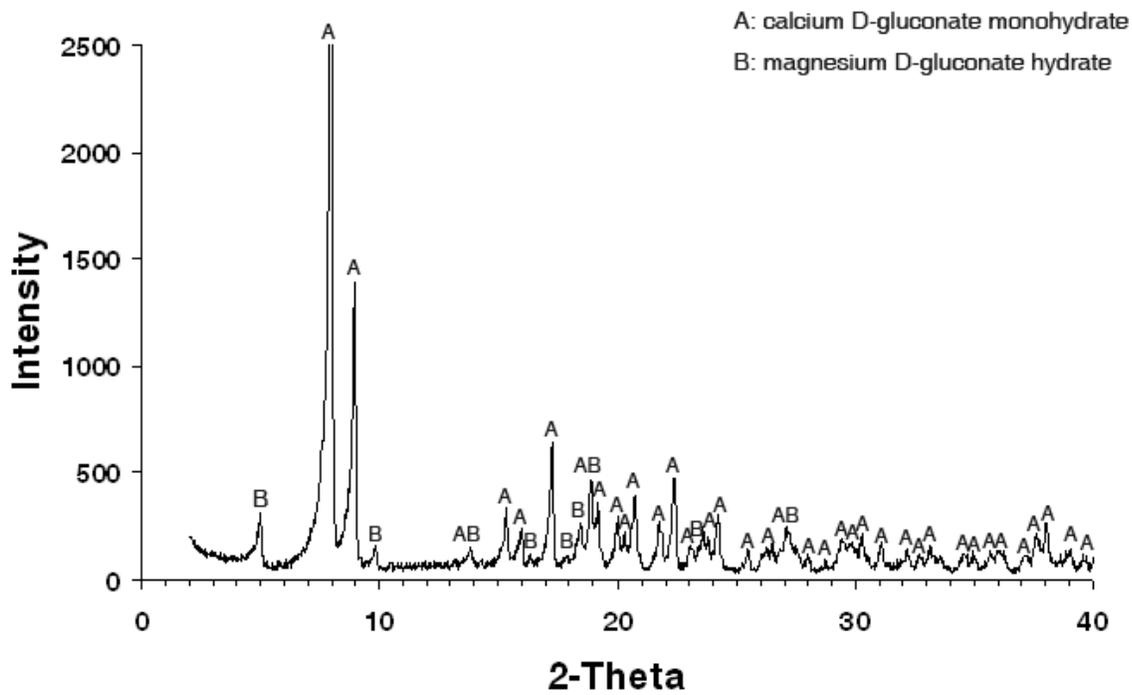


## Synthesis of sintering-resistant sorbents for CO<sub>2</sub> capture

*Wenqiang Liu,<sup>†</sup> Bo Feng,<sup>\*</sup> Yueqin Wu,<sup>†</sup> Guoxiong Wang,<sup>‡</sup> John Barry,<sup>§</sup> and João C. Diniz da Costa<sup>‡</sup>*  
<sup>†</sup>School of Mechanical and Mining Engineering, <sup>‡</sup>School of Chemical Engineering, The University of Queensland, St Lucia, Qld 4072, Australia, <sup>§</sup>PicaMs Pty Ltd., PO Box 378, Kenmore, QLD 4069, Australia

Environmental Science & Technology, 22<sup>nd</sup> February 2010

7 pages, 5 figures included



**Figure S1 XRD patterns of solids after first-heating-step (drying) from solution mixture of calcium D-gluconate monohydrate and magnesium D-gluconate hydrate.**

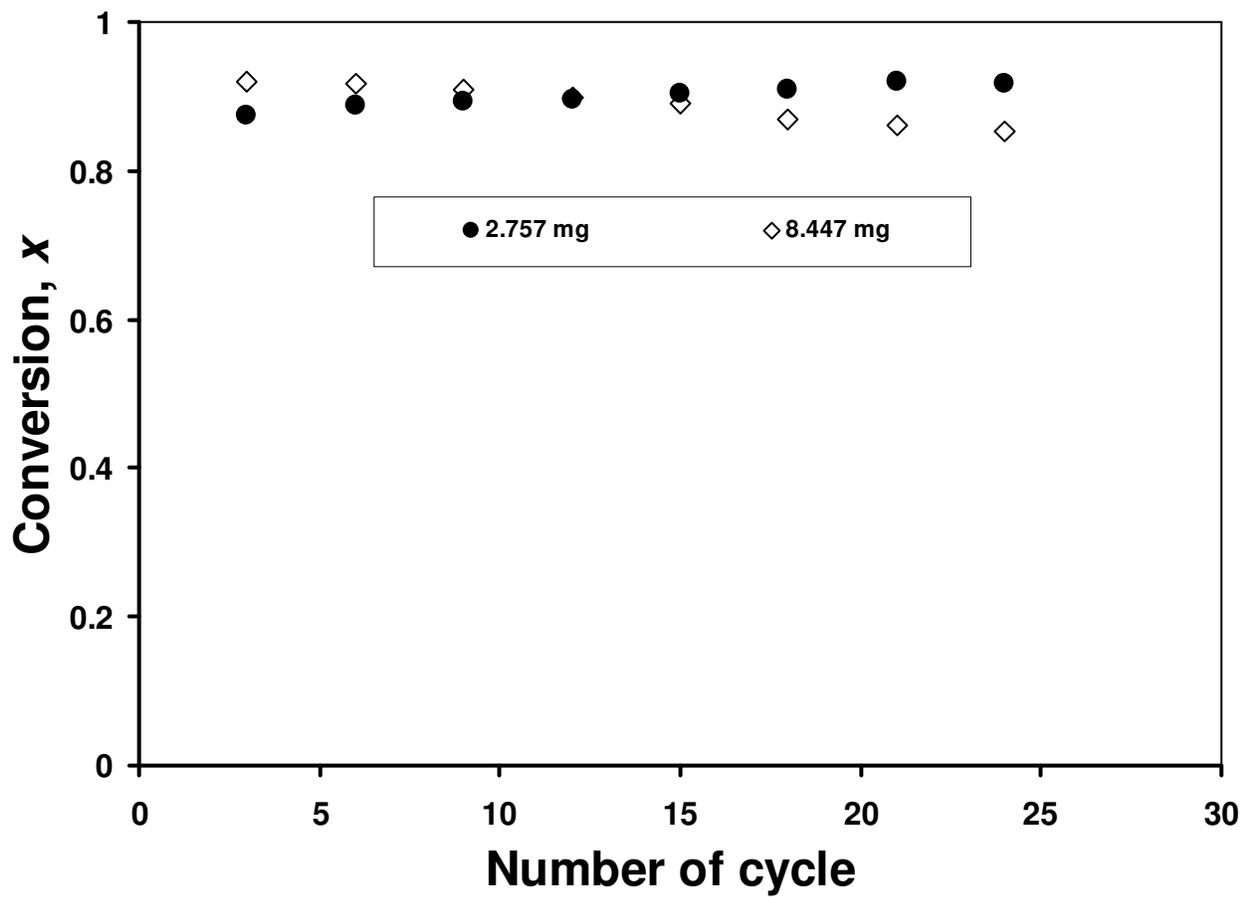
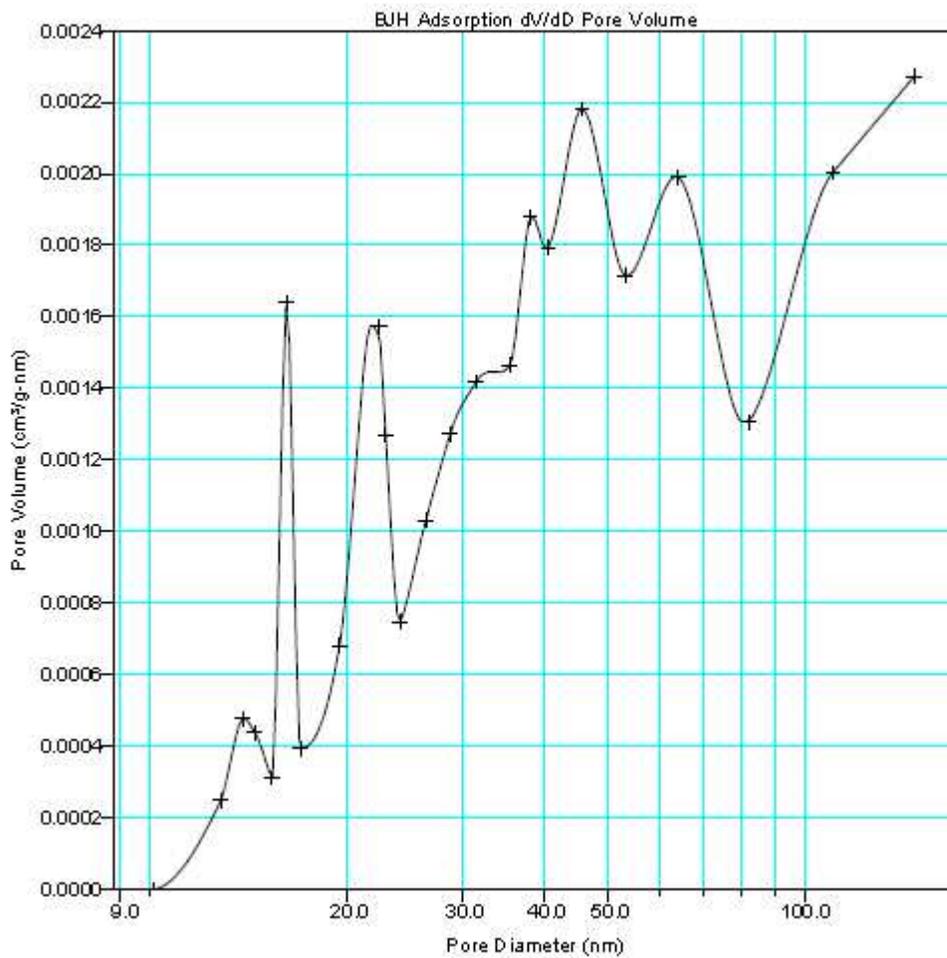


Figure S2 The influence of sample mass on the conversion of the solid sorbent CGMG75.



**Figure S3 Pore size distribution for sorbent CGMG75.**

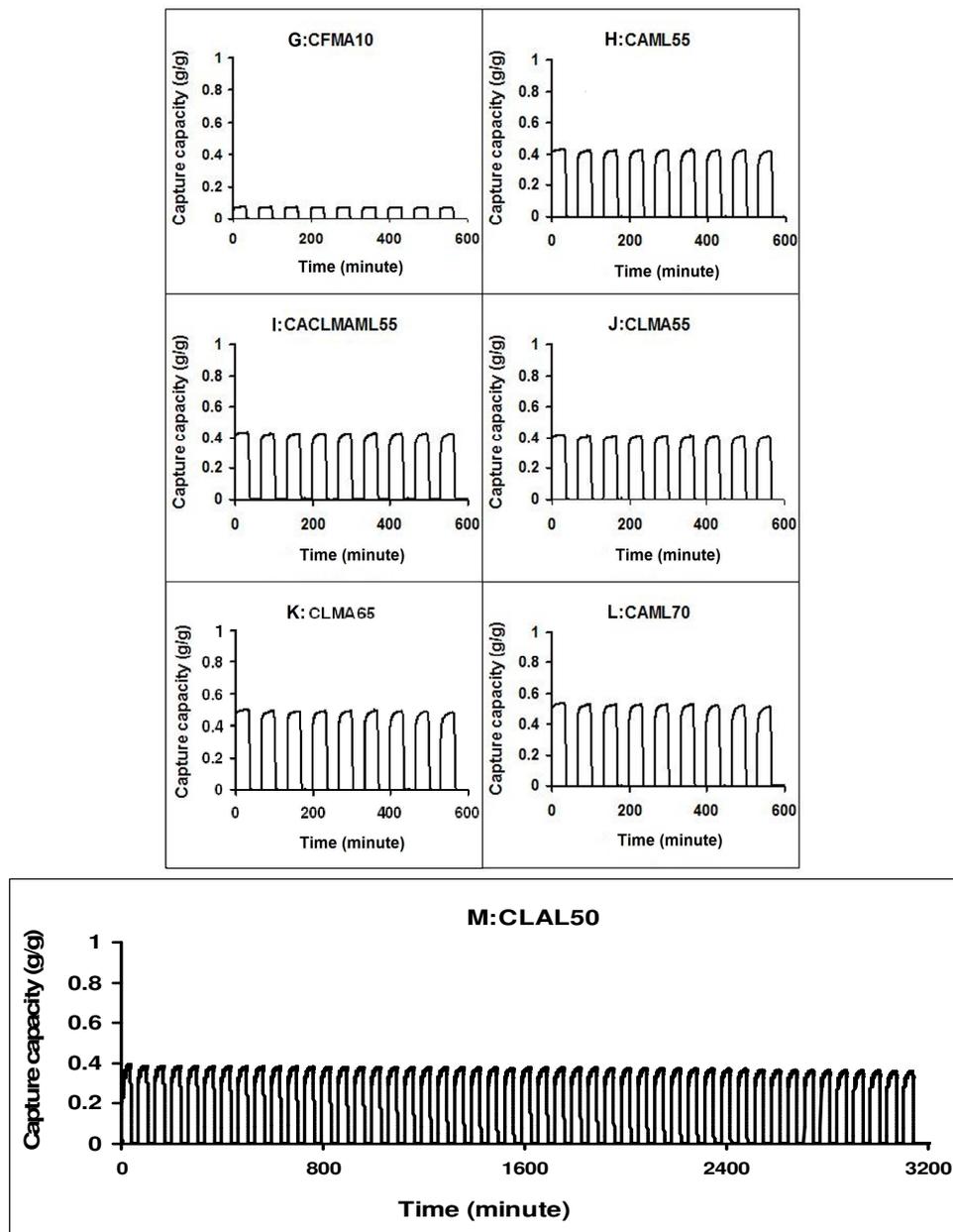
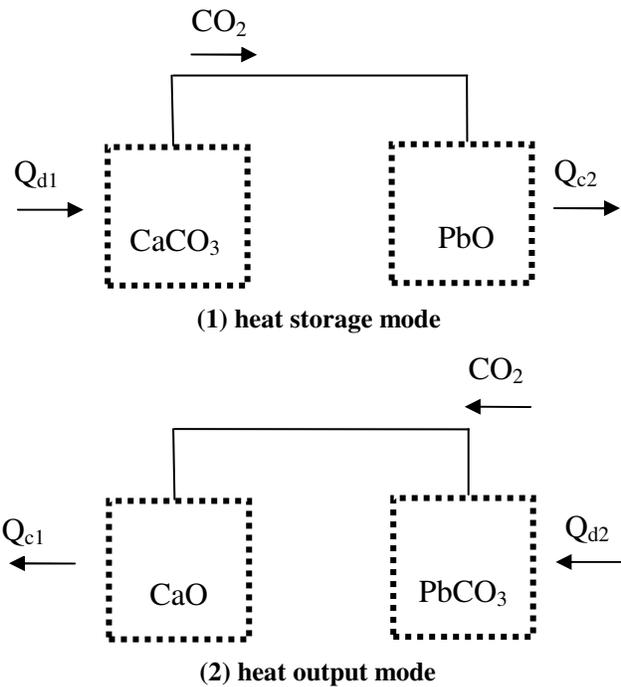


Figure S4 TGA profiles of CO<sub>2</sub> capture capacity for sorbents synthesized from various precursors.



**Figure S5 A schematic description of process of a chemical heat pump.**

**Principle of a chemical heat pump:** Kato et al. (S1) proposed a  $\text{CaO/PbO/CO}_2$  chemical heat pump, the principle of which is illustrated in Figure S5. The system has  $\text{CaO}$  and  $\text{PbO}$  reactors that originally charged with  $\text{CaCO}_3$  and  $\text{PbO}$ . With the operation of this system, a heat that has a higher temperature than the original heat source can be obtained. There are two operation modes in this system:

Storage mode: the  $\text{CaO}$  reactor received heat from a heat source and  $\text{CaCO}_3$  was decarbonated to  $\text{CaO}$  and  $\text{CO}_2$ .  $\text{CO}_2$  was reacted with  $\text{PbO}$  in the  $\text{PbO}$  reactor to form  $\text{PbCO}_3$  and the exothermic heat of the carbonation was recovered. It was suggested that over  $860\text{ }^\circ\text{C}$  was the optimal temperature for  $\text{CaCO}_3$  decarbonation and  $300\text{ }^\circ\text{C}$  was the optimal for the carbonation.

Heat supply mode:  $\text{PbCO}_3$  was decomposed by the heat and  $\text{CO}_2$  was formed and introduced into the  $\text{CaO}$  reactor. Then  $\text{CaO}$  was reacted with the  $\text{CO}_2$  to generate heat because of the exothermic reaction. It was suggested that optimal decarbonation temperatures were  $440\text{ }^\circ\text{C}$  or  $450\text{ }^\circ\text{C}$  and  $880\text{ }^\circ\text{C}$  for  $\text{CaO}$  carbonation.

**3D percolation theory:** This theory (see the reference for details. Ewen, P. J. S. & Robertson, J. M. A percolation model of conduction in segregated systems of metallic and insulating materials: Application to thick film resistors. *J. Phys. D: Appl. Phys.* **1981**, *14*, 2253-2268.) predicts that minimum weight percentage of support material (MgO) to maintain a continuum framework to separate is 15 vol.%. Therefore the maximum CaO can be calculated to be 85 vol.%. Assuming the particles are spherical, the corresponding weight fraction (82.7 wt.% for CaO and 17.3 wt.% for MgO) then can be calculated by their densities.

**Theoretical value of maximum CO<sub>2</sub> capture capacity** is calculated when assuming 100% CaO conversion. Theoretical value of maximum CO<sub>2</sub> capture capacity= CaO weight fraction x (molecular weight of CO<sub>2</sub>/molecular weight of CaO). For example when CaO content is 50%, the theoretical value of max CO<sub>2</sub> capture capacity = 0.5 x (44/56)=0.393 g-CO<sub>2</sub>/g-sorbent.

(S1) Kato, Y., Harada, N. & Yoshizawa, Y. Kinetic feasibility of a chemical heat pump for heat utilization of high-temperature processes. *Appl. Therm. Eng.* **1999**, *19*, 239-254.