1	Supporting Information for
2	Combination of On-Chip Field Amplification
3	and Bovine Serum Albumin Sweeping for
4	Ultra-Sensitive Detection of Green Fluorescent
5	Protein
6	Qiong Pan <sup>†</sup> , Meiping Zhao* <sup>†</sup> , Shaorong Liu* <sup>‡</sup>
7	$^\dagger$ Beijing National Laboratory for Molecular Sciences, Key Laboratory of Bioorganic Chemistry &
8	Molecular Engineering of Ministry of Education, College of Chemistry and Molecular
9	Engineering, Peking University, Beijing, 100871, China and $^{\ddagger}$ Department of Chemistry and
10	Biochemistry, The University of Oklahoma, Norman, Oklahoma 73019, USA
11	
12	Corresponding authors: mpzhao@pku.edu.cn; shaorong.liu@ou.edu

# Theoretical consideration of field amplified pre-concentration and reversed-voltage concentration

At the moment ( $t_0=0$ ) of voltage switching from the loading step to the pre-concentration step,  $L_2$  is all filled with sample buffer,  $L_1$  and  $L_3$  are filled with running buffer with a short zone of sample buffer to the end of the cross section (Figure 2a). Electric field strengths across  $L_2$  ( $E_{20}$ ) is described by eq 1.

21 
$$E_{20} = U_2/l$$
 eq 1

where  $U_2$  is the potential on L<sub>2</sub>. After time  $t_x$ , the sample zone is pushed back toward S due to EOF, and the length of the sample zone is  $l_x$  (see Figure 2b). Then, the electric field strength across L<sub>2</sub> is described by eq 2.

25 
$$E_{2x} = \frac{\gamma U_2}{[(l-l_x) + \gamma l_x]} \qquad \text{eq 2a}$$

26 
$$E_{x0} = \frac{U_2}{\left[(l-l_x) + \gamma l_x\right]} \qquad \text{eq 2b}$$

where  $E_{2x}$  and  $E_{x0}$  are the electric field strength across  $L_x$  and  $(l-l_x)$ ,  $\gamma$  is the conductivity ratio of the running buffer and the sample buffer.

Accordingly, bulk flow  $(V_2)$  in channel  $L_2$  is the vector sum of the local electroosmotic velocity  $(V_{eo2})$  and the pressure-driven velocity  $(V_{h2})$  in each channel, because of the uneven liquid level between SR and other reservoirs, there exists a hydrodynamic pressure from SR to the intersection. It creates an addictive flow rate  $(V_{h2})$  which adds up to the bulk flow in  $L_2$   $(V_{2b})$  together with EOF, as expressed in eq3.

35 
$$V_{2b} = V_{eo2} - V_{h2}$$
 eq 3

In addition, there is the pressure-driven velocity usually produced by the imbalance of local EOFs in the low-conductivity sample buffer and the running buffer. However, in our case, the hydrodynamic pressure is much more notable than the back-pressure caused by EOF imbalance, so the pressure-driven velocity is mostly produced by hydrodynamic force, defined as  $V_{h2}$ . Since  $L_2$  is occupied with a sample zone, whose length is  $L_x$ , and a running buffer zone, whose length is  $(l-l_x)$ ,  $V_{eo2}$  is the average of two parts weighted by the ratios, as described by eq 4.

44 
$$V_{eo2} = (1 - \frac{l_x}{l})\mu_{eox0}E_{x0} + (\frac{l_x}{l})\mu_{eo2x}E_{2x}$$
 eq 4

45 where  $\mu_{eox0}$  and  $\mu_{eo2x}$  are the electroosmotic mobility for the running buffer and the 46 sample buffer. If we define  $x = \frac{l_x}{l}$ , as the ratio of sample zone length in L<sub>2</sub>, from eq 2, 47 3 and 4, the bulk flow in L<sub>2</sub> (V<sub>2b</sub>) in terms of x can be obtained as in eq 5.

48 
$$V_{2b} = \frac{(1-x)\mu_{eox0} + \gamma x \mu_{eo2x}}{1+(\gamma-1)x} \bullet \frac{U_2}{l} - V_{h2}$$
 eq 5

50 
$$U_i \propto I_i l_i$$
,  $U_2 + U_3 = V_3 - V_2$ ,  $U_4 + U_3 = V_3 - V_4$ 

where  $U_i$  and  $I_i$  represent the potential and current on each channel,  $l_i$  stands for the length of each channel, and  $V_i$  stands for the voltage applied to the reservoir.  $U_2$  can be calculated with voltages on each reservoir and the current on each channel.  $U_2$ under different voltage applied to the reservoir is shown in Table 1.

Under the applied voltage, the negatively charged analyte in the sample buffer has an electrophoretic velocity ( $V_{ep}=\mu_{ep}E_{2x}$ ) and in the direction opposite to EOF. In the two buffer system, the analytes are in low-conductivity buffer with much higher local electric field strength than the high-conductivity buffer. The electrophoretic velocity,  $V_{ep}$  of the analyte anions can be expressed as in eq 6.

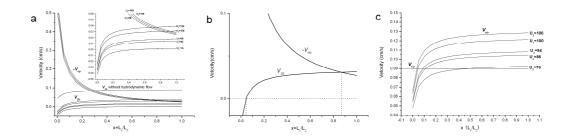
60 
$$V_{ep} = \mu_{ep} E_{2x} = \frac{\mu_{ep} \gamma}{\left[(1-x) + \gamma x\right]} \cdot \frac{U_2}{l} \quad \text{eq 6}$$

It should be noted that  $U_2$  is a variable depending on x. In this experiment, we monitored the electric current through  $L_2$ . It increased initially within the first few seconds and then remained virtually a constant during the FASI, indicating a relatively stable potential along  $L_2$ . In order to simplify the calculation,  $U_2$  is assumed to be a constant. Then  $U_2$  can be calculated with the final current in each channel and the voltages applied to each reservoir. The calculated  $U_2$  values are listed in Table S1.

Table S1. $U_2$ under Different Voltage Applied to Each Reservoir											
	$V_{l}\left(\mathbf{V}\right)$	$V_2(\mathbf{V})$	$V_{3}\left(\mathbf{V}\right)$	$V_4\left(\mathbf{V}\right)$	$I_1$ (mA)	$I_2$ (mA)	$I_3$ (mA)	$I_4 (\mathrm{mA})$	$U_2(\mathbf{V})$		
	1680	1680	2000	0	4.5	4.5	20.5	11.5	76		
	1620	1620	2000	0	5.0	5.0	21.0	11.0	86		
	1600	1600	2000	0	5.5	5.5	22.0	11.0	94		
	1550	1550	2000	0	6.0	6.0	23.0	11.0	100		
	1510	1510	2000	0	6.5	6.5	24.0	11.0	106		

68 For a given  $\mu$ CE, the voltages applied to all reservoirs and the buffer conductivity ratio was kept constant. In our case,  $U_2=100$  V and  $\gamma=20$ ; l=0.50 cm. The 69 electroosmotic mobility for sample solution (2.2 mM Tris base, 2.2 mM tetraborate 70 acid, pH 7.5) and BGE solution (44.5 mM Tris base, 44.5 mM tetraborate acid, 71 pH8.0) are  $6.07 \times 10^{-4}$  and  $3.14 \times 10^{-4}$  cm<sup>2</sup>/Vs, respectively. The electrophoretic 72 mobility of GFP in 20-fold diluted TB buffer is  $1.35 \times 10^{-4} \text{ cm}^2/\text{Vs}$ . The bulk velocity 73 driven by the static pressure is 0.09 cm/s. Substituting these values into equations 1a 74 and 1b,  $V_{2b}$  and  $V_{ep}$  can be expressed as a function of x.  $V_{2b}$  and  $V_{ep}$  will also change 75 76 with  $U_2$ , as displayed in Figure S1.

77 A lot of insightful information can be extracted from the relationships presented in Figure S1 for us to understand the concentration approach described in this paper. 78 79 Referring to eq 5, the bulk solution flow (V<sub>2b</sub>) consists of the hydrodynamic flow 80  $(V_{h2})$  and EOF  $(V_{eo})$ .  $V_{h2}$  is a constant if only the relative liquid levels in all reservoirs are maintained the same. Veo, however, decreases when x decreases. Under certain 81 conditions (see Figure S1b),  $-V_{ep}$  curve intersects with  $V_{2b}$  curve at a particular x 82 value, indicating that the bulk solution moves in one direction while analyte migrates 83 84 in the opposite direction but at the same scale. Then  $-V_{ep}$  becomes greater than  $V_{2b}$ after the intersection, which means the apparent velocity of GFP changes direction. 85 Eventually,  $V_{eo}$  and  $V_{h2}$  balance one another (at the intersection of  $V_{eo}$  and  $V_{h2}$  curves, 86 see Figure S1c) and  $V_{2b}$  equals to zero. That is, the sample/BGE boundary stays 87 88 stagnant while the concentrated anion analyte migrates into L<sub>2</sub>.



90

89

Figure S1. a) Plot of the calculated bulk flow velocities and electrophoretic velocities of GFP during field amplified pre-concentration under different potential along L<sub>2</sub>. The inset shows the expanded view of the lower part of the *y* axis. b) Plot of the calculated bulk flow and electrophoretic velocities of GFP when  $U_2$ =100V. c) Plot of the calculated electroosmotic flow ( $V_{eo}$ ) along L<sub>2</sub> and the detected hydrodynamic flow ( $V_{h2}$ ). Calculation is based on eq 1, channel length of  $L_2$ =0.5cm, conductivity ratio  $\gamma$ =20.  $V_{2b}$  is the bulk flow velocity in channel L<sub>2</sub>, and  $V_{ep}$  is the electrophoretic velocity of GFP.

98 Initially in step 2, the sample/BGE boundary was pushed back, against the 99 hydrodynamic flow, toward SR by EOF. The sample zone was narrowed. In the 100 course of this process,  $l_x$  decreased with time. Referring to Figure S1b, the value of x 101 progressed from right to left. When x was at the right-hand side of the intersection, 102  $V_{2b}$ - $V_{ep}$  and GFP moved in the direction to SR (see Figures 2a and 2b), but due to the different velocity of GFP in the sample zone and the BGE, GFP decelerated and 103 104 stacked at the sample/BGE boundary. As x went to the left-hand side of the 105 intersection,  $V_{2b}$ <- $V_{ep}$  and GFP moved in the direction to channel intersection and 106 GFP in SR also moved into  $L_2$  (see Figures 2c), thus increased the amount of sample 107 injected. When  $V_{eo}=V_{h2}$ , sample/BGE boundary and the bulk solution became stagnant 108 while GFP kept migrating into L<sub>2</sub>. Because GFP was concentrated moving toward the channel intersection, L<sub>2</sub> was filled with the GFP sample but at a much higher 109 110 concentration (see Figures 2d and 2e). In our experiment, this step took ~35 seconds.

## 111 Guidelines for Voltage Setting in *Step 2*

Depending on the magnitude of the hydrodynamic flow, the voltage on  $L_2$  should be set within an appropriate range to guarantee the balance between the hydrodynamic flow and EOF. When the EOF and the hydrodynamic flow balance with each other,  $V_{2b}$  is zero. So

116 
$$\frac{(1-x)\mu_{eox0} + \gamma x \mu_{eo2x}}{1+(\gamma-1)x} \bullet \frac{U_2}{l} = V_{h2}$$

110

117 As we want the stagnant point to be inside  $L_2$ , x should be in the range of 0 to 1. So

118 
$$U_2 = \frac{V_{h2} \cdot l}{\mu_{eox0}}$$
 (x=0) and  $U_2 = \frac{V_{h2} \cdot l}{\mu_{eo2x}}$  (x=1)

Entering all the variations, we can get the range of  $U_2$ . Referring to Table 2, we can get the appropriate voltage setting. In our case, the voltage setting range was 74~143 V. If the voltage is below 74 V, EOF would not be able to push the sample/BGE boundary toward SR; if the voltage is above 143 V, the hydrodynamic flow would not be able to balance EOF inside the channel.

#### 124 Video record of the whole concentration process during *Step 2*

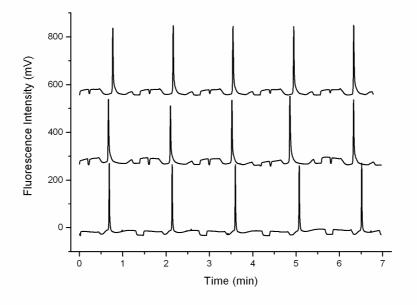
A series of fluorescent images of L2 during the concentration process was obtained using a Leica TCS-SP2 Confocal Laser Scanning Microscope (Leica Microsystems, Heidelberg, Germany) with a 488 nm laser at a line scanning frequency of 400 Hz and a 1× objective. These images were assembled into movies using the Leica Confocal software.

In the attached video file (video of *Step2*), the channel on the right side is  $L_2$ . At t = 130 3 s, 2 kV was applied to BR, 1.55 kV was applied to SR and SW, while BW was 131 132 grounded. This voltage setting created an overall (EOF plus hydrodynamic) flow from 133 BR to all other reservoirs. During  $t=3\sim11$  s, the sample solution being pushed toward SR by the high conductivity BGE. Due to the conductivity difference between sample 134 135 solution and BGE, GFP was stacked in the BGE near the sample/BGE boundary. During  $t=12\sim18$  s, the GFP sample zone moved back toward the intersection and L2 136 137 was filled with the concentrated GFP. The excessive sample is removed via L1.

#### 138 Video record of the whole concentration process during *Step 3 and 4*

139 To show more detail of the short-period process of step 4, a scan frequency of 800 Hz and a  $2\times$  objective were used. The attached video file (video of *Step* 3 and 4) 140 shows the process during *Step 3* and 4. The channel on the right side is  $L_2$ . From 0 to 141 15 s, all voltages were turned off, and the concentrated sample zone was allowed to 142 143 hydrodynamically flow across the intersection to channel  $L_4$ ,  $L_2$  and  $L_3$ . At t = 15 s, the fluorescence intensity at the channel intersection became weak, indicating the 144 concentrated sample has been totally moved out of L<sub>2</sub>, so the reversed voltage was 145 146 turned on. The record from 16 to 22 s corresponds to the reversed-voltage concentration process. The GFP zone in  $L_4$  was pushed to the intersection. At t = 23 s, 147 voltages of 1.60 kV, 1.60 kV and 2 kV were applied to SW, SR and BR, respectively, 148 149 and BW was grounded as described in Step 5. Then the sample zone at the top end of  $L_4$  was pushed into  $L_4$  and separated. 150

### 151 Reproducibility test results of BSA sweeping



152

Figure S2. Electrophorograms of three parallel runs of separation, including washing,
conditioning the microchip and consecutive 5-step electrophoresis. Each electrophorogram
represents for 5 consecutive 5-step electrophoresis in one run.

## 156 Further investigation and discussion on the separation of GFP and GFP-IGF-I

For the separation of the mixture sample of GFP and GFP-IGF-I, very sharp GFP 157 peaks were obtained. However, the GFP-IGF-I peak was relatively broad. The 158 159 isoelectric points of GFP and IGF-I are 5.3 and 8.2, respectively, it is assumed that the 160 fusion protein GFP-IGF-I has a pI value higher than GFP. We have also examined the 161 electrophoresis of only GFP-IGF-I under the same concentration condition (Fig. S3a), 162 it can be seen that the sweeping is pretty effective, although the signal enhancement factor is smaller than that of GFP, which may be caused by the less affinity of BSA 163 164 with GFP-IGF-I than with GFP. But it can be presumed that with further optimization of the BSA concentration, pH and sweeping length, the signal enhancement factor 165 could be improved. While in the mixture of the two proteins, limited amount of BSA 166 167 would first interact with GFP, which has more affinity, and GFP-IGF-I could not be 168 swept as effective as it is swept alone. This may explain why the peak of GFP-IGF-I was not as much sharpened as the peak of GFP in the mixture of the two proteins (Fig. 169 S3b). This provides a very interesting aspect of the competition affinity reaction 170 between different proteins. Also, as the channel surface is negatively charged, the 171 172 peak broadening is presumably also due to the protein adsorption to the channels wall, because GFP-IGF-I may be closer to its neutral state under pH 7.5. 173

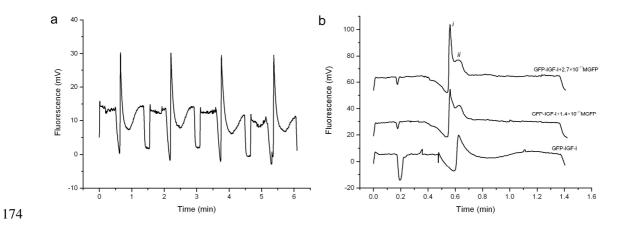


Figure S3. a) Four consecutive electropherograms of GFP-IGF-I. b) Comparison of the
electropherograms of GFP-IGF-I mixed with different concentrations of GFP. Based on the peak
height, it is deduced that peak *i* corresponds to GFP and peak *ii* corresponds to GFP-IGF-I.
Electrophoresis condition: running buffer, TB with 2% BSA; sample buffer, TB.