3)	. . . ?
C38	C37	C42	119.7(2)	. . . ?
C38	C37	P3	117.87(18)	. . . ?
C42	C37	P3	122.5(2)	. . . ?
C37	C38	C39	119.3(2)	. . . ?
C37	C38	S5	122.32(19)	. . . ?
C39	C38	S5	118.3(2)	. . . ?
C40	C39	C38	120.0(3)	. . . ?
C41	C40	C39	120.9(3)	. . . ?
C40	C41	C42	119.6(3)	. . . ?
C41	C42	C37	120.6(3)	. . . ?
C48	C43	C44	120.8(3)	. . . ?
C48	C43	P3	120.3(2)	. . . ?
C44	C43	P3	118.8(2)	. . . ?
C43	C44	C45	117.4(3)	. . . ?
C45	C44	S6	125.4(2)	. . . ?
C45	C44	S6	117.2(3)	. . . ?
C46	C45	C44	121.0(3)	. . . ?
C45	C46	C47	121.0(3)	. . . ?
C48	C47	C46	119.2(4)	. . . ?
C47	C48	C43	120.5(3)	. . . ?
C50	C49	C54	118.7(3)	. . . ?
C50	C49	P3	122.7(3)	. . . ?
C54	C49	P3	118.4(2)	. . . ?
C49	C50	C51	118.8(4)	. . . ?
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C53	C52	C51	119.8(4)	. . . ?
C52	C53	C54	120.1(4)	. . . ?
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## Compound 2\*

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    Refinement of F^2 against ALL reflections. The weighted R-factor wR
and
    goodness of fit S are based on F^2, conventional R-factors R are
based

```

on F, with F set to zero for negative F<sup>2</sup>. The threshold expression of  
 $F^2 > 2\text{sigma}(F^2)$  is used only for calculating R-factors(gt) etc.  
 and is  
 not relevant to the choice of reflections for refinement. R-factors  
 based  
 on F<sup>2</sup> are statistically about twice as large as those based on F,  
 and R-  
 factors based on ALL data will be even larger.  
;

_refine_ls_structure_factor_coef	Fsqd
_refine_ls_matrix_type	full
_refine_ls_weighting_scheme	calc
_refine_ls_weighting_details	'calc w=1/[\\$s^2^(Fo^2)+(0.0000P)^2+0.0000P] where P=(Fo^2+2Fc^2)/3'
_atom_sites_solution_primary	direct
_atom_sites_solution_secondary	difmap
_atom_sites_solution_hydrogens	geom
_refine_ls_hydrogen_treatment	'constr'
_refine_ls_extinction_method	none
_refine_ls_extinction_coef	?
_refine_ls_number_reflns	7976
_refine_ls_number_parameters	776
_refine_ls_number_restraints	0
_refine_ls_R_factor_all	0.1249
_refine_ls_R_factor_gt	0.0415
_refine_ls_wR_factor_ref	0.0595
_refine_ls_wR_factor_gt	0.0486
_refine_ls_goodness_of_fit_ref	0.790
_refine_ls_restrained_S_all	0.790
_refine_ls_shift/su_max	0.001
_refine_ls_shift/su_mean	0.000

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_atom_site_fract_z	
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_atom_site_refinement_flags	
_atom_site_disorder_assembly	
_atom_site_disorder_group	

Cd1 Cd	0.21071(2)	0.01640(4)	0.42048(2)	0.05460(17)	Uani	1	1	d	.	.	.
Cd2 Cd	0.26267(2)	-0.00721(4)	0.58586(2)	0.05603(17)	Uani	1	1	d	.	.	.
O1 O	0.1612(3)	0.1603(5)	0.4270(3)	0.162(3)	Uani	1	1	d	.	.	.
S1 S	0.22798(9)	0.06998(14)	0.32273(9)	0.0718(7)	Uani	1	1	d	.	.	.
S2 S	0.16319(8)	-0.04636(13)	0.51779(8)	0.0537(6)	Uani	1	1	d	.	.	.
S3 S	0.31710(7)	0.01782(13)	0.48317(7)	0.0546(5)	Uani	1	1	d	.	.	.
S4 S	0.24150(8)	-0.01347(15)	0.68710(8)	0.0737(6)	Uani	1	1	d	.	.	.
P1 P	0.14247(11)	0.22363(19)	0.38207(10)	0.0716(8)	Uani	1	1	d	.	.	.
P2 P	0.13589(9)	-0.14451(14)	0.39569(9)	0.0536(6)	Uani	1	1	d	.	.	.
P3 P	0.36117(8)	-0.12347(14)	0.59189(9)	0.0548(6)	Uani	1	1	d	.	.	.
P4 P	0.27833(9)	0.19002(15)	0.62129(9)	0.0623(6)	Uani	1	1	d	.	.	.
C1 C	0.1157(4)	0.1714(5)	0.3118(3)	0.049(2)	Uani	1	1	d	.	.	.

C2 C 0.1522(3) 0.1025(5) 0.2884(3) 0.055(2) Uani 1 1 d . . .
 C3 C 0.1272(4) 0.0605(5) 0.2364(4) 0.069(2) Uani 1 1 d . . .
 H3 H 0.1500 0.0122 0.2205 0.082 Uiso 1 1 calc R .
 C4 C 0.0689(4) 0.0873(7) 0.2067(3) 0.080(3) Uani 1 1 d . . .
 H4 H 0.0536 0.0580 0.1713 0.096 Uiso 1 1 calc R .
 C5 C 0.0334(4) 0.1585(6) 0.2302(4) 0.070(3) Uani 1 1 d . . .
 H5 H -0.0055 0.1780 0.2109 0.084 Uiso 1 1 calc R .
 C6 C 0.0574(4) 0.1978(5) 0.2816(3) 0.061(2) Uani 1 1 d . . .
 H6 H 0.0341 0.2448 0.2978 0.073 Uiso 1 1 calc R .
 C7 C 0.1989(3) 0.3218(5) 0.3784(4) 0.057(2) Uani 1 1 d . . .
 C8 C 0.1980(4) 0.3738(6) 0.3277(4) 0.082(3) Uani 1 1 d . . .
 H8 H 0.1704 0.3530 0.2952 0.099 Uiso 1 1 calc R .
 C9 C 0.2371(4) 0.4554(7) 0.3246(4) 0.113(4) Uani 1 1 d . . .
 H9 H 0.2376 0.4886 0.2902 0.135 Uiso 1 1 calc R .
 C10 C 0.2750(5) 0.4858(8) 0.3733(6) 0.116(4) Uani 1 1 d . . .
 H10 H 0.3005 0.5430 0.3725 0.139 Uiso 1 1 calc R .
 C11 C 0.2769(5) 0.4346(9) 0.4236(4) 0.121(4) Uani 1 1 d . . .
 H11 H 0.3043 0.4557 0.4562 0.145 Uiso 1 1 calc R .
 C12 C 0.2380(4) 0.3516(7) 0.4259(4) 0.099(3) Uani 1 1 d . . .
 H12 H 0.2388 0.3165 0.4600 0.119 Uiso 1 1 calc R .
 C13 C 0.0788(3) 0.2918(8) 0.4037(3) 0.061(2) Uani 1 1 d . . .
 C14 C 0.0751(4) 0.3971(8) 0.4056(4) 0.098(3) Uani 1 1 d . . .
 H14 H 0.1055 0.4376 0.3947 0.118 Uiso 1 1 calc R .
 C15 C 0.0269(6) 0.4442(9) 0.4235(5) 0.127(4) Uani 1 1 d . . .
 H15 H 0.0250 0.5164 0.4255 0.152 Uiso 1 1 calc R .
 C16 C -0.0187(6) 0.3842(11) 0.4385(5) 0.123(5) Uani 1 1 d . . .
 H16 H -0.0516 0.4162 0.4503 0.148 Uiso 1 1 calc R .
 C17 C -0.0163(5) 0.2807(10) 0.4362(4) 0.111(4) Uani 1 1 d . . .
 H17 H -0.0480 0.2412 0.4454 0.133 Uiso 1 1 calc R .
 C18 C 0.0330(5) 0.2318(7) 0.4202(3) 0.085(3) Uani 1 1 d . . .
 H18 H 0.0356 0.1595 0.4204 0.102 Uiso 1 1 calc R .
 C19 C 0.1536(3) -0.2284(6) 0.4566(3) 0.048(2) Uani 1 1 d . . .
 C20 C 0.1678(3) -0.1821(5) 0.5096(3) 0.0435(19) Uani 1 1 d . . .
 C21 C 0.1830(3) -0.2460(6) 0.5576(3) 0.057(2) Uani 1 1 d . . .
 H21 H 0.1896 -0.2168 0.5938 0.069 Uiso 1 1 calc R .
 C22 C 0.1883(3) -0.3523(7) 0.5515(4) 0.074(3) Uani 1 1 d . . .
 H22 H 0.2000 -0.3936 0.5837 0.089 Uiso 1 1 calc R .
 C23 C 0.1765(4) -0.3981(6) 0.4991(4) 0.082(3) Uani 1 1 d . . .
 H23 H 0.1797 -0.4697 0.4952 0.098 Uiso 1 1 calc R .
 C24 C 0.1597(3) -0.3347(6) 0.4518(3) 0.066(2) Uani 1 1 d . . .
 H24 H 0.1523 -0.3647 0.4159 0.079 Uiso 1 1 calc R .
 C25 C 0.1295(4) -0.2256(5) 0.3338(3) 0.054(2) Uani 1 1 d . . .
 C26 C 0.0802(4) -0.2884(6) 0.3156(4) 0.094(3) Uani 1 1 d . . .
 H26 H 0.0479 -0.2890 0.3351 0.112 Uiso 1 1 calc R .
 C27 C 0.0772(5) -0.3520(8) 0.2679(5) 0.122(4) Uani 1 1 d . . .
 H27 H 0.0429 -0.3929 0.2544 0.146 Uiso 1 1 calc R .
 C28 C 0.1271(6) -0.3519(8) 0.2416(5) 0.121(5) Uani 1 1 d . . .
 H28 H 0.1268 -0.3960 0.2109 0.146 Uiso 1 1 calc R .
 C29 C 0.1762(5) -0.2900(8) 0.2591(5) 0.120(4) Uani 1 1 d . . .
 H29 H 0.2088 -0.2893 0.2400 0.144 Uiso 1 1 calc R .
 C30 C 0.1773(4) -0.2280(6) 0.3057(4) 0.088(3) Uani 1 1 d . . .
 H30 H 0.2115 -0.1864 0.3185 0.106 Uiso 1 1 calc R .
 C31 C 0.0574(3) -0.1009(5) 0.3931(4) 0.051(2) Uani 1 1 d . . .
 C32 C 0.0318(4) -0.0399(5) 0.3478(3) 0.062(2) Uani 1 1 d . . .
 H32 H 0.0541 -0.0244 0.3199 0.074 Uiso 1 1 calc R .
 C33 C -0.0267(4) -0.0015(6) 0.3433(3) 0.076(2) Uani 1 1 d . . .
 H33 H -0.0438 0.0383 0.3118 0.092 Uiso 1 1 calc R .
 C34 C -0.0600(3) -0.0205(6) 0.3838(4) 0.078(3) Uani 1 1 d . . .
 H34 H -0.0996 0.0059 0.3804 0.094 Uiso 1 1 calc R .
 C35 C -0.0343(4) -0.0792(6) 0.4297(4) 0.085(3) Uani 1 1 d . . .
 H35 H -0.0561 -0.0920 0.4584 0.102 Uiso 1 1 calc R .

C36 C 0.0239(4) -0.1195(6) 0.4337(4) 0.078(3) Uani 1 1 d . . .
 H36 H 0.0407 -0.1604 0.4649 0.094 Uiso 1 1 calc R . .
 C37 C 0.3645(3) -0.1728(6) 0.5217(3) 0.049(2) Uani 1 1 d . . .
 C38 C 0.3399(3) -0.1107(5) 0.4749(3) 0.049(2) Uani 1 1 d . . .
 C39 C 0.3374(3) -0.1540(6) 0.4207(3) 0.062(2) Uani 1 1 d . . .
 H39 H 0.3204 -0.1155 0.3886 0.075 Uiso 1 1 calc R . .
 C40 C 0.3597(3) -0.2526(7) 0.4142(4) 0.066(3) Uani 1 1 d . . .
 H40 H 0.3576 -0.2797 0.3780 0.080 Uiso 1 1 calc R . .
 C41 C 0.3850(4) -0.3110(6) 0.4609(4) 0.078(3) Uani 1 1 d . . .
 H41 H 0.4004 -0.3771 0.4564 0.094 Uiso 1 1 calc R . .
 C42 C 0.3874(3) -0.2708(6) 0.5146(4) 0.065(2) Uani 1 1 d . . .
 H42 H 0.4046 -0.3100 0.5463 0.078 Uiso 1 1 calc R . .
 C43 C 0.3766(4) -0.2297(5) 0.6405(3) 0.056(2) Uani 1 1 d . . .
 C44 C 0.3286(4) -0.2756(6) 0.6611(3) 0.075(3) Uani 1 1 d . . .
 H44 H 0.2891 -0.2487 0.6501 0.090 Uiso 1 1 calc R . .
 C45 C 0.3378(5) -0.3594(8) 0.6974(4) 0.106(4) Uani 1 1 d . . .
 H45 H 0.3048 -0.3885 0.7106 0.127 Uiso 1 1 calc R . .
 C46 C 0.3952(6) -0.3994(8) 0.7138(5) 0.131(5) Uani 1 1 d . . .
 H46 H 0.4014 -0.4577 0.7373 0.157 Uiso 1 1 calc R . .
 C47 C 0.4431(5) -0.3549(9) 0.6963(5) 0.128(4) Uani 1 1 d . . .
 H47 H 0.4825 -0.3809 0.7091 0.153 Uiso 1 1 calc R . .
 C48 C 0.4345(4) -0.2719(7) 0.6599(4) 0.092(3) Uani 1 1 d . . .
 H48 H 0.4683 -0.2431 0.6480 0.110 Uiso 1 1 calc R . .
 C49 C 0.4276(3) -0.0407(5) 0.6131(4) 0.055(2) Uani 1 1 d . . .
 C50 C 0.4688(4) -0.0205(6) 0.5787(3) 0.079(3) Uani 1 1 d . . .
 H50 H 0.4632 -0.0506 0.5428 0.094 Uiso 1 1 calc R . .
 C51 C 0.5185(4) 0.0439(7) 0.5969(4) 0.102(3) Uani 1 1 d . . .
 H51 H 0.5465 0.0565 0.5735 0.122 Uiso 1 1 calc R . .
 C52 C 0.5264(4) 0.0892(6) 0.6494(5) 0.091(3) Uani 1 1 d . . .
 H52 H 0.5593 0.1342 0.6611 0.109 Uiso 1 1 calc R . .
 C53 C 0.4868(4) 0.0695(6) 0.6846(4) 0.077(3) Uani 1 1 d . . .
 H53 H 0.4933 0.0990 0.7207 0.092 Uiso 1 1 calc R . .
 C54 C 0.4366(3) 0.0050(6) 0.6665(3) 0.064(2) Uani 1 1 d . . .
 H54 H 0.4089 -0.0077 0.6902 0.077 Uiso 1 1 calc R . .
 C55 C 0.3113(3) 0.1677(6) 0.6947(3) 0.052(2) Uani 1 1 d . . .
 C56 C 0.2953(3) 0.0773(6) 0.7207(3) 0.059(2) Uani 1 1 d . . .
 C57 C 0.3232(4) 0.0595(6) 0.7767(4) 0.081(3) Uani 1 1 d . . .
 H57 H 0.3134 -0.0005 0.7947 0.097 Uiso 1 1 calc R . .
 C58 C 0.3653(4) 0.1287(9) 0.8067(4) 0.105(4) Uani 1 1 d . . .
 H58 H 0.3844 0.1136 0.8439 0.125 Uiso 1 1 calc R . .
 C59 C 0.3786(4) 0.2182(7) 0.7820(4) 0.096(3) Uani 1 1 d . . .
 H59 H 0.4050 0.2666 0.8029 0.115 Uiso 1 1 calc R . .
 C60 C 0.3530(3) 0.2373(5) 0.7264(4) 0.070(2) Uani 1 1 d . . .
 H60 H 0.3636 0.2977 0.7093 0.084 Uiso 1 1 calc R . .
 C61 C 0.3266(4) 0.2888(7) 0.6000(3) 0.069(3) Uani 1 1 d . . .
 C62 C 0.3144(4) 0.3935(9) 0.5982(3) 0.099(3) Uani 1 1 d . . .
 H62 H 0.2785 0.4174 0.6083 0.118 Uiso 1 1 calc R . .
 C63 C 0.3548(5) 0.4650(7) 0.5814(4) 0.120(4) Uani 1 1 d . . .
 H63 H 0.3443 0.5351 0.5784 0.144 Uiso 1 1 calc R . .
 C64 C 0.4095(5) 0.4330(9) 0.5694(4) 0.106(4) Uani 1 1 d . . .
 H64 H 0.4373 0.4813 0.5604 0.127 Uiso 1 1 calc R . .
 C65 C 0.4230(4) 0.3301(10) 0.5709(4) 0.100(3) Uani 1 1 d . . .
 H65 H 0.4599 0.3074 0.5623 0.121 Uiso 1 1 calc R . .
 C66 C 0.3811(5) 0.2572(6) 0.5854(4) 0.083(3) Uani 1 1 d . . .
 H66 H 0.3902 0.1866 0.5851 0.099 Uiso 1 1 calc R . .
 C67 C 0.2064(4) 0.2505(6) 0.6222(4) 0.062(2) Uani 1 1 d . . .
 C68 C 0.1683(5) 0.2771(7) 0.5721(4) 0.101(3) Uani 1 1 d . . .
 H68 H 0.1811 0.2638 0.5382 0.121 Uiso 1 1 calc R . .
 C69 C 0.1107(6) 0.3235(9) 0.5702(5) 0.132(5) Uani 1 1 d . . .
 H69 H 0.0865 0.3442 0.5359 0.158 Uiso 1 1 calc R . .
 C70 C 0.0912(5) 0.3373(7) 0.6201(6) 0.111(4) Uani 1 1 d . . .

H70 H 0.0529 0.3673 0.6195 0.134 Uiso 1 1 calc R . . .  
 C71 C 0.1259(5) 0.3088(7) 0.6699(5) 0.105(4) Uani 1 1 d . . .  
 H71 H 0.1117 0.3167 0.7036 0.126 Uiso 1 1 calc R . . .  
 C72 C 0.1829(4) 0.2675(6) 0.6697(4) 0.089(3) Uani 1 1 d . . .  
 H72 H 0.2073 0.2499 0.7046 0.107 Uiso 1 1 calc R . . .  
 N1S N 0.4495(5) 0.4070(9) 0.4159(6) 0.174(5) Uani 1 1 d . . .  
 C1S C 0.4246(6) 0.3328(10) 0.4148(6) 0.134(5) Uani 1 1 d . . .  
 C2S C 0.3921(5) 0.2356(7) 0.4153(4) 0.172(5) Uani 1 1 d . . .  
 H2S1 H 0.3764 0.2304 0.4497 0.258 Uiso 1 1 calc R . . .  
 H2S2 H 0.4197 0.1788 0.4134 0.258 Uiso 1 1 calc R . . .  
 H2S3 H 0.3586 0.2328 0.3832 0.258 Uiso 1 1 calc R . . .

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 \_atom\_site\_aniso\_U\_22  
 \_atom\_site\_aniso\_U\_33  
 \_atom\_site\_aniso\_U\_23  
 \_atom\_site\_aniso\_U\_13  
 \_atom\_site\_aniso\_U\_12

Cd1 0.0508(4) 0.0596(4) 0.0544(4) 0.0035(3) 0.0128(3) 0.0000(3)  
 Cd2 0.0502(3) 0.0607(4) 0.0569(4) -0.0084(3) 0.0098(3) -0.0035(3)  
 O1 0.159(7) 0.157(7) 0.176(9) -0.023(6) 0.048(6) -0.024(5)  
 S1 0.0604(15) 0.0945(16) 0.0653(17) 0.0191(12) 0.0235(13) 0.0058(12)  
 S2 0.0502(13) 0.0657(14) 0.0471(14) -0.0068(10) 0.0141(10) 0.0000(10)  
 S3 0.0515(12) 0.0586(13) 0.0543(13) 0.0025(11) 0.0117(10) -0.0042(11)  
 S4 0.0827(15) 0.0768(15) 0.0692(15) -0.0088(13) 0.0337(12) -0.0193(13)  
 P1 0.0693(18) 0.094(2) 0.0499(19) 0.0105(14) 0.0085(15) -0.0190(15)  
 P2 0.0536(14) 0.0624(14) 0.0471(15) -0.0018(11) 0.0153(12) -0.0035(11)  
 P3 0.0456(14) 0.0636(14) 0.0546(16) 0.0022(12) 0.0082(12) -0.0035(11)  
 P4 0.0553(15) 0.0779(16) 0.0533(16) 0.0123(12) 0.0097(13) -0.0039(12)  
 C1 0.057(6) 0.059(5) 0.030(5) 0.001(4) 0.011(5) -0.015(4)  
 C2 0.063(6) 0.063(6) 0.043(6) 0.002(4) 0.019(5) -0.004(5)  
 C3 0.088(7) 0.077(6) 0.047(7) -0.012(5) 0.026(5) -0.009(5)  
 C4 0.088(8) 0.114(8) 0.037(6) 0.005(5) 0.010(6) -0.031(6)  
 C5 0.069(7) 0.087(7) 0.049(7) 0.006(5) 0.001(6) -0.005(5)  
 C6 0.064(6) 0.063(5) 0.051(6) 0.005(5) -0.001(5) 0.000(4)  
 C7 0.041(5) 0.077(6) 0.057(7) -0.007(5) 0.017(5) -0.022(4)  
 C8 0.072(7) 0.091(7) 0.086(9) 0.014(6) 0.020(6) -0.020(5)  
 C9 0.113(9) 0.115(9) 0.119(10) 0.001(7) 0.047(7) -0.055(6)  
 C10 0.107(9) 0.107(8) 0.150(12) -0.044(9) 0.064(9) -0.062(7)  
 C11 0.097(8) 0.181(12) 0.086(10) -0.059(8) 0.024(8) -0.064(8)  
 C12 0.079(7) 0.143(9) 0.078(9) -0.041(6) 0.025(6) -0.058(6)  
 C13 0.037(6) 0.098(7) 0.055(6) -0.015(5) 0.023(4) -0.004(5)  
 C14 0.090(9) 0.096(9) 0.112(9) -0.018(7) 0.030(7) 0.002(7)  
 C15 0.092(10) 0.134(11) 0.151(12) -0.033(8) 0.015(8) 0.014(8)  
 C16 0.073(9) 0.214(16) 0.076(9) -0.032(10) 0.000(7) 0.023(12)  
 C17 0.045(8) 0.236(14) 0.053(7) -0.002(9) 0.016(6) -0.026(10)  
 C18 0.056(7) 0.145(8) 0.055(7) -0.003(6) 0.012(5) -0.018(7)  
 C19 0.045(5) 0.050(5) 0.048(6) -0.008(4) 0.012(4) -0.001(4)  
 C20 0.030(4) 0.060(5) 0.043(6) 0.008(5) 0.011(4) -0.003(4)  
 C21 0.050(5) 0.086(6) 0.036(6) 0.005(5) 0.010(4) -0.003(5)  
 C22 0.070(6) 0.070(7) 0.078(8) 0.025(6) 0.003(6) 0.000(5)  
 C23 0.104(7) 0.043(6) 0.097(9) -0.013(6) 0.018(7) -0.005(5)  
 C24 0.073(6) 0.073(7) 0.054(6) 0.008(5) 0.018(5) -0.008(5)  
 C25 0.056(6) 0.060(5) 0.047(6) -0.009(4) 0.012(5) 0.000(5)  
 C26 0.099(8) 0.110(8) 0.071(8) -0.042(6) 0.016(6) -0.023(6)  
 C27 0.109(10) 0.148(10) 0.096(11) -0.049(8) -0.010(8) -0.010(8)  
 C28 0.156(13) 0.102(9) 0.098(10) -0.052(7) 0.006(10) 0.026(9)  
 C29 0.146(11) 0.118(9) 0.110(11) -0.045(7) 0.057(9) -0.011(8)  
 C30 0.093(8) 0.092(7) 0.085(8) -0.036(6) 0.030(7) 0.001(6)

C31	0.061(6)	0.043(5)	0.048(6)	0.000(4)	0.007(5)	-0.002(4)
C32	0.057(6)	0.064(6)	0.070(7)	0.000(5)	0.027(5)	-0.004(4)
C33	0.074(7)	0.083(6)	0.073(7)	0.005(6)	0.015(5)	0.006(6)
C34	0.040(5)	0.103(7)	0.083(7)	-0.009(6)	-0.006(5)	0.005(5)
C35	0.047(6)	0.141(8)	0.076(8)	0.014(6)	0.032(5)	0.017(5)
C36	0.060(7)	0.103(7)	0.073(8)	0.033(5)	0.014(6)	0.002(6)
C37	0.038(5)	0.049(5)	0.060(6)	-0.007(5)	0.014(4)	-0.001(4)
C38	0.034(5)	0.067(6)	0.045(6)	-0.010(5)	0.009(4)	-0.014(4)
C39	0.052(5)	0.075(6)	0.059(7)	-0.005(5)	0.009(5)	-0.022(5)
C40	0.069(7)	0.071(7)	0.068(7)	-0.029(6)	0.035(5)	-0.022(5)
C41	0.092(7)	0.039(6)	0.105(9)	-0.010(6)	0.024(7)	-0.009(5)
C42	0.066(6)	0.061(6)	0.067(7)	-0.006(5)	0.008(5)	0.002(5)
C43	0.041(5)	0.066(6)	0.061(6)	0.012(4)	0.007(5)	0.004(5)
C44	0.060(7)	0.093(7)	0.072(7)	0.023(5)	0.017(5)	0.002(5)
C45	0.135(11)	0.108(9)	0.074(8)	0.033(6)	0.018(7)	-0.041(7)
C46	0.161(14)	0.113(9)	0.104(10)	0.055(7)	-0.012(10)	0.013(10)
C47	0.099(10)	0.131(11)	0.141(12)	0.050(8)	-0.004(8)	0.020(8)
C48	0.074(8)	0.094(7)	0.101(9)	0.025(6)	-0.002(6)	0.010(6)
C49	0.042(5)	0.069(6)	0.055(6)	0.006(5)	0.010(5)	0.006(4)
C50	0.061(6)	0.104(7)	0.072(7)	-0.034(5)	0.015(5)	-0.034(5)
C51	0.091(8)	0.145(9)	0.074(8)	-0.036(6)	0.031(6)	-0.053(6)
C52	0.070(7)	0.093(7)	0.105(10)	-0.018(6)	0.004(7)	-0.037(5)
C53	0.070(7)	0.084(7)	0.074(8)	-0.018(5)	0.009(6)	-0.013(5)
C54	0.056(5)	0.079(6)	0.058(6)	0.002(5)	0.012(4)	0.002(5)
C55	0.042(5)	0.059(5)	0.054(6)	-0.003(5)	0.010(4)	-0.003(4)
C56	0.059(6)	0.086(6)	0.032(6)	0.003(5)	0.009(5)	0.012(5)
C57	0.072(7)	0.104(7)	0.069(8)	0.031(6)	0.019(6)	0.001(5)
C58	0.079(8)	0.187(12)	0.040(7)	0.022(7)	-0.009(6)	0.000(7)
C59	0.077(7)	0.149(10)	0.055(8)	-0.023(7)	-0.002(6)	-0.038(7)
C60	0.069(6)	0.081(6)	0.052(7)	-0.010(5)	-0.004(5)	-0.018(5)
C61	0.077(7)	0.068(7)	0.058(6)	0.008(5)	0.005(5)	0.005(6)
C62	0.109(9)	0.090(8)	0.106(9)	0.014(6)	0.044(6)	0.007(7)
C63	0.120(10)	0.081(8)	0.162(11)	0.030(7)	0.038(8)	-0.020(8)
C64	0.091(9)	0.109(10)	0.112(9)	0.026(7)	0.007(7)	-0.036(8)
C65	0.065(7)	0.140(10)	0.097(8)	0.026(8)	0.018(6)	-0.017(8)
C66	0.084(8)	0.078(7)	0.084(8)	0.013(5)	0.014(6)	0.006(7)
C67	0.063(6)	0.077(6)	0.043(6)	0.014(5)	0.001(6)	-0.004(5)
C68	0.085(8)	0.142(9)	0.074(9)	0.026(6)	0.008(7)	-0.003(7)
C69	0.089(11)	0.171(11)	0.115(12)	0.058(10)	-0.029(9)	0.008(8)
C70	0.078(9)	0.101(8)	0.154(14)	0.033(9)	0.018(10)	0.023(6)
C71	0.090(9)	0.112(8)	0.116(11)	0.020(7)	0.031(8)	0.040(6)
C72	0.079(8)	0.101(7)	0.084(9)	0.003(6)	0.007(7)	0.044(6)
N1S	0.128(10)	0.203(12)	0.211(12)	0.029(10)	0.085(8)	-0.019(7)
C1S	0.114(12)	0.171(16)	0.143(11)	0.035(12)	0.083(9)	-0.010(10)
C2S	0.199(13)	0.136(10)	0.205(14)	-0.010(9)	0.101(10)	-0.028(9)

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All esds (except the esd in the dihedral angle between two l.s.
planes)
are estimated using the full covariance matrix. The cell esds are
taken
into account individually in the estimation of esds in distances,
angles
and torsion angles; correlations between esds in cell parameters are
only
used when they are defined by crystal symmetry. An approximate
(isotropic)
treatment of cell esds is used for estimating esds involving l.s.
planes.
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P1 C13 1.823(8) . ?  
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_reflns_number_gt                 6047
_reflns_threshold_expression      >2sigma(I)

_computing_data_collection         'BRUKER Smart'
_computing_cell_refinement         'BRUKER Smart'
_computing_data_reduction          ?
_computing_structure_solution     'SHELXS-97 (Sheldrick, 1990)'
_computing_structure_refinement   'SHELXL-97 (Sheldrick, 1997)'
_computing_molecular_graphics     ?
_computing_publication_material   ?

_refine_special_details
;
    Refinement of F^2 against ALL reflections. The weighted R-factor wR
and
    goodness of fit S are based on F^2, conventional R-factors R are
based
    on F, with F set to zero for negative F^2. The threshold expression
of
    F^2 > 2sigma(F^2) is used only for calculating R-factors(gt) etc.
and is
    not relevant to the choice of reflections for refinement. R-factors
based
    on F^2 are statistically about twice as large as those based on F,
and R-
    factors based on ALL data will be even larger.
;

_refine_ls_structure_factor_coef   Fsqd
_refine_ls_matrix_type             full
_refine_ls_weighting_scheme        calc
_refine_ls_weighting_details
    'calc w=1/[s^2(Fo^2)+(0.0352P)^2+3.7419P] where
P=(Fo^2+2Fc^2)/3'
_atom_sites_solution_primary       direct
_atom_sites_solution_secondary     difmap
_atom_sites_solution_hydrogens    geom
_refine_ls_hydrogen_treatment     'constr'
_refine_ls_extinction_method      none
_refine_ls_extinction_coef        ?
_refine_ls_number_reflns          9748
_refine_ls_number_parameters      561

```

_refine_ls_number_restraints	0
_refine_ls_R_factor_all	0.0873
_refine_ls_R_factor_gt	0.0380
_refine_ls_wR_factor_ref	0.1049
_refine_ls_wR_factor_gt	0.0817
_refine_ls_goodness_of_fit_ref	1.049
_refine_ls_restrained_S_all	1.049
_refine_ls_shift/su_max	0.001
_refine_ls_shift/su_mean	0.000
loop_	
_atom_site_label	
_atom_site_type_symbol	
_atom_site_fract_x	
_atom_site_fract_y	
_atom_site_fract_z	
_atom_site_U_iso_or_equiv	
_atom_site_adp_type	
_atom_site_occupancy	
_atom_site_symmetry_multiplicity	
_atom_site_calc_flag	
_atom_site_refinement_flags	
_atom_site_disorder_assembly	
_atom_site_disorder_group	
Zn1 Zn 0.13201(4) 0.48014(2) 0.256418(17) 0.03693(11) Uani 1 1 d . . .	
Zn2 Zn 0.36685(4) 0.29076(2) 0.252605(18) 0.03786(12) Uani 1 1 d . . .	
S1 S -0.06512(9) 0.44246(5) 0.24693(4) 0.0469(2) Uani 1 1 d . . .	
S2 S 0.18773(8) 0.32324(5) 0.19035(4) 0.0416(2) Uani 1 1 d . . .	
S3 S 0.56148(9) 0.33184(5) 0.26113(5) 0.0497(3) Uani 1 1 d . . .	
S4 S 0.30944(8) 0.44661(5) 0.32032(4) 0.0415(2) Uani 1 1 d . . .	
P1 P 0.10445(7) 0.47696(4) 0.15035(4) 0.02995(19) Uani 1 1 d . . .	
P2 P 0.39551(7) 0.29159(5) 0.35776(4) 0.0312(2) Uani 1 1 d . . .	
N1 N 0.1200(2) 0.59269(14) 0.26848(12) 0.0381(7) Uani 1 1 d . . .	
N2 N 0.3820(3) 0.17925(14) 0.23486(12) 0.0385(7) Uani 1 1 d . . .	
C1 C -0.0436(3) 0.43367(17) 0.12861(15) 0.0339(8) Uani 1 1 d . . .	
C2 C -0.1123(3) 0.42182(17) 0.17098(15) 0.0356(8) Uani 1 1 d . . .	
C3 C -0.2273(3) 0.38979(19) 0.15140(19) 0.0497(10) Uani 1 1 d . . .	
H3 H -0.2755 0.3823 0.1782 0.060 Uiso 1 1 calc R . .	
C4 C -0.2702(4) 0.3692(2) 0.0937(2) 0.0609(12) Uani 1 1 d . . .	
H4 H -0.3472 0.3487 0.0819 0.073 Uiso 1 1 calc R . .	
C5 C -0.1999(4) 0.3788(2) 0.05290(19) 0.0580(11) Uani 1 1 d . . .	
H5 H -0.2279 0.3635 0.0141 0.070 Uiso 1 1 calc R . .	
C6 C -0.0876(3) 0.41144(19) 0.07087(16) 0.0450(9) Uani 1 1 d . . .	
H6 H -0.0404 0.4187 0.0436 0.054 Uiso 1 1 calc R . .	
C7 C 0.2014(3) 0.42939(17) 0.11114(14) 0.0312(7) Uani 1 1 d . . .	
C8 C 0.2425(3) 0.36099(18) 0.13203(14) 0.0352(8) Uani 1 1 d . . .	
C9 C 0.3226(3) 0.3246(2) 0.10473(16) 0.0492(10) Uani 1 1 d . . .	
H9 H 0.3511 0.2793 0.1181 0.059 Uiso 1 1 calc R . .	
C10 C 0.3599(3) 0.3554(2) 0.05793(17) 0.0536(11) Uani 1 1 d . . .	
H10 H 0.4149 0.3312 0.0408 0.064 Uiso 1 1 calc R . .	
C11 C 0.3166(3) 0.4216(2) 0.03644(17) 0.0517(10) Uani 1 1 d . . .	
H11 H 0.3404 0.4413 0.0042 0.062 Uiso 1 1 calc R . .	
C12 C 0.2376(3) 0.4584(2) 0.06303(15) 0.0420(9) Uani 1 1 d . . .	
H12 H 0.2083 0.5031 0.0486 0.050 Uiso 1 1 calc R . .	
C13 C 0.0839(3) 0.56622(17) 0.11688(14) 0.0329(7) Uani 1 1 d . . .	
C14 C -0.0241(3) 0.59016(19) 0.08106(16) 0.0428(9) Uani 1 1 d . . .	
H14 H -0.0891 0.5585 0.0694 0.051 Uiso 1 1 calc R . .	
C15 C -0.0366(4) 0.6612(2) 0.06226(18) 0.0568(11) Uani 1 1 d . . .	
H15 H -0.1097 0.6767 0.0379 0.068 Uiso 1 1 calc R . .	
C16 C 0.0578(4) 0.7084(2) 0.07936(18) 0.0561(11) Uani 1 1 d . . .	
H16 H 0.0486 0.7560 0.0672 0.067 Uiso 1 1 calc R . .	

C17 C 0.1661(4) 0.6853(2) 0.11440(18) 0.0550(10) Uani 1 1 d . . .
 H17 H 0.2307 0.7172 0.1256 0.066 Uiso 1 1 calc R . .
 C18 C 0.1798(3) 0.61516(19) 0.13312(17) 0.0465(9) Uani 1 1 d . . .
 H18 H 0.2538 0.6001 0.1569 0.056 Uiso 1 1 calc R . .
 C19 C 0.0188(3) 0.6283(2) 0.24350(18) 0.0508(10) Uani 1 1 d . . .
 H19 H -0.0516 0.6022 0.2277 0.061 Uiso 1 1 calc R . .
 C20 C 0.0137(4) 0.7018(2) 0.24004(19) 0.0590(11) Uani 1 1 d . . .
 H20 H -0.0590 0.7247 0.2223 0.071 Uiso 1 1 calc R . .
 C21 C 0.1156(4) 0.7411(2) 0.26266(19) 0.0642(12) Uani 1 1 d . . .
 H21 H 0.1145 0.7909 0.2600 0.077 Uiso 1 1 calc R . .
 C22 C 0.2202(4) 0.7051(2) 0.28963(19) 0.0628(12) Uani 1 1 d . . .
 H22 H 0.2912 0.7303 0.3060 0.075 Uiso 1 1 calc R . .
 C23 C 0.2188(3) 0.6319(2) 0.29214(17) 0.0484(10) Uani 1 1 d . . .
 H23 H 0.2897 0.6081 0.3111 0.058 Uiso 1 1 calc R . .
 C24 C 0.5458(3) 0.33210(17) 0.38016(16) 0.0377(8) Uani 1 1 d . . .
 C25 C 0.6121(3) 0.34710(17) 0.33766(17) 0.0412(9) Uani 1 1 d . . .
 C26 C 0.7285(3) 0.3781(2) 0.3576(2) 0.0570(11) Uani 1 1 d . . .
 H26 H 0.7752 0.3877 0.3305 0.068 Uiso 1 1 calc R . .
 C27 C 0.7743(4) 0.3942(2) 0.4155(2) 0.0715(14) Uani 1 1 d . . .
 H27 H 0.8509 0.4153 0.4271 0.086 Uiso 1 1 calc R . .
 C28 C 0.7090(4) 0.3799(2) 0.4572(2) 0.0695(13) Uani 1 1 d . . .
 H28 H 0.7409 0.3909 0.4968 0.083 Uiso 1 1 calc R . .
 C29 C 0.5945(4) 0.3486(2) 0.43908(18) 0.0529(10) Uani 1 1 d . . .
 H29 H 0.5497 0.3386 0.4669 0.064 Uiso 1 1 calc R . .
 C30 C 0.3007(3) 0.33822(17) 0.39876(14) 0.0331(7) Uani 1 1 d . . .
 C31 C 0.2577(3) 0.40680(18) 0.37898(15) 0.0369(8) Uani 1 1 d . . .
 C32 C 0.1807(3) 0.4420(2) 0.40824(17) 0.0505(10) Uani 1 1 d . . .
 H32 H 0.1502 0.4870 0.3952 0.061 Uiso 1 1 calc R . .
 C33 C 0.1488(4) 0.4113(2) 0.45640(18) 0.0586(11) Uani 1 1 d . . .
 H33 H 0.0965 0.4355 0.4752 0.070 Uiso 1 1 calc R . .
 C34 C 0.1939(4) 0.3448(2) 0.47688(17) 0.0540(10) Uani 1 1 d . . .
 H34 H 0.1741 0.3249 0.5100 0.065 Uiso 1 1 calc R . .
 C35 C 0.2688(3) 0.3081(2) 0.44764(16) 0.0445(9) Uani 1 1 d . . .
 H35 H 0.2980 0.2629 0.4608 0.053 Uiso 1 1 calc R . .
 C36 C 0.4113(3) 0.19935(17) 0.38523(14) 0.0322(7) Uani 1 1 d . . .
 C37 C 0.3136(3) 0.15344(19) 0.36485(16) 0.0453(9) Uani 1 1 d . . .
 H37 H 0.2396 0.1724 0.3442 0.054 Uiso 1 1 calc R . .
 C38 C 0.3236(3) 0.08040(19) 0.37445(17) 0.0483(9) Uani 1 1 d . . .
 H38 H 0.2572 0.0505 0.3602 0.058 Uiso 1 1 calc R . .
 C39 C 0.4319(4) 0.05230(19) 0.40497(17) 0.0476(9) Uani 1 1 d . . .
 H39 H 0.4403 0.0030 0.4106 0.057 Uiso 1 1 calc R . .
 C40 C 0.5276(4) 0.0969(2) 0.42719(18) 0.0533(10) Uani 1 1 d . . .
 H40 H 0.6001 0.0777 0.4493 0.064 Uiso 1 1 calc R . .
 C41 C 0.5187(3) 0.1699(2) 0.41747(16) 0.0452(9) Uani 1 1 d . . .
 H41 H 0.5852 0.1994 0.4327 0.054 Uiso 1 1 calc R . .
 C42 C 0.2867(3) 0.1407(2) 0.20649(17) 0.0492(10) Uani 1 1 d . . .
 H42 H 0.2152 0.1647 0.1889 0.059 Uiso 1 1 calc R . .
 C43 C 0.2888(4) 0.0672(2) 0.2019(2) 0.0660(12) Uani 1 1 d . . .
 H43 H 0.2198 0.0420 0.1825 0.079 Uiso 1 1 calc R . .
 C44 C 0.3949(4) 0.0319(2) 0.2267(2) 0.0667(12) Uani 1 1 d . . .
 H44 H 0.3992 -0.0178 0.2245 0.080 Uiso 1 1 calc R . .
 C45 C 0.4936(4) 0.0703(2) 0.25437(19) 0.0593(11) Uani 1 1 d . . .
 H45 H 0.5668 0.0473 0.2709 0.071 Uiso 1 1 calc R . .
 C46 C 0.4846(3) 0.14337(19) 0.25782(17) 0.0466(9) Uani 1 1 d . . .
 H46 H 0.5530 0.1692 0.2770 0.056 Uiso 1 1 calc R . .
 N1S N 1.0188(5) 0.4129(3) 0.5858(3) 0.1177(19) Uani 1 1 d . . .
 C1S C 0.9853(5) 0.3565(4) 0.5849(2) 0.0821(16) Uani 1 1 d . . .
 C2S C 0.9415(6) 0.2842(3) 0.5830(3) 0.121(2) Uani 1 1 d . . .
 H2S1 H 0.8581 0.2843 0.5859 0.181 Uiso 1 1 calc R . .
 H2S2 H 0.9900 0.2575 0.6153 0.181 Uiso 1 1 calc R . .
 H2S3 H 0.9472 0.2623 0.5464 0.181 Uiso 1 1 calc R . .

N2S N 0.5263(6) 0.3216(4) 0.5923(3) 0.140(3) Uani 1 1 d . . .
 C3S C 0.4911(6) 0.3770(4) 0.5823(2) 0.096(2) Uani 1 1 d . . .
 C4S C 0.4470(7) 0.4478(4) 0.5697(3) 0.135(3) Uani 1 1 d . . .
 H4S1 H 0.4378 0.4574 0.5284 0.202 Uiso 1 1 calc R . .
 H4S2 H 0.5039 0.4812 0.5925 0.202 Uiso 1 1 calc R . .
 H4S3 H 0.3695 0.4526 0.5797 0.202 Uiso 1 1 calc R . .

 loop\_
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 \_atom\_site\_aniso\_U\_11
 \_atom\_site\_aniso\_U\_22
 \_atom\_site\_aniso\_U\_33
 \_atom\_site\_aniso\_U\_23
 \_atom\_site\_aniso\_U\_13
 \_atom\_site\_aniso\_U\_12
 Zn1 0.0381(2) 0.0309(2) 0.0410(2) 0.00326(18) 0.00772(18) 0.00011(17)
 Zn2 0.0403(2) 0.0304(2) 0.0428(2) 0.00344(18) 0.00958(19) 0.00155(17)
 S1 0.0487(6) 0.0425(5) 0.0567(6) -0.0040(4) 0.0270(5) -0.0109(4)
 S2 0.0417(5) 0.0352(5) 0.0479(5) 0.0097(4) 0.0107(4) 0.0063(4)
 S3 0.0506(6) 0.0408(5) 0.0663(7) -0.0036(5) 0.0310(5) -0.0104(4)
 S4 0.0413(5) 0.0342(5) 0.0477(5) 0.0077(4) 0.0079(4) 0.0056(4)
 P1 0.0273(4) 0.0276(4) 0.0345(5) 0.0035(4) 0.0065(4) 0.0004(3)
 P2 0.0272(5) 0.0283(5) 0.0378(5) 0.0036(4) 0.0069(4) 0.0013(3)
 N1 0.0352(16) 0.0314(16) 0.0468(17) -0.0017(13) 0.0075(14) 0.0005(13)
 N2 0.0414(17) 0.0298(15) 0.0448(17) -0.0017(13) 0.0108(14) 0.0038(13)
 C1 0.0273(17) 0.0268(17) 0.046(2) 0.0054(15) 0.0053(15) 0.0002(14)
 C2 0.0299(18) 0.0264(17) 0.051(2) 0.0069(15) 0.0098(16) 0.0013(14)
 C3 0.030(2) 0.042(2) 0.078(3) 0.013(2) 0.015(2) -0.0005(16)
 C4 0.035(2) 0.055(3) 0.083(3) 0.013(2) -0.006(2) -0.0092(19)
 C5 0.049(3) 0.058(3) 0.057(3) 0.002(2) -0.007(2) -0.008(2)
 C6 0.039(2) 0.045(2) 0.045(2) 0.0065(17) -0.0005(17) -0.0016(17)
 C7 0.0272(17) 0.0333(18) 0.0325(18) -0.0028(14) 0.0056(14) -0.0031(14)
 C8 0.0274(18) 0.038(2) 0.0390(19) -0.0038(15) 0.0046(15) 0.0013(14)
 C9 0.046(2) 0.050(2) 0.051(2) -0.0104(19) 0.0095(19) 0.0119(18)
 C10 0.040(2) 0.071(3) 0.052(2) -0.026(2) 0.0165(19) -0.002(2)
 C11 0.050(2) 0.067(3) 0.041(2) -0.008(2) 0.0185(19) -0.014(2)
 C12 0.039(2) 0.044(2) 0.042(2) 0.0027(17) 0.0098(17) -0.0046(16)
 C13 0.0316(18) 0.0307(18) 0.0371(19) 0.0036(15) 0.0092(15) 0.0021(14)
 C14 0.037(2) 0.036(2) 0.052(2) 0.0054(17) 0.0029(17) -0.0023(16)
 C15 0.050(2) 0.046(2) 0.068(3) 0.019(2) 0.000(2) 0.0092(19)
 C16 0.065(3) 0.033(2) 0.070(3) 0.013(2) 0.015(2) 0.002(2)
 C17 0.055(3) 0.039(2) 0.072(3) 0.002(2) 0.015(2) -0.0098(19)
 C18 0.039(2) 0.038(2) 0.059(2) 0.0061(18) 0.0051(18) -0.0025(16)
 C19 0.040(2) 0.041(2) 0.067(3) -0.009(2) 0.006(2) 0.0014(18)
 C20 0.058(3) 0.038(2) 0.074(3) -0.007(2) 0.002(2) 0.016(2)
 C21 0.079(3) 0.029(2) 0.079(3) -0.007(2) 0.009(3) 0.004(2)
 C22 0.062(3) 0.040(2) 0.083(3) -0.011(2) 0.009(2) -0.009(2)
 C23 0.041(2) 0.040(2) 0.061(3) -0.0058(18) 0.0050(19) 0.0016(17)
 C24 0.0328(19) 0.0250(18) 0.051(2) 0.0041(15) 0.0019(17) 0.0013(14)
 C25 0.0316(19) 0.0249(18) 0.067(2) 0.0082(17) 0.0107(18) 0.0015(14)
 C26 0.036(2) 0.041(2) 0.095(4) 0.007(2) 0.016(2) -0.0021(17)
 C27 0.039(3) 0.059(3) 0.106(4) 0.009(3) -0.005(3) -0.012(2)
 C28 0.047(3) 0.069(3) 0.076(3) -0.002(3) -0.018(2) -0.008(2)
 C29 0.046(2) 0.049(2) 0.059(3) 0.005(2) 0.002(2) -0.0026(19)
 C30 0.0297(18) 0.0311(18) 0.0380(19) -0.0011(14) 0.0069(15) -
 0.0011(14)
 C31 0.0325(19) 0.0360(19) 0.040(2) -0.0017(15) 0.0040(16) 0.0022(15)
 C32 0.049(2) 0.050(2) 0.053(2) -0.0004(19) 0.013(2) 0.0149(19)
 C33 0.049(2) 0.072(3) 0.061(3) -0.013(2) 0.024(2) 0.007(2)
 C34 0.054(3) 0.063(3) 0.050(2) 0.000(2) 0.022(2) -0.005(2)
 C35 0.044(2) 0.042(2) 0.048(2) 0.0039(17) 0.0143(18) 0.0004(17)

C36	0.0308(18)	0.0301(18)	0.0366(18)	0.0047(14)	0.0095(15)	0.0020(14)
C37	0.035(2)	0.039(2)	0.059(2)	0.0086(18)	0.0055(18)	0.0015(16)
C38	0.047(2)	0.037(2)	0.060(3)	0.0031(18)	0.010(2)	-0.0094(17)
C39	0.060(3)	0.0281(19)	0.058(2)	0.0070(17)	0.020(2)	0.0036(18)
C40	0.045(2)	0.038(2)	0.071(3)	0.012(2)	0.001(2)	0.0128(18)
C41	0.035(2)	0.041(2)	0.057(2)	0.0027(18)	0.0033(18)	0.0017(16)
C42	0.044(2)	0.035(2)	0.064(3)	-0.0036(18)	0.004(2)	0.0011(17)
C43	0.060(3)	0.042(2)	0.087(3)	-0.016(2)	0.000(2)	-0.008(2)
C44	0.076(3)	0.035(2)	0.086(3)	-0.009(2)	0.012(3)	0.004(2)
C45	0.056(3)	0.043(2)	0.071(3)	-0.007(2)	-0.002(2)	0.015(2)
C46	0.043(2)	0.039(2)	0.057(2)	-0.0052(18)	0.0100(19)	0.0025(17)
N1S	0.113(4)	0.100(4)	0.142(5)	-0.015(4)	0.034(4)	0.015(4)
C1S	0.080(4)	0.089(4)	0.075(4)	-0.005(4)	0.012(3)	0.017(3)
C2S	0.154(6)	0.096(5)	0.100(5)	0.015(4)	0.007(4)	-0.006(4)
N2S	0.135(5)	0.132(6)	0.127(5)	0.025(4)	-0.023(4)	-0.017(5)
C3S	0.104(5)	0.116(6)	0.053(3)	0.006(4)	-0.009(3)	-0.034(5)
C4S	0.166(7)	0.096(5)	0.116(6)	-0.014(4)	-0.017(5)	-0.014(5)

\_geom\_special\_details

;

All esds (except the esd in the dihedral angle between two l.s. planes)

are estimated using the full covariance matrix. The cell esds are taken

into account individually in the estimation of esds in distances, angles

and torsion angles; correlations between esds in cell parameters are only

used when they are defined by crystal symmetry. An approximate (isotropic)

treatment of cell esds is used for estimating esds involving l.s. planes.

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loop\_

\_geom\_bond\_atom\_site\_label\_1

\_geom\_bond\_atom\_site\_label\_2

\_geom\_bond\_distance

\_geom\_bond\_site\_symmetry\_2

\_geom\_bond\_publ\_flag

Zn1 N1 2.124(3) . ?

Zn1 S4 2.2841(10) . ?

Zn1 S1 2.2932(11) . ?

Zn1 P1 2.4172(10) . ?

Zn2 N2 2.132(3) . ?

Zn2 S2 2.2760(10) . ?

Zn2 S3 2.2899(11) . ?

Zn2 P2 2.3941(11) . ?

S1 C2 1.766(4) . ?

S2 C8 1.765(3) . ?

S3 C25 1.763(4) . ?

S4 C31 1.769(4) . ?

P1 C7 1.812(3) . ?

P1 C1 1.816(3) . ?

P1 C13 1.828(3) . ?

P2 C30 1.814(3) . ?

P2 C24 1.817(3) . ?

P2 C36 1.827(3) . ?

N1 C19 1.331(4) . ?

N1 C23 1.339(4) . ?

N2 C42 1.333(4) . ?

N2 C46 1.336(4) . ?  
 C1 C6 1.383(5) . ?  
 C1 C2 1.408(4) . ?  
 C2 C3 1.404(5) . ?  
 C3 C4 1.372(6) . ?  
 C4 C5 1.385(6) . ?  
 C5 C6 1.379(5) . ?  
 C7 C12 1.389(4) . ?  
 C7 C8 1.403(4) . ?  
 C8 C9 1.396(5) . ?  
 C9 C10 1.382(5) . ?  
 C10 C11 1.375(6) . ?  
 C11 C12 1.381(5) . ?  
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## Compound (5)

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'H'   'H'   0.0000  0.0000
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'P'   'P'   0.1023  0.0942
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'x+1/2, y+1/2, z'
'-x+1/2, y+1/2, -z+1/2'
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'x+1/2, -y+1/2, z-1/2'

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_cell_angle_beta                 98.067(3)
_cell_angle_gamma                90.00
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_refine_special_details
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  Refinement of F^2 against ALL reflections. The weighted R-factor wR
  and
  goodness of fit S are based on F^2, conventional R-factors R are
  based

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on F, with F set to zero for negative F<sup>2</sup>. The threshold expression of  
 $F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc.  
 and is  
 not relevant to the choice of reflections for refinement. R-factors based  
 on F<sup>2</sup> are statistically about twice as large as those based on F,  
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Hg1 Hg	0.0000	0.116245(18)	0.7500	0.03693(6)	Uani	1	2	d	s	.	.
S1 S	0.06533(5)	-0.00722(8)	0.66370(3)	0.03932(17)	Uani	1	1	d	.	.	.
P1 P	-0.09069(4)	0.23109(7)	0.65707(3)	0.02823(14)	Uani	1	1	d	.	.	.
C1 C	-0.02944(17)	0.2092(3)	0.59204(12)	0.0307(6)	Uani	1	1	d	.	.	.
C2 C	0.03616(17)	0.1091(3)	0.59775(13)	0.0303(5)	Uani	1	1	d	.	.	.
C3 C	0.0819(2)	0.0987(3)	0.54569(14)	0.0403(7)	Uani	1	1	d	.	.	.
H3 H	0.1258	0.0339	0.5484	0.048	Uiiso	1	1	calc	R	.	.
C4 C	0.0636(2)	0.1814(4)	0.49096(15)	0.0470(8)	Uani	1	1	d	.	.	.
H4 H	0.0945	0.1712	0.4571	0.056	Uiiso	1	1	calc	R	.	.
C5 C	-0.0005(2)	0.2797(4)	0.48622(15)	0.0504(8)	Uani	1	1	d	.	.	.
H5 H	-0.0124	0.3363	0.4494	0.061	Uiiso	1	1	calc	R	.	.
C6 C	-0.0465(2)	0.2936(3)	0.53591(14)	0.0427(7)	Uani	1	1	d	.	.	.

H6 H -0.0897 0.3599 0.5324 0.051 Uiso 1 1 calc R . . .  
 C7 C -0.18615(17) 0.1311(3) 0.63577(13) 0.0318(6) Uani 1 1 d . . .  
 C8 C -0.2106(2) 0.0763(3) 0.57414(15) 0.0415(7) Uani 1 1 d . . .  
 H8 H -0.1789 0.0944 0.5413 0.050 Uiso 1 1 calc R . . .  
 C9 C -0.2827(2) -0.0059(4) 0.56154(17) 0.0513(8) Uani 1 1 d . . .  
 H9 H -0.2982 -0.0449 0.5206 0.062 Uiso 1 1 calc R . . .  
 C10 C -0.3305(2) -0.0294(4) 0.60907(18) 0.0548(9) Uani 1 1 d . . .  
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 C11 C -0.3073(2) 0.0251(4) 0.66987(18) 0.0581(9) Uani 1 1 d . . .  
 H11 H -0.3402 0.0087 0.7021 0.070 Uiso 1 1 calc R . . .  
 C12 C -0.2352(2) 0.1044(4) 0.68346(17) 0.0476(8) Uani 1 1 d . . .  
 H12 H -0.2195 0.1400 0.7249 0.057 Uiso 1 1 calc R . . .  
 C13 C -0.11886(18) 0.4209(3) 0.65674(13) 0.0307(6) Uani 1 1 d . . .  
 C14 C -0.19954(19) 0.4710(3) 0.64591(15) 0.0415(7) Uani 1 1 d . . .  
 H14 H -0.2431 0.4063 0.6362 0.050 Uiso 1 1 calc R . . .  
 C15 C -0.2156(2) 0.6177(3) 0.64951(18) 0.0535(9) Uani 1 1 d . . .  
 H15 H -0.2699 0.6511 0.6422 0.064 Uiso 1 1 calc R . . .  
 C16 C -0.1513(2) 0.7137(3) 0.66395(17) 0.0529(9) Uani 1 1 d . . .  
 H16 H -0.1623 0.8117 0.6667 0.064 Uiso 1 1 calc R . . .  
 C17 C -0.0714(2) 0.6651(4) 0.67428(17) 0.0533(9) Uani 1 1 d . . .  
 H17 H -0.0282 0.7308 0.6833 0.064 Uiso 1 1 calc R . . .  
 C18 C -0.0541(2) 0.5189(3) 0.67150(15) 0.0433(7) Uani 1 1 d . . .  
 H18 H 0.0003 0.4865 0.6794 0.052 Uiso 1 1 calc R . . .

loop\_

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 P1 0.0256(3) 0.0317(3) 0.0282(3) 0.0002(3) 0.0065(3) 0.0016(3)  
 C1 0.0294(14) 0.0348(14) 0.0286(13) -0.0013(11) 0.0068(11) -0.0007(11)  
 C2 0.0286(14) 0.0314(13) 0.0314(13) -0.0073(11) 0.0062(10) -0.0067(11)  
 C3 0.0379(17) 0.0441(17) 0.0413(16) -0.0091(13) 0.0144(13) -0.0011(13)  
 C4 0.051(2) 0.058(2) 0.0365(16) -0.0045(14) 0.0211(14) -0.0029(16)  
 C5 0.062(2) 0.058(2) 0.0343(16) 0.0104(14) 0.0146(15) 0.0015(17)  
 C6 0.0473(18) 0.0472(18) 0.0345(15) 0.0058(13) 0.0092(13) 0.0056(14)  
 C7 0.0302(14) 0.0288(14) 0.0367(14) 0.0001(11) 0.0057(11) 0.0037(11)  
 C8 0.0411(18) 0.0452(17) 0.0384(16) -0.0030(13) 0.0063(13) 0.0010(13)  
 C9 0.046(2) 0.053(2) 0.0505(19) -0.0119(15) -0.0079(15) -0.0043(15)  
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 C15 0.050(2) 0.0449(18) 0.064(2) 0.0011(16) 0.0048(17) 0.0140(16)  
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\_geom\_special\_details

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All esds (except the esd in the dihedral angle between two l.s. planes)  
 are estimated using the full covariance matrix. The cell esds are taken

into account individually in the estimation of esds in distances,  
angles  
and torsion angles; correlations between esds in cell parameters are  
only  
used when they are defined by crystal symmetry. An approximate  
(isotropic)  
treatment of cell esds is used for estimating esds involving l.s.  
planes.  
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S1 Hg1 P1 119.24(3) . 2\_556 ?  
S1 Hg1 P1 119.24(3) 2\_556 . ?  
S1 Hg1 P1 84.28(3) . . ?  
P1 Hg1 P1 129.77(3) 2\_556 . ?  
C2 S1 Hg1 100.89(9) . . ?  
C1 P1 C7 107.73(13) . . ?  
C1 P1 C13 105.78(12) . . ?  
C7 P1 C13 106.59(13) . . ?

C1 P1 Hg1 101.90(9) . . ?  
C7 P1 Hg1 111.49(9) . . ?  
C13 P1 Hg1 122.34(9) . . ?  
C6 C1 C2 119.8(2) . . ?  
C6 C1 P1 119.9(2) . . ?  
C2 C1 P1 120.3(2) . . ?  
C3 C2 C1 117.3(3) . . ?  
C3 C2 S1 116.7(2) . . ?  
C1 C2 S1 126.0(2) . . ?  
C4 C3 C2 121.9(3) . . ?  
C3 C4 C5 120.1(3) . . ?  
C6 C5 C4 119.9(3) . . ?  
C5 C6 C1 121.0(3) . . ?  
C12 C7 C8 118.8(3) . . ?  
C12 C7 P1 118.5(2) . . ?  
C8 C7 P1 122.6(2) . . ?  
C7 C8 C9 120.0(3) . . ?  
C10 C9 C8 120.2(3) . . ?  
C9 C10 C11 120.4(3) . . ?  
C10 C11 C12 120.1(3) . . ?  
C11 C12 C7 120.6(3) . . ?  
C14 C13 C18 119.4(3) . . ?  
C14 C13 P1 124.0(2) . . ?  
C18 C13 P1 116.5(2) . . ?  
C13 C14 C15 120.2(3) . . ?  
C16 C15 C14 120.0(3) . . ?  
C17 C16 C15 120.2(3) . . ?  
C16 C17 C18 120.6(3) . . ?  
C17 C18 C13 119.6(3) . . ?

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\_diffrn\_reflns\_theta\_full 26.37  
\_diffrn\_measured\_fraction\_theta\_full 0.995  
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\_refine\_diff\_density\_min -0.540  
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## Compound (6)

data\_p382

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'H' 'H' 0.0000 0.0000	
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'Cl' 'Cl' 0.1484 0.1585	
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'-x, -y, -z'	
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_cell_length_a	51.447(4)
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_exptl_absorpt_coefficient_mu	3.656
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Refinement of  $F^2$  against ALL reflections. The weighted R-factor wR and goodness of fit S are based on  $F^2$ , conventional R-factors R are based on F, with F set to zero for negative  $F^2$ . The threshold expression of  $F^2 > 2\text{sigma}(F^2)$  is used only for calculating R-factors(gt) etc. and is not relevant to the choice of reflections for refinement. R-factors based on  $F^2$  are statistically about twice as large as those based on F, and R-factors based on ALL data will be even larger.

;

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_refine_ls_extinction_method	none
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_refine_ls_number_reflns	13353
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_refine_ls_R_factor_gt	0.0442
_refine_ls_wR_factor_ref	0.1341
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_refine_ls_restrained_S_all	1.036
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loop\_

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Hg1 Hg 0.606826(8) 0.31875(3) 0.173785(13) 0.05491(13) Uani 1 1 d . . .  
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 S1 S 0.65533(5) 0.3159(2) 0.24017(8) 0.0547(6) Uani 1 1 d . . .  
 S2 S 0.57199(6) 0.4432(3) 0.18779(9) 0.0763(9) Uani 1 1 d . . .  
 P1 P 0.61037(5) 0.1155(2) 0.18878(8) 0.0484(6) Uani 1 1 d . . .  
 P2 P 0.59562(5) 0.4423(2) 0.10911(8) 0.0457(6) Uani 1 1 d . . .  
 Si1 Si 0.72357(6) 0.2743(3) 0.28630(9) 0.0604(8) Uani 1 1 d . . .  
 Si2 Si 0.51139(8) 0.5563(5) 0.17165(13) 0.1103(16) Uani 1 1 d . . .

C1 C 0.64830(18) 0.0895(8) 0.2144(3) 0.044(2) Uani 1 1 d . . .
 C2 C 0.66713(18) 0.1788(8) 0.2362(3) 0.045(2) Uani 1 1 d . . .
 C3 C 0.69697(19) 0.1596(8) 0.2565(3) 0.048(2) Uani 1 1 d . . .
 C4 C 0.7064(2) 0.0519(9) 0.2543(3) 0.056(3) Uani 1 1 d . . .
 H4 H 0.7260 0.0377 0.2672 0.067 Uiso 1 1 calc R . .
 C5 C 0.6881(2) -0.0346(9) 0.2340(3) 0.060(3) Uani 1 1 d . . .
 H5 H 0.6954 -0.1062 0.2340 0.072 Uiso 1 1 calc R . .
 C6 C 0.6591(2) -0.0171(8) 0.2137(3) 0.058(3) Uani 1 1 d . . .
 H6 H 0.6468 -0.0762 0.1997 0.069 Uiso 1 1 calc R . .
 C7 C 0.7193(2) 0.3215(10) 0.3363(3) 0.086(4) Uani 1 1 d . . .
 H7A H 0.7008 0.3544 0.3278 0.129 Uiso 1 1 calc R . .
 H7B H 0.7338 0.3763 0.3517 0.129 Uiso 1 1 calc R . .
 H7C H 0.7213 0.2580 0.3552 0.129 Uiso 1 1 calc R . .
 C8 C 0.7599(2) 0.2112(11) 0.3047(4) 0.089(4) Uani 1 1 d . . .
 H8A H 0.7614 0.1468 0.3230 0.133 Uiso 1 1 calc R . .
 H8B H 0.7740 0.2660 0.3212 0.133 Uiso 1 1 calc R . .
 H8C H 0.7629 0.1884 0.2793 0.133 Uiso 1 1 calc R . .
 C9 C 0.7222(2) 0.3980(10) 0.2515(4) 0.081(3) Uani 1 1 d . . .
 H9A H 0.7037 0.4329 0.2415 0.122 Uiso 1 1 calc R . .
 H9B H 0.7255 0.3740 0.2265 0.122 Uiso 1 1 calc R . .
 H9C H 0.7366 0.4512 0.2685 0.122 Uiso 1 1 calc R . .
 C10 C 0.59471(19) 0.0175(8) 0.1437(3) 0.056(3) Uani 1 1 d . . .
 C11 C 0.5957(2) 0.0424(10) 0.1038(4) 0.077(3) Uani 1 1 d . . .
 H11 H 0.6058 0.1055 0.1018 0.093 Uiso 1 1 calc R . .
 C12 C 0.5821(3) -0.0237(13) 0.0673(4) 0.096(4) Uani 1 1 d . . .
 H12 H 0.5831 -0.0057 0.0407 0.115 Uiso 1 1 calc R . .
 C13 C 0.5674(3) -0.1149(14) 0.0701(6) 0.113(6) Uani 1 1 d . . .
 H13 H 0.5582 -0.1595 0.0452 0.136 Uiso 1 1 calc R . .
 C14 C 0.5658(3) -0.1432(12) 0.1082(6) 0.109(5) Uani 1 1 d . . .
 H14 H 0.5555 -0.2065 0.1095 0.131 Uiso 1 1 calc R . .
 C15 C 0.5797(2) -0.0766(10) 0.1460(4) 0.080(3) Uani 1 1 d . . .
 H15 H 0.5788 -0.0959 0.1724 0.096 Uiso 1 1 calc R . .
 C16 C 0.5970(2) 0.0821(8) 0.2295(3) 0.058(3) Uani 1 1 d . . .
 C17 C 0.6140(3) 0.0352(11) 0.2697(4) 0.091(4) Uani 1 1 d . . .
 H17 H 0.6329 0.0171 0.2761 0.109 Uiso 1 1 calc R . .
 C18 C 0.6033(3) 0.0148(14) 0.3004(5) 0.133(7) Uani 1 1 d . . .
 H18 H 0.6152 -0.0167 0.3275 0.160 Uiso 1 1 calc R . .
 C19 C 0.5756(3) 0.0396(13) 0.2923(5) 0.109(5) Uani 1 1 d . . .
 H19 H 0.5683 0.0220 0.3127 0.131 Uiso 1 1 calc R . .
 C20 C 0.5590(3) 0.0915(13) 0.2530(5) 0.097(4) Uani 1 1 d . . .
 H20 H 0.5403 0.1113 0.2471 0.117 Uiso 1 1 calc R . .
 C21 C 0.5698(2) 0.1145(11) 0.2223(4) 0.082(4) Uani 1 1 d . . .
 H21 H 0.5585 0.1524 0.1964 0.098 Uiso 1 1 calc R . .
 C22 C 0.56139(18) 0.5003(7) 0.1008(3) 0.046(2) Uani 1 1 d . . .
 C23 C 0.55235(18) 0.5010(8) 0.1351(3) 0.050(2) Uani 1 1 d . . .
 C24 C 0.5256(2) 0.5515(9) 0.1277(4) 0.062(3) Uani 1 1 d . . .
 C25 C 0.5097(2) 0.5963(9) 0.0861(4) 0.072(3) Uani 1 1 d . . .
 H25 H 0.4922 0.6294 0.0810 0.086 Uiso 1 1 calc R . .
 C26 C 0.5180(2) 0.5949(9) 0.0524(4) 0.072(3) Uani 1 1 d . . .
 H26 H 0.5064 0.6253 0.0250 0.086 Uiso 1 1 calc R . .
 C27 C 0.5442(2) 0.5472(8) 0.0598(3) 0.060(3) Uani 1 1 d . . .
 H27 H 0.5504 0.5463 0.0372 0.072 Uiso 1 1 calc R . .
 C28 C 0.5033(4) 0.4134(17) 0.1866(6) 0.168(8) Uani 1 1 d . . .
 H28A H 0.5206 0.3706 0.1996 0.253 Uiso 1 1 calc R . .
 H28B H 0.4902 0.3758 0.1604 0.253 Uiso 1 1 calc R . .
 H28C H 0.4948 0.4203 0.2073 0.253 Uiso 1 1 calc R . .
 C29 C 0.5350(3) 0.6310(17) 0.2218(5) 0.172(9) Uani 1 1 d . . .
 H29A H 0.5532 0.5936 0.2346 0.258 Uiso 1 1 calc R . .
 H29B H 0.5265 0.6314 0.2426 0.258 Uiso 1 1 calc R . .
 H29C H 0.5376 0.7071 0.2144 0.258 Uiso 1 1 calc R . .
 C30 C 0.4769(3) 0.6366(19) 0.1483(6) 0.198(11) Uani 1 1 d . . .

H30A H 0.4803 0.7112 0.1405 0.297 Uiso 1 1 calc R . . .  
 H30B H 0.4692 0.6410 0.1700 0.297 Uiso 1 1 calc R . . .  
 H30C H 0.4635 0.5986 0.1225 0.297 Uiso 1 1 calc R . . .  
 C31 C 0.62015(18) 0.5590(8) 0.1205(3) 0.050(2) Uani 1 1 d . . .  
 C32 C 0.6465(2) 0.5524(11) 0.1553(4) 0.079(4) Uani 1 1 d . . .  
 H32 H 0.6516 0.4876 0.1726 0.095 Uiso 1 1 calc R . . .  
 C33 C 0.6654(3) 0.6419(14) 0.1649(5) 0.105(5) Uani 1 1 d . . .  
 H33 H 0.6832 0.6366 0.1887 0.126 Uiso 1 1 calc R . . .  
 C34 C 0.6584(3) 0.7352(12) 0.1406(6) 0.099(5) Uani 1 1 d . . .  
 H34 H 0.6710 0.7959 0.1483 0.118 Uiso 1 1 calc R . . .  
 C35 C 0.6331(3) 0.7426(11) 0.1046(6) 0.110(5) Uani 1 1 d . . .  
 H35 H 0.6286 0.8058 0.0864 0.132 Uiso 1 1 calc R . . .  
 C36 C 0.6138(2) 0.6536(9) 0.0953(4) 0.084(4) Uani 1 1 d . . .  
 H36 H 0.5962 0.6591 0.0712 0.100 Uiso 1 1 calc R . . .  
 C37 C 0.5917(2) 0.3838(8) 0.0569(3) 0.049(2) Uani 1 1 d . . .  
 C38 C 0.5690(3) 0.3140(9) 0.0335(4) 0.079(3) Uani 1 1 d . . .  
 H38 H 0.5552 0.3003 0.0440 0.095 Uiso 1 1 calc R . . .  
 C39 C 0.5666(3) 0.2645(11) -0.0050(4) 0.097(4) Uani 1 1 d . . .  
 H39 H 0.5506 0.2204 -0.0211 0.116 Uiso 1 1 calc R . . .  
 C40 C 0.5866(4) 0.2789(11) -0.0197(4) 0.092(4) Uani 1 1 d . . .  
 H40 H 0.5850 0.2434 -0.0456 0.111 Uiso 1 1 calc R . . .  
 C41 C 0.6093(3) 0.3443(10) 0.0026(4) 0.081(4) Uani 1 1 d . . .  
 H41 H 0.6233 0.3534 -0.0080 0.097 Uiso 1 1 calc R . . .  
 C42 C 0.6123(2) 0.3987(8) 0.0410(3) 0.060(3) Uani 1 1 d . . .  
 H42 H 0.6280 0.4448 0.0560 0.072 Uiso 1 1 calc R . . .  
 Hg2 Hg 0.630624(9) 0.98162(4) -0.035109(16) 0.06836(15) Uani 1 1 d . . .  
 .  
 S3 S 0.65447(6) 1.0827(3) 0.03652(9) 0.0700(8) Uani 1 1 d . . .  
 S4 S 0.57648(5) 0.9689(2) -0.06940(11) 0.0746(9) Uani 1 1 d . . .  
 P3 P 0.65769(5) 1.1158(2) -0.06093(8) 0.0497(6) Uani 1 1 d . . .  
 P4 P 0.62637(5) 0.7761(2) -0.04578(9) 0.0527(7) Uani 1 1 d . . .  
 Si3 Si 0.70562(7) 1.1721(3) 0.12643(10) 0.0737(9) Uani 1 1 d . . .  
 Si4 Si 0.51111(6) 0.8959(3) -0.08639(12) 0.0745(9) Uani 1 1 d . . .  
 C43 C 0.6841(2) 1.1763(8) -0.0102(3) 0.049(2) Uani 1 1 d . . .  
 C44 C 0.68219(18) 1.1574(7) 0.0306(3) 0.047(2) Uani 1 1 d . . .  
 C45 C 0.7043(2) 1.1988(8) 0.0701(3) 0.054(2) Uani 1 1 d . . .  
 C46 C 0.7257(2) 1.2638(9) 0.0659(3) 0.062(3) Uani 1 1 d . . .  
 H46 H 0.7399 1.2949 0.0913 0.075 Uiso 1 1 calc R . . .  
 C47 C 0.7268(2) 1.2836(8) 0.0260(4) 0.062(3) Uani 1 1 d . . .  
 H47 H 0.7412 1.3277 0.0243 0.074 Uiso 1 1 calc R . . .  
 C48 C 0.7062(2) 1.2372(8) -0.0111(3) 0.056(3) Uani 1 1 d . . .  
 H48 H 0.7074 1.2477 -0.0380 0.067 Uiso 1 1 calc R . . .  
 C49 C 0.7406(3) 1.2295(16) 0.1680(4) 0.135(6) Uani 1 1 d . . .  
 H49A H 0.7420 1.2173 0.1973 0.202 Uiso 1 1 calc R . . .  
 H49B H 0.7417 1.3088 0.1631 0.202 Uiso 1 1 calc R . . .  
 H49C H 0.7561 1.1917 0.1647 0.202 Uiso 1 1 calc R . . .  
 C50 C 0.7063(4) 1.0172(12) 0.1373(5) 0.128(6) Uani 1 1 d . . .  
 H50A H 0.7067 1.0049 0.1661 0.191 Uiso 1 1 calc R . . .  
 H50B H 0.7230 0.9844 0.1360 0.191 Uiso 1 1 calc R . . .  
 H50C H 0.6895 0.9827 0.1155 0.191 Uiso 1 1 calc R . . .  
 C51 C 0.6757(3) 1.2454(12) 0.1327(4) 0.097(4) Uani 1 1 d . . .  
 H51A H 0.6765 1.2305 0.1616 0.145 Uiso 1 1 calc R . . .  
 H51B H 0.6579 1.2186 0.1107 0.145 Uiso 1 1 calc R . . .  
 H51C H 0.6772 1.3250 0.1292 0.145 Uiso 1 1 calc R . . .  
 C52 C 0.6790(2) 1.0708(8) -0.0896(3) 0.052(2) Uani 1 1 d . . .  
 C53 C 0.6759(2) 1.1113(10) -0.1300(3) 0.074(3) Uani 1 1 d . . .  
 H53 H 0.6621 1.1654 -0.1441 0.089 Uiso 1 1 calc R . . .  
 C54 C 0.6927(3) 1.0741(13) -0.1497(4) 0.099(4) Uani 1 1 d . . .  
 H54 H 0.6904 1.1038 -0.1769 0.119 Uiso 1 1 calc R . . .  
 C55 C 0.7127(3) 0.9945(12) -0.1302(5) 0.090(4) Uani 1 1 d . . .  
 H55 H 0.7237 0.9674 -0.1443 0.108 Uiso 1 1 calc R . . .

C56 C 0.7168(3) 0.9540(11) -0.0899(5) 0.094(4) Uani 1 1 d . . .
 H56 H 0.7312 0.9018 -0.0758 0.113 Uiso 1 1 calc R . .
 C57 C 0.6996(3) 0.9899(10) -0.0700(4) 0.081(4) Uani 1 1 d . . .
 H57 H 0.7019 0.9592 -0.0431 0.098 Uiso 1 1 calc R . .
 C58 C 0.6347(2) 1.2269(8) -0.0946(3) 0.053(2) Uani 1 1 d . . .
 C59 C 0.6069(2) 1.1969(9) -0.1212(3) 0.065(3) Uani 1 1 d . . .
 H59 H 0.6004 1.1245 -0.1200 0.077 Uiso 1 1 calc R . .
 C60 C 0.5891(3) 1.2755(13) -0.1497(5) 0.101(4) Uani 1 1 d . . .
 H60 H 0.5704 1.2551 -0.1677 0.121 Uiso 1 1 calc R . .
 C61 C 0.5979(3) 1.3812(13) -0.1522(5) 0.108(5) Uani 1 1 d . . .
 H61 H 0.5856 1.4326 -0.1723 0.130 Uiso 1 1 calc R . .
 C62 C 0.6253(3) 1.4115(11) -0.1245(5) 0.105(5) Uani 1 1 d . . .
 H62 H 0.6315 1.4851 -0.1248 0.126 Uiso 1 1 calc R . .
 C63 C 0.6440(3) 1.3332(9) -0.0960(4) 0.076(3) Uani 1 1 d . . .
 H63 H 0.6627 1.3533 -0.0780 0.091 Uiso 1 1 calc R . .
 C64 C 0.59219(19) 0.7458(8) -0.0454(3) 0.047(2) Uani 1 1 d . . .
 C65 C 0.57067(19) 0.8283(8) -0.0584(3) 0.050(2) Uani 1 1 d . . .
 C66 C 0.54281(19) 0.7972(8) -0.0639(3) 0.051(2) Uani 1 1 d . . .
 C67 C 0.5381(2) 0.6857(9) -0.0550(3) 0.068(3) Uani 1 1 d . . .
 H67 H 0.5198 0.6647 -0.0585 0.082 Uiso 1 1 calc R . .
 C68 C 0.5597(2) 0.6049(9) -0.0411(3) 0.065(3) Uani 1 1 d . . .
 H68 H 0.5561 0.5315 -0.0350 0.078 Uiso 1 1 calc R . .
 C69 C 0.5865(2) 0.6360(8) -0.0365(3) 0.056(3) Uani 1 1 d . . .
 H69 H 0.6011 0.5829 -0.0273 0.067 Uiso 1 1 calc R . .
 C70 C 0.5053(3) 0.9429(13) -0.1426(4) 0.123(6) Uani 1 1 d . . .
 H70A H 0.5032 0.8783 -0.1610 0.185 Uiso 1 1 calc R . .
 H70B H 0.5215 0.9865 -0.1409 0.185 Uiso 1 1 calc R . .
 H70C H 0.4884 0.9882 -0.1548 0.185 Uiso 1 1 calc R . .
 C71 C 0.5150(3) 1.0178(12) -0.0499(5) 0.125(6) Uani 1 1 d . . .
 H71A H 0.4985 1.0651 -0.0627 0.187 Uiso 1 1 calc R . .
 H71B H 0.5317 1.0600 -0.0466 0.187 Uiso 1 1 calc R . .
 H71C H 0.5170 0.9917 -0.0215 0.187 Uiso 1 1 calc R . .
 C72 C 0.4792(2) 0.8159(11) -0.0898(5) 0.107(5) Uani 1 1 d . . .
 H72A H 0.4762 0.7523 -0.1090 0.160 Uiso 1 1 calc R . .
 H72B H 0.4627 0.8640 -0.1012 0.160 Uiso 1 1 calc R . .
 H72C H 0.4822 0.7901 -0.0608 0.160 Uiso 1 1 calc R . .
 C73 C 0.6220(2) 0.7360(8) -0.1008(3) 0.055(3) Uani 1 1 d . . .
 C74 C 0.5961(3) 0.7039(10) -0.1334(4) 0.075(3) Uani 1 1 d . . .
 H74 H 0.5801 0.6994 -0.1270 0.090 Uiso 1 1 calc R . .
 C75 C 0.5934(3) 0.6780(11) -0.1758(4) 0.093(4) Uani 1 1 d . . .
 H75 H 0.5759 0.6557 -0.1975 0.112 Uiso 1 1 calc R . .
 C76 C 0.6166(4) 0.6857(13) -0.1850(5) 0.107(5) Uani 1 1 d . . .
 H76 H 0.6146 0.6692 -0.2134 0.128 Uiso 1 1 calc R . .
 C77 C 0.6422(4) 0.7161(13) -0.1546(5) 0.104(5) Uani 1 1 d . . .
 H77 H 0.6578 0.7200 -0.1617 0.124 Uiso 1 1 calc R . .
 C78 C 0.6453(3) 0.7424(11) -0.1114(4) 0.087(4) Uani 1 1 d . . .
 H78 H 0.6630 0.7641 -0.0901 0.104 Uiso 1 1 calc R . .
 C79 C 0.65294(19) 0.6856(9) -0.0063(3) 0.055(2) Uani 1 1 d . . .
 C80 C 0.6573(2) 0.5744(10) -0.0142(4) 0.082(3) Uani 1 1 d . . .
 H80 H 0.6463 0.5436 -0.0418 0.098 Uiso 1 1 calc R . .
 C81 C 0.6772(3) 0.5081(12) 0.0173(5) 0.103(5) Uani 1 1 d . . .
 H81 H 0.6792 0.4329 0.0113 0.124 Uiso 1 1 calc R . .
 C82 C 0.6938(3) 0.5512(14) 0.0566(5) 0.107(5) Uani 1 1 d . . .
 H82 H 0.7077 0.5072 0.0779 0.128 Uiso 1 1 calc R . .
 C83 C 0.6901(4) 0.6579(16) 0.0650(5) 0.137(7) Uani 1 1 d . . .
 H83 H 0.7014 0.6875 0.0928 0.165 Uiso 1 1 calc R . .
 C84 C 0.6701(3) 0.7263(12) 0.0339(4) 0.101(4) Uani 1 1 d . . .
 H84 H 0.6685 0.8012 0.0407 0.121 Uiso 1 1 calc R . .
 C11S Cl 0.62243(18) 1.2618(7) -0.2445(3) 0.262(4) Uani 1 1 d . . .
 C12S Cl 0.6723(2) 1.3774(7) -0.2060(3) 0.304(5) Uani 1 1 d . . .
 C1S C 0.6384(5) 1.3892(15) -0.2355(8) 0.196(10) Uani 1 1 d . . .

H1S1 H 0.6351 1.4240 -0.2636 0.235 Uiso 1 1 calc R . .
 H1S2 H 0.6301 1.4373 -0.2204 0.235 Uiso 1 1 calc R . .
 C13A Cl 0.7166(6) 0.449(3) 0.4484(13) 0.262(18) Uani 0.30 1 d PD A 1
 C14A Cl 0.7662(5) 0.3622(16) 0.4579(5) 0.178(9) Uani 0.30 1 d PD A 1
 C2SA C 0.7483(5) 0.4863(18) 0.4484(9) 0.141(17) Uani 0.30 1 d PD A 1
 H2S1 H 0.7583 0.5404 0.4716 0.169 Uiso 0.30 1 calc PR A 1
 H2S2 H 0.7458 0.5180 0.4202 0.169 Uiso 0.30 1 calc PR A 1
 C13B Cl 0.7367(9) 0.367(3) 0.4646(10) 0.24(2) Uani 0.20 1 d PD B 2
 C14B Cl 0.7175(7) 0.543(2) 0.4126(8) 0.177(13) Uani 0.20 1 d PD B 2
 C2SB C 0.7483(5) 0.4863(18) 0.4484(9) 0.141(17) Uani 0.20 1 d PD B 2
 H2S3 H 0.7582 0.5361 0.4732 0.169 Uiso 0.20 1 calc PR B 2
 H2S4 H 0.7609 0.4684 0.4342 0.169 Uiso 0.20 1 calc PR B 2

loop\_
   
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 \_atom\_site\_aniso\_U\_12

Hg1 0.0471(2) 0.0589(3) 0.0530(2) 0.0040(2) 0.01514(18) 0.00414(19)
 S1 0.0445(14) 0.0563(15) 0.0510(14) -0.0092(13) 0.0078(11) 0.0025(12)
 S2 0.0715(19) 0.110(2) 0.0504(16) 0.0019(16) 0.0283(14) 0.0294(17)
 P1 0.0390(14) 0.0505(15) 0.0502(15) -0.0050(12) 0.0131(12) -0.0061(12)
 P2 0.0404(14) 0.0494(14) 0.0458(14) 0.0004(12) 0.0165(11) -0.0003(11)
 Si1 0.0422(16) 0.076(2) 0.0524(17) -0.0071(15) 0.0094(13) -0.0080(14)
 Si2 0.068(2) 0.188(5) 0.083(3) -0.024(3) 0.039(2) 0.028(3)
 C1 0.044(5) 0.057(6) 0.035(5) 0.003(4) 0.019(4) -0.005(5)
 C2 0.043(5) 0.058(6) 0.034(5) -0.001(5) 0.017(4) 0.002(5)
 C3 0.045(6) 0.058(6) 0.036(5) 0.001(4) 0.013(4) 0.003(5)
 C4 0.043(6) 0.073(7) 0.044(6) -0.003(5) 0.011(5) 0.003(5)
 C5 0.047(6) 0.070(7) 0.061(7) -0.005(6) 0.021(5) 0.017(5)
 C6 0.055(7) 0.051(6) 0.061(6) -0.010(5) 0.018(5) -0.009(5)
 C7 0.070(8) 0.109(10) 0.062(7) -0.017(7) 0.012(6) -0.014(7)
 C8 0.034(6) 0.118(10) 0.090(9) -0.014(8) 0.002(6) -0.008(6)
 C9 0.065(7) 0.086(9) 0.086(8) 0.008(7) 0.024(6) -0.018(6)
 C10 0.036(5) 0.056(6) 0.058(7) -0.016(5) 0.002(5) -0.001(5)
 C11 0.070(8) 0.078(8) 0.059(8) -0.014(7) 0.002(6) 0.012(6)
 C12 0.092(10) 0.102(11) 0.060(8) -0.016(8) -0.001(7) 0.022(9)
 C13 0.069(10) 0.091(12) 0.124(14) -0.048(11) -0.016(10) 0.022(9)
 C14 0.068(9) 0.070(9) 0.154(15) -0.043(11) 0.013(11) -0.014(7)
 C15 0.075(8) 0.073(8) 0.093(9) -0.023(7) 0.034(7) -0.017(7)
 C16 0.048(6) 0.063(7) 0.059(7) -0.007(5) 0.020(5) -0.009(5)
 C17 0.088(9) 0.108(10) 0.095(9) 0.050(8) 0.058(8) 0.033(8)
 C18 0.119(13) 0.171(16) 0.136(14) 0.089(12) 0.078(11) 0.066(12)
 C19 0.100(11) 0.125(12) 0.125(13) 0.036(10) 0.068(10) 0.017(10)
 C20 0.056(8) 0.135(12) 0.107(11) 0.003(10) 0.040(8) 0.002(8)
 C21 0.044(7) 0.137(11) 0.059(7) 0.017(7) 0.016(6) -0.003(7)
 C22 0.039(5) 0.045(6) 0.049(6) 0.000(4) 0.012(5) 0.002(4)
 C23 0.039(5) 0.059(6) 0.048(6) -0.011(5) 0.014(4) 0.002(4)
 C24 0.049(6) 0.070(7) 0.074(8) -0.011(6) 0.032(6) 0.004(5)
 C25 0.040(6) 0.081(8) 0.079(8) -0.010(7) 0.009(6) 0.010(6)
 C26 0.061(7) 0.083(8) 0.059(7) 0.010(6) 0.013(6) 0.008(6)
 C27 0.053(6) 0.066(7) 0.056(7) -0.007(5) 0.019(5) -0.002(5)
 C28 0.159(17) 0.24(2) 0.157(17) 0.005(16) 0.117(14) -0.028(16)
 C29 0.140(15) 0.26(2) 0.129(14) -0.095(15) 0.063(12) 0.024(15)
 C30 0.109(13) 0.34(3) 0.155(16) -0.021(18) 0.068(12) 0.105(16)
 C31 0.035(5) 0.057(6) 0.060(6) -0.011(5) 0.021(5) -0.004(4)
 C32 0.056(7) 0.109(10) 0.061(7) 0.018(7) 0.013(6) -0.026(7)
 C33 0.055(8) 0.146(14) 0.097(10) -0.011(10) 0.014(7) -0.045(9)

C34	0.093(11)	0.066(9)	0.151(14)	-0.026(9)	0.065(11)	-0.032(8)
C35	0.066(9)	0.059(8)	0.194(16)	0.016(9)	0.043(10)	0.004(7)
C36	0.052(7)	0.048(7)	0.133(11)	0.010(7)	0.021(7)	-0.008(5)
C37	0.053(6)	0.047(6)	0.045(6)	0.008(5)	0.018(5)	0.009(5)
C38	0.088(9)	0.070(8)	0.081(8)	-0.015(7)	0.038(7)	-0.023(7)
C39	0.119(12)	0.074(9)	0.071(9)	-0.027(7)	0.015(8)	-0.020(8)
C40	0.141(14)	0.068(9)	0.073(9)	-0.012(7)	0.049(10)	0.012(9)
C41	0.109(10)	0.074(8)	0.087(9)	0.007(7)	0.067(8)	0.015(8)
C42	0.075(7)	0.051(6)	0.062(7)	-0.009(5)	0.035(6)	0.005(5)
Hg2	0.0584(3)	0.0616(3)	0.0871(3)	-0.0072(2)	0.0324(2)	-0.0139(2)
S3	0.0713(19)	0.088(2)	0.0637(18)	-0.0085(15)	0.0407(15)	-0.0223(16)
S4	0.0441(15)	0.0521(16)	0.119(3)	0.0134(16)	0.0248(16)	-0.0009(13)
P3	0.0484(15)	0.0533(15)	0.0494(15)	-0.0023(12)	0.0223(12)	-0.0050(12)
P4	0.0461(15)	0.0495(15)	0.0641(17)	0.0019(13)	0.0244(13)	0.0013(12)
Si3	0.074(2)	0.098(3)	0.0491(17)	0.0069(17)	0.0262(16)	0.0135(19)
Si4	0.0399(16)	0.073(2)	0.097(2)	0.0031(19)	0.0151(16)	-0.0033(15)
C43	0.059(6)	0.047(5)	0.046(6)	0.002(5)	0.026(5)	0.002(5)
C44	0.041(5)	0.044(5)	0.056(6)	0.005(5)	0.021(5)	0.001(4)
C45	0.045(6)	0.065(7)	0.051(6)	-0.003(5)	0.017(5)	0.002(5)
C46	0.053(6)	0.079(7)	0.050(6)	-0.008(6)	0.015(5)	0.003(6)
C47	0.048(6)	0.062(7)	0.079(8)	-0.005(6)	0.031(6)	-0.014(5)
C48	0.049(6)	0.057(6)	0.060(6)	-0.004(5)	0.021(5)	-0.012(5)
C49	0.092(10)	0.24(2)	0.057(8)	-0.020(10)	0.014(7)	-0.011(12)
C50	0.173(15)	0.116(12)	0.116(12)	0.063(10)	0.081(11)	0.050(11)
C51	0.105(10)	0.132(12)	0.061(8)	0.010(8)	0.042(7)	0.036(9)
C52	0.056(6)	0.054(6)	0.044(6)	-0.004(5)	0.018(5)	0.000(5)
C53	0.074(8)	0.093(9)	0.055(7)	0.013(6)	0.026(6)	0.015(7)
C54	0.110(11)	0.138(13)	0.079(9)	-0.002(9)	0.068(9)	0.012(10)
C55	0.088(9)	0.115(11)	0.083(10)	-0.025(8)	0.052(8)	0.010(8)
C56	0.103(10)	0.095(10)	0.096(10)	0.004(8)	0.053(9)	0.043(8)
C57	0.104(9)	0.074(8)	0.082(8)	0.011(7)	0.054(8)	0.028(7)
C58	0.051(6)	0.057(6)	0.050(6)	0.001(5)	0.018(5)	0.006(5)
C59	0.041(6)	0.071(7)	0.072(7)	-0.005(6)	0.014(5)	0.012(6)
C60	0.065(8)	0.102(11)	0.119(12)	-0.007(10)	0.021(8)	0.017(8)
C61	0.096(11)	0.093(11)	0.092(10)	0.001(9)	-0.003(9)	0.030(9)
C62	0.114(12)	0.073(9)	0.099(10)	-0.001(8)	0.015(9)	0.008(8)
C63	0.084(8)	0.055(7)	0.072(8)	0.007(6)	0.015(6)	0.001(6)
C64	0.046(6)	0.051(6)	0.048(6)	0.001(5)	0.021(5)	0.000(5)
C65	0.047(6)	0.048(6)	0.052(6)	0.001(5)	0.018(5)	0.002(5)
C66	0.042(5)	0.060(6)	0.046(6)	0.005(5)	0.015(4)	-0.007(5)
C67	0.060(7)	0.076(8)	0.071(7)	-0.001(6)	0.029(6)	-0.020(6)
C68	0.067(7)	0.056(7)	0.071(7)	0.013(6)	0.027(6)	-0.007(6)
C69	0.050(6)	0.056(6)	0.063(7)	0.009(5)	0.025(5)	0.005(5)
C70	0.072(9)	0.141(13)	0.112(11)	0.054(10)	-0.005(8)	-0.008(9)
C71	0.059(8)	0.119(12)	0.179(15)	-0.056(11)	0.031(9)	-0.001(8)
C72	0.039(6)	0.122(11)	0.150(13)	0.027(10)	0.030(7)	-0.004(7)
C73	0.064(7)	0.049(6)	0.065(7)	0.021(5)	0.040(6)	0.007(5)
C74	0.073(8)	0.089(9)	0.058(7)	0.006(6)	0.022(6)	0.007(7)
C75	0.121(12)	0.102(10)	0.058(8)	0.011(7)	0.039(8)	0.009(9)
C76	0.154(15)	0.110(12)	0.076(10)	0.018(9)	0.067(11)	0.016(12)
C77	0.126(13)	0.125(13)	0.100(11)	0.002(10)	0.085(11)	-0.003(10)
C78	0.090(9)	0.095(9)	0.090(9)	-0.003(8)	0.052(8)	-0.005(7)
C79	0.036(5)	0.066(7)	0.061(7)	0.000(6)	0.019(5)	0.004(5)
C80	0.077(8)	0.077(8)	0.077(8)	-0.011(7)	0.018(7)	0.013(7)
C81	0.090(10)	0.091(10)	0.112(12)	0.010(9)	0.026(9)	0.047(8)
C82	0.093(11)	0.125(13)	0.081(10)	0.006(10)	0.014(9)	0.044(10)
C83	0.146(15)	0.148(16)	0.070(10)	-0.013(10)	-0.002(9)	0.057(13)
C84	0.105(11)	0.099(10)	0.077(9)	-0.012(8)	0.016(8)	0.027(9)
C11S	0.248(8)	0.179(7)	0.317(10)	-0.022(7)	0.077(7)	0.017(6)
C12S	0.237(9)	0.223(8)	0.386(13)	0.141(9)	0.064(9)	-0.023(7)
C1S	0.23(3)	0.085(13)	0.26(3)	0.058(15)	0.09(2)	0.058(15)

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C13A 0.20(2) 0.26(3) 0.43(5) -0.19(3) 0.23(3) -0.07(2)
C14A 0.198(19) 0.168(16) 0.093(10) -0.061(10) -0.015(11) 0.044(14)
C2SA 0.19(4) 0.14(3) 0.10(2) -0.07(2) 0.06(2) -0.14(3)
C13B 0.20(4) 0.35(6) 0.16(3) -0.14(3) 0.06(3) -0.01(4)
C14B 0.27(4) 0.12(2) 0.23(3) -0.08(2) 0.18(3) -0.02(2)
C2SB 0.19(4) 0.14(3) 0.10(2) -0.07(2) 0.06(2) -0.14(3)

_geom_special_details
;
All esds (except the esd in the dihedral angle between two l.s.
planes)
are estimated using the full covariance matrix. The cell esds are
taken
into account individually in the estimation of esds in distances,
angles
and torsion angles; correlations between esds in cell parameters are
only
used when they are defined by crystal symmetry. An approximate
(isotropic)
treatment of cell esds is used for estimating esds involving l.s.
planes.
;

loop_
_geom_bond_atom_site_label_1
_geom_bond_atom_site_label_2
_geom_bond_distance
_geom_bond_site_symmetry_2
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Hg1 P1 2.455(3) . ?
Hg1 P2 2.467(2) . ?
Hg1 S2 2.512(3) . ?
Hg1 S1 2.553(2) . ?
S1 C2 1.761(9) . ?
S2 C23 1.759(9) . ?
P1 C10 1.801(9) . ?
P1 C1 1.801(9) . ?
P1 C16 1.802(10) . ?
P2 C22 1.801(9) . ?
P2 C37 1.805(9) . ?
P2 C31 1.805(9) . ?
Si1 C7 1.852(11) . ?
Si1 C9 1.854(11) . ?
Si1 C8 1.864(10) . ?
Si1 C3 1.891(9) . ?
Si2 C29 1.833(15) . ?
Si2 C28 1.862(19) . ?
Si2 C30 1.874(15) . ?
Si2 C24 1.888(10) . ?
C1 C6 1.386(12) . ?
C1 C2 1.416(12) . ?
C2 C3 1.414(12) . ?
C3 C4 1.380(12) . ?
C4 C5 1.366(13) . ?
C5 C6 1.375(12) . ?
C10 C15 1.379(14) . ?
C10 C11 1.382(15) . ?
C11 C12 1.371(16) . ?
C12 C13 1.35(2) . ?
C13 C14 1.35(2) . ?
C14 C15 1.402(17) . ?

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C16 C21 1.373(13) . ?  
C16 C17 1.375(14) . ?  
C17 C18 1.368(16) . ?  
C18 C19 1.366(17) . ?  
C19 C20 1.375(17) . ?  
C20 C21 1.379(15) . ?  
C22 C27 1.396(12) . ?  
C22 C23 1.403(12) . ?  
C23 C24 1.426(12) . ?  
C24 C25 1.388(14) . ?  
C25 C26 1.361(14) . ?  
C26 C27 1.384(13) . ?  
C31 C36 1.358(14) . ?  
C31 C32 1.369(13) . ?  
C32 C33 1.386(16) . ?  
C33 C34 1.331(18) . ?  
C34 C35 1.359(18) . ?  
C35 C36 1.391(15) . ?  
C37 C38 1.377(13) . ?  
C37 C42 1.377(13) . ?  
C38 C39 1.367(16) . ?  
C39 C40 1.324(18) . ?  
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Refinement of F^2 against ALL reflections. The weighted R-factor wR
and
goodness of fit S are based on F^2, conventional R-factors R are
based
on F, with F set to zero for negative F^2. The threshold expression
of

```

$F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc.  
and is  
not relevant to the choice of reflections for refinement. R-factors  
based  
on  $F^2$  are statistically about twice as large as those based on F,  
and R-  
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loop\_

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P1 P 0.7132(9) 0.6440(13) 0.4575(4) 0.018(3) Uani 1 1 d U . .
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 H19A H 1.0181 0.9774 0.4319 0.042 Uiso 1 1 calc R . .
 H19B H 1.1279 0.9442 0.4557 0.042 Uiso 1 1 calc R . .
 C20 C 1.098(7) 0.809(11) 0.411(2) 0.12(3) Uiso 1 1 d . . .
 H20A H 1.1315 0.8767 0.3938 0.182 Uiso 1 1 calc R . .
 H20B H 1.0367 0.7616 0.3968 0.182 Uiso 1 1 calc R . .
 H20C H 1.1470 0.7296 0.4204 0.182 Uiso 1 1 calc R . .
 Hg2 Hg 0.51031(17) 0.5313(2) 0.30338(7) 0.0407(7) Uani 1 1 d . . .
 S2 S 0.4355(11) 0.7128(15) 0.2563(4) 0.043(4) Uani 1 1 d . . .
 P2 P 0.2229(10) 0.5307(14) 0.2828(4) 0.029(3) Uani 1 1 d . . .
 O2 O 0.311(3) 0.441(4) 0.3057(9) 0.038(9) Uiso 1 1 d . . .
 C21 C 0.240(3) 0.741(5) 0.2885(12) 0.019(11) Uiso 1 1 d . . .
 C22 C 0.332(4) 0.805(6) 0.2788(15) 0.041(14) Uiso 1 1 d . . .
 C23 C 0.351(5) 0.971(8) 0.2870(17) 0.064(18) Uiso 1 1 d . . .
 H23 H 0.4135 1.0197 0.2821 0.077 Uiso 1 1 calc R . .
 C24 C 0.266(5) 1.056(8) 0.3033(17) 0.057(17) Uiso 1 1 d . . .
 H24 H 0.2755 1.1616 0.3083 0.069 Uiso 1 1 calc R . .
 C25 C 0.177(5) 0.989(7) 0.3112(17) 0.060(18) Uiso 1 1 d . . .
 H25 H 0.1234 1.0475 0.3206 0.071 Uiso 1 1 calc R . .
 C26 C 0.163(4) 0.822(6) 0.3049(15) 0.039(14) Uiso 1 1 d . . .
 H26 H 0.1033 0.7709 0.3120 0.046 Uiso 1 1 calc R . .
 C27 C 0.095(4) 0.494(6) 0.3016(14) 0.033(13) Uiso 1 1 d . . .
 C28 C 0.102(4) 0.452(6) 0.3398(14) 0.034(13) Uiso 1 1 d . . .
 H28 H 0.1683 0.4342 0.3535 0.040 Uiso 1 1 calc R . .
 C29 C 0.006(5) 0.438(7) 0.3583(19) 0.059(17) Uiso 1 1 d . . .
 H29 H 0.0081 0.4179 0.3846 0.070 Uiso 1 1 calc R . .
 C30 C -0.085(5) 0.454(8) 0.3359(18) 0.066(19) Uiso 1 1 d . . .
 H30 H -0.1476 0.4435 0.3473 0.079 Uiso 1 1 calc R . .
 C31 C -0.092(5) 0.486(7) 0.2949(17) 0.056(17) Uiso 1 1 d . . .
 H31 H -0.1582 0.4925 0.2804 0.067 Uiso 1 1 calc R . .
 C32 C -0.001(4) 0.506(6) 0.2777(16) 0.045(15) Uiso 1 1 d . . .
 H32 H -0.0022 0.5271 0.2514 0.054 Uiso 1 1 calc R . .
 C33 C 0.212(4) 0.486(5) 0.2330(13) 0.028(12) Uiso 1 1 d . . .
 C34 C 0.148(5) 0.573(8) 0.2074(19) 0.067(19) Uiso 1 1 d . . .
 H34 H 0.1121 0.6573 0.2165 0.081 Uiso 1 1 calc R . .
 C35 C 0.135(5) 0.538(8) 0.1665(19) 0.067(19) Uiso 1 1 d . . .
 H35 H 0.0945 0.6010 0.1490 0.081 Uiso 1 1 calc R . .
 C36 C 0.189(4) 0.400(6) 0.1539(16) 0.042(15) Uiso 1 1 d . . .
 H36 H 0.1814 0.3702 0.1280 0.050 Uiso 1 1 calc R . .

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C37 C 0.251(4) 0.314(6) 0.1809(15) 0.040(14) Uiso 1 1 d . .
H37 H 0.2888 0.2294 0.1729 0.048 Uiso 1 1 calc R . .
C38 C 0.259(4) 0.351(6) 0.2191(16) 0.045(15) Uiso 1 1 d . .
H38 H 0.2964 0.2851 0.2368 0.054 Uiso 1 1 calc R . .
C39 C 0.596(4) 0.401(6) 0.3408(15) 0.036(14) Uiso 1 1 d . .
H39A H 0.6619 0.3765 0.3300 0.043 Uiso 1 1 calc R . .
H39B H 0.6149 0.4626 0.3639 0.043 Uiso 1 1 calc R . .
C40 C 0.549(5) 0.248(8) 0.3534(19) 0.08(2) Uiso 1 1 d . .
H40A H 0.5990 0.1966 0.3716 0.113 Uiso 1 1 calc R . .
H40B H 0.5318 0.1831 0.3312 0.113 Uiso 1 1 calc R . .
H40C H 0.4849 0.2695 0.3653 0.113 Uiso 1 1 calc R . .

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S1 0.016(7) 0.036(8) 0.060(10) 0.010(7) 0.024(7) -0.001(6)
P1 0.013(6) 0.010(6) 0.032(7) 0.002(5) 0.012(5) -0.006(5)
Hg2 0.0346(13) 0.0265(12) 0.0623(16) -0.0009(12) 0.0111(11) -
0.0009(10)
S2 0.036(8) 0.027(8) 0.071(11) 0.015(7) 0.031(8) 0.000(6)
P2 0.032(8) 0.006(6) 0.050(9) -0.002(7) 0.010(7) 0.005(6)

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All esds (except the esd in the dihedral angle between two l.s.
planes)
are estimated using the full covariance matrix. The cell esds are
taken
into account individually in the estimation of esds in distances,
angles
and torsion angles; correlations between esds in cell parameters are
only
used when they are defined by crystal symmetry. An approximate
(isotropic)
treatment of cell esds is used for estimating esds involving l.s.
planes.
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P1 O1 1.50(3) . ?
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C2 C3 1.41(6) . ?

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C2 C3 C4 114(5) . . ?  
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C21 C22 C23 118(5) . . ?  
C21 C22 S2 128(4) . . ?  
C23 C22 S2 114(4) . . ?  
C24 C23 C22 117(6) . . ?  
C25 C24 C23 122(6) . . ?  
C24 C25 C26 119(6) . . ?  
C21 C26 C25 119(5) . . ?  
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and
goodness of fit S are based on F^2, conventional R-factors R are
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on F, with F set to zero for negative F^2. The threshold expression
of

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$F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc.  
and is  
not relevant to the choice of reflections for refinement. R-factors  
based  
on  $F^2$  are statistically about twice as large as those based on F,  
and R-  
factors based on ALL data will be even larger.  
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S1 S 0.37951(11) 0.92296(10) 0.87784(8) 0.0527(2) Uani 1 1 d . .
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P1 P 0.39688(10) 1.13069(9) 0.71847(9) 0.0449(2) Uani 1 1 d . .
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Si1 Si 0.19368(12) 0.66914(11) 0.77512(10) 0.0538(3) Uani 1 1 d . .
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O1 O 0.5432(3) 1.1179(3) 0.7639(3) 0.0585(7) Uani 1 1 d . .
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C1 C 0.2864(4) 0.9021(3) 0.7331(3) 0.0415(8) Uani 1 1 d . .
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C2 C 0.2941(4) 0.9900(3) 0.6635(3) 0.0441(8) Uani 1 1 d . .
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C3 C 0.2164(5) 0.9697(4) 0.5519(4) 0.0561(10) Uani 1 1 d . .
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H3 H 0.2220 1.0266 0.5049 0.067 Uiso 1 1 calc R . .
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C4 C 0.1318(5) 0.8674(4) 0.5100(4) 0.0673(13) Uani 1 1 d . .
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H4 H 0.0796 0.8559 0.4355 0.081 Uiso 1 1 calc R . .
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C5 C 0.1241(5) 0.7824(4) 0.5776(4) 0.0576(11) Uani 1 1 d . .
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H5 H 0.0665 0.7132 0.5476 0.069 Uiso 1 1 calc R . .
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C6 C 0.2008(4) 0.7957(3) 0.6916(3) 0.0458(8) Uani 1 1 d . . .
 C7 C 0.1478(6) 0.7180(5) 0.9189(5) 0.0900(17) Uani 1 1 d . . .
 H7A H 0.1457 0.6495 0.9568 0.135 Uiso 1 1 calc R . .
 H7B H 0.0598 0.7508 0.9085 0.135 Uiso 1 1 calc R . .
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 C8 C 0.0584(6) 0.5526(5) 0.6892(5) 0.0829(16) Uani 1 1 d . . .
 H8A H 0.0785 0.5251 0.6143 0.124 Uiso 1 1 calc R . .
 H8B H -0.0284 0.5877 0.6807 0.124 Uiso 1 1 calc R . .
 H8C H 0.0558 0.4852 0.7284 0.124 Uiso 1 1 calc R . .
 C9 C 0.3600(5) 0.5981(4) 0.7883(4) 0.0676(12) Uani 1 1 d . . .
 H9A H 0.3805 0.5748 0.7130 0.101 Uiso 1 1 calc R . .
 H9B H 0.3551 0.5278 0.8232 0.101 Uiso 1 1 calc R . .
 H9C H 0.4301 0.6552 0.8355 0.101 Uiso 1 1 calc R . .
 C10 C 0.3109(4) 1.2172(3) 0.8214(3) 0.0462(9) Uani 1 1 d . . .
 C11 C 0.3872(5) 1.2978(4) 0.9135(4) 0.0570(10) Uani 1 1 d . . .
 H11 H 0.4818 1.3029 0.9250 0.068 Uiso 1 1 calc R . .
 C12 C 0.3216(6) 1.3706(4) 0.9884(4) 0.0684(12) Uani 1 1 d . . .
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 C13 C 0.1826(6) 1.3620(5) 0.9722(4) 0.0689(13) Uani 1 1 d . . .
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 C14 C 0.1066(5) 1.2805(5) 0.8834(4) 0.0683(12) Uani 1 1 d . . .
 H14 H 0.0123 1.2739 0.8741 0.082 Uiso 1 1 calc R . .
 C15 C 0.1703(5) 1.2084(4) 0.8082(4) 0.0604(11) Uani 1 1 d . . .
 H15 H 0.1186 1.1529 0.7476 0.073 Uiso 1 1 calc R . .
 C16 C 0.3822(4) 1.2114(3) 0.5986(3) 0.0482(9) Uani 1 1 d . . .
 C17 C 0.2927(5) 1.2989(4) 0.5793(4) 0.0630(11) Uani 1 1 d . . .
 H17 H 0.2294 1.3159 0.6263 0.076 Uiso 1 1 calc R . .
 C18 C 0.2954(6) 1.3627(5) 0.4905(5) 0.0787(15) Uani 1 1 d . . .
 H18 H 0.2343 1.4223 0.4784 0.094 Uiso 1 1 calc R . .
 C19 C 0.3874(6) 1.3381(5) 0.4207(4) 0.0777(15) Uani 1 1 d . . .
 H19 H 0.3894 1.3812 0.3614 0.093 Uiso 1 1 calc R . .
 C20 C 0.4765(6) 1.2499(5) 0.4382(4) 0.0769(14) Uani 1 1 d . . .
 H20 H 0.5388 1.2328 0.3903 0.092 Uiso 1 1 calc R . .
 C21 C 0.4747(5) 1.1864(4) 0.5261(4) 0.0621(11) Uani 1 1 d . . .
 H21 H 0.5355 1.1265 0.5372 0.075 Uiso 1 1 calc R . .
 C22 C 0.8181(6) 0.9132(8) 0.8611(6) 0.110(2) Uani 1 1 d . . .
 H22A H 0.8700 0.9551 0.9350 0.132 Uiso 1 1 calc R . .
 H22B H 0.8385 0.8286 0.8541 0.132 Uiso 1 1 calc R . .
 C23 C 0.8660(9) 0.9610(9) 0.7722(9) 0.146(4) Uani 1 1 d . . .
 H23A H 0.9620 0.9514 0.7797 0.219 Uiso 1 1 calc R . .
 H23B H 0.8494 1.0455 0.7789 0.219 Uiso 1 1 calc R . .
 H23C H 0.8189 0.9183 0.6981 0.219 Uiso 1 1 calc R . .
 O1S O 0.7568(7) 1.2884(9) 0.7798(8) 0.230(5) Uani 1 1 d . . .
 H1S H 0.7112 1.2282 0.7414 0.346 Uiso 1 1 calc R . .
 C1S C 0.7246(10) 1.3792(7) 0.7345(9) 0.139(3) Uani 1 1 d . . .
 H1S1 H 0.6408 1.4068 0.7538 0.208 Uiso 1 1 calc R . .
 H1S2 H 0.7133 1.3572 0.6522 0.208 Uiso 1 1 calc R . .
 H1S3 H 0.7952 1.4427 0.7630 0.208 Uiso 1 1 calc R . .

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 0.01360(8)
   
 S1 0.0543(6) 0.0649(6) 0.0373(5) 0.0109(4) 0.0048(4) -0.0016(5)
   
 P1 0.0413(5) 0.0456(5) 0.0489(5) 0.0125(4) 0.0089(4) 0.0019(4)

Si1 0.0484(7) 0.0566(7) 0.0610(7) 0.0208(5) 0.0138(5) -0.0005(5)  
 O1 0.0450(16) 0.0586(17) 0.0737(19) 0.0230(14) 0.0069(14) 0.0029(13)  
 C1 0.038(2) 0.049(2) 0.0380(18) 0.0072(15) 0.0072(15) 0.0046(16)  
 C2 0.042(2) 0.049(2) 0.0435(19) 0.0101(16) 0.0110(16) 0.0072(16)  
 C3 0.063(3) 0.056(2) 0.050(2) 0.0185(18) 0.0051(19) 0.000(2)  
 C4 0.075(3) 0.069(3) 0.048(2) 0.011(2) -0.012(2) -0.007(2)  
 C5 0.055(3) 0.057(2) 0.054(2) 0.0103(19) -0.0033(19) -0.011(2)  
 C6 0.038(2) 0.051(2) 0.048(2) 0.0101(16) 0.0086(16) 0.0032(17)  
 C7 0.100(5) 0.102(4) 0.089(4) 0.039(3) 0.050(3) 0.011(3)  
 C8 0.069(3) 0.070(3) 0.109(4) 0.035(3) 0.003(3) -0.018(3)  
 C9 0.063(3) 0.057(3) 0.083(3) 0.022(2) 0.008(2) 0.007(2)  
 C10 0.049(2) 0.048(2) 0.045(2) 0.0166(16) 0.0089(17) 0.0008(17)  
 C11 0.051(3) 0.058(2) 0.057(2) 0.0076(19) 0.0039(19) -0.001(2)  
 C12 0.079(4) 0.064(3) 0.055(3) 0.000(2) 0.009(2) 0.003(2)  
 C13 0.078(4) 0.076(3) 0.058(3) 0.012(2) 0.026(2) 0.019(3)  
 C14 0.055(3) 0.089(3) 0.066(3) 0.017(3) 0.024(2) 0.006(3)  
 C15 0.049(3) 0.071(3) 0.060(3) 0.009(2) 0.012(2) -0.005(2)  
 C16 0.047(2) 0.047(2) 0.054(2) 0.0131(17) 0.0138(18) -0.0006(18)  
 C17 0.067(3) 0.070(3) 0.063(3) 0.028(2) 0.025(2) 0.017(2)  
 C18 0.094(4) 0.080(3) 0.076(3) 0.040(3) 0.025(3) 0.032(3)  
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 C20 0.087(4) 0.087(4) 0.069(3) 0.021(3) 0.041(3) 0.009(3)  
 C21 0.068(3) 0.060(3) 0.069(3) 0.020(2) 0.029(2) 0.015(2)  
 C22 0.063(4) 0.175(7) 0.108(5) 0.054(5) 0.023(3) 0.050(4)  
 C23 0.099(6) 0.171(8) 0.210(10) 0.091(7) 0.078(6) 0.027(5)  
 O1S 0.126(5) 0.295(10) 0.267(9) 0.202(8) -0.085(5) -0.111(6)  
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planes)
  are estimated using the full covariance matrix. The cell esds are
taken
  into account individually in the estimation of esds in distances,
angles
  and torsion angles; correlations between esds in cell parameters are
only
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P1 C10 1.805(4) . ?
P1 C2 1.810(4) . ?
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Si1 C9 1.859(5) . ?
Si1 C7 1.867(5) . ?
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C2 P1 C16 106.00(18) . . ?  
C9 Si1 C7 111.8(3) . . ?  
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C7 Si1 C8 107.0(3) . . ?  
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C8 Si1 C6 108.0(2) . . ?  
C6 C1 C2 121.0(3) . . ?  
C6 C1 S1 117.4(3) . . ?  
C2 C1 S1 121.5(3) . . ?  
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C5 C4 C3 119.9(4) . . ?  
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C11 C10 P1 119.0(3) . . ?  
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C13 C14 C15 119.5(5) . . ?  
C14 C15 C10 120.7(4) . . ?  
C17 C16 C21 118.6(4) . . ?  
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C21 C16 P1 116.8(3) . . ?  
C16 C17 C18 120.7(4) . . ?  
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## Compound (9)

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Refinement of F^2 against ALL reflections. The weighted R-factor wR
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on F, with F set to zero for negative F^2. The threshold expression
of
F^2 > 2sigma(F^2) is used only for calculating R-factors(gt) etc.
and is
not relevant to the choice of reflections for refinement. R-factors
based

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on  $F^2$  are statistically about twice as large as those based on  $F$ ,  
 and  $R$ -  
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Hg2 Hg	1.44051(5)	0.01122(3)	0.66388(3)	0.06200(14)	Uani	1	1	d	.	.	.
S1 S	0.9207(3)	0.0963(3)	0.7048(2)	0.0657(7)	Uani	1	1	d	.	.	.
S2 S	1.3541(3)	0.1286(2)	0.55737(19)	0.0536(6)	Uani	1	1	d	.	.	.
P1 P	1.2299(2)	0.33950(19)	0.74201(18)	0.0404(5)	Uani	1	1	d	.	.	.
C1 C	1.2342(9)	0.2380(7)	0.8234(6)	0.0418(19)	Uani	1	1	d	.	.	.
C2 C	1.1012(9)	0.1372(7)	0.8040(7)	0.0427(19)	Uani	1	1	d	.	.	.
C3 C	1.1100(11)	0.0625(8)	0.8689(8)	0.058(2)	Uani	1	1	d	.	.	.
H3 H	1.0234	-0.0050	0.8560	0.070	Uiso	1	1	calc	R	.	.
C4 C	1.2435(11)	0.0849(8)	0.9524(8)	0.060(2)	Uani	1	1	d	.	.	.
H4 H	1.2444	0.0355	0.9965	0.072	Uiso	1	1	calc	R	.	.
C5 C	1.3732(11)	0.1809(9)	0.9685(8)	0.059(2)	Uani	1	1	d	.	.	.
H5 H	1.4642	0.1958	1.0229	0.071	Uiso	1	1	calc	R	.	.
C6 C	1.3702(10)	0.2558(8)	0.9046(7)	0.052(2)	Uani	1	1	d	.	.	.
H6 H	1.4604	0.3196	0.9156	0.062	Uiso	1	1	calc	R	.	.
C7 C	1.4356(9)	0.3763(7)	0.7267(7)	0.0408(19)	Uani	1	1	d	.	.	.
C8 C	1.4851(9)	0.2814(7)	0.6431(7)	0.0430(19)	Uani	1	1	d	.	.	.
C9 C	1.6409(10)	0.3087(9)	0.6265(8)	0.060(2)	Uani	1	1	d	.	.	.

H9 H 1.6749 0.2461 0.5711 0.072 Uiso 1 1 calc R . . .  
 C10 C 1.7448(10) 0.4263(10) 0.6904(9) 0.068(3) Uani 1 1 d . . .  
 H10 H 1.8481 0.4424 0.6783 0.082 Uiso 1 1 calc R . . .  
 C11 C 1.6960(10) 0.5202(8) 0.7724(8) 0.057(2) Uani 1 1 d . . .  
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 C12 C 1.5434(9) 0.4948(8) 0.7896(7) 0.048(2) Uani 1 1 d . . .  
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 C13 C 1.2078(9) 0.4940(7) 0.8429(7) 0.0428(19) Uani 1 1 d . . .  
 C14 C 1.1855(9) 0.5845(8) 0.7977(8) 0.053(2) Uani 1 1 d . . .  
 H14 H 1.1860 0.5656 0.7206 0.064 Uiso 1 1 calc R . . .  
 C15 C 1.1625(11) 0.7033(8) 0.8658(9) 0.062(3) Uani 1 1 d . . .  
 H15 H 1.1515 0.7649 0.8354 0.074 Uiso 1 1 calc R . . .  
 C16 C 1.1562(11) 0.7281(9) 0.9780(10) 0.067(3) Uani 1 1 d . . .  
 H16 H 1.1405 0.8071 1.0242 0.081 Uiso 1 1 calc R . . .  
 C17 C 1.1729(11) 0.6373(9) 1.0231(9) 0.067(3) Uani 1 1 d . . .  
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 C18 C 1.2002(9) 0.5195(8) 0.9555(7) 0.051(2) Uani 1 1 d . . .  
 H18 H 1.2132 0.4587 0.9864 0.061 Uiso 1 1 calc R . . .  
 C19 C 0.9650(13) 0.2301(11) 0.4208(8) 0.076(3) Uani 1 1 d . . .  
 H19A H 0.9571 0.1548 0.3519 0.092 Uiso 1 1 calc R . . .  
 H19B H 0.8687 0.2604 0.4119 0.092 Uiso 1 1 calc R . . .  
 C20 C 1.0977(19) 0.3280(16) 0.4303(14) 0.164(7) Uani 1 1 d . . .  
 H20A H 1.0846 0.3475 0.3630 0.246 Uiso 1 1 calc R . . .  
 H20B H 1.1937 0.2984 0.4375 0.246 Uiso 1 1 calc R . . .  
 H20C H 1.1046 0.4042 0.4967 0.246 Uiso 1 1 calc R . . .  
 C21 C 1.5155(16) -0.0901(12) 0.7615(10) 0.100(4) Uani 1 1 d . . .  
 H21A H 1.6149 -0.0377 0.8142 0.119 Uiso 1 1 calc R . . .  
 H21B H 1.4370 -0.0998 0.8072 0.119 Uiso 1 1 calc R . . .  
 C22 C 1.539(2) -0.2127(15) 0.7006(13) 0.164(8) Uani 1 1 d . . .  
 H22A H 1.5721 -0.2500 0.7534 0.246 Uiso 1 1 calc R . . .  
 H22B H 1.6196 -0.2048 0.6572 0.246 Uiso 1 1 calc R . . .  
 H22C H 1.4408 -0.2670 0.6493 0.246 Uiso 1 1 calc R . . .

loop\_  
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 Hg1 0.0511(2) 0.0575(2) 0.0505(2) 0.01890(18) 0.00324(15) 0.01477(16)  
 Hg2 0.0800(3) 0.0478(2) 0.0609(3) 0.02389(19) 0.0144(2) 0.01636(19)  
 S1 0.0452(12) 0.0731(17) 0.0759(17) 0.0385(14) 0.0016(11) -0.0058(12)  
 S2 0.0631(13) 0.0402(12) 0.0489(13) 0.0088(10) 0.0046(11) 0.0142(10)  
 P1 0.0417(11) 0.0357(11) 0.0401(12) 0.0139(9) 0.0054(9) 0.0046(9)  
 C1 0.046(4) 0.037(4) 0.041(5) 0.013(4) 0.011(4) 0.008(4)  
 C2 0.048(5) 0.038(4) 0.042(5) 0.015(4) 0.010(4) 0.011(4)  
 C3 0.072(6) 0.045(5) 0.055(6) 0.021(5) 0.018(5) 0.005(5)  
 C4 0.079(7) 0.048(5) 0.055(6) 0.023(5) 0.012(5) 0.018(5)  
 C5 0.066(6) 0.063(6) 0.050(6) 0.025(5) 0.002(5) 0.020(5)  
 C6 0.054(5) 0.042(5) 0.050(5) 0.011(4) -0.001(4) 0.009(4)  
 C7 0.052(5) 0.034(4) 0.042(5) 0.017(4) 0.018(4) 0.014(4)  
 C8 0.046(4) 0.042(5) 0.042(5) 0.016(4) 0.005(4) 0.015(4)  
 C9 0.057(5) 0.065(6) 0.065(6) 0.026(5) 0.018(5) 0.027(5)  
 C10 0.043(5) 0.072(7) 0.092(8) 0.035(6) 0.015(5) 0.014(5)  
 C11 0.058(5) 0.042(5) 0.067(6) 0.026(5) 0.002(5) -0.001(4)  
 C12 0.048(5) 0.039(5) 0.044(5) 0.008(4) 0.002(4) 0.001(4)  
 C13 0.038(4) 0.034(4) 0.049(5) 0.013(4) 0.000(4) 0.004(3)  
 C14 0.051(5) 0.057(6) 0.057(6) 0.026(5) 0.016(4) 0.013(4)  
 C15 0.074(6) 0.040(5) 0.080(7) 0.029(5) 0.020(5) 0.020(5)

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C16 0.071(6) 0.038(5) 0.089(8) 0.012(5) 0.027(6) 0.021(5)
C17 0.078(7) 0.054(6) 0.066(6) 0.015(5) 0.033(5) 0.016(5)
C18 0.055(5) 0.047(5) 0.056(6) 0.023(4) 0.022(4) 0.011(4)
C19 0.083(7) 0.103(9) 0.050(6) 0.041(6) 0.007(5) 0.021(7)
C20 0.152(14) 0.22(2) 0.168(16) 0.164(16) 0.013(12) 0.004(13)
C21 0.145(11) 0.101(10) 0.084(9) 0.059(8) 0.027(8) 0.054(9)
C22 0.30(2) 0.152(15) 0.146(14) 0.111(13) 0.112(15) 0.158(16)

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  All esds (except the esd in the dihedral angle between two l.s.
planes)
  are estimated using the full covariance matrix. The cell esds are
taken
  into account individually in the estimation of esds in distances,
angles
  and torsion angles; correlations between esds in cell parameters are
only
  used when they are defined by crystal symmetry. An approximate
(isotropic)
  treatment of cell esds is used for estimating esds involving l.s.
planes.
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Hg1 S1 2.386(3) . ?
Hg1 P1 2.807(2) . ?
Hg2 C21 2.100(11) . ?
Hg2 S2 2.368(2) . ?
S1 C2 1.760(8) . ?
S2 C8 1.778(8) . ?
P1 C1 1.815(8) . ?
P1 C7 1.818(8) . ?
P1 C13 1.835(8) . ?
C1 C6 1.402(11) . ?
C1 C2 1.408(10) . ?
C2 C3 1.391(11) . ?
C3 C4 1.390(12) . ?
C4 C5 1.366(12) . ?
C5 C6 1.379(12) . ?
C7 C12 1.394(10) . ?
C7 C8 1.399(10) . ?
C8 C9 1.397(11) . ?
C9 C10 1.375(12) . ?
C10 C11 1.377(12) . ?
C11 C12 1.372(11) . ?
C13 C18 1.373(11) . ?
C13 C14 1.381(11) . ?
C14 C15 1.391(12) . ?
C15 C16 1.367(13) . ?
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C21 C22 1.402(16) . ?

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C19 Hg1 P1 111.6(3) . . ?
S1 Hg1 P1 80.27(7) . . ?
C21 Hg2 S2 178.7(3) . . ?
C2 S1 Hg1 107.2(3) . . ?
C8 S2 Hg2 98.0(3) . . ?
C1 P1 C7 103.0(4) . . ?
C1 P1 C13 105.2(4) . . ?
C7 P1 C13 103.2(3) . . ?
C1 P1 Hg1 97.9(2) . . ?
C7 P1 Hg1 123.9(3) . . ?
C13 P1 Hg1 120.4(2) . . ?
C6 C1 C2 118.6(8) . . ?
C6 C1 P1 121.1(6) . . ?
C2 C1 P1 120.3(6) . . ?
C3 C2 C1 118.1(8) . . ?
C3 C2 S1 115.9(6) . . ?
C1 C2 S1 126.0(6) . . ?
C4 C3 C2 122.5(8) . . ?
C5 C4 C3 118.8(9) . . ?
C4 C5 C6 120.4(9) . . ?
C5 C6 C1 121.4(8) . . ?
C12 C7 C8 118.6(7) . . ?
C12 C7 P1 123.9(6) . . ?
C8 C7 P1 117.5(6) . . ?
C9 C8 C7 118.7(7) . . ?
C9 C8 S2 119.8(6) . . ?
C7 C8 S2 121.5(6) . . ?
C10 C9 C8 121.3(8) . . ?
C9 C10 C11 120.0(8) . . ?
C12 C11 C10 119.3(8) . . ?
C11 C12 C7 122.0(8) . . ?
C18 C13 C14 119.5(8) . . ?
C18 C13 P1 124.0(7) . . ?
C14 C13 P1 116.2(7) . . ?
C13 C14 C15 121.0(9) . . ?
C16 C15 C14 119.0(9) . . ?
C15 C16 C17 120.6(9) . . ?
C16 C17 C18 120.3(9) . . ?
C13 C18 C17 119.5(9) . . ?
C20 C19 Hg1 114.3(8) . . ?
C22 C21 Hg2 116.7(9) . . ?

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## Compound (10\*)

data\_p169b

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'P' 'P' 0.1023 0.0942	
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'O' 'O' 0.0106 0.0060	
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'-x, -y, -z'	
'x, -y-1/2, z-1/2'	
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_cell_length_b	19.760(5)
_cell_length_c	14.774(4)
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_cell_angle_gamma	90.00
_cell_volume	3393.0(15)
_cell_formula_units_Z	4
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_diffrn_measurement_method      'omega scans'
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_computing_cell_refinement      'BRUKER Smart'
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_computing_publication_material  ?

_refine_special_details
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Refinement of F^2 against ALL reflections. The weighted R-factor wR
and
goodness of fit S are based on F^2, conventional R-factors R are
based

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on F, with F set to zero for negative F<sup>2</sup>. The threshold expression of  
 $F^2 > 2\sigma(F^2)$  is used only for calculating R-factors(gt) etc.  
 and is  
 not relevant to the choice of reflections for refinement. R-factors based  
 on F<sup>2</sup> are statistically about twice as large as those based on F,  
 and R-factors based on ALL data will be even larger.  
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loop\_

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Hg1	Hg	0.30030(3)	0.262439(17)	0.94285(2)	0.05349(12)	Uani	1	1	d	.	.	.
Hg2	Hg	0.53230(3)	0.102068(19)	1.07595(3)	0.06247(13)	Uani	1	1	d	.	.	.
S1	S	0.22682(18)	0.23830(12)	1.06797(14)	0.0550(5)	Uani	1	1	d	.	.	.
S2	S	0.45531(17)	-0.00350(10)	1.09662(15)	0.0523(5)	Uani	1	1	d	.	.	.
P1	P	0.22317(16)	0.08734(10)	0.97608(13)	0.0395(4)	Uani	1	1	d	.	.	.
Si1	Si	-0.0127(2)	0.32077(13)	1.0365(2)	0.0720(8)	Uani	1	1	d	.	.	.
Si2	Si	0.5003(2)	-0.05956(13)	1.31470(17)	0.0627(7)	Uani	1	1	d	.	.	.
O1	O	0.3144(4)	0.1237(3)	0.9530(3)	0.0446(12)	Uani	1	1	d	.	.	.
C1	C	0.0938(6)	0.2022(4)	0.9888(5)	0.0411(17)	Uani	1	1	d	.	.	.
C2	C	0.0914(6)	0.1379(4)	0.9472(5)	0.0386(16)	Uani	1	1	d	.	.	.
C3	C	-0.0133(6)	0.1120(4)	0.8846(5)	0.0470(19)	Uani	1	1	d	.	.	.
H3	H	-0.0159	0.0701	0.8554	0.056	Uiso	1	1	calc	R	.	.

C4 C -0.1126(7) 0.1485(4) 0.8664(6) 0.054(2) Uani 1 1 d . . .
 H4 H -0.1825 0.1312 0.8249 0.065 Uiso 1 1 calc R . .
 C5 C -0.1092(7) 0.2102(4) 0.9089(6) 0.054(2) Uani 1 1 d . . .
 H5 H -0.1777 0.2339 0.8953 0.065 Uiso 1 1 calc R . .
 C6 C -0.0084(7) 0.2391(4) 0.9715(5) 0.0498(19) Uani 1 1 d . . .
 C7 C -0.1672(10) 0.3478(6) 0.9941(9) 0.115(4) Uani 1 1 d . . .
 H7A H -0.1952 0.3553 0.9252 0.173 Uiso 1 1 calc R . .
 H7B H -0.1734 0.3889 1.0264 0.173 Uiso 1 1 calc R . .
 H7C H -0.2121 0.3130 1.0088 0.173 Uiso 1 1 calc R . .
 C8 C 0.0358(11) 0.3051(6) 1.1679(7) 0.115(4) Uani 1 1 d . . .
 H8A H -0.0089 0.2692 1.1802 0.173 Uiso 1 1 calc R . .
 H8B H 0.0261 0.3455 1.2002 0.173 Uiso 1 1 calc R . .
 H8C H 0.1156 0.2925 1.1918 0.173 Uiso 1 1 calc R . .
 C9 C 0.0695(10) 0.3897(5) 1.0072(9) 0.108(4) Uani 1 1 d . . .
 H9A H 0.0421 0.3962 0.9382 0.163 Uiso 1 1 calc R . .
 H9B H 0.1496 0.3780 1.0303 0.163 Uiso 1 1 calc R . .
 H9C H 0.0594 0.4308 1.0380 0.163 Uiso 1 1 calc R . .
 C10 C 0.3511(6) 0.0184(3) 1.1487(5) 0.0387(16) Uani 1 1 d . . .
 C11 C 0.2548(6) 0.0574(3) 1.1000(5) 0.0370(16) Uani 1 1 d . . .
 C12 C 0.1756(6) 0.0698(4) 1.1438(5) 0.0491(19) Uani 1 1 d . . .
 H12 H 0.1122 0.0970 1.1122 0.059 Uiso 1 1 calc R . .
 C13 C 0.1885(7) 0.0427(4) 1.2338(5) 0.053(2) Uani 1 1 d . . .
 H13 H 0.1338 0.0507 1.2616 0.064 Uiso 1 1 calc R . .
 C14 C 0.2830(6) 0.0039(4) 1.2807(5) 0.0486(19) Uani 1 1 d . . .
 H14 H 0.2914 -0.0142 1.3410 0.058 Uiso 1 1 calc R . .
 C15 C 0.3684(6) -0.0097(3) 1.2417(5) 0.0409(17) Uani 1 1 d . . .
 C16 C 0.4782(9) -0.0912(5) 1.4256(6) 0.090(3) Uani 1 1 d . . .
 H16A H 0.5442 -0.1168 1.4645 0.135 Uiso 1 1 calc R . .
 H16B H 0.4112 -0.1196 1.4069 0.135 Uiso 1 1 calc R . .
 H16C H 0.4677 -0.0536 1.4626 0.135 Uiso 1 1 calc R . .
 C17 C 0.6263(7) -0.0015(6) 1.3531(7) 0.093(3) Uani 1 1 d . . .
 H17A H 0.6942 -0.0262 1.3908 0.140 Uiso 1 1 calc R . .
 H17B H 0.6135 0.0345 1.3916 0.140 Uiso 1 1 calc R . .
 H17C H 0.6364 0.0171 1.2967 0.140 Uiso 1 1 calc R . .
 C18 C 0.5257(11) -0.1350(5) 1.2501(8) 0.114(4) Uani 1 1 d . . .
 H18A H 0.5936 -0.1581 1.2911 0.172 Uiso 1 1 calc R . .
 H18B H 0.5358 -0.1209 1.1915 0.172 Uiso 1 1 calc R . .
 H18C H 0.4608 -0.1649 1.2342 0.172 Uiso 1 1 calc R . .
 C19 C 0.1812(6) 0.0115(4) 0.9031(5) 0.0415(17) Uani 1 1 d . . .
 C20 C 0.1849(7) 0.0130(4) 0.8096(6) 0.059(2) Uani 1 1 d . . .
 H20 H 0.2112 0.0515 0.7880 0.070 Uiso 1 1 calc R . .
 C21 C 0.1493(8) -0.0426(5) 0.7493(7) 0.074(3) Uani 1 1 d . . .
 H21 H 0.1504 -0.0411 0.6867 0.089 Uiso 1 1 calc R . .
 C22 C 0.1125(7) -0.0999(4) 0.7815(7) 0.063(2) Uani 1 1 d . . .
 H22 H 0.0901 -0.1374 0.7410 0.076 Uiso 1 1 calc R . .
 C23 C 0.1085(6) -0.1021(4) 0.8730(7) 0.061(2) Uani 1 1 d . . .
 H23 H 0.0822 -0.1408 0.8942 0.073 Uiso 1 1 calc R . .
 C24 C 0.1439(6) -0.0464(4) 0.9338(5) 0.0468(18) Uani 1 1 d . . .
 H24 H 0.1424 -0.0484 0.9962 0.056 Uiso 1 1 calc R . .
 C25 C 0.3481(12) 0.2880(6) 0.8242(7) 0.100(4) Uani 1 1 d . . .
 H25A H 0.3507 0.2461 0.7908 0.120 Uiso 1 1 calc R . .
 H25B H 0.2856 0.3146 0.7800 0.120 Uiso 1 1 calc R . .
 C26 C 0.4508(10) 0.3232(6) 0.8364(8) 0.104(4) Uani 1 1 d . . .
 H26A H 0.4567 0.3306 0.7741 0.156 Uiso 1 1 calc R . .
 H26B H 0.5154 0.2970 0.8764 0.156 Uiso 1 1 calc R . .
 H26C H 0.4502 0.3660 0.8670 0.156 Uiso 1 1 calc R . .
 C27 C 0.6097(9) 0.1932(5) 1.0678(9) 0.097(4) Uani 1 1 d . . .
 H27A H 0.6686 0.1850 1.0407 0.117 Uiso 1 1 calc R . .
 H27B H 0.5524 0.2227 1.0232 0.117 Uiso 1 1 calc R . .
 C28 C 0.6631(14) 0.2293(7) 1.1623(13) 0.160(6) Uani 1 1 d . . .
 H28A H 0.6973 0.2707 1.1521 0.240 Uiso 1 1 calc R . .

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H28B H 0.7213 0.2011 1.2067 0.240 Uiso 1 1 calc R . .
H28C H 0.6051 0.2392 1.1889 0.240 Uiso 1 1 calc R . .

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0.00850(16)
Hg2 0.0508(2) 0.0696(3) 0.0668(2) 0.00752(17) 0.02101(16) -0.00253(17)
S1 0.0558(12) 0.0673(14) 0.0369(11) -0.0099(10) 0.0109(9) -0.0081(11)
S2 0.0590(12) 0.0533(13) 0.0564(13) 0.0085(10) 0.0351(10) 0.0131(10)
P1 0.0436(10) 0.0455(12) 0.0316(10) 0.0028(8) 0.0162(8) 0.0000(9)
Si1 0.0795(18) 0.0570(16) 0.0763(19) -0.0092(13) 0.0242(15) 0.0148(14)
Si2 0.0800(16) 0.0615(16) 0.0484(14) 0.0156(12) 0.0255(12) 0.0288(14)
O1 0.045(3) 0.052(3) 0.038(3) 0.006(2) 0.017(2) -0.002(2)
C1 0.047(4) 0.047(5) 0.028(4) 0.004(3) 0.012(3) -0.001(4)
C2 0.042(4) 0.045(4) 0.030(4) 0.003(3) 0.015(3) -0.003(3)
C3 0.047(4) 0.045(5) 0.046(4) 0.005(4) 0.013(4) -0.005(4)
C4 0.045(5) 0.060(6) 0.051(5) 0.000(4) 0.008(4) -0.004(4)
C5 0.046(5) 0.059(6) 0.053(5) 0.011(4) 0.013(4) 0.010(4)
C6 0.058(5) 0.047(5) 0.043(4) 0.009(4) 0.016(4) 0.004(4)
C7 0.114(9) 0.085(8) 0.145(11) -0.014(8) 0.045(8) 0.042(7)
C8 0.140(11) 0.138(11) 0.076(8) -0.024(7) 0.050(7) 0.020(9)
C9 0.112(9) 0.054(7) 0.128(10) -0.008(6) 0.006(8) 0.006(6)
C10 0.044(4) 0.038(4) 0.038(4) -0.006(3) 0.020(3) -0.006(3)
C11 0.040(4) 0.043(4) 0.031(4) 0.003(3) 0.017(3) 0.004(3)
C12 0.045(4) 0.065(5) 0.039(4) 0.004(4) 0.017(3) 0.005(4)
C13 0.053(5) 0.065(6) 0.053(5) 0.007(4) 0.032(4) 0.005(4)
C14 0.062(5) 0.053(5) 0.035(4) 0.008(4) 0.023(4) 0.001(4)
C15 0.047(4) 0.037(4) 0.042(4) -0.001(3) 0.020(3) -0.001(3)
C16 0.116(9) 0.090(8) 0.058(6) 0.034(5) 0.023(6) 0.036(6)
C17 0.057(6) 0.142(11) 0.071(7) 0.005(7) 0.012(5) 0.006(6)
C18 0.193(13) 0.068(7) 0.101(9) 0.032(6) 0.076(9) 0.062(8)
C19 0.044(4) 0.041(4) 0.042(4) 0.003(3) 0.018(3) -0.001(3)
C20 0.076(6) 0.059(6) 0.048(5) -0.003(4) 0.031(4) -0.015(5)
C21 0.078(6) 0.088(8) 0.059(6) -0.021(5) 0.029(5) -0.013(6)
C22 0.062(5) 0.057(6) 0.071(6) -0.021(5) 0.025(5) -0.005(5)
C23 0.044(5) 0.055(6) 0.084(7) 0.004(5) 0.025(4) 0.002(4)
C24 0.049(4) 0.050(5) 0.048(5) 0.003(4) 0.025(4) 0.005(4)
C25 0.168(12) 0.082(8) 0.055(6) 0.001(5) 0.048(7) -0.007(8)
C26 0.135(10) 0.120(10) 0.082(8) -0.012(7) 0.070(7) -0.047(8)
C27 0.071(7) 0.064(7) 0.126(10) 0.006(7) -0.001(6) -0.012(6)
C28 0.174(15) 0.083(10) 0.215(19) -0.001(11) 0.060(14) 0.013(10)

_geom_special_details
;
All esds (except the esd in the dihedral angle between two l.s.
planes)
are estimated using the full covariance matrix. The cell esds are
taken
into account individually in the estimation of esds in distances,
angles
and torsion angles; correlations between esds in cell parameters are
only
used when they are defined by crystal symmetry. An approximate
(isotropic)

```

treatment of cell esds is used for estimating esds involving l.s.  
 planes.  
 ;

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 Hg1 C25 2.108(10) . ?  
 Hg1 S1 2.390(2) . ?  
 Hg2 C27 2.067(10) . ?  
 Hg2 S2 2.362(2) . ?  
 S1 C1 1.795(7) . ?  
 S2 C10 1.787(7) . ?  
 P1 O1 1.486(5) . ?  
 P1 C19 1.809(7) . ?  
 P1 C11 1.825(7) . ?  
 P1 C2 1.837(7) . ?  
 Si1 C8 1.837(11) . ?  
 Si1 C9 1.848(11) . ?  
 Si1 C7 1.875(11) . ?  
 Si1 C6 1.887(8) . ?  
 Si2 C18 1.858(10) . ?  
 Si2 C17 1.860(10) . ?  
 Si2 C16 1.866(9) . ?  
 Si2 C15 1.886(7) . ?  
 C1 C2 1.407(10) . ?  
 C1 C6 1.409(10) . ?  
 C2 C3 1.395(9) . ?  
 C3 C4 1.373(10) . ?  
 C4 C5 1.364(11) . ?  
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 C10 C11 1.388(9) . ?  
 C10 C15 1.425(9) . ?  
 C11 C12 1.385(9) . ?  
 C12 C13 1.387(10) . ?  
 C13 C14 1.365(10) . ?  
 C14 C15 1.408(10) . ?  
 C19 C24 1.373(10) . ?  
 C19 C20 1.399(10) . ?  
 C20 C21 1.383(11) . ?  
 C21 C22 1.369(12) . ?  
 C22 C23 1.371(12) . ?  
 C23 C24 1.388(11) . ?  
 C25 C26 1.411(14) . ?  
 C27 C28 1.491(17) . ?

loop\_  
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 C25 Hg1 S1 174.0(4) . . ?  
 C27 Hg2 S2 175.7(3) . . ?  
 C1 S1 Hg1 95.6(2) . . ?  
 C10 S2 Hg2 103.6(2) . . ?

O1 P1 C19 110.1(3) . . ?  
 O1 P1 C11 118.8(3) . . ?  
 C19 P1 C11 103.9(3) . . ?  
 O1 P1 C2 112.3(3) . . ?  
 C19 P1 C2 105.7(3) . . ?  
 C11 P1 C2 105.0(3) . . ?  
 C8 Si1 C9 111.9(6) . . ?  
 C8 Si1 C7 107.8(6) . . ?  
 C9 Si1 C7 107.6(5) . . ?  
 C8 Si1 C6 109.5(5) . . ?  
 C9 Si1 C6 113.0(5) . . ?  
 C7 Si1 C6 106.8(4) . . ?  
 C18 Si2 C17 111.6(6) . . ?  
 C18 Si2 C16 106.8(5) . . ?  
 C17 Si2 C16 108.5(5) . . ?  
 C18 Si2 C15 113.7(4) . . ?  
 C17 Si2 C15 108.5(4) . . ?  
 C16 Si2 C15 107.5(4) . . ?  
 C2 C1 C6 120.9(7) . . ?  
 C2 C1 S1 120.8(5) . . ?  
 C6 C1 S1 118.3(6) . . ?  
 C3 C2 C1 119.1(7) . . ?  
 C3 C2 P1 119.9(6) . . ?  
 C1 C2 P1 121.0(5) . . ?  
 C4 C3 C2 119.9(7) . . ?  
 C5 C4 C3 120.2(7) . . ?  
 C4 C5 C6 123.1(8) . . ?  
 C5 C6 C1 116.7(7) . . ?  
 C5 C6 Si1 120.4(6) . . ?  
 C1 C6 Si1 122.7(6) . . ?  
 C11 C10 C15 121.1(6) . . ?  
 C11 C10 S2 122.6(5) . . ?  
 C15 C10 S2 116.2(5) . . ?  
 C12 C11 C10 119.0(6) . . ?  
 C12 C11 P1 118.7(5) . . ?  
 C10 C11 P1 122.1(5) . . ?  
 C11 C12 C13 121.6(7) . . ?  
 C14 C13 C12 118.9(7) . . ?  
 C13 C14 C15 122.8(7) . . ?  
 C14 C15 C10 116.6(6) . . ?  
 C14 C15 Si2 119.9(5) . . ?  
 C10 C15 Si2 123.4(5) . . ?  
 C24 C19 C20 118.7(7) . . ?  
 C24 C19 P1 123.6(6) . . ?  
 C20 C19 P1 117.7(6) . . ?  
 C21 C20 C19 120.1(8) . . ?  
 C22 C21 C20 120.2(9) . . ?  
 C21 C22 C23 120.4(8) . . ?  
 C22 C23 C24 119.7(8) . . ?  
 C19 C24 C23 120.9(7) . . ?  
 C26 C25 Hg1 121.9(8) . . ?  
 C28 C27 Hg2 114.9(9) . . ?  
  
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 \_diffrn\_reflns\_theta\_full 26.36  
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## Compound (11)

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'C52 H68 Hg3 O2 P2 S4 Si4'
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loop_
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_atom_type_description
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_atom_type_scat_source
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'H'   'H'   0.0000   0.0000
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'Si'  'Si'  0.0817   0.0704
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
'P'   'P'   0.1023   0.0942
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
'S'   'S'   0.1246   0.1234
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'Hg'  'Hg'  -2.3894   9.2266
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'
'O'   'O'   0.0106   0.0060
'International Tables Vol C Tables 4.2.6.8 and 6.1.1.4'

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_symmetry_space_group_name_H-M   'P 2(1)/n'

loop_
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'x, y, z'
'-x+1/2, y+1/2, -z+1/2'
'-x, -y, -z'
'x-1/2, -y-1/2, z-1/2'

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_cell_length_b                  28.822(4)
_cell_length_c                  20.742(3)
_cell_angle_alpha                90.00
_cell_angle_beta                 101.891(4)
_cell_angle_gamma                90.00
_cell_volume                     6773.5(17)
_cell_formula_units_Z            4
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_cell_measurement_reflns_used   949
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_exptl_crystal_density_method   'not measured'
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_exptl_special_details
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_diffrn_radiation_wavelength    0.71073
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_diffrn_radiation_source        'fine-focus sealed tube'
_diffrn_radiation_monochromator graphite
_diffrn_measurement_device_type 'Smart-CCD-1000 BRUKER'
_diffrn_measurement_method      'omega scans'
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_diffrn_standards_number         ?
_diffrn_standards_interval_count ?
_diffrn_standards_interval_time ?
_diffrn_standards_decay_%       ?
_diffrn_reflns_number            42799
_diffrn_reflns_av_R_equivalents 0.0547
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_diffrn_reflns_limit_k_max      32
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_reflns_number_gt                5486
_reflns_threshold_expression    >2sigma(I)

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_computing_cell_refinement      'BRUKER Smart'
_computing_data_reduction        ?
_computing_structure_solution   ?
_computing_structure_refinement 'SHELXL-97 (Sheldrick, 1997)'
_computing_molecular_graphics   ?
_computing_publication_material  ?

_refine_special_details
;
  Refinement of F^2 against ALL reflections. The weighted R-factor wR
  and
  goodness of fit S are based on F^2, conventional R-factors R are
  based

```

on F, with F set to zero for negative F<sup>2</sup>. The threshold expression of  
 F<sup>2</sup> > 2sigma(F<sup>2</sup>) is used only for calculating R-factors(gt) etc.  
 and is  
 not relevant to the choice of reflections for refinement. R-factors  
 based  
 on F<sup>2</sup> are statistically about twice as large as those based on F,  
 and R-  
 factors based on ALL data will be even larger.  
;

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_refine_ls_weighting_details	'calc w=1/[\\$s^2^(Fo^2)+(0.0789P)^2+0.0000P] where P=(Fo^2+2Fc^2)/3'
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_atom_sites_solution_secondary	difmap
_atom_sites_solution_hydrogens	geom
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_refine_ls_extinction_method	none
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loop\_

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_atom_site_type_symbol
_atom_site_fract_x
_atom_site_fract_y
_atom_site_fract_z
_atom_site_U_iso_or_equiv
_atom_site_adp_type
_atom_site_occupancy
_atom_site_symmetry_multiplicity
_atom_site_calc_flag
_atom_site_refinement_flags
_atom_site_disorder_assembly
_atom_site_disorder_group

Hg1 Hg 0.46186(5) 0.030201(18) 0.20808(3) 0.0674(2) Uani 1 1 d . . . .  
Hg2 Hg 0.68192(6) 0.23950(3) 0.05134(3) 0.0957(3) Uani 1 1 d . . . .  
Hg3 Hg 0.52216(5) 0.158364(19) 0.14647(3) 0.06433(19) Uani 1 1 d . . . .  
S1 S 0.2537(3) 0.03844(12) 0.17969(18) 0.0695(10) Uani 1 1 d . . . .  
S2 S 0.4241(3) 0.18709(12) 0.04508(18) 0.0687(10) Uani 1 1 d . . . .  
S3 S 0.6710(3) 0.29310(15) 0.1372(2) 0.0903(13) Uani 1 1 d . . . .  
S4 S 0.5956(3) 0.13783(11) 0.25576(17) 0.0659(10) Uani 1 1 d . . . .  
P1 P 0.3352(3) 0.08007(11) 0.04719(16) 0.0503(8) Uani 1 1 d . . . .  
P2 P 0.8006(3) 0.20678(13) 0.22207(19) 0.0636(10) Uani 1 1 d . . . .  
Si1 Si 0.1255(3) -0.06501(13) 0.1748(2) 0.0747(12) Uani 1 1 d . . . .  
Si2 Si 0.2483(4) 0.27522(14) 0.0576(2) 0.0805(13) Uani 1 1 d . . . .  
Si3 Si 0.8112(4) 0.39034(16) 0.1200(2) 0.0834(13) Uani 1 1 d . . . .

Si4 Si 0.3947(4) 0.17650(14) 0.3323(2) 0.0796(13) Uani 1 1 d . . .
 O1 O 0.4462(7) 0.0774(3) 0.0985(4) 0.054(2) Uani 1 1 d . . .
 O2 O 0.7478(7) 0.1850(3) 0.1568(4) 0.073(3) Uani 1 1 d . . .
 C1 C 0.2227(10) 0.0079(4) 0.1042(6) 0.054(3) Uani 1 1 d . . .
 C2 C 0.2498(10) 0.0269(4) 0.0456(6) 0.051(3) Uani 1 1 d . . .
 C3 C 0.2154(12) 0.0038(5) -0.0127(7) 0.070(4) Uani 1 1 d . . .
 H3 H 0.2324 0.0168 -0.0507 0.084 Uiso 1 1 calc R . .
 C4 C 0.1568(14) -0.0380(6) -0.0174(8) 0.090(5) Uani 1 1 d . . .
 H4 H 0.1352 -0.0534 -0.0575 0.108 Uiso 1 1 calc R . .
 C5 C 0.1312(12) -0.0563(5) 0.0392(8) 0.077(4) Uani 1 1 d . . .
 H5 H 0.0895 -0.0840 0.0363 0.092 Uiso 1 1 calc R . .
 C6 C 0.1651(10) -0.0351(4) 0.1016(7) 0.058(3) Uani 1 1 d . . .
 C7 C 0.0090(15) -0.0329(6) 0.2039(9) 0.121(7) Uani 1 1 d . . .
 H7A H -0.0569 -0.0283 0.1680 0.181 Uiso 1 1 calc R . .
 H7B H 0.0390 -0.0033 0.2210 0.181 Uiso 1 1 calc R . .
 H7C H -0.0161 -0.0502 0.2381 0.181 Uiso 1 1 calc R . .
 C8 C 0.2569(14) -0.0756(6) 0.2408(9) 0.126(7) Uani 1 1 d . . .
 H8A H 0.3145 -0.0927 0.2232 0.189 Uiso 1 1 calc R . .
 H8B H 0.2344 -0.0931 0.2756 0.189 Uiso 1 1 calc R . .
 H8C H 0.2899 -0.0464 0.2579 0.189 Uiso 1 1 calc R . .
 C9 C 0.0696(16) -0.1245(6) 0.1474(9) 0.121(6) Uani 1 1 d . . .
 H9A H 0.1307 -0.1416 0.1330 0.181 Uiso 1 1 calc R . .
 H9B H 0.0024 -0.1218 0.1118 0.181 Uiso 1 1 calc R . .
 H9C H 0.0472 -0.1404 0.1836 0.181 Uiso 1 1 calc R . .
 C10 C 0.2785(11) 0.1745(5) 0.0533(6) 0.059(3) Uani 1 1 d . . .
 C11 C 0.2378(11) 0.1286(4) 0.0540(6) 0.052(3) Uani 1 1 d . . .
 C12 C 0.1216(12) 0.1200(5) 0.0573(6) 0.062(4) Uani 1 1 d . . .
 H12 H 0.0950 0.0896 0.0587 0.075 Uiso 1 1 calc R . .
 C13 C 0.0461(12) 0.1562(5) 0.0584(7) 0.073(4) Uani 1 1 d . . .
 H13 H -0.0323 0.1504 0.0598 0.087 Uiso 1 1 calc R . .
 C14 C 0.0846(13) 0.2012(5) 0.0574(6) 0.068(4) Uani 1 1 d . . .
 H14 H 0.0314 0.2252 0.0586 0.081 Uiso 1 1 calc R . .
 C15 C 0.2001(12) 0.2122(4) 0.0547(6) 0.056(3) Uani 1 1 d . . .
 C16 C 0.3261(16) 0.2925(5) -0.0107(8) 0.107(6) Uani 1 1 d . . .
 H16A H 0.2760 0.2858 -0.0526 0.160 Uiso 1 1 calc R . .
 H16B H 0.3983 0.2753 -0.0063 0.160 Uiso 1 1 calc R . .
 H16C H 0.3434 0.3251 -0.0077 0.160 Uiso 1 1 calc R . .
 C17 C 0.1132(16) 0.3120(5) 0.0466(8) 0.106(6) Uani 1 1 d . . .
 H17A H 0.0639 0.3060 0.0042 0.159 Uiso 1 1 calc R . .
 H17B H 0.1354 0.3442 0.0495 0.159 Uiso 1 1 calc R . .
 H17C H 0.0705 0.3049 0.0804 0.159 Uiso 1 1 calc R . .
 C18 C 0.3406(14) 0.2872(5) 0.1387(8) 0.100(5) Uani 1 1 d . . .
 H18A H 0.4114 0.2690 0.1444 0.149 Uiso 1 1 calc R . .
 H18B H 0.2980 0.2794 0.1723 0.149 Uiso 1 1 calc R . .
 H18C H 0.3608 0.3195 0.1418 0.149 Uiso 1 1 calc R . .
 C19 C 0.3724(10) 0.0848(4) -0.0324(6) 0.049(3) Uani 1 1 d . . .
 C20 C 0.2971(13) 0.1023(5) -0.0854(7) 0.074(4) Uani 1 1 d . . .
 H20 H 0.2221 0.1116 -0.0810 0.089 Uiso 1 1 calc R . .
 C21 C 0.3285(16) 0.1068(4) -0.1461(7) 0.077(4) Uani 1 1 d . . .
 H21 H 0.2776 0.1204 -0.1816 0.093 Uiso 1 1 calc R . .
 C22 C 0.4389(17) 0.0903(6) -0.1519(9) 0.090(5) Uani 1 1 d . . .
 H22 H 0.4611 0.0920 -0.1925 0.108 Uiso 1 1 calc R . .
 C23 C 0.5148(13) 0.0718(5) -0.0995(9) 0.086(5) Uani 1 1 d . . .
 H23 H 0.5887 0.0613 -0.1038 0.103 Uiso 1 1 calc R . .
 C24 C 0.4804(12) 0.0690(5) -0.0394(7) 0.066(4) Uani 1 1 d . . .
 H24 H 0.5316 0.0561 -0.0033 0.079 Uiso 1 1 calc R . .
 C25 C 0.6452(14) 0.0208(5) 0.2352(10) 0.120(7) Uani 1 1 d . . .
 H25A H 0.6765 0.0400 0.2731 0.144 Uiso 1 1 calc R . .
 H25B H 0.6620 -0.0114 0.2477 0.144 Uiso 1 1 calc R . .
 C26 C 0.7077(16) 0.0335(7) 0.1775(11) 0.135(8) Uani 1 1 d . . .
 H26A H 0.7912 0.0289 0.1914 0.203 Uiso 1 1 calc R . .

H26B H 0.6921 0.0654 0.1655 0.203 Uiso 1 1 calc R . .  
 H26C H 0.6779 0.0140 0.1402 0.203 Uiso 1 1 calc R . .  
 C27 C 0.8235(11) 0.2945(5) 0.1732(6) 0.063(4) Uani 1 1 d . . .  
 C28 C 0.8801(12) 0.2599(5) 0.2100(7) 0.061(4) Uani 1 1 d . . .  
 C29 C 0.9989(12) 0.2635(5) 0.2373(6) 0.068(4) Uani 1 1 d . . .  
 H29 H 1.0388 0.2385 0.2599 0.082 Uiso 1 1 calc R . .  
 C30 C 1.0586(13) 0.3041(6) 0.2314(7) 0.077(4) Uani 1 1 d . . .  
 H30 H 1.1380 0.3069 0.2512 0.093 Uiso 1 1 calc R . .  
 C31 C 1.0024(13) 0.3391(5) 0.1973(7) 0.071(4) Uani 1 1 d . . .  
 H31 H 1.0448 0.3661 0.1938 0.085 Uiso 1 1 calc R . .  
 C32 C 0.8803(12) 0.3380(5) 0.1656(6) 0.066(4) Uani 1 1 d . . .  
 C33 C 0.7601(17) 0.3761(6) 0.0312(7) 0.126(7) Uani 1 1 d . . .  
 H33A H 0.8249 0.3640 0.0141 0.189 Uiso 1 1 calc R . .  
 H33B H 0.7307 0.4037 0.0074 0.189 Uiso 1 1 calc R . .  
 H33C H 0.6984 0.3534 0.0263 0.189 Uiso 1 1 calc R . .  
 C34 C 0.6933(14) 0.4139(5) 0.1562(7) 0.105(6) Uani 1 1 d . . .  
 H34A H 0.6601 0.4407 0.1317 0.158 Uiso 1 1 calc R . .  
 H34B H 0.7246 0.4226 0.2011 0.158 Uiso 1 1 calc R . .  
 H34C H 0.6331 0.3908 0.1551 0.158 Uiso 1 1 calc R . .  
 C35 C 0.9269(17) 0.4356(6) 0.1261(9) 0.129(7) Uani 1 1 d . . .  
 H35A H 0.9904 0.4241 0.1072 0.193 Uiso 1 1 calc R . .  
 H35B H 0.9564 0.4432 0.1716 0.193 Uiso 1 1 calc R . .  
 H35C H 0.8939 0.4628 0.1028 0.193 Uiso 1 1 calc R . .  
 C36 C 0.6122(11) 0.1954(4) 0.2883(6) 0.058(3) Uani 1 1 d . . .  
 C37 C 0.7025(11) 0.2242(4) 0.2767(6) 0.058(3) Uani 1 1 d . . .  
 C38 C 0.7253(12) 0.2657(5) 0.3110(7) 0.075(4) Uani 1 1 d . . .  
 H38 H 0.7897 0.2838 0.3064 0.090 Uiso 1 1 calc R . .  
 C39 C 0.6542(14) 0.2799(5) 0.3511(9) 0.093(5) Uani 1 1 d . . .  
 H39 H 0.6678 0.3080 0.3735 0.111 Uiso 1 1 calc R . .  
 C40 C 0.5626(15) 0.2525(5) 0.3582(8) 0.090(5) Uani 1 1 d . . .  
 H40 H 0.5139 0.2630 0.3857 0.108 Uiso 1 1 calc R . .  
 C41 C 0.5359(12) 0.2094(5) 0.3271(7) 0.071(4) Uani 1 1 d . . .  
 C42 C 0.2951(12) 0.1726(6) 0.2492(8) 0.099(5) Uani 1 1 d . . .  
 H42A H 0.3331 0.1550 0.2203 0.148 Uiso 1 1 calc R . .  
 H42B H 0.2783 0.2033 0.2316 0.148 Uiso 1 1 calc R . .  
 H42C H 0.2228 0.1576 0.2530 0.148 Uiso 1 1 calc R . .  
 C43 C 0.4301(15) 0.1182(5) 0.3718(8) 0.106(6) Uani 1 1 d . . .  
 H43A H 0.4808 0.1221 0.4143 0.159 Uiso 1 1 calc R . .  
 H43B H 0.4692 0.0994 0.3445 0.159 Uiso 1 1 calc R . .  
 H43C H 0.3583 0.1032 0.3767 0.159 Uiso 1 1 calc R . .  
 C44 C 0.3168(16) 0.2108(6) 0.3846(10) 0.127(7) Uani 1 1 d . . .  
 H44A H 0.3660 0.2140 0.4277 0.190 Uiso 1 1 calc R . .  
 H44B H 0.2449 0.1953 0.3881 0.190 Uiso 1 1 calc R . .  
 H44C H 0.2989 0.2409 0.3655 0.190 Uiso 1 1 calc R . .  
 C45 C 0.9027(12) 0.1677(5) 0.2707(8) 0.066(4) Uani 1 1 d . . .  
 C46 C 0.9323(15) 0.1710(6) 0.3363(10) 0.096(5) Uani 1 1 d . . .  
 H46 H 0.8985 0.1943 0.3575 0.115 Uiso 1 1 calc R . .  
 C47 C 1.0165(19) 0.1390(9) 0.3756(12) 0.132(7) Uani 1 1 d . . .  
 H47 H 1.0391 0.1411 0.4212 0.159 Uiso 1 1 calc R . .  
 C48 C 1.0592(19) 0.1058(9) 0.3400(17) 0.142(9) Uani 1 1 d . . .  
 H48 H 1.1120 0.0844 0.3632 0.170 Uiso 1 1 calc R . .  
 C49 C 1.032(2) 0.1013(8) 0.2745(15) 0.136(9) Uani 1 1 d . . .  
 H49 H 1.0642 0.0780 0.2528 0.163 Uiso 1 1 calc R . .  
 C50 C 0.9536(16) 0.1327(7) 0.2412(9) 0.100(5) Uani 1 1 d . . .  
 H50 H 0.9335 0.1303 0.1956 0.120 Uiso 1 1 calc R . .  
 C51 C 0.6948(18) 0.1902(7) -0.0234(9) 0.120(7) Uani 1 1 d . . .  
 H51A H 0.7727 0.1924 -0.0335 0.144 Uiso 1 1 calc R . .  
 H51B H 0.6868 0.1593 -0.0063 0.144 Uiso 1 1 calc R . .  
 C52 C 0.611(2) 0.1958(8) -0.0814(12) 0.182(11) Uani 1 1 d . . .  
 H52A H 0.6219 0.1724 -0.1125 0.272 Uiso 1 1 calc R . .  
 H52B H 0.6194 0.2259 -0.0995 0.272 Uiso 1 1 calc R . .

H52C H 0.5332 0.1929 -0.0721 0.272 Uiso 1 1 calc R . .

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Hg1 0.0743(4) 0.0567(3) 0.0640(4) 0.0030(3) -0.0022(3) -0.0010(3)  
Hg2 0.0904(5) 0.1194(6) 0.0739(4) -0.0084(4) 0.0089(4) -0.0509(4)  
Hg3 0.0506(3) 0.0675(4) 0.0721(4) -0.0097(3) 0.0061(3) -0.0128(3)  
S1 0.071(3) 0.069(2) 0.072(2) -0.0038(19) 0.0199(19) -0.0074(19)  
S2 0.053(2) 0.072(2) 0.082(3) 0.008(2) 0.0141(19) -0.0116(18)  
S3 0.053(2) 0.101(3) 0.108(3) -0.014(3) -0.006(2) -0.013(2)  
S4 0.068(2) 0.056(2) 0.072(2) -0.0089(18) 0.0105(19) -0.0072(18)  
P1 0.044(2) 0.0471(19) 0.057(2) 0.0012(16) 0.0047(16) -0.0013(15)  
P2 0.048(2) 0.069(2) 0.075(3) -0.021(2) 0.0172(19) -0.0135(18)  
Si1 0.051(2) 0.064(3) 0.109(3) 0.027(2) 0.016(2) -0.003(2)  
Si2 0.112(4) 0.051(2) 0.084(3) -0.003(2) 0.033(3) 0.003(2)  
Si3 0.093(3) 0.087(3) 0.067(3) -0.010(2) 0.008(2) -0.009(3)  
Si4 0.066(3) 0.072(3) 0.110(4) -0.007(3) 0.039(3) -0.007(2)  
O1 0.050(5) 0.056(5) 0.052(5) 0.008(4) 0.000(4) 0.000(4)  
O2 0.061(6) 0.089(7) 0.071(6) -0.026(5) 0.018(5) -0.020(5)  
C1 0.031(7) 0.058(8) 0.067(9) -0.005(7) -0.002(6) -0.003(6)  
C2 0.051(8) 0.053(8) 0.047(8) -0.001(7) 0.003(6) -0.007(6)  
C3 0.066(10) 0.060(9) 0.084(11) -0.004(8) 0.013(8) -0.017(8)  
C4 0.100(13) 0.100(13) 0.065(11) -0.014(9) 0.008(9) -0.019(10)  
C5 0.068(10) 0.060(9) 0.099(13) -0.012(9) 0.007(9) -0.033(8)  
C6 0.036(7) 0.048(8) 0.089(10) 0.008(7) 0.010(7) 0.005(6)  
C7 0.099(14) 0.126(15) 0.159(18) 0.038(13) 0.077(13) 0.023(11)  
C8 0.083(13) 0.126(15) 0.154(17) 0.060(13) -0.014(12) -0.001(11)  
C9 0.118(15) 0.101(13) 0.142(17) 0.015(12) 0.022(12) -0.045(11)  
C10 0.049(8) 0.065(9) 0.063(9) -0.004(7) 0.014(7) 0.006(7)  
C11 0.052(9) 0.040(7) 0.061(8) 0.004(6) 0.006(6) 0.000(6)  
C12 0.055(9) 0.061(9) 0.065(9) 0.010(7) 0.000(7) -0.006(8)  
C13 0.044(8) 0.074(10) 0.100(12) 0.015(9) 0.016(8) 0.003(8)  
C14 0.067(10) 0.072(10) 0.065(9) 0.009(8) 0.016(8) 0.027(8)  
C15 0.058(9) 0.052(8) 0.060(9) 0.005(6) 0.011(7) -0.002(7)  
C16 0.163(18) 0.061(10) 0.106(13) 0.018(9) 0.052(12) -0.001(10)  
C17 0.153(17) 0.070(11) 0.101(13) -0.017(9) 0.044(12) 0.023(10)  
C18 0.102(13) 0.090(12) 0.112(14) -0.020(10) 0.033(11) -0.010(10)  
C19 0.041(8) 0.040(7) 0.061(8) 0.002(6) 0.002(6) 0.002(6)  
C20 0.069(10) 0.075(10) 0.080(11) 0.005(8) 0.020(9) 0.031(8)  
C21 0.117(14) 0.054(9) 0.058(10) 0.009(7) 0.012(9) 0.009(9)  
C22 0.100(14) 0.087(12) 0.092(14) -0.030(10) 0.039(12) -0.006(10)  
C23 0.048(10) 0.098(12) 0.112(14) -0.018(11) 0.015(10) 0.006(9)  
C24 0.060(10) 0.074(10) 0.069(10) 0.001(8) 0.022(8) 0.006(7)  
C25 0.072(12) 0.075(12) 0.19(2) -0.003(12) -0.039(13) 0.025(9)  
C26 0.090(14) 0.126(17) 0.20(2) -0.003(15) 0.063(15) 0.024(12)  
C27 0.048(9) 0.074(10) 0.064(9) -0.005(8) 0.009(7) -0.014(8)  
C28 0.047(9) 0.068(9) 0.072(10) -0.026(8) 0.021(7) -0.015(7)  
C29 0.045(9) 0.096(11) 0.067(9) -0.012(8) 0.020(7) -0.011(8)  
C30 0.052(10) 0.087(11) 0.088(11) -0.008(9) 0.004(8) 0.001(9)  
C31 0.065(10) 0.071(10) 0.082(11) -0.009(9) 0.027(8) -0.018(8)  
C32 0.060(9) 0.088(11) 0.054(9) -0.009(7) 0.018(7) -0.013(8)  
C33 0.169(19) 0.140(16) 0.058(11) 0.002(10) -0.003(11) 0.019(14)  
C34 0.117(15) 0.095(12) 0.095(12) -0.018(10) 0.001(11) 0.001(10)  
C35 0.155(19) 0.100(14) 0.130(16) 0.004(12) 0.023(13) -0.006(13)  
C36 0.045(8) 0.060(8) 0.071(9) -0.004(7) 0.015(7) 0.009(7)

```

C37 0.049(8) 0.062(9) 0.069(9) -0.012(7) 0.023(7) 0.000(7)
C38 0.061(10) 0.076(10) 0.092(11) -0.036(9) 0.028(8) -0.027(8)
C39 0.078(12) 0.065(10) 0.145(16) -0.029(10) 0.048(11) -0.018(9)
C40 0.108(14) 0.069(11) 0.105(13) -0.024(9) 0.052(11) 0.013(10)
C41 0.076(10) 0.054(9) 0.089(11) -0.004(8) 0.032(9) 0.003(7)
C42 0.059(10) 0.125(14) 0.117(14) -0.006(11) 0.029(9) -0.016(9)
C43 0.107(14) 0.090(12) 0.136(15) 0.004(11) 0.059(12) -0.016(10)
C44 0.113(15) 0.092(13) 0.20(2) -0.017(13) 0.095(14) -0.006(11)
C45 0.057(9) 0.067(9) 0.078(11) -0.031(8) 0.024(8) -0.005(7)
C46 0.079(12) 0.100(13) 0.109(15) -0.010(11) 0.017(11) 0.005(10)
C47 0.109(18) 0.15(2) 0.139(19) 0.040(17) 0.026(15) 0.006(15)
C48 0.072(15) 0.13(2) 0.23(3) 0.01(2) 0.04(2) 0.015(13)
C49 0.086(17) 0.125(18) 0.20(3) -0.03(2) 0.035(18) 0.026(13)
C50 0.077(13) 0.118(15) 0.112(14) -0.033(13) 0.036(11) -0.011(11)
C51 0.128(17) 0.155(18) 0.077(13) -0.003(12) 0.018(12) -0.056(14)
C52 0.19(3) 0.22(3) 0.15(2) 0.01(2) 0.06(2) -0.10(2)

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;
All esds (except the esd in the dihedral angle between two l.s.
planes)
are estimated using the full covariance matrix. The cell esds are
taken
into account individually in the estimation of esds in distances,
angles
and torsion angles; correlations between esds in cell parameters are
only
used when they are defined by crystal symmetry. An approximate
(isotropic)
treatment of cell esds is used for estimating esds involving l.s.
planes.
;

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Hg1 C25 2.099(15) . ?
Hg1 S1 2.372(4) . ?
Hg1 O1 2.622(7) . ?
Hg2 C51 2.131(18) . ?
Hg2 S3 2.380(4) . ?
Hg3 S2 2.326(4) . ?
Hg3 S4 2.328(4) . ?
Hg3 O1 2.617(7) . ?
S1 C1 1.768(12) . ?
S2 C10 1.766(13) . ?
S3 C27 1.771(13) . ?
S4 C36 1.785(13) . ?
P1 O1 1.492(7) . ?
P1 C19 1.796(13) . ?
P1 C2 1.820(12) . ?
P1 C11 1.821(12) . ?
P2 O2 1.502(9) . ?
P2 C45 1.787(15) . ?
P2 C28 1.831(13) . ?
P2 C37 1.832(12) . ?
Si1 C7 1.839(16) . ?
Si1 C8 1.850(15) . ?

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Si1 C9 1.878(16) . ?  
Si1 C6 1.883(14) . ?  
Si2 C18 1.830(15) . ?  
Si2 C17 1.866(16) . ?  
Si2 C16 1.894(15) . ?  
Si2 C15 1.898(13) . ?  
Si3 C34 1.820(16) . ?  
Si3 C35 1.855(18) . ?  
Si3 C33 1.861(15) . ?  
Si3 C32 1.871(15) . ?  
Si4 C44 1.836(16) . ?  
Si4 C42 1.869(16) . ?  
Si4 C43 1.878(16) . ?  
Si4 C41 1.913(14) . ?  
C1 C6 1.403(15) . ?  
C1 C2 1.426(16) . ?  
C2 C3 1.366(16) . ?  
C3 C4 1.376(18) . ?  
C4 C5 1.374(19) . ?  
C5 C6 1.410(18) . ?  
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C19 C24 1.366(16) . ?  
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C22 C23 1.36(2) . ?  
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C25 C26 1.56(2) . ?  
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C28 C29 1.379(17) . ?  
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C51 C52 1.39(2) . ?

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S1 Hg1 O1 81.23(19) . . ?  
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S2 Hg3 S4 169.45(13) . . ?  
S2 Hg3 O1 84.88(18) . . ?  
S4 Hg3 O1 99.79(17) . . ?  
C1 S1 Hg1 100.4(4) . . ?  
C10 S2 Hg3 97.9(4) . . ?  
C27 S3 Hg2 97.4(5) . . ?  
C36 S4 Hg3 96.9(4) . . ?  
O1 P1 C19 109.0(5) . . ?  
O1 P1 C2 110.7(5) . . ?  
C19 P1 C2 106.3(6) . . ?  
O1 P1 C11 116.1(5) . . ?  
C19 P1 C11 106.4(5) . . ?  
C2 P1 C11 107.8(6) . . ?  
O2 P2 C45 110.2(6) . . ?  
O2 P2 C28 110.4(6) . . ?  
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O2 P2 C37 118.9(5) . . ?  
C45 P2 C37 104.2(7) . . ?  
C28 P2 C37 104.4(6) . . ?  
C7 Si1 C8 112.8(9) . . ?  
C7 Si1 C9 109.2(8) . . ?  
C8 Si1 C9 104.7(8) . . ?  
C7 Si1 C6 110.6(6) . . ?  
C8 Si1 C6 111.9(7) . . ?  
C9 Si1 C6 107.4(7) . . ?  
C18 Si2 C17 108.7(7) . . ?  
C18 Si2 C16 111.1(8) . . ?  
C17 Si2 C16 106.0(7) . . ?  
C18 Si2 C15 108.8(6) . . ?  
C17 Si2 C15 107.9(7) . . ?  
C16 Si2 C15 114.2(6) . . ?  
C34 Si3 C35 107.6(8) . . ?  
C34 Si3 C33 112.3(8) . . ?  
C35 Si3 C33 107.5(9) . . ?  
C34 Si3 C32 111.8(7) . . ?  
C35 Si3 C32 107.7(8) . . ?  
C33 Si3 C32 109.8(7) . . ?  
C44 Si4 C42 107.0(8) . . ?  
C44 Si4 C43 108.3(8) . . ?  
C42 Si4 C43 112.7(8) . . ?  
C44 Si4 C41 107.2(7) . . ?  
C42 Si4 C41 110.5(7) . . ?  
C43 Si4 C41 110.9(7) . . ?  
P1 O1 Hg3 113.4(4) . . ?  
P1 O1 Hg1 122.7(4) . . ?  
Hg3 O1 Hg1 100.1(2) . . ?  
C6 C1 C2 119.6(11) . . ?  
C6 C1 S1 118.8(10) . . ?  
C2 C1 S1 121.5(9) . . ?  
C3 C2 C1 119.4(11) . . ?  
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C5 C4 C3 117.7(14) . . ?  
C4 C5 C6 123.4(13) . . ?  
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C1 C6 Si1 124.5(11) . . ?

C5 C6 Si1 118.3(10) . . ?  
 C11 C10 C15 120.2(11) . . ?  
 C11 C10 S2 121.6(10) . . ?  
 C15 C10 S2 118.1(10) . . ?  
 C12 C11 C10 120.2(11) . . ?  
 C12 C11 P1 119.3(9) . . ?  
 C10 C11 P1 120.5(10) . . ?  
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 C19 C20 C21 121.7(13) . . ?  
 C20 C21 C22 117.7(14) . . ?  
 C23 C22 C21 121.2(15) . . ?  
 C22 C23 C24 119.1(14) . . ?  
 C19 C24 C23 120.8(13) . . ?  
 C26 C25 Hg1 111.5(12) . . ?  
 C28 C27 C32 121.9(12) . . ?  
 C28 C27 S3 123.5(11) . . ?  
 C32 C27 S3 114.3(11) . . ?  
 C27 C28 C29 120.4(13) . . ?  
 C27 C28 P2 119.9(10) . . ?  
 C29 C28 P2 119.6(12) . . ?  
 C30 C29 C28 120.3(14) . . ?  
 C31 C30 C29 119.6(14) . . ?  
 C30 C31 C32 123.9(13) . . ?  
 C31 C32 C27 113.5(12) . . ?  
 C31 C32 Si3 119.5(11) . . ?  
 C27 C32 Si3 126.9(10) . . ?  
 C41 C36 C37 121.4(12) . . ?  
 C41 C36 S4 117.6(10) . . ?  
 C37 C36 S4 121.0(10) . . ?  
 C38 C37 C36 119.7(12) . . ?  
 C38 C37 P2 118.5(10) . . ?  
 C36 C37 P2 121.6(10) . . ?  
 C39 C38 C37 120.1(13) . . ?  
 C38 C39 C40 118.8(14) . . ?  
 C39 C40 C41 124.6(14) . . ?  
 C36 C41 C40 115.0(13) . . ?  
 C36 C41 Si4 123.2(11) . . ?  
 C40 C41 Si4 121.5(11) . . ?  
 C46 C45 C50 117.5(16) . . ?  
 C46 C45 P2 122.1(12) . . ?  
 C50 C45 P2 120.4(14) . . ?  
 C45 C46 C47 121.6(18) . . ?  
 C48 C47 C46 115(2) . . ?  
 C49 C48 C47 126(3) . . ?  
 C48 C49 C50 116(2) . . ?  
 C49 C50 C45 124.3(19) . . ?  
 C52 C51 Hg2 114.2(18) . . ?

_diffrn_measured_fraction_theta_max	0.999
_diffrn_reflns_theta_full	23.26
_diffrn_measured_fraction_theta_full	0.999
_refine_diff_density_max	2.341
_refine_diff_density_min	-2.059

\_refine\_diff\_density\_rms 0.143