

## SUPPORTING INFORMATION

### A physico-chemical characterisation of particulate emissions from a compression ignition engine employing two injection technologies and three fuels

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**Table S1:** Engine specifications.

Item	Specification
Model	Perkins 1104C-44
Cylinders	4 in-line
Capacity (L)	4.41
Bore × stroke (mm)	105 × 127
Maximum power (kW/rpm)	64/2400
Maximum torque (Nm/rpm)	302/1400
Compression ratio	19.25:1
Aspiration	Naturally aspirated
Emissions certification	EU Stage II non-road

**Table S2:** Speed and load settings investigated in this study.

Mode number	Speed (rpm)	Load (%)
1	1400 (Intermediate)	50
2	1400 (Intermediate)	100
3	2400 (Rated)	50
4	2400 (Rated)	100

**Table S3:** Fuel specifications.

Property	ULSD	B20	Synthetic
Density (kg/L) ASTM	0.8354	0.8393	0.8308
D4052			
Kinematic viscosity (mm <sup>2</sup> /s) @ 40 °C ASTM	2.7189	3.1228	3.2195
D445			
Flash point (°C) ASTM	66.5	71.5	73.5
D93			
Distillation (°C) ASTM			
D86	205	220	225
10%	266	289	277
50%	327	335	335
90%	340	344	344
95%			
Calculated cetane index	51.6	55.2	57.4
ASTM D4737			
Sulphur content (mg/kg)	4.5	5.9	5.0
ASTM D 5453			
Carbon (% mass) ASTM	84.6	85.4	84.2
D5291			
Hydrogen (% mass) ASTM	14.2	13.4	14.4
D5291			
Water and sediment (%)	< 0.01	< 0.01	< 0.01

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volume) ASTM D2709

Polycyclic aromatic hydrocarbons (% mass) IP	1.2	0.96	1.5
391			
Fatty Acid Methyl Ester content (% volume) EN	-	19.6	-
14078			
Acid number ASTM D664 (mg KOH/g)	-	0.07	-

**Table S4:** Tabulated results for all emissions parameters reported in this study. Uncertainties are calculated as  $\pm$  one standard error of the mean.

NC denotes that the standard error was not computed as the measurement was not replicated.

Fuel	Speed/load (rpm/%)	Injection configuration	Primary Dilution Ratio	Secondary Dilution Ratio	Total Dilution Ratio	PM <sub>2.5</sub> (g/kWh)	Particle number concentration (#/cm <sup>3</sup> )	CMD (nm)	ROS (nmol/mg)	PAHs (mg/kWh)	Organic volume percentage (%)
ULSD	1400/50	Direct Injection	26.7	10.2	270.6	0.20 $\pm$ 0.003	2.6E+14 $\pm$ 2.0E+13	72.3 $\pm$ 1.6	14.2 $\pm$ 5.3	10.8 $\pm$ 7.4	0.004
ULSD	1400/100	Direct Injection	26.8	10.0	266.6	3.03 $\pm$ 0.18	1.2E+15 $\pm$ 1.3E+13	115.6 ± 0.4	0.1 $\pm$ 0.1	4.7 $\pm$ 1.8	20.2
ULSD	2400/50	Direct Injection	20.4	9.8	163.7	0.25 $\pm$ 0.01	1.0E+15 $\pm$ 2.3E+13	68.3 ± 0.3	12.1 $\pm$ 2.7	5.8 $\pm$ 0.5	0.2
ULSD	2400/100	Direct Injection	14.2	10.7	151.6	0.68 $\pm$ 0.01	1.3E+15 $\pm$ 8.0E+13	82.0 ± 0.3	3.8 $\pm$ 0.9	7.0 $\pm$ 1.8	0.8
B20	1400/50	Direct	30.1	9.6	288.6	0.16	2.3E+14	71.7	32.8 ± 17.8	9.1 $\pm$ 8.2	17.6

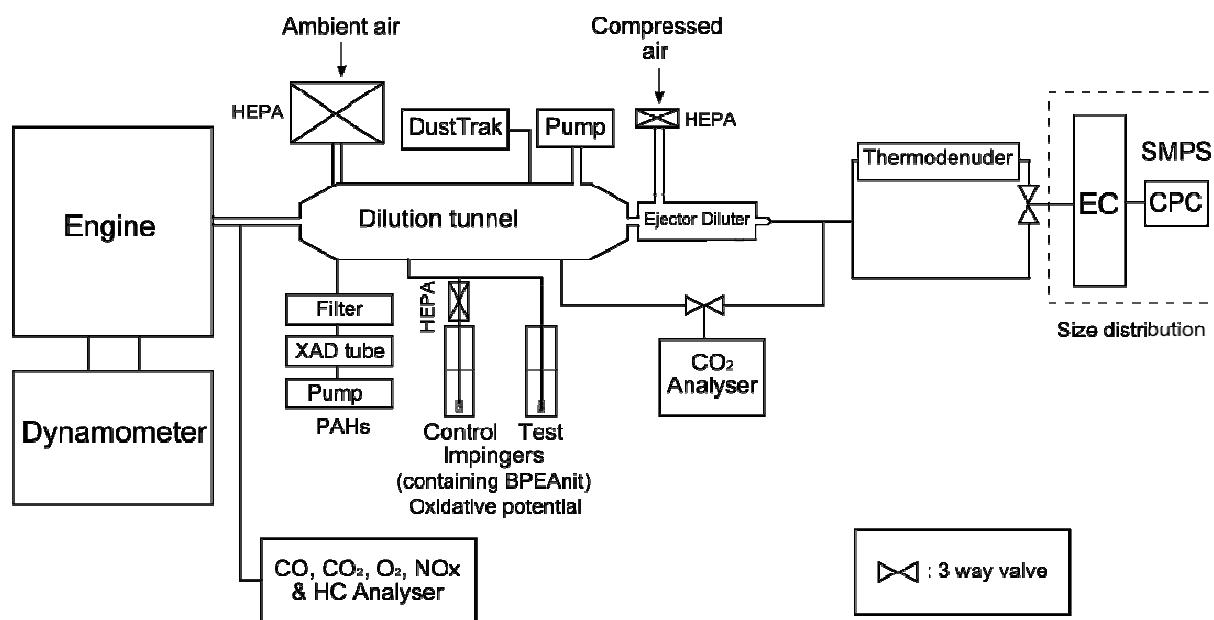
		Injection				$\pm 0.02$	$\pm 1.7E+12$	$\pm 2.2$			
B20	1400/100	Direct Injection	30.0	9.7	290.9	2.16 $\pm 0.11$	1.1E+15 $\pm 1.4E+13$	109.9 $\pm$ 1.7	2.1 $\pm 1.0$	5.1 $\pm 4.6$	14.1
B20	2400/50	Direct Injection	17.3	11.4	197.0	0.22 $\pm 0.01$	1.1E+15 $\pm 4.3E+13$	67.5 $\pm$ 1.4	18.6 $\pm 8.3$	21.5 $\pm 9.7$	20.1
B20	2400/100	Direct Injection	16.7	10.5	175.0	0.55 $\pm 0.002$	1.3E+15 $\pm 9.5E+12$	79.0 $\pm$ 0.7	0.9 $\pm 0.9$	3.2 $\pm 0.3$	31.4
Synthetic	1400/50	Direct Injection	38.1	8.2	313.6	0.20 $\pm 0.01$	2.4E+14 $\pm 1.5E+13$	71.9 $\pm 0.6$	27.8 $\pm$ 3.3	10.2 $\pm 7.5$	1.0
Synthetic	1400/100	Direct Injection	41.2	7.9	326.3	3.38 $\pm 0.07$	1.1E+15 $\pm 3.3E+13$	120.0 $\pm$ 0.4	1.1 $\pm$ 0.3	6.6 $\pm 3.8$	10.9
Synthetic	2400/50	Direct Injection	21.1	9.2	192.5	0.29 $\pm$ 0.01	9.1E+14 $\pm 4.3E+13$	69.9 $\pm$ 0.3	8.4 $\pm$ 2.1	20.9 $\pm 9.6$	0.4
Synthetic	2400/100	Direct Injection	21.3	9.2	196.2	0.81 $\pm 0.005$	1.3E+15 $\pm 6.4E+13$	86.0 $\pm$ 0.4	2.1 $\pm 0.9$	28.7 $\pm 28.3$	6.1
ULSD	1400/50	Common	24.5	8.1	198.2	0.048 $\pm$	1.2E+14	68.1 $\pm$	284.1	28.6	3.2

		Rail				0.03	$\pm 2.8E+12$	0.6	$\pm NC$	$\pm NC$	
ULSD	1400/100	Common Rail	26.6	8.8	234.4	1.59 $\pm$ 0.17	8.6E+14 $\pm 5.2E+13$	120.8 $\pm 2.8$	7.9 $\pm NC$	26.8 $\pm 5.8$	10.7
ULSD	2400/50	Common Rail	15.8	9.9	155.4	0.36 $\pm$ 0.03	2.1E+14 $\pm 6.6E+12$	60.9 $\pm$ 0.9	149.0 $\pm NC$	16.9 $\pm 9.5$	0.8
ULSD	2400/100	Common Rail	16.2	9.2	148.5	0.805 $\pm$ 0.12	1.3E+15 $\pm 4.7E+13$	91.9 $\pm$ 1.3	13.2 $\pm NC$	6.4 $\pm 2.6$	12.5
B20	1400/50	Common Rail	19.9	10.9	215.1	0.029 $\pm$ 0.05	9.1E+13 $\pm$ 9.4E+12	65.8 $\pm$ 1.2	202.2 $\pm 43.4$	7.5 $\pm 0.6$	7.9
B20	1400/100	Common Rail	24.5	10.3	251.4	0.972 $\pm$ 0.14	7.2E+14 $\pm 5.9E+13$	110.4 $\pm$ 0.3	8.1 $\pm 4.5$	34.6 $\pm 20.8$	38.4
B20	2400/50	Common Rail	16.9	10.7	180.7	0.028 $\pm$ 0.04	1.7E+14 $\pm 2.4E+13$	58.3 $\pm$ 0.03	233.0 $\pm 18.7$	14.0 $\pm NC$	11.7
B20	2400/100	Common Rail	17.5	9.63	168.6	0.538 $\pm$ 0.10	1.1E+15 $\pm 5.2E+13$	84.8 $\pm$ 0.5	5.1 $\pm 2.9$	14.7 $\pm 11.7$	36.3
Synthetic	1400/50	Common	28.8	6.9	200.1	0.035	7.9E+13 $\pm$	66.9	139.9	10.5	35.7

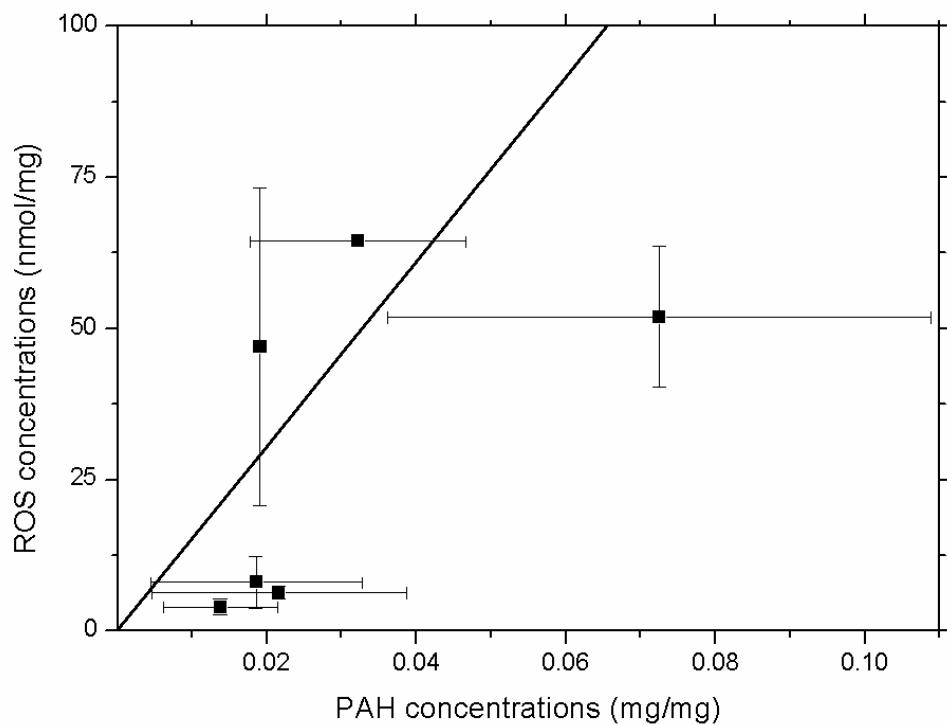
		Rail				$\pm 0.03$	$1.2\text{E}+13$	$\pm 1.2$	$\pm 139.9$	$\pm \text{NC}$	
Synthetic	1400/100	Common Rail	32.5	8.4	272.4	$0.954 \pm 0.11$	$6.3\text{E}+14 \pm 2.6\text{E}+13$	$113.2 \pm 0.4$	$6.2 \pm 0.1$	$29.7 \pm \text{NC}$	56.9
Synthetic	2400/50	Common Rail	18.3	9.5	175.2	$0.030 \pm 0.03$	$1.6\text{E}+14 \pm 2.0\text{E}+12$	$60.2 \pm 0.7$	$358.4 \pm 21.1$	$80.4 \pm \text{NC}$	30.5
Synthetic	2400/100	Common Rail	20.2	9.3	188.8	$0.522 \pm 0.03$	$9.7\text{E}+14 \pm 2.2\text{E}+13$	$89.9 \pm 1.0$	$12.7 \pm 2.1$	$5.9 \pm \text{NC}$	54.3

**Table S5:** Weighting factors for the 4 mode test cycle adopted in this study.

Mode number	Speed (rpm)	Load (%)	ECE R49 weighting	Test cycle averaging (this study)
1	1400	50	0.08	0.178
2	1400	100	0.25	0.556
3	2400	50	0.02	0.044
4	2400	100	0.10	0.222

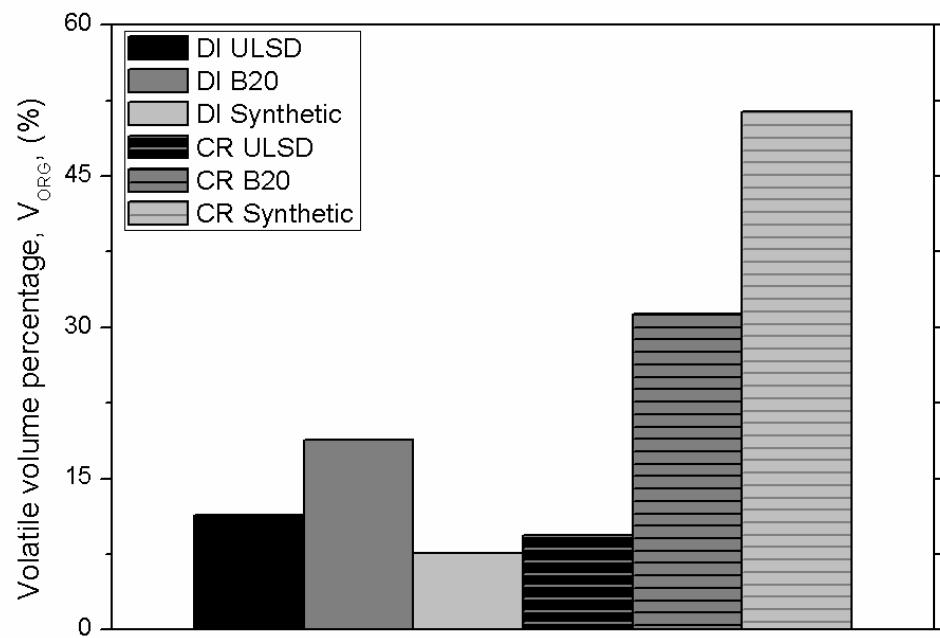


**Figure S1:** A schematic of the experimental set-up utilised in this study.



**Figure S2:** A graph demonstrating correlation between the ROS and PAH measurements.

Note: both the PAHs and ROS are expressed on a per unit mg of DPM basis. The Pearson correlation co-efficient,  $r$ , is 0.913.



**Figure S3:** Test cycle averaged volatile volume percentage of particles for both injection technologies, and all three fuels.