

Improved Design and Efficiency of the Extractive Distillation Process for Acetone-Methanol with Water

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Supporting information

Appendix S1 Sizing and economic cost calculation

The diameter of a distillation column is calculated using the *tray sizing* tool in Aspen Plus software.

The height of a distillation column is calculated from the equation:

$$H = \frac{N}{e_T} \times 0.6096 \quad \text{N tray stage except condenser and reboiler, } e_T \text{ tray efficiency is taken as 100% in}$$

this work.

The heat transfer areas of the condenser and reboiler are calculated using following equations:

$$A = \frac{Q}{u \times \Delta T} \quad u: \text{overall heat transfer coefficient(kW}\cdot\text{K}^{-1}\cdot\text{m}^{-2}), u=0.852 \text{ for condenser, } 0.568 \text{ for reboiler.}$$

The capital costs of a distillation column are estimated by the following equations:

$$\text{Shell cost} = 22522.8D^{1.066}H^{0.802}$$

$$\text{Tray cost} = 1423.7D^{1.55}H$$

$$\text{HeatExchanger cost} = 9367.8A^{0.65}$$

Table S1. Binary Interaction Parameters* for UNIQUAC Model of Acetone-Methanol-Water

| Component i | Acetone | Acetone | Methanol |
|-------------|----------|----------|----------|
| Component j | Methanol | Water | Water |
| Aij | 0 | 8.6051 | -1.0662 |
| Aji | 0 | -4.8338 | 0.6437 |
| Bij | -225.153 | -3122.58 | 432.8785 |
| Bji | 52.7705 | 1612.196 | -322.131 |

$$* \text{ K unit, } \tau_{ij} = \exp(A_{ij} + B_{ij}/T + C_{ij}\ln T + D_{ij}T + E_{ij}/T^2)$$

Table S2. Sizing parameters for the optimal designed columns and cost data from closed loop simulation for the extractive distillation of acetone – methanol with water

| column | Case 1 | | Case 2b | | Case 3opt | |
|--|----------------|----------------|----------------|----------------|----------------|----------------|
| | C ₁ | C ₂ | C ₁ | C ₂ | C ₁ | C ₂ |
| Diameter / m | 2.88 | 1.92 | 2.66 | 1.77 | 2.88 | 1.72 |
| Height / m | 33.53 | 14.63 | 33.53 | 14.63 | 33.53 | 14.63 |
| I _{CS} / 10 ⁶ \$ | 1.164 | 0.389 | 1.069 | 0.356 | 1.164 | 0.346 |
| A _C / m ² | 601 | 284 | 518 | 244 | 679 | 229 |
| A _R / m ² | 551 | 371 | 469 | 319 | 412 | 309 |
| I _{HE} / 10 ⁶ \$ | 1.166 | 0.807 | 1.055 | 0.731 | 1.118 | 0.709 |
| Cost _{cap} / 10 ⁶ \$ | 2.576 | 1.252 | 2.341 | 1.137 | 2.528 | 1.102 |
| Cost _{ope} / 10 ⁶ \$ | 1.290 | 0.869 | 1.097 | 0.746 | 0.967 | 0.722 |
| Cost _{CA} / 10 ⁶ \$ | 2.148 | 1.287 | 1.877 | 1.125 | 1.809 | 1.089 |
| Q _{HA} / MW | 1.24 | | 0.91 | | 0.58 | |
| Cost _{HA} / 10 ⁶ \$ | 0.035 | | 0.028 | | 0.021 | |
| TAC / 10 ⁶ \$ | 3.469 | | 3.030 | | 2.918 | |
| OF / kJ/kmol | 36247.5 | | 30916.2 | | 28318.5 | |