

# **SUPPORTING INFORMATION**

## **Modeling the global fate and transport of perfluorooctanoic acid (PFOA) and perfluorooctanoate (PFO) emitted from direct sources using a multi-species mass balance model**

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## S1. Distribution ratio approach

The distribution ratio approach calculates a weighted-average of the partition coefficients of each species of the molecule for a given physical-chemical property. The weighted-average is based on the ratio of ionic to nonionic forms of the substance, estimated using the Henderson-Hasselbalch relationship so that,

$$Ratio = 10^{[pH(i) - pKa]} \quad (S1)$$

where pH(i) is the pH of the environmental media. The distribution of PFO(A) in aqueous media (e.g. organic carbon-water partitioning) is then calculated using the partition coefficients of both species as follows.

$$D_{OC}^{PFO(A)} = \frac{1}{1 + Ratio} K_{OC}^{PFOA} + \frac{Ratio}{1 + Ratio} K_{OC}^{PFO} \quad (S2)$$

where  $D_{OC}^{PFO(A)}$  is the effective  $K_{OC}$  considering the relative presence of both forms of the compound and  $K_{OC}^{PFOA}$  and  $K_{OC}^{PFO}$  are the  $K_{OC}$ s of the neutral and anionic form respectively. The effective  $K_{AW}$  of PFO(A) was calculated using only the  $K_{AW}$  of the neutral form (PFOA) since the  $K_{AW}$  of PFO was assigned a negligible value:

$$D_{AW}^{PFO(A)} = \frac{1}{1 + Ratio} K_{AW}^{PFOA} \quad (S3)$$

This expression reflects the influence of the ionized species which acts to increase the affinity of the substance for the water phase. PFO does not directly volatilize to the atmosphere in this model, however neutral molecules which volatilize into the atmosphere and partition to non-gaseous phases (e.g. rain, aerosols) can be deprotonated to yield the anion. So, for example, the concentration of PFO in rain is a function of the concentration of PFOA in the gas phase, the  $K_{AW}$  of PFOA (partitioning of PFOA into

rain water) and the ratio of PFO:PFOA (reflecting the equilibrium between ionized and neutral form).

## **S2. Surface ocean exchange (lateral)**

The representation of surface ocean exchange in BETR-Global was updated to incorporate data from global drift buoy arrays now available on a 1 x 1° resolution from NOAA (1), [www.aoml.noaa.gov/phod/dac/drifter\\_climatology.html](http://www.aoml.noaa.gov/phod/dac/drifter_climatology.html). The drift buoys consist of a surface and subsurface float attached to a “holey sock” drogue which is centred at a depth of 15 m. The mean current velocity data recorded by these devices reflects the sum of the Ekman (i.e. wind-driven or ageostrophic component) and underlying geostrophic component of the flow but is only representative of the sampling depth (i.e. 0 – 15 m). However, it is possible to decompose the mean surface current velocities into the Ekman/ageostrophic and geostrophic velocity components, as demonstrated in (1). Since the surface flow (Ekman + geostrophic) and geostrophic flow represent upper and lower boundary conditions (Lumpkin R, pers. commun), it is possible to estimate the near-surface current velocities at a given depth as long as the decay in the Ekman component is accounted for. The NOAA website provides mean current velocities (m s<sup>-1</sup>) for the north-south and east-west components which are presented as a surface velocities (total, 0 – 15 m) and Ekman-removed velocities. Screened data are available for latitude 60°N to 70°S.

The Ekman layer depth ( $D_E$ , in m) was estimated using the following simplified equation:

$$D_E = \frac{7.12}{\sqrt{\sin \vartheta}} U_{10} \quad (\text{S4})$$

1 where  $\vartheta$  is the absolute value of latitude (for  $|\vartheta| > 10^\circ$ ) and  $U_{10}$  is the mean wind speed  
 2 ( $\text{m s}^{-1}$ ). Mean wind speed for each BETR-Global region was estimated using data from  
 3 the NCEP/NCAR reanalysis ([www.cdc.noaa.gov/cdc/data.ncep.reanalysis.derived.html](http://www.cdc.noaa.gov/cdc/data.ncep.reanalysis.derived.html))  
 4 over the period 1948 – 2006. The mixed layer depth (MLD) in the model was set to 100  
 5 m for all model regions except regions 1 – 48 and 241 – 288 (MLD = 200 m). For depths  
 6 0 – 15 m, the surface current velocities can be used directly while the Ekman-removed  
 7 current velocities can be used directly for depth  $D_E$  – 100 m. To simplify the  
 8 calculations, the Ekman-component was assumed to decay linearly with depth below 15  
 9 m and become negligible at the  $D_E$ . From this assumption, the mean current velocity  
 10 over depth 15 –  $D_E$  m is simply the average of the surface current velocity and the  
 11 Ekman-removed current velocity (see Figure S1). The overall mean current velocity for  
 12 the entire 100 m is then the depth-weighted average of the three values.

0 – 15 m	Ageostrophic + geostrophic current velocity (i.e. surface current velocities)
15 - $D_E$ m	Assume linear decay of ageostrophic component over depth 15 – $D_E$ m  Average current velocity over 15 – $D_E$ m is simply the average of (ageostrophic + geostrophic) and (geostrophic ONLY).
$D_E$ – 100 m	Geostrophic current velocity ONLY (i.e. Ekman-removed current velocities)

13  
 14  
 15 **Figure S1.** Schematic representation of utilization of mean current velocities taken from  
 16 the global drift buoy array.

1  
2 Mean current velocities for latitudes and longitudes representing the borders between  
3 regions were extracted from the database. For example, the north/south mean current  
4 velocities ( $\text{m s}^{-1}$ ) for region 82/58 (see Figure S2) are represented by the data at  $45^\circ\text{N}$   
5 between  $45 - 30^\circ\text{W}$ . The overall mean current velocity for each  $1^\circ$  was then multiplied  
6 by the assumed mixed layer depth (m) and the horizontal distance represented by the  $1^\circ$   
7 (m) to arrive at a volumetric flow rate ( $\text{m}^3 \text{s}^{-1}$ ). The use of the data in this way results in a  
8 representation of time-averaged advective flows. Since the surface ocean compartments  
9 were assumed to be well-mixed boxes (over  $15 \times 15^\circ$ ), the eddy kinetic energy of the  
10 ocean was not included as an additional diffusive transport term. The assumption of  
11 well-mixed boxes introduces a bias in the sense that emissions entering a given box are  
12 instantaneously distributed across the entire geographic region. This assumption results  
13 in dilution of the initial source strength and precludes estimation of transport times of a  
14 pulse of contaminant. The resulting bias in modeled concentrations in receptor regions  
15 (i.e. far-field) is particularly evident for short-term simulations but is reduced  
16 substantially as the length of simulation increases (2).

17  
18 Since drift buoy data were lacking or deemed unreliable, the surface ocean exchange in  
19 the Arctic region of the model (regions 1 – 48, see Figure S2) was based on estimates of  
20 water inflows/outflows (3, 4), consideration of available Arctic Ocean models (5 – 7),  
21 and basic information about the distribution of Pacific and Atlantic-sourced water in this  
22 region (8 – 12). Li et al. (5) developed and applied the Arctic Mass Balance Box Model  
23 (AMBBM) to model the fate and transport of  $\alpha$ -HCH in the Arctic Ocean. AMBBM

1 divides its 'Arctic Ocean' (defined as waters above 65°N, excluding Baffin Bay, Hudson  
2 Bay, the Bering Sea, the Norwegian Sea and the Greenland Sea) into two domains, the  
3 North American Arctic Ocean (NAAO) and the Eurasian Arctic Ocean (EAO). The  
4 NAAO included waters north of the Bering Strait and 50°W – 180°W whereas the EAO  
5 comprised the rest of the surface ocean domain. The NAAO corresponds roughly to  
6 BETR-Global regions 1 – 8 and 25 – 32 and is expected to be strongly dominated by  
7 waters of Pacific origin over the depth of 0 – 200 m (8, 11). BETR-Global regions 13 –  
8 22, 37 – 46 were assumed to be strongly influenced by waters of Atlantic origin only  
9 whereas regions 9 – 12 and 23, 24, 47 and 48 were assumed to be transitional regions (i.e.  
10 mixed influence). Flow through the Bering Strait is the most well-known exchange rate  
11 and has been estimated in the range of 0.6 – 1 Sv (13). In the BETR-Global model, a  
12 value of 0.8 Sv was selected as the default flow from region 49 to region 25. Northward  
13 flowing waters from the North Atlantic into the Arctic Ocean are not as well-  
14 characterized and estimates vary substantially (e.g. see 3). Atlantic water can enter the  
15 Arctic Ocean via the Fram Strait and the Barents Sea (9, 14) and there is some debate  
16 over the relative importance of these two routes (7). Using a coupled ice-ocean model of  
17 the pan-Arctic region configured at a resolution of 1/12 x 1/12° and 45 depth-levels,  
18 Maslowski et al. (7) estimated mean gross flows (1979 – 2001) into the Arctic Ocean of  
19 6.4 Sv through the Fram Strait and 5.9 Sv through the Bear Island Trough into the  
20 Barents Sea for the entire depth of the water column. Since BETR-Global explicitly  
21 considers only the upper 200 m, the gross northbound flow via the Fram Strait (region 36,  
22 37 to region 12, 13) was assumed to be ~ 4.5 Sv while the gross eastbound flow into the  
23 Barents Sea (region 38 eastwards to 39) was assumed to be ~ 3.5 Sv. These volumetric

flows correspond to average current velocities of  $\sim 0.05$  and  $0.03 \text{ m s}^{-1}$  respectively. The most important gross outflow estimated by Maslowski et al. (7) was  $\sim 9 \text{ Sv}$  via the Fram Strait. This flow was represented in BETR-Global by southward flow across regions 12 and 13 of  $\sim 7 \text{ Sv}$  (upper 200 m only) while the gross flow into the Barents Sea was countered by a reverse flow (region 39 to 38) yielding a net inflow of  $\sim 2.5 \text{ Sv}$ . Due to the spatial resolution of the model, it was problematic to represent ocean circulation within the Arctic Ocean with a great degree of fidelity. Woodgate et al. (15) estimated mean boundary current velocities in the range of  $1 - 5 \text{ cm s}^{-1}$  in 1995 – 96 in the Eurasian Basin over the depths sampled (1700 m) with mean flow of  $2 - 6 \text{ cm s}^{-1}$  and episodic currents up to  $40 \text{ cm s}^{-1}$  measured in the upper water column (at 100 m depth). However, it is difficult to use this information directly. As discussed earlier though, the surface layer of the Arctic Ocean can be crudely represented as two distinct domains, one primarily influenced by Pacific-inflow via the Bering Strait and the other primarily influenced by Atlantic-inflow. Flow between the individual regions can then be estimated as a function of ocean horizontal eddy diffusivity, as was done to derive the surface ocean exchange regime in GloboPOP (16). GloboPOP used the following equation to estimate volumetric exchanges.

$$G_{ij} = \frac{K_X}{L} A_E \quad (\text{S5})$$

where  $G_{ij}$  is the volumetric flow between region  $i$  and  $j$  ( $\text{m}^3 \text{ s}^{-1}$ ),  $K_X$  is the horizontal eddy diffusivity ( $\text{m}^2 \text{ s}^{-1}$ ),  $L$  is the path length (m) and  $A_E$  is the area of exchange ( $\text{m}^2$ ), which is calculated as a function of mixed layer depth (m) and the length of the surface ocean water interface between the two regions (m). Based on empirical observations, Stewart (17) presented the following equation to estimate  $K_X$ .

$$K_x = UL \quad (S6)$$

where  $K_x$  is the horizontal eddy diffusivity ( $\text{m}^2 \text{s}^{-1}$ ),  $U$  is a constant ( $0.01 \pm 0.005 \text{ m s}^{-1}$ ) and  $L$  is the path length (m). This expression appears to be valid for  $L$  ranging from 10 – 1500 km. For BETR-Global,  $L$  can be calculated as the square root of the total surface ocean water area ( $\text{m}^2$ ) which varies by latitude and % of the region that is covered by ocean water. However, since  $L$  cancels out in Equation S5,  $U$  can be viewed as a mass transfer coefficient ( $\text{L T}^{-1}$ ) suggesting an effective water velocity of  $0.5 - 1.5 \text{ cm s}^{-1}$ . The volumetric flow is then a function of this MTC and the area of exchange. To derive the flow regime for this region of the BETR-Global model, a MTC of  $1 \text{ cm s}^{-1}$  was initially assumed for exchange between regions in all directions. Flow between regions representing the boundary of the NAAO and EAO (e.g. region 22, 23) were reduced ( $U \sim 0.1 \text{ cm s}^{-1}$ ). In this way, contaminants are distributed through the NAAO and EAO without becoming well-mixed over the time period of the simulation. Where data were available, flows through certain regions (e.g.  $\sim 2 \text{ Sv}$  through the Canadian Archipelago, Prinsenberg, S.J. (18); Davis Strait,  $\sim 2 \pm 1.0 \text{ Sv}$  northward,  $4.6 \pm 1.1 \text{ Sv}$  southward, Cuny et al., (19)) were represented as well as possible.

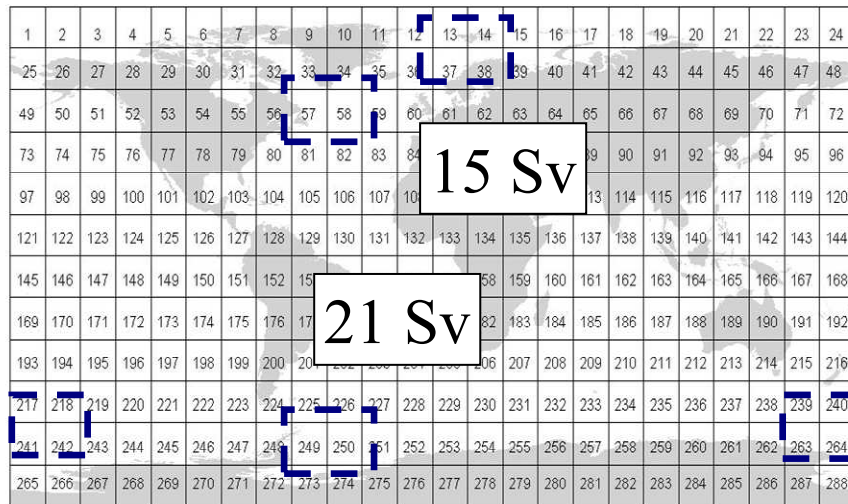
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### 18 **S3. Deep water formation**

Deep water formation was represented by including the estimated sinking fluxes provided by Lohmann et al. (20). The data from Lohmann et al. was also compared to information provided in Kahana et al. (21). The regions considered by Lohmann et al. (20) to have relevant deep water formation were the Norwegian Sea ( $68^\circ\text{N} - 80^\circ\text{N}$ ,  $0 - 25^\circ\text{E}$ ,  $10 \text{ Sv}$ , where  $1 \text{ Sv} = 10^6 \text{ m}^3 \text{s}^{-1}$ ), the Labrador Sea ( $50^\circ\text{N} - 60^\circ\text{N}$ ,  $60^\circ\text{W} - 40^\circ\text{W}$ ,  $5 \text{ Sv}$ ), the



1 Weddell Sea (60°S – 85°S, 70°W – 20°W, 11 Sv ) and the Ross Sea (60°S – 80°S, 170°E –  
2 155°W, 10 Sv). The total sinking fluxes were apportioned to the corresponding BETR-  
3 Global regions (see Figure S2). For all other BETR-Global regions, the default surface –  
4 deep water exchange mass transfer coefficients ( $\text{m h}^{-1}$ ) from GloboPOP (16) for the  
5 appropriate latitudinal band were used. These MTCs are multiplied by the surface area of  
6 the ocean compartment ( $\text{m}^2$ ) to arrive at a volumetric exchange rate. Based on these  
7 assumptions, the mixing time of the deep ocean (estimated from total ocean surface area  
8 and assumed average deep ocean depth of 3600 m) due to surface-deep water exchange  
9 was  $\sim 650$  years, in agreement with published estimates (500 – 1500 years, see  
10 Johanneson & Burdige (22))



11 **Figure S2.** Regions with enhanced surface-deep water exchange as suggested by  
12 Lohmann et al (20).  
13

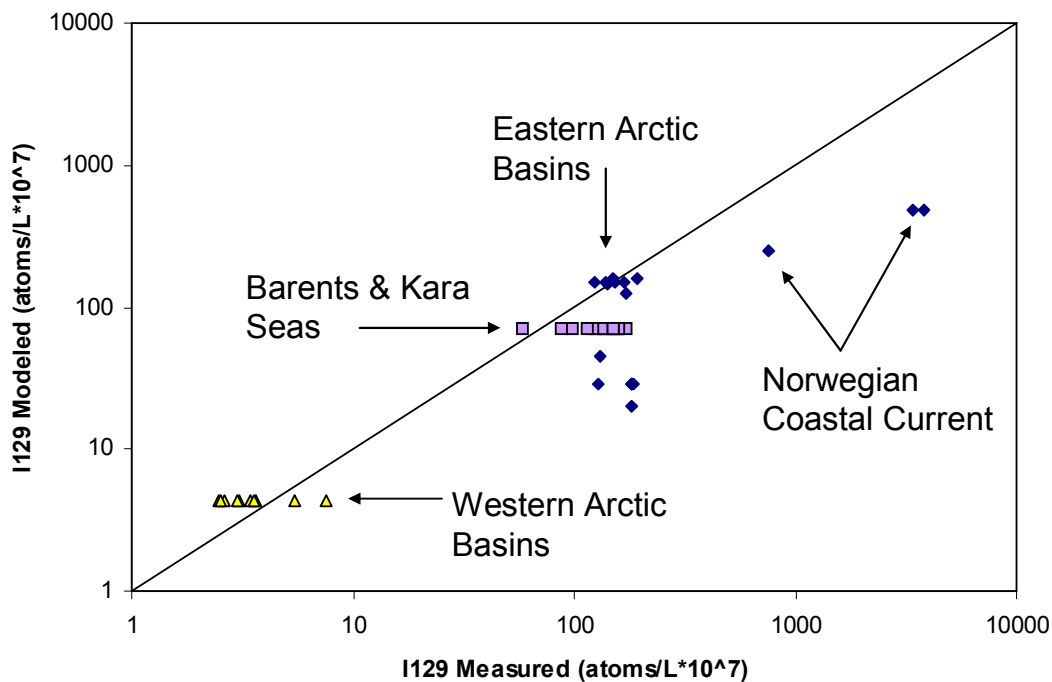
14 Once all horizontal and vertical flows were estimated, it was important to ensure that a  
15 water mass balance was established (i.e. water flow in = water flow out). The median  
16 ratio of water in:water out based on the drift buoy data for the model domain was 0.95

(IQR = 0.75 – 1.21). To obtain a complete mass balance, the iterative algorithm proposed by Woodfine et al. (23) was adapted for use with the BETR-Global flow matrices. In this procedure, the proportion of flow in each direction is calculated using the input flow regime. These proportions are held constant and then total volume fluxes across the entire flow matrix are adjusted to arrive at a complete water mass balance. The average adjustment factor for the Arctic Ocean regions was 1.4 while the overall average adjustment factor for the entire flow regime was 1.5. While in some cases the flows may have increased/decreased more substantially, the general features of the flow regime are maintained and the more serious error related to water mass imbalances is eliminated.

#### **S4. Preliminary Model Simulations**

Since it was unclear whether the simplified exchange regime adequately captured the desired features, in particular the domains of Atlantic and Pacific-influence, the model was evaluated in two ways. First, the long-term fate and transport of iodine-129 (I-129) into the Arctic Oceans from sources in the North Sea was used to test the reasonableness of the surface ocean exchange parameterization. Alfimov et al. (6) modeled the fate and transport of I-129 into the Arctic Ocean over the period 1950 – 2010 using a modified version of the ANWAP RAIG model (13). I-129 is emitted from two nuclear reprocessing facilities at Sellafield, UK and La Hague, France. Since these locations were outside the model domain, Alfimov et al. (6) generated an emission function for the Norwegian Sea which accounts for the time delay for transport from source to this region. This emission function was used as the source term for the BETR-Global simulations and was directed into region 37 (see Figure S2). Modeled concentrations in the Arctic

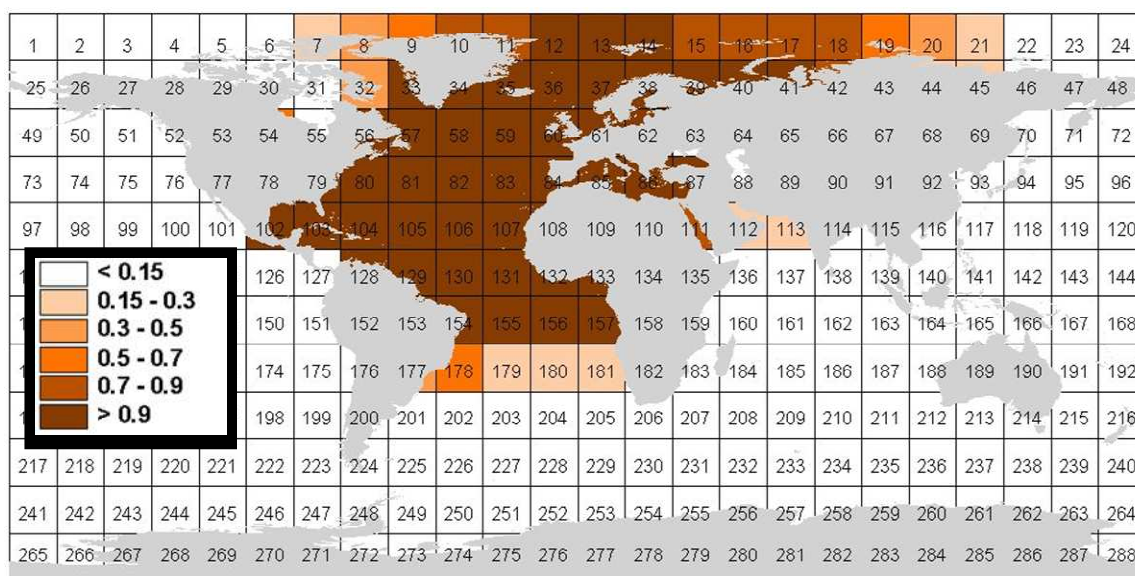
regions of the model were compared to observations (24, 25) in different locations of the Arctic (e.g. Western Arctic Basins, Eastern Arctic Basins, Barents Sea) from 1993 and 2001 (see Figure S3).



**Figure S3.** Modeled (BETR-Global) versus observed concentrations of I-129 in 1993 (Western Arctic Basins, Barents & Kara Seas) and 2001 (Norwegian Coastal Current, Eastern Arctic Basins)

Transport of Atlantic-sourced I-129 to Western Arctic Basin surface water (0 – 200 m) is known to be limited (14, 24). This feature of Arctic Ocean circulation appears to be well-represented by the BETR-Global model. There is also good agreement overall between modeled and observed concentrations in the Barents Sea and Eastern Arctic Basins. Concentrations in the Norwegian Coastal Current are under-predicted but this result is not surprising since all ocean regions are assumed to be well-mixed (hence diluting the emissions which might otherwise be largely entrained in a smaller volume of water).

1 Another series of model simulations were conducted using the single-species version of  
 2 BETR-Global and the physical-chemical properties of the anion only. Here, emissions  
 3 from each major source region (Europe/Russia, North America, Asia; see section S5)  
 4 were simulated separately. These simulations allow the contribution of each source  
 5 region to the total modeled concentration in every region to be assessed. For the Arctic  
 6 region of the model (regions 1 – 48), these simulations give an indication of the extent to  
 7 which emissions from North America and Europe contaminate the various regions of the  
 8 Arctic Ocean. Simulations were conducted from 1950 – 2010 and model results for 2005  
 9 are presented in Figure S4.



10  
 11 **Figure S4.** Contribution (%) to total modeled concentrations in the surface ocean  
 12 compartment from North American + Europe emissions. The contribution from Asian  
 13 sources is equal to  $[1 - (\text{the displayed values})]$ .  
 14  
 15 As shown in Figure S4, emissions from North American and Europe/Russia are largely  
 16 confined to what would be considered the Eastern Arctic Ocean (EAO) in AMBBM  
 17 developed by Li et al. (5). Overall, these model simulations confirm that the desired

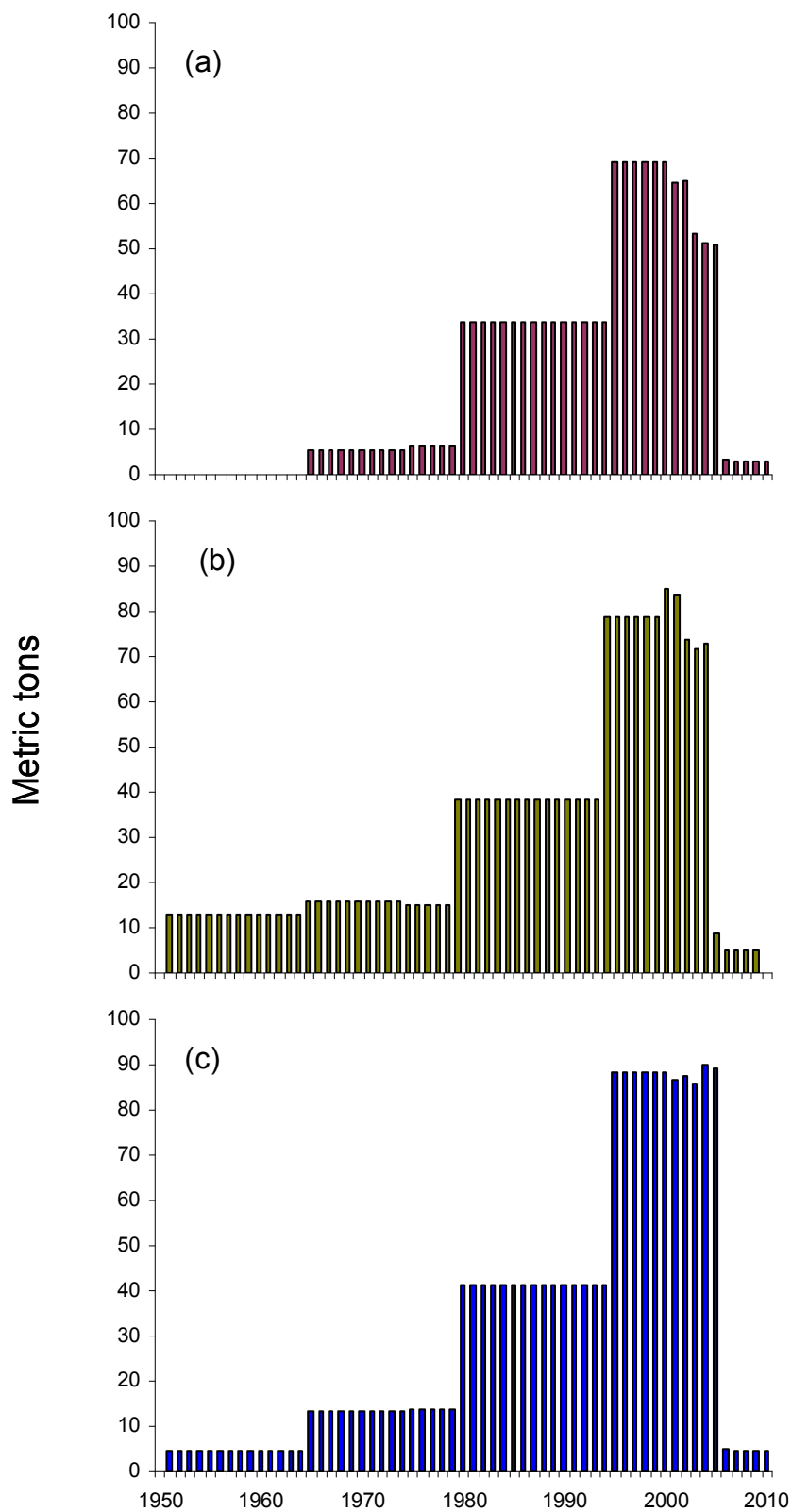
features of ocean circulation within the Arctic Ocean are broadly represented, given the coarse resolution of the model.

## **S5. Supporting Information for Emission Estimates**

*Global Distribution of Emissions.* Will et al. (26) compiled information on the type of fluoropolymer produced, production process and estimated production capacity for more than 30 manufacturing facilities. Each site was assigned to the appropriate model region based on the longitude and latitude of the facility. Fluoropolymer (FP) production facilities using APFO are located in the United States (regions 78 – 80; see Figure S2), Europe (regions 60 – 62, 85), Russia (region 64) and Asia (regions 92 – 94, 114 – 116). The total production capacity of facilities (26) in each model region was used as the primary basis to apportion the total estimated historic emissions of APFO emitted as a result of FP manufacturing. This simplifying assumption means that emissions per unit FP produced are identical across all sites. In Prevedouros et al (27), APFO production (and hence emissions from direct sources) was estimated for four periods (1951 – 1964, 1965 – 1979, 1980 – 1994, 1995 – 2002). Since the majority of FP plants have not been operational since 1951, emissions assigned to each region were adjusted accordingly. However, complete historical emission estimates are currently available for only one FP production site in the United States (28). To address this data gap, information on temporal trends (1970s – present) in overall FP production in the United States and Europe compiled by Will et al. (26) was considered. Other sources included patent submissions (see (27)), voluntary disclosures to regulatory agencies by manufacturers (29 – 31) and company websites detailing corporate history.

1  
2 With respect to the direct manufacture of APFO, the ECF process was estimated to  
3 account for 80 – 90% of the historical production with the largest manufacturing sites in  
4 the United States and Belgium (27). Significant ECF production capacity was developed  
5 in Italy and to a lesser extent, Japan. Beginning in 1975, additional production capacity  
6 based on direct oxidation of perfluorooctyl iodide (27) came online at one site in  
7 Germany and at least one site in Japan. Note that this production process, estimated to  
8 account for the remaining 10 – 20% of historical production, yields exclusively linear  
9 isomers. While there is some information on emissions from the facilities in the United  
10 States (30), no information about other locations was found in the public domain. Based  
11 on available information and expert opinion, all emissions from 1951 – 1964 were  
12 assumed to occur in the United States (region 78). From 1965 – 1974, 75% of emissions  
13 occurred in the United States (regions 78, 79) and 25% in Europe (regions 61, 85). After  
14 1975, approximately 50% of total historic emissions were assigned to locations in the  
15 United States (regions 78, 79), 40% to locations in Europe (regions 61, 85) and 10% to  
16 locations in Japan (region 94).

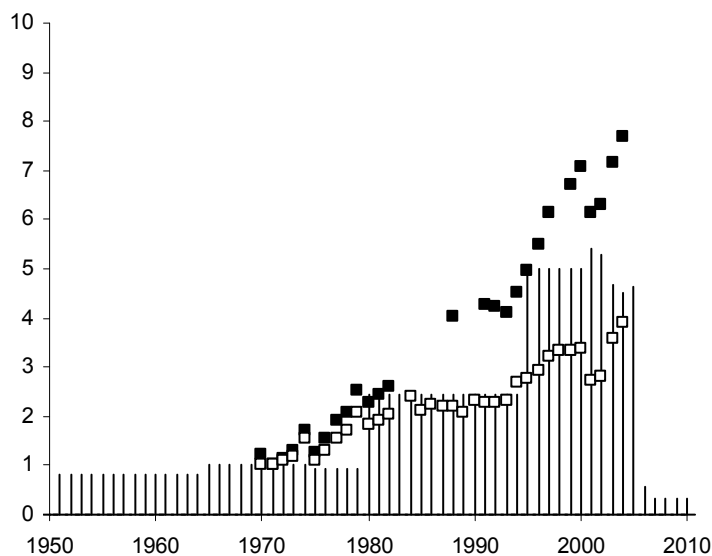
17  
18 The resulting temporal trends in emissions of APFO and the associated emission of  
19 PFO(A) from the two main direct sources in North America, Europe/Russia and East  
20 Asia are below (Figure S5a-c). Note that emissions in Europe/Russia were assumed to  
21 begin in 1965 while emissions in North America and Asia were assumed to begin in  
22 1951.



1 **Figure S5.** Emission estimates of APFO (metric tons) from 1950 – 2010 for (a)  
2 Europe/Russia, (b) North America and (c) Asia.  
3

*Comparison between source inventories and production data*

Will et al. (26) reported estimates of historic production of PTFE and other FPs manufactured using APFO (e.g. FEP, PFA) in the United States over the period 1970 – 2004. In Prevedouros et al. (27), 60% of the APFO used in FP manufacturing was assumed to be released to the environment and total APFO production estimates were used as the basis for estimating total emissions. Since the amount of APFO required per unit production FP is not likely to be constant over time (due to production efficiency improvements, improved APFO recovery/recycling), a direct relationship between FP production and APFO emissions cannot be expected. However, it is still useful to compare the relative FP production to the relative APFO emissions used in the current simulations. This comparison is shown in Figure S6.

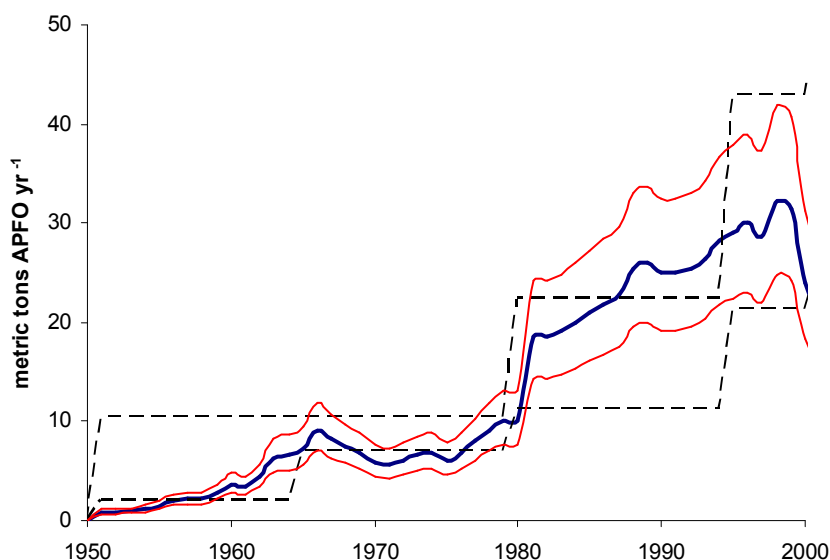


**Figure S6.** PTFE (open squares) and total FP production (closed squares) in the United States relative to 1970 over the period 1970 – 2004 in comparison to APFO emission estimates from FP production (bars) in the United States relative to 1970.



1 As shown in Figure S6, PTFE production increased approximately 4-fold over the period  
2 1970 – 2004 while total FP production increased approximately 8-fold. In comparison,  
3 APFO emissions from FP production increased by a factor of 5 over the same period  
4 illustrating the reasonable overlap between estimated FP production and APFO emissions  
5 related to FP manufacturing activity over the same time period.

6  
7 More detailed information on historic emissions from a single FP manufacturing facility  
8 in the United States (DuPont Washington Works) was reported by Paustenbach et al.  
9 (28). The amount of APFO used by the plant was based on accounting records while  
10 releases were based on information from APFO mass balances for the production lines as  
11 contained in internal DuPont documents (which are not available to the general public  
12 however). The DuPont Washington Works FP facility is located in BETR-Global region  
13 79 and is the only FP facility assigned to that region. Therefore, it is possible to make a  
14 direct comparison between emission estimates reported in Paustenbach et al. (28) and the  
15 emission estimates derived from Prevedouros et al. (27), as shown in Figure S7.



**Figure S7.** Estimated emissions of APFO (1950 – 2000, in metric tons  $\text{yr}^{-1}$ ) taken from Paustenbach et al. (29) (blue line)  $\pm 30\%$  estimated uncertainty (red lines) versus minimum and maximum emission estimates (dotted lines) derived from Prevedouros et al. (28) for BETR-Global region 79, FP production

The total estimated releases under the minimum and maximum scenario from 1950 –

2000 are  $\sim 440$  and  $900$  metric tons respectively whereas the total estimated emissions

based on Paustenbach et al. (28) are  $\sim 660$  metric tons ( $505 - 855$ ). While the maximum

emission scenario substantially overestimates the reported emissions from 1950 – 1965,

reported emissions from 1985 – 1995 appear to be underestimated by up to 50%.

However, considering the uncertainties inherent to all emission inventory estimations, the

overall agreement between the two emission functions is acceptable.

## **S6. Summary tables and additional figures of model outputs**

Summary tables and additional figures characterizing various atmospheric model outputs

are presented in the following section.

**Table S1** – Modeled gross deposition fluxes ( $\text{ng m}^{-2}$ ) in the year 2005 for regions representing North America, below 60 °N, assuming  $\text{pK}_a = 0$  (see Figure S2). Note that modeled values were similar for the period 2000 – 2005 and that the gross deposition flux in source regions (78 – 80) assuming No E to Air were not calculated using model output, since they are assumed to be equivalent to yearly emissions to air.

	With Emissions to Air					No Emissions to Air				
BETR	< 1%	25%	50%	75%	> 99%	< 1%	25%	50%	75%	> 99%
52	57	54	51	49	81	neg.	neg.	neg.	neg.	neg.
53	49	46	44	42	51	neg.	neg.	neg.	neg.	neg.
54	41	40	38	37	52	neg.	neg.	neg.	neg.	neg.
55	117	114	111	109	121	neg.	neg.	neg.	neg.	neg.
56	71	69	66	64	86	neg.	neg.	neg.	neg.	neg.
57	77	73	69	66	83	neg.	neg.	neg.	neg.	neg.
76	57	55	52	50	65	neg.	neg.	neg.	neg.	neg.
77	24	24	24	25	38	neg.	neg.	neg.	neg.	neg.
<b>78*</b>	99	107	114	120	142	NOT CALCULATED				
<b>79*</b>	962	1005	1046	1084	1140					
<b>80*</b>	665	655	647	639	531					
101	18	18	18	18	29	neg.	neg.	neg.	neg.	neg.
102	13	14	14	15	22	neg.	neg.	neg.	neg.	neg.
103	55	54	52	50	61	neg.	neg.	neg.	neg.	neg.
127	22	21	20	18	25	neg.	neg.	neg.	neg.	neg.
AVERAGE	155	157	158	159	168	NOT CALCULATED				
<b>*Source</b>	575	589	602	614	605					
Non-Source	50	49	47	45	59	neg.	neg.	neg.	neg.	neg.

1 **Table S2** – Modeled gross deposition fluxes ( $\text{ng m}^{-2}$ ) in the year 2005 for regions representing North America, below 60 °N, assuming  
2  $\text{pK}_a = 1.5$  (see Figure S2). Note that modeled values were similar for the period 2000 – 2005 and that the gross deposition flux in  
3 source regions (78 – 80) assuming No E to Air were not calculated using model output, since they are assumed to be equivalent to  
4 yearly emissions to air.

BETR	With Emissions to Air					No Emissions to Air				
	< 1%	25%	50%	75%	> 99%	< 1%	25%	50%	75%	> 99%
52	72	71	69	69	87	2	2	2	2	2
53	62	61	60	59	53	2	2	2	2	1
54	51	51	51	51	55	1	1	1	1	1
55	133	131	129	127	123	5	5	5	5	5
56	87	86	83	80	93	3	3	3	3	3
57	94	90	88	87	86	3	3	3	3	3
76	72	71	70	70	66	2	2	2	2	2
77	30	31	32	34	40	1	1	1	1	1
<b>78*</b>	107	117	126	134	150	NOT CALCULATED				
<b>79*</b>	1000	1047	1092	1133	1182					
<b>80*</b>	614	591	569	548	540					
101	23	23	24	24	31	1	1	1	1	1
102	16	17	19	20	25	1	1	1	1	1
103	64	62	60	59	65	2	2	2	2	2
127	27	26	24	23	27	1	1	1	1	1
AVERAGE	163	165	166	168	175	NOT CALCULATED				
<b>*Source</b>	574	585	596	605	624					
Non-Source	61	60	59	59	63	2	2	2	2	2

1 **Table S3** – Modeled gross deposition fluxes ( $\text{ng m}^{-2}$ ) in the year 2005 for regions representing North America, below 60 °N, assuming  
2  $\text{pK}_a = 3.5$  (see Figure S2). Note that modeled values were similar for the period 2000 – 2005 and that the gross deposition flux in  
3 source regions (78 – 80) assuming No E to Air were not calculated using model output, since they are assumed to be equivalent to  
4 yearly emissions to air.

	With Emissions to Air					No Emissions to Air				
BETR	< 1%	25%	50%	75%	> 99%	< 1%	25%	50%	75%	> 99%
52	514	363	281	230	195	253	197	160	134	116
53	224	187	162	144	130	108	98	88	80	73
54	253	201	173	154	141	123	107	96	88	82
55	482	426	399	381	372	283	282	279	274	273
56	221	289	285	268	252	123	177	182	175	167
57	488	351	280	235	205	263	210	175	151	134
76	318	219	175	149	130	156	119	100	87	78
77	118	108	100	93	88	57	57	55	53	51
<b>78*</b>	145	300	384	416	438	NOT CALCULATED				
<b>79*</b>	814	1882	2643	3215	3530					
<b>80*</b>	672	989	1132	1202	1262					
101	158	104	82	70	62	73	53	44	39	36
102	185	130	116	113	114	108	91	90	92	97
103	188	218	202	186	165	106	139	137	131	119
127	262	142	95	72	58	125	75	53	42	35
AVERAGE	336	394	434	462	476	NOT CALCULATED				
<b>*Source</b>	544	1057	1386	1611	1744					
Non-Source	284	228	196	175	159	148	134	122	112	105

1 **Table S4** – Modeled concentrations in source regions in the lower atmosphere ( $\text{pg m}^{-3}$ ), precipitation levels ( $\text{ng L}^{-1}$ ) and gross  
2 deposition flux to the Arctic region ( $\text{kg yr}^{-1}$ ) for 2005, assuming  $\text{pK}_a = 0$ . Note that modeled values were similar for the period 2000 –  
3 2005. Modeled air concentrations in source regions (78 – 80) assuming No E to Air reflect the extent of volatilization from terrestrial  
4 surfaces. Precipitation levels under this mode of entry assumption were not calculated (NC) using model output.

		Lower Atmosphere ( $\text{pg m}^{-3}$ )		Precipitation ( $\text{ng L}^{-1}$ )		Gross Deposition Flux to Arctic ( $\text{kg yr}^{-1}$ )		
	BETR	E direct to air	No E to air	E direct to air	No E to air	BETR	E direct to air	No E to air
< 1%	78 - 80	1.2 - 6.5	$\leq 0.01$	0.05 - 0.5	NC	1 - 24	244	0.2
	60 - 62	0.7 - 3.6	$\leq 0.01$	0.25 - 1.6		1 - 48	1542	1.4
	92 - 94	1.0 - 4.2	$\leq 0.01$	0.25 - 1.3				
25%	78 - 80	1.1 - 6.3	$\leq 0.01$	0.05 - 0.5	NC	1 - 24	239	0.2
	60 - 62	0.7 - 3.6	$\leq 0.01$	0.24 - 1.5		1 - 48	1479	1.3
	92 - 94	1.0 - 4.1	$\leq 0.01$	0.24 - 1.3				
50%	78 - 80	1.1 - 6.1	$\leq 0.01$	0.04 - 0.4	NC	1 - 24	234	0.2
	60 - 62	0.7 - 3.5	$\leq 0.01$	0.23 - 1.5		1 - 48	1419	1.3
	92 - 94	0.9 - 4.0	$\leq 0.01$	0.23 - 1.2				
75%	78 - 80	1.0 - 5.8	$\leq 0.01$	0.04 - 0.4	NC	1 - 24	229	0.2
	60 - 62	0.6 - 3.4	$\leq 0.01$	0.23 - 1.4		1 - 48	1367	1.3
	92 - 94	0.9 - 3.9	$\leq 0.01$	0.22 - 1.2				
> 99%	78 - 80	1.1 - 5.8	$\leq 0.01$	0.04 - 0.4	NC	1 - 24	354	0.3
	60 - 62	1.0 - 4.7	$\leq 0.01$	0.16 - 0.7		1 - 48	1852	1.6
	92 - 94	1.4 - 5.4	$\leq 0.01$	0.22 - 0.9				

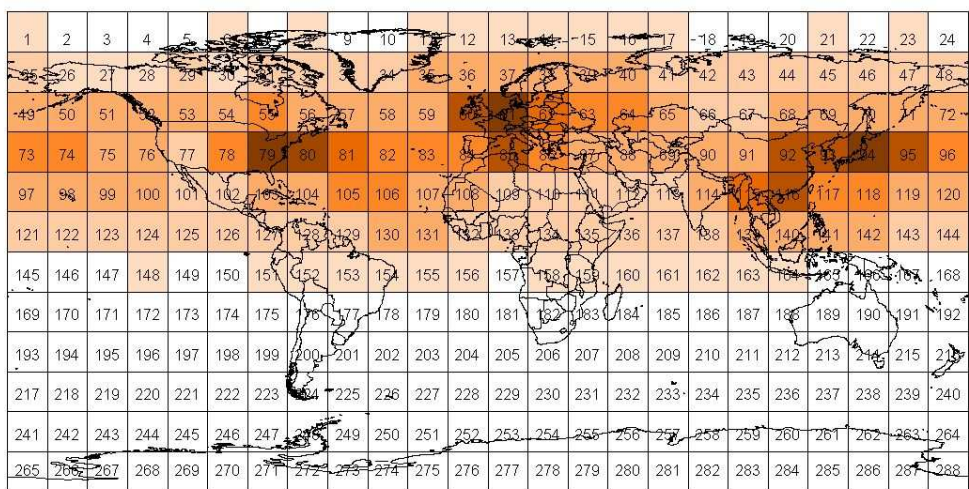
1 **Table S5** – Modeled concentrations in source regions in the lower atmosphere ( $\text{pg m}^{-3}$ ), precipitation levels ( $\text{ng L}^{-1}$ ) and gross  
2 deposition flux to the Arctic region ( $\text{kg yr}^{-1}$ ) for 2005, assuming  $\text{pK}_a = 1.5$ . Note that modeled values were similar for the period 2000  
3 – 2005. Modeled air concentrations in source regions (78 – 80) assuming No E to Air reflect the extent of volatilization from  
4 terrestrial surfaces. Precipitation levels under this mode of entry assumption were not calculated (NC) using model output.

		Lower Atmosphere ( $\text{pg m}^{-3}$ )		Precipitation ( $\text{ng L}^{-1}$ )		Gross Deposition Flux to Arctic ( $\text{kg yr}^{-1}$ )		
	BETR	E direct to air	No E to air	E direct to air	No E to air	BETR	E direct to air	No E to air
< 1%	78 - 80	1.3 - 6.8	< 0.5	0.06 - 0.4	NC	1 - 24	307	7
	60 - 62	0.9 - 4.8	< 0.5	0.22 - 1.1		1 - 48	1954	54
	92 - 94	1.5 - 4.9	< 0.5	0.35 - 1.2				
25%	78 - 80	1.2 - 6.6	< 0.5	0.05 - 0.4	NC	1 - 24	310	7
	60 - 62	1.0 - 4.8	< 0.5	0.20 - 1.0		1 - 48	1923	54
	92 - 94	1.5 - 5.0	< 0.5	0.32 - 1.1				
50%	78 - 80	1.2 - 6.3	< 0.5	0.05 - 0.4	NC	1 - 24	312	7
	60 - 62	1.0 - 4.8	< 0.5	0.18 - 0.9		1 - 48	1900	53
	92 - 94	1.5 - 5.2	< 0.5	0.28 - 1.0				
75%	78 - 80	1.1 - 6.1	< 0.5	0.05 - 0.4	NC	1 - 24	317	7
	60 - 62	1.0 - 4.8	< 0.5	0.17 - 0.8		1 - 48	1869	52
	92 - 94	1.5 - 5.3	< 0.5	0.25 - 0.9				
> 99%	78 - 80	1.1 - 6.0	< 0.5	0.05 - 0.4	NC	1 - 24	378	8
	60 - 62	1.1 - 4.9	< 0.5	0.16 - 0.7		1 - 48	1948	51
	92 - 94	1.5 - 5.5	< 0.5	0.22 - 0.8				

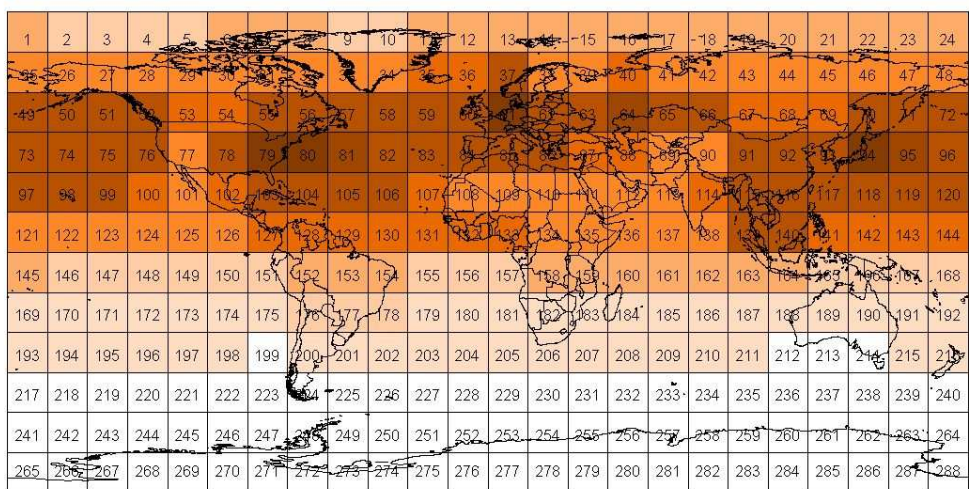
1 **Table S6** – Modeled concentrations in source regions in the lower atmosphere ( $\text{pg m}^{-3}$ ), precipitation levels ( $\text{ng L}^{-1}$ ) and gross  
2 deposition flux to the Arctic region ( $\text{kg yr}^{-1}$ ) for 2005, assuming  $\text{pK}_a = 3.5$ . Note that modeled values were similar for the period 2000  
3 – 2005. Modeled air concentrations in source regions (78 – 80) assuming No E to Air reflect the extent of volatilization from  
4 terrestrial surfaces. Precipitation levels under this mode of entry assumption were not calculated (NC) using model output.

		Lower Atmosphere ( $\text{pg m}^{-3}$ )		Precipitation ( $\text{ng L}^{-1}$ )		Gross Deposition Flux to Arctic ( $\text{kg yr}^{-1}$ )		
	BETR	E direct to air	No E to air	E direct to air	No E to air	BETR	E direct to air	No E to air
< 1%	78 - 80	9 - 32	6 - 26	0.02 - 0.08	NC	1 - 24	2526	1184
	60 - 62	8 - 24	4 - 17	0.02 - 0.06		1 - 48	10109	5016
	92 - 94	9 - 19	6 - 10	0.03 - 0.05				
25%	78 - 80	5 - 26	4 - 22	0.21 - 1.0	NC	1 - 24	1543	799
	60 - 62	4 - 18	2 - 13	0.15 - 0.7		1 - 48	7406	4111
	92 - 94	6 - 13	4 - 7	0.22 - 0.5				
50%	78 - 80	4 - 22	3 - 18	0.21 - 1.4	NC	1 - 24	1153	631
	60 - 62	3 - 15	2 - 11	0.20 - 1.1		1 - 48	6094	3584
	92 - 94	5 - 10	3 - 6	0.34 - 0.8				
75%	78 - 80	4 - 19	3 - 16	0.17 - 1.2	NC	1 - 24	938	531
	60 - 62	2 - 13	1 - 10	0.23 - 1.5		1 - 48	5266	3205
	92 - 94	4 - 9	3 - 5	0.42 - 1.0				
> 99%	78 - 80	3 - 18	2 - 15	0.16 - 1.1	NC	1 - 24	801	465
	60 - 62	2 - 12	1 - 9	0.25 - 1.8		1 - 48	4691	2921
	92 - 94	3 - 7	2 - 4	0.48 - 1.1				

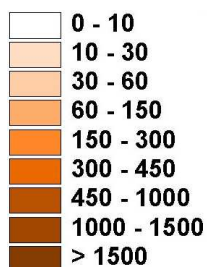




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**Figure S8.** Gross deposition flux ( $\text{kg yr}^{-1}$ , see legend) in 2005 assuming emissions to air,  $\phi = 25\%$  and  $pK_a = 0$  (top map) and  $pK_a = 3.5$  (bottom map).

## **S7. Marine aerosol flux of PFO(A)**

There has been some speculation in the literature as to importance of marine aerosols for the transport of PFCAs (27, 32). Marine aerosols are produced in the world's oceans and contribute significantly to the global aerosol load. Most of the focus of research on marine aerosols has been on sea salt aerosols, which are the most abundant natural atmospheric aerosol in terms of mass. Sea salt aerosols are generated from bubbles bursting at the sea surface producing "film" droplets ( $0.5 - 5 \mu\text{m}$ ) and "jet" droplets ( $3 - 50 \mu\text{m}$ ) or when high winds tear larger "spume" droplets ( $>20 \mu\text{m}$ ) off the wave crests (33). Research has recently shown that that submicron marine aerosols ( $<1 \mu\text{m}$ ) can also make an important contribution to the total marine aerosol flux (34). The chemical composition of the aerosol has been shown to change with aerosol size with a clear transition from saline for the larger particles to almost entirely organic particles for the smaller fractions of marine aerosols (35). An important parameter that will determine the long range potential of the marine aerosols is the atmospheric residence time. For large particles ( $1.0 - 10 \mu\text{m}$ ) the residence time is of the order of hours to a few days and is essentially determined by sedimentation and dry deposition (33). These large particles are saline in nature and will have only short range atmospheric transport potential, nicely illustrated in the work of Benassai et al. (36), who demonstrated that sea salt aerosol depositional fluxes decreased inland by two orders of magnitude in the first 200 km distance from the sea. The smaller more organic-rich particles ( $0.05 - 1.0 \mu\text{m}$ ; the so-called accumulation mode) have a residence time of many days, mostly determined by removal through wet deposition (33) and will have considerable long range atmospheric transport potential. Spatially resolved global production fluxes ( $\text{mg m}^{-2} \text{d}^{-1}$ ) of marine

aerosols have been estimated for total marine aerosols of differing size fractions (0.03 – 25  $\mu\text{m}$ ) (37) and also for accumulation mode marine aerosols only (0.1 – 0.5  $\mu\text{m}$ ) (34). Estimated global sea salt aerosol production fluxes were on average 24  $\text{mg m}^{-2} \text{d}^{-1}$  and peaked at a value of 420  $\text{mg m}^{-2} \text{d}^{-1}$  (37). Estimated global accumulation mode sea-spray aerosol production fluxes were much lower and peaked at 6.0  $\text{mg m}^{-2} \text{d}^{-1}$  (34).

Here we attempt to estimate the amount of PFO(A) that could be associated with these aerosol production fluxes. To calculate the concentration of PFO(A) on marine aerosol particles it is necessary to multiply PFO(A) concentrations in surface ocean water with an enrichment factor (EF) (35), as it has been long understood that certain organic materials are enriched at the air water interface (38). Enrichment factors for PFO(A) in the surface microlayer of coastal waters were reported to range from 1.2 – 1.8 (39) while McMurdo et al. (32) reported an EF of 55.7 for PFO(A) in seawater measured in the laboratory. Another study reported an EF of 3 for PFO(A) in foam generated in a laboratory (40). The gross flux of PFO(A) ( $F_{\text{PFO(A)}}$ ) on marine aerosols ( $\text{kg m}^{-2} \text{year}^{-1}$ ) ejected from the ocean surface can be calculated using equation S7.

$$F_{\text{PFO(A)}} = [\text{PFO(A)}](\text{EF})(F_{\phi})(3.65 \times 10^{-19}) \quad (\text{S7})$$

where  $[\text{PFO(A)}]$  is the ocean water concentration of PFO(A) ( $\text{pg L}^{-1}$ ), EF is the enrichment factor for PFO(A) in the surface microlayer/marine aerosols,  $F_{\phi}$  is the marine aerosol production flux ( $\text{mg m}^{-2} \text{d}^{-1}$ ) and the factor  $3.65 \times 10^{-19}$  is to convert  $F_{\text{PFO(A)}}$  into the correct units. We assume that the marine aerosol has the same density as the seawater. This flux can be used to estimate mass flows of PFO(A) from the ocean to the atmosphere by multiplying by the surface area of the ocean being considered. Studies

1 over the period 2002 – 2005 measuring the concentrations of PFO(A) in surface seawater  
2 (cited in the main article) report seawater concentrations from <20 (in remote ocean  
3 regions) to 1060 pg L<sup>-1</sup> (in a polluted coastal region offshore Japan). We estimate a  
4 PFO(A) flux from ocean to atmosphere for the Northern Hemisphere (NH) using the  
5 average value for  $F_0$  of 24 mg m<sup>-2</sup> d<sup>-1</sup> (which includes both coarse and accumulation  
6 mode aerosols), an EF of 55.7, the NH observed open ocean water concentration range  
7 (<20 – 439 pg L<sup>-1</sup>) and NH ocean surface area ( $1.53 \times 10^{14}$  m<sup>2</sup>). This calculation results  
8 in a gross mass flow of <1.5 to 33 kg year<sup>-1</sup> PFO(A) for the entire hemisphere. Assuming  
9 the average EF reported in (39) of 1.4, the estimated mass flow is reduced to <0.04 – 0.84  
10 kg year<sup>-1</sup>. The potential for this PFO(A) to undergo long range transport depends on the  
11 fate of the marine aerosols themselves and the fate of the PFO(A) associated with the  
12 marine aerosols. For example, McMurdo et al. (32) concluded that a significant fraction  
13 of PFO(A) associated with aerosols will be released into the gas phase. However, even if  
14 we assume that 100% of the PFO(A) associated with newly ejected marine aerosols is  
15 released into the gas phase, the mass of PFO(A) is insignificant compared to estimated  
16 global stack emissions in 2005 (20 – 45 metric tons). In terms of LRT to the Arctic, our  
17 estimated total PFO(A) mass flux from marine aerosol generation is also lower than  
18 modeled gross deposition fluxes related to transport and degradation of FTOHs (113 –  
19 226 kg yr<sup>-1</sup> (41); 50 – 500 kg yr<sup>-1</sup> (42) in 2005) and measurements (114 – 587 kg in 2005  
20 (43)). In conclusion, we find that long-range transport of PFO(A) associated with marine  
21 aerosol generation is not likely to be an important transport process. However, we  
22 encourage others to challenge and refine these calculations using more sophisticated  
23 approaches.

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