

**Molecular characterization of the gas/particle interface of soot sampled from a  
diesel engine using a titration method**

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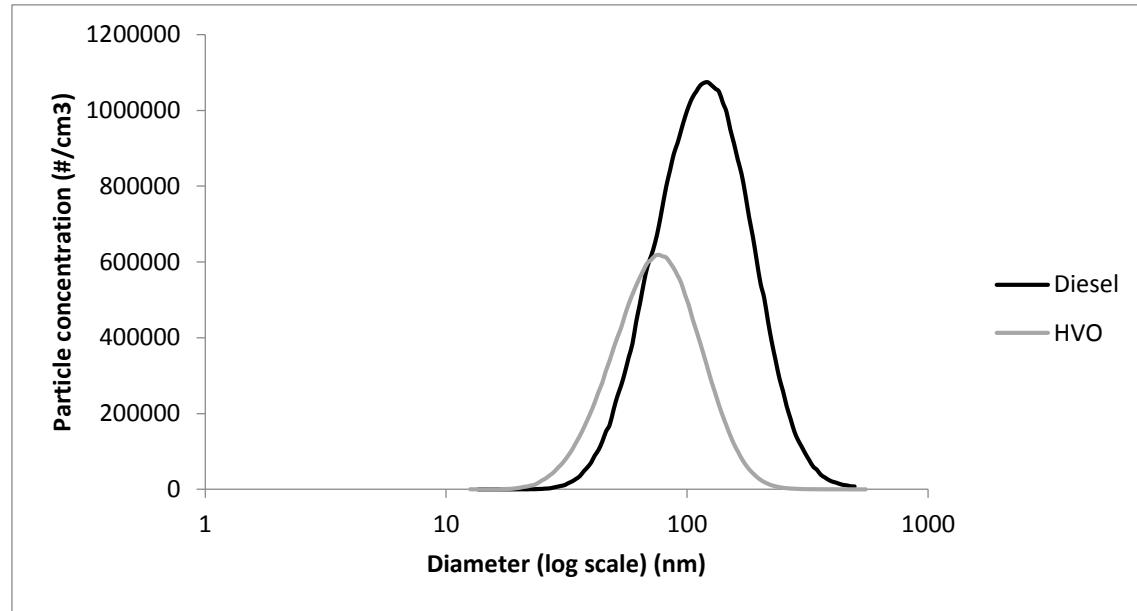
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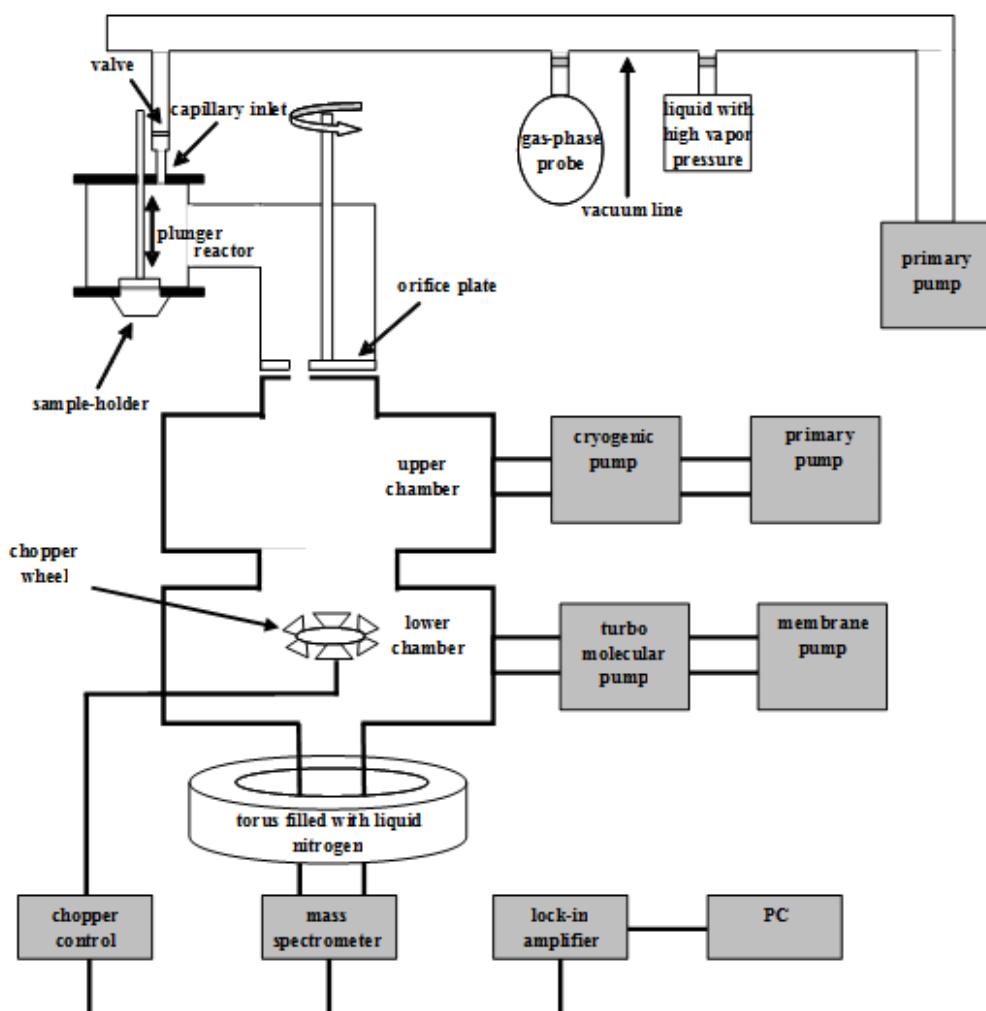
**Figure 1S.** Particle size distribution of the recovered diesel and HVO soot samples measured using a Scanning Mobility Particle Sizer (SMPS) device with Differential Mobility Analyser (DMA).

**Table 1S.** Parameters defining running conditions in the engine mode (U9) selected for the experiments.

Measured variables	Units	U9 Mode
Engine speed	rpm	1667
Effective torque	Nm	78
EGR Ratio	%	22-23
Air flow	kg/h	≈78
Start of main injection	°CA (aTDC)	5
Start of pilot injection	°CA (bTDC)	12.7
Fuel injected during pilot injection	µL/inj	1.86
Injection pressure	bar	660

**Table 2S.** Physico-chemical properties of pure fuels.

Properties	Diesel	HVO
Density at 15 °C / kg m <sup>-3</sup>	811	779.6
Viscosity at 40 °C / cSt	2	2.99
Lower heating value/ MJ kg <sup>-1</sup>	43.13	43.955
Lubricity (WS1.4) / µm	253	339.6
Cold filter plugging point / °C	-30	-21
Acid number / mgKOH g <sup>-1</sup>	0.16	0.056
Water content / mg kg <sup>-1</sup>	60	19.2
Cetane number	58.10	94.8
% C / wt.	85.74	84.68
% H / wt.	14.26	14.525
% O / wt.	0	0
Molecular formula	C <sub>13.39</sub> H <sub>26.72</sub>	C <sub>13.95</sub> H <sub>28.7</sub>
Molecular weight	187,4	196.1
Sulfur content / mg kg <sup>-1</sup>	< 10	<10

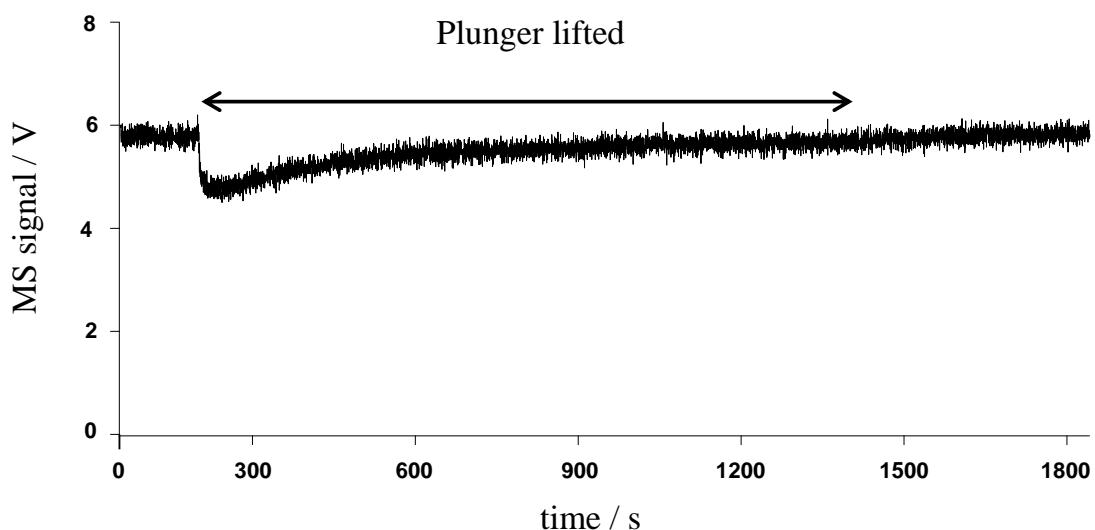


**Figure 2S.** Schematic drawing of the Knudsen flow reactor.

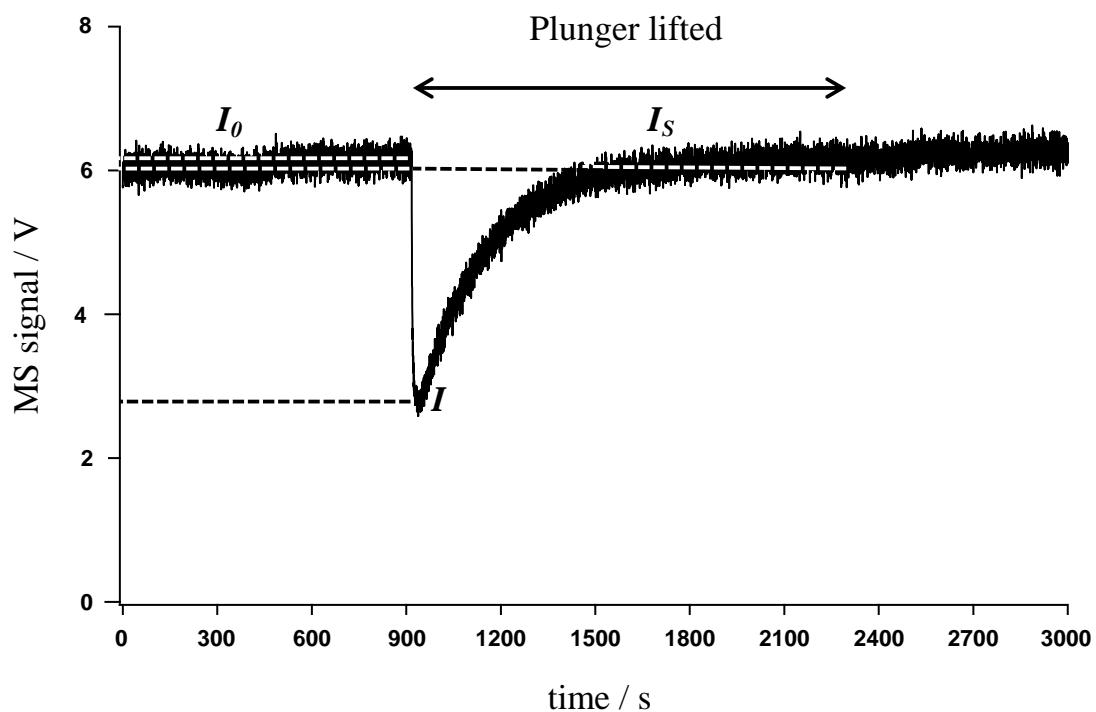
**Table 3S.** Knudsen flow reactor parameters for the 1 mm nominal diameter aperture.

Parameter	Value
Volume of the reactor	$V = 1830 \text{ cm}^3$
Estimated surface area of the reactor	$S = 1300 \text{ cm}^2$
Geometric surface area of the samples	$A_s = 10.75 \text{ cm}^2$
Escape orifice diameter	$\emptyset = 1 \text{ mm}$
Chopper frequency	225 Hz
Escape rate constant <sup>a</sup>	$k_{\text{esc}} = 0.0058 \sqrt{T/M} \text{ s}^{-1}$

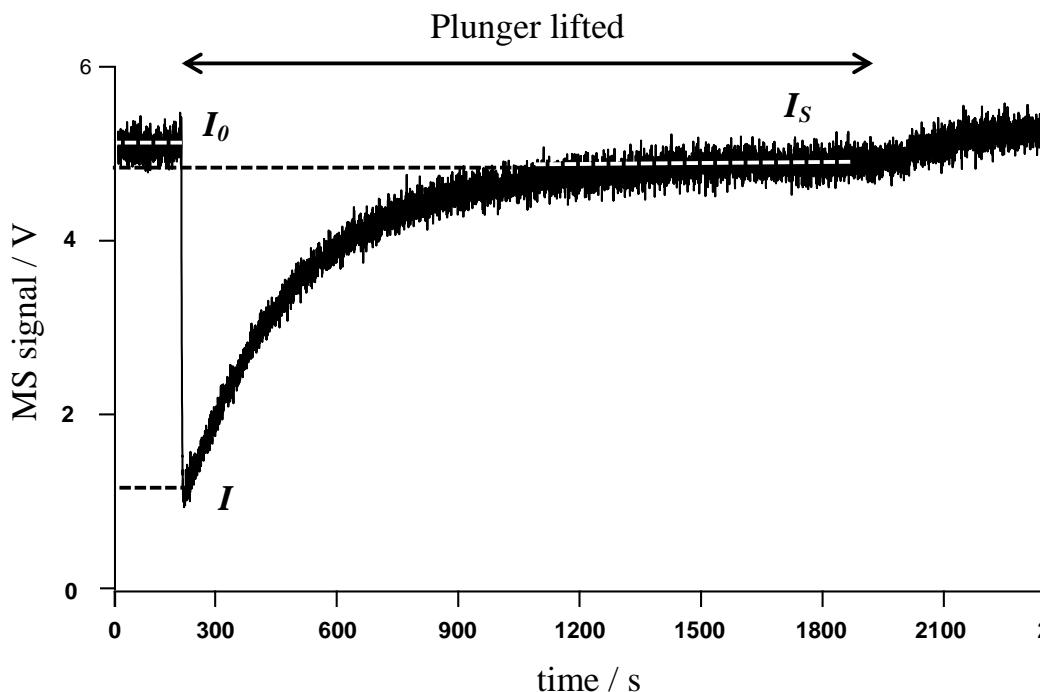
<sup>a</sup> T = temperature/K, M = molecular mass / g mol<sup>-1</sup>



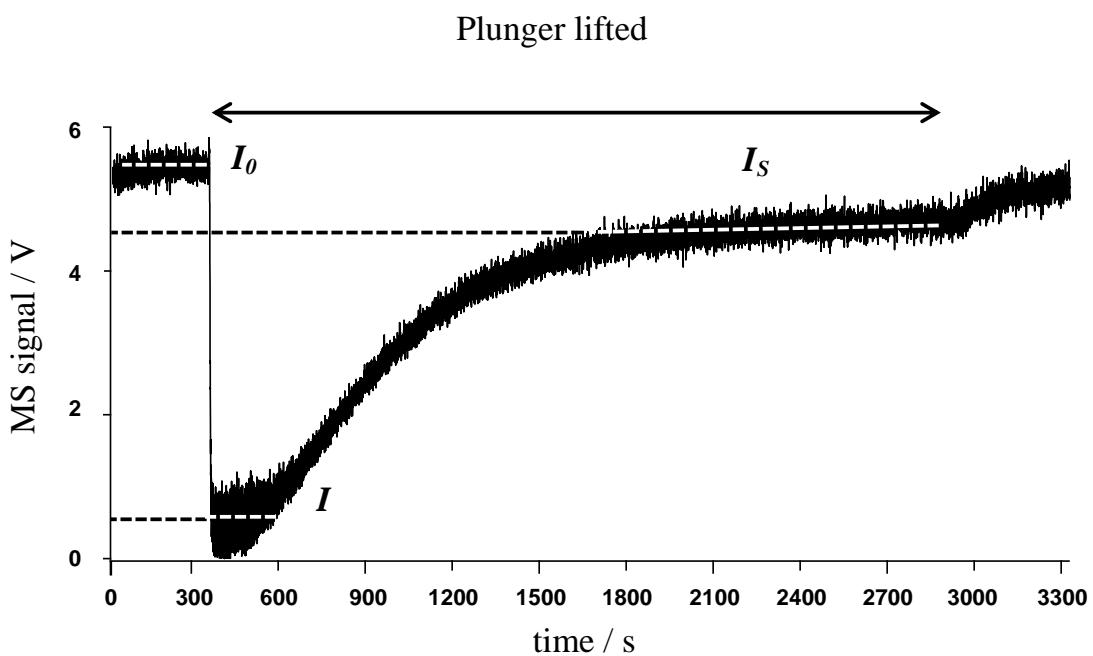
**Figure 3S.** Raw data of  $\text{NH}_2\text{OH}$  uptake on empty cup at a flow rate of  $2.95 \times 10^{15} \text{ molecule s}^{-1}$  monitored at m/z 33 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0173 \text{ s}^{-1}$ ).



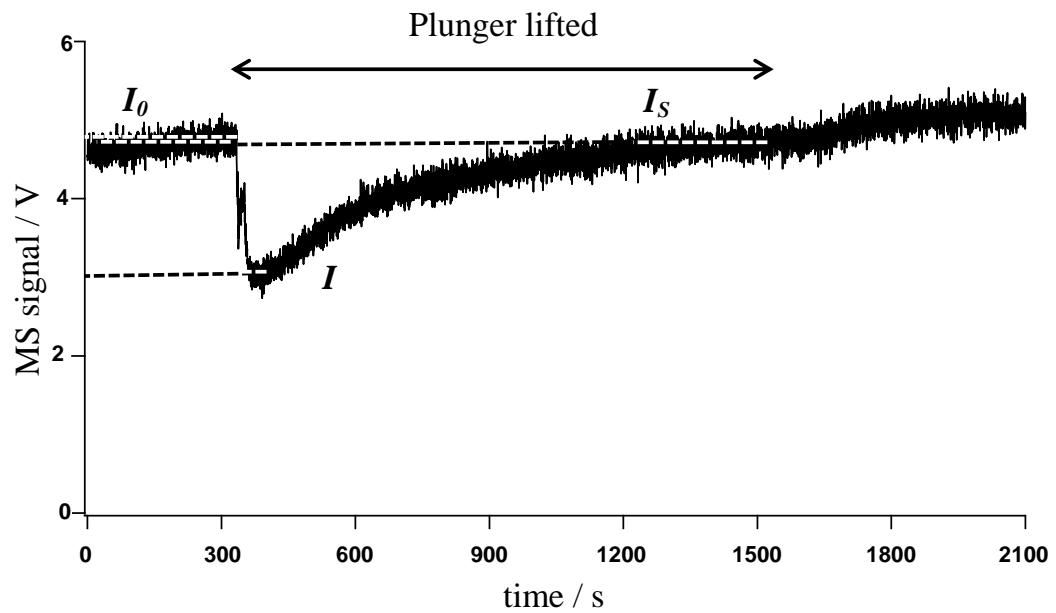
**Figure 4S.** Raw data of  $\text{N}(\text{CH}_3)_3$  uptake on 16.02 mg PRINTEX XE2-B soot at a flow rate of  $3.41 \times 10^{15}$  molecule  $\text{s}^{-1}$  monitored at  $\text{m/z}$  58 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.013 \text{ s}^{-1}$ ) leading to the initial uptake coefficient  $\gamma_0 = 3.37 \times 10^{-4}$ .



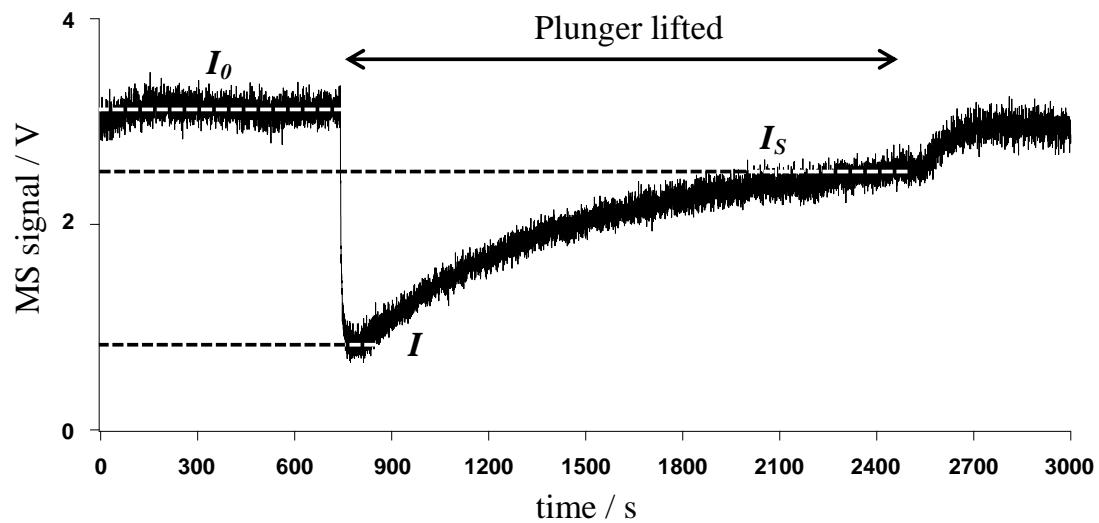
**Figure 5S.** Raw data of  $\text{NH}_2\text{OH}$  uptake on 20.71 mg Diesel soot at a flow rate of  $6.07 \times 10^{15}$  molecule  $\text{s}^{-1}$  monitored at  $\text{m/z}$  33 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0173 \text{ s}^{-1}$ ) leading to the initial uptake coefficient  $\gamma_0 = 1.02 \times 10^{-3}$ .



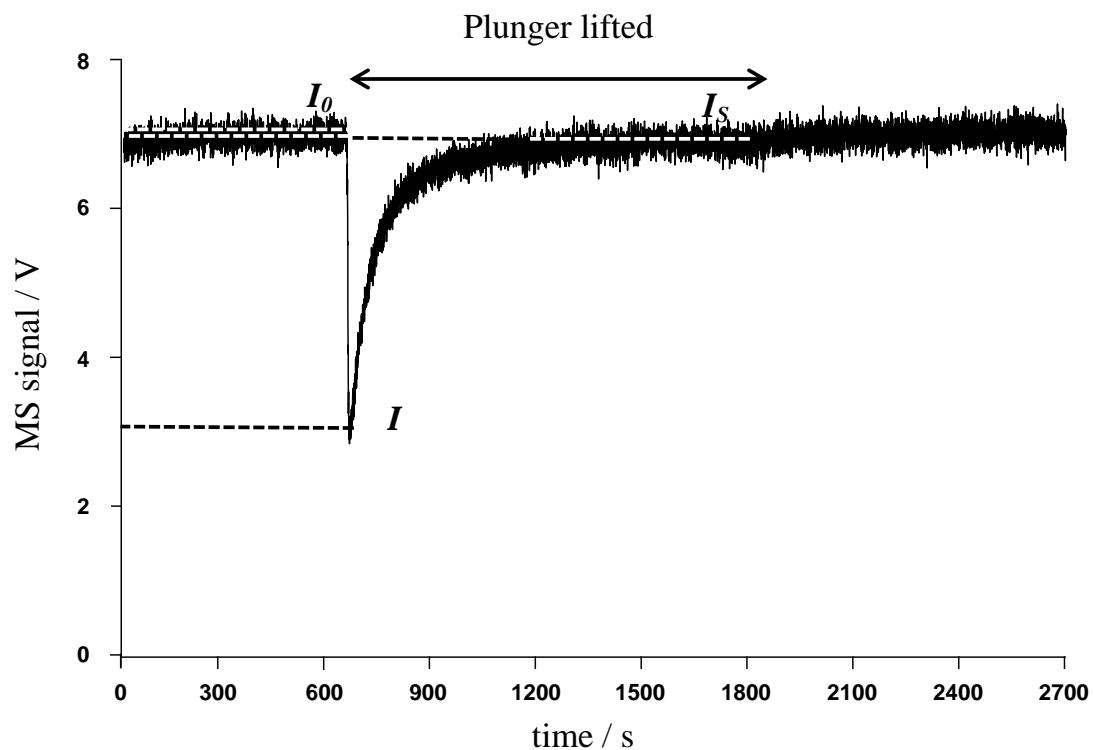
**Figure 6S.** Raw data of  $\text{NH}_2\text{OH}$  uptake on 16.13 mg HVO soot at a flow rate of  $2.90 \times 10^{15}$  molecule  $\text{s}^{-1}$  monitored at  $\text{m/z}$  33 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0173 \text{ s}^{-1}$ ) leading to the initial uptake coefficient  $\gamma_0 = 4.40 \times 10^{-3}$ .



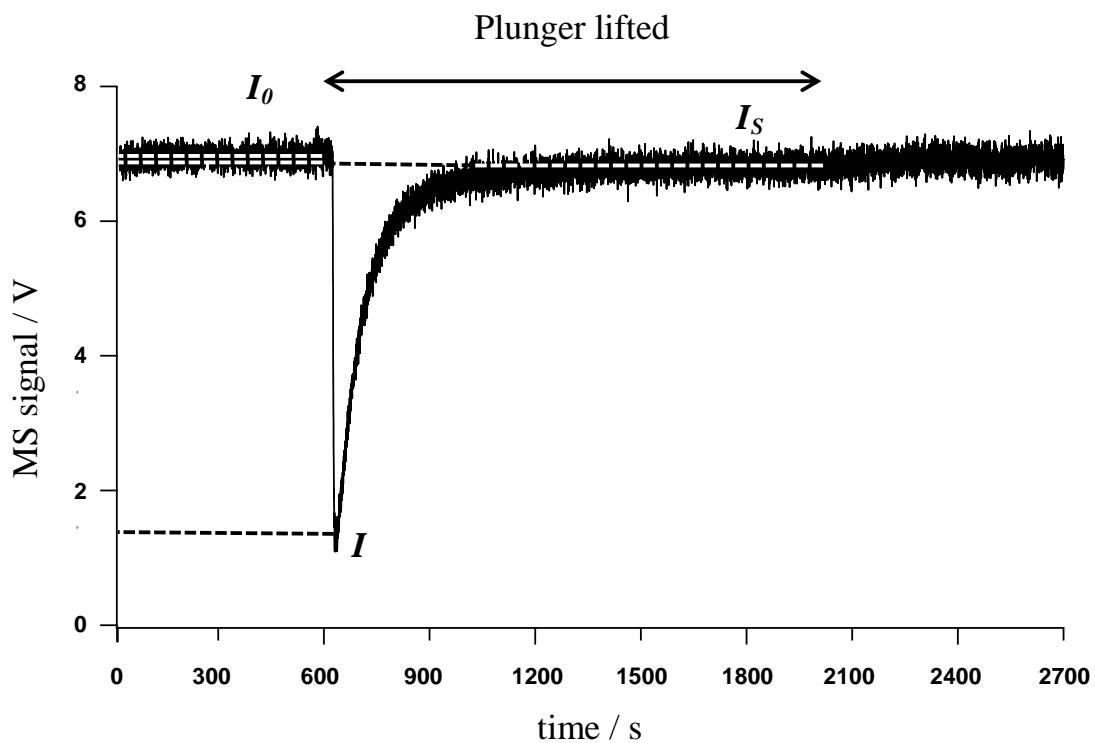
**Figure 7S.** Raw data of  $\text{NH}_2\text{OH}$  uptake on 10.38 mg PRINTEX XE-B soot at a flow rate of  $6.15 \times 10^{15}$  molecule  $\text{s}^{-1}$  monitored at  $m/z$  33 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0173 \text{ s}^{-1}$ ) leading to the initial uptake coefficient  $\gamma_0 = 1.58 \times 10^{-4}$ .



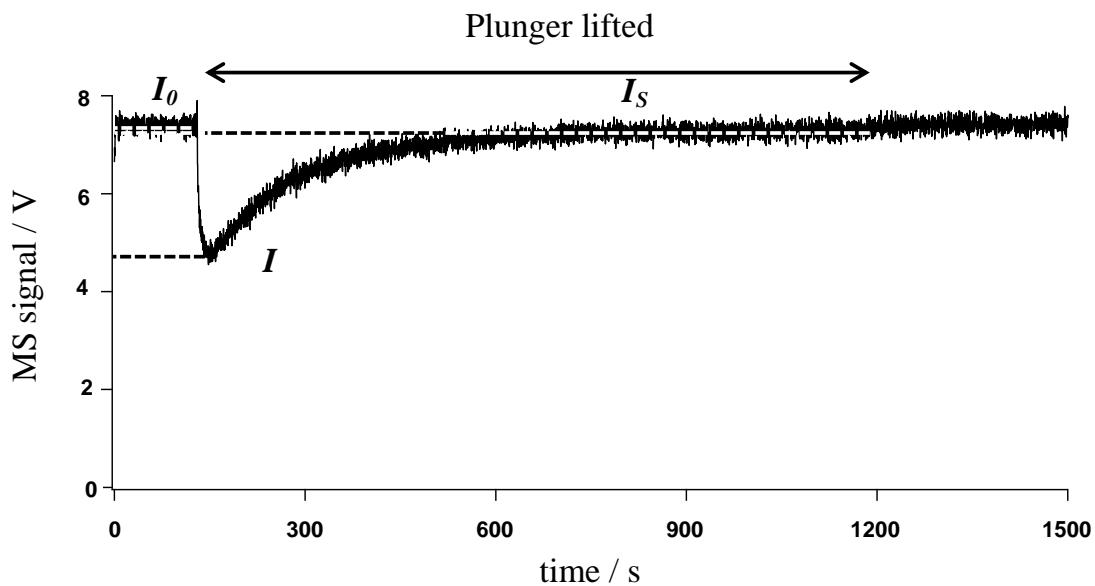
**Figure 8S.** Raw data of  $\text{CF}_3\text{COOH}$  uptake on 15.15 mg PRINTEX XE-B soot at a flow rate of  $2.93 \times 10^{15}$  molecule  $\text{s}^{-1}$  monitored at  $m/z$  69 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0093 \text{ s}^{-1}$ ) leading to the initial uptake coefficient  $\gamma_0 = 7.86 \times 10^{-4}$ .



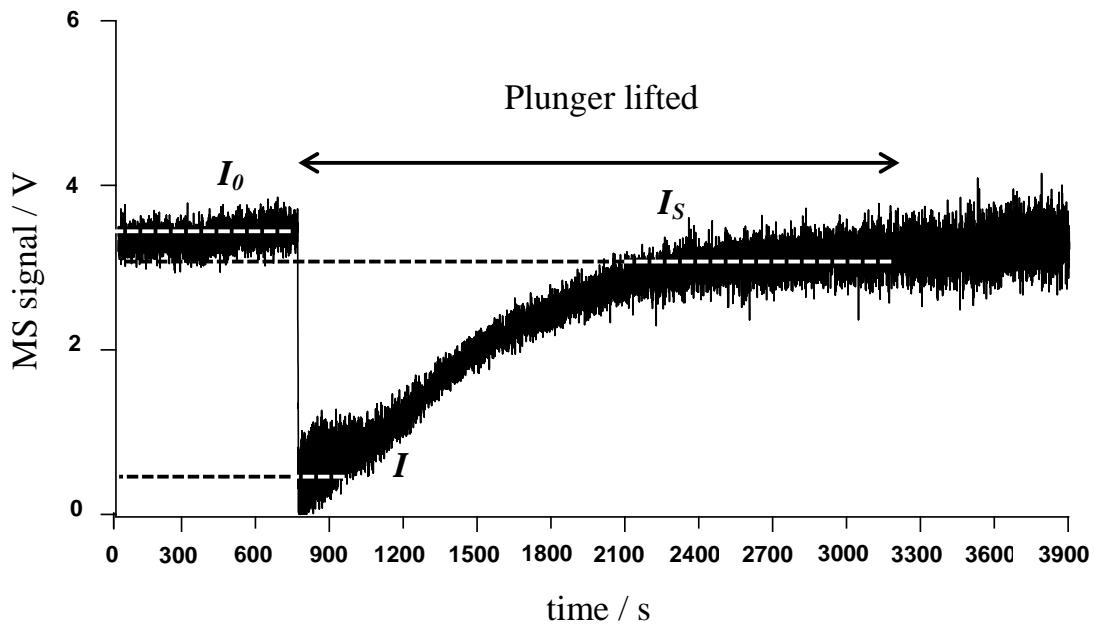
**Figure 9S.** Raw data of HCl uptake on 10.5 mg Diesel soot at a flow rate of  $4.66 \times 10^{15}$  molecule s<sup>-1</sup> monitored at m/z 36 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0165$  s<sup>-1</sup>) leading to the initial uptake coefficient  $\gamma_0 = 3.52 \times 10^{-4}$ .



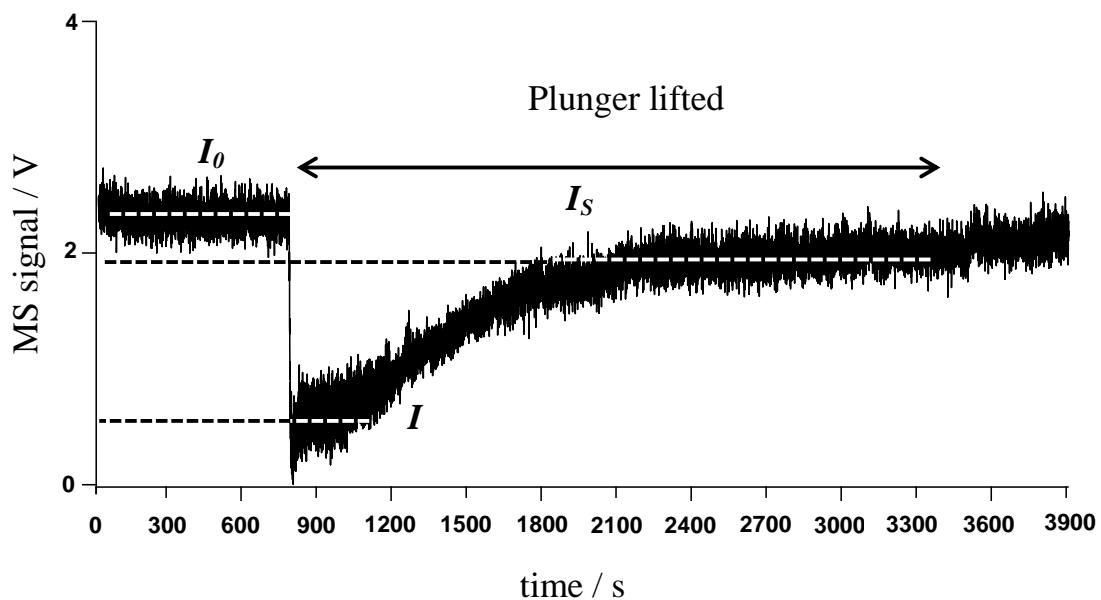
**Figure 10S.** Raw data of HCl uptake on 10.6 mg HVO soot at a flow rate of  $4.48 \times 10^{15}$  molecule s<sup>-1</sup> monitored at m/z 36 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0165$  s<sup>-1</sup>) leading to the initial uptake coefficient  $\gamma_0 = 1.25 \times 10^{-3}$ .



**Figure 11S.** Raw data of HCl uptake on 15.55 mg PRINTEX XE-B soot at a flow rate of  $5.32 \times 10^{15}$  molecule s<sup>-1</sup> monitored at m/z 36 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0165$  s<sup>-1</sup>) leading to the initial uptake coefficient  $\gamma_0 = 1.48 \times 10^{-4}$ .



**Figure 12S.** Raw data of  $\text{NO}_2$  uptake on 16.4 mg Diesel soot at a flow rate of  $1.13 \times 10^{16}$  molecule  $\text{s}^{-1}$  monitored at  $m/z$  46 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.0167 \text{ s}^{-1}$ ) leading to the initial uptake coefficient  $\gamma_0 = 3.56 \times 10^{-3}$ .



**Figure 13S.** Raw data of  $\text{NO}_2$  uptake on 11.85 mg HVO soot at a flow rate of  $8.36 \times 10^{15}$  molecule  $\text{s}^{-1}$  monitored at  $m/z$  46 in the 1 mm diameter aperture Knudsen flow reactor ( $k_{\text{esc}} = 0.010 \text{ s}^{-1}$ ) leading to the initial uptake coefficient  $\gamma_0 = 6.16 \times 10^{-4}$ .