Supporting information

Electrokinetic control of bacterial deposition and transport

Jinyi Qin¹, Xiaohui Sun², Yang Liu², Tom Berthold¹, Hauke Harms¹, Lukas Y. Wick^{1,2}*

¹ UFZ - Helmholtz Centre for Environmental Research, Department of Environmental Microbiology, 04318 Leipzig, Germany

² University of Alberta, Department of Civil and Environmental Engineering, 3-133 Markin/CNRL Natural Resources Engineering Facility, Edmonton, AB, T6G 2W2, Canada

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*Corresponding author: Mailing address: Helmholtz Centre for Environmental Research - UFZ. Department of Environmental Microbiology; Permoserstrasse 15; 04318 Leipzig, Germany. phone: +49 341 235 1316, fax: +49 341 235 1351, e-mail: <u>lukas.wick@ufz.de</u>.

1 Theory and Calculations

2

3 *Calculation of the collision efficiency* (α_t)

4 The collision efficiency (α_t) of bacteria was calculated applying the clean-bed filtration 5 theory ¹ (eq. 2). The α_t of bacteria is defined as the ratio of the rate of attachment (n_t) to the 6 rate of bacterial transport to the surfaces (n_{trans}) . Therefore, α_t represents the relative affinity 7 of bacteria for the packing material and $\alpha_{t,0}$ represents the initial collision efficiency. DC free 8 control runs $(\alpha_{t,0} \text{ control})$ and runs in the presence of an electric field $(\alpha_{t,DC})$ are subject to the 9 different percolation regimes and were compared with the percentage change was

10
$$Percentage \ change = \frac{\alpha_{t,control} - \alpha_{t,DC}}{\alpha_{t,0}} \times 100$$
(1)

11 Values of n_{trans} were calculated taking into account the contributions of convection, diffusion, 12 van der Waals attraction, and sedimentation ². For the calculations, we assumed spheres of 13 identical size glass beads (diameter: 0.1 mm) in their closest packing, and identical effective 14 bacterial radius (1 μ m) of the bacteria. Values of n_t were calculated from C/C₀ values 15 obtained in column experiments.

16
$$C = C_0 \exp\left(-\frac{3(1-\varepsilon)}{4a_s}n_{trans}\alpha_t L\right)$$
(2)

where *C* is the effluent cell concentration, C_0 the influent cell concentration, ε the porosity of the packed bed, a_s the radius of the glass beads, *L* the length of the column, and n_t the transport of bacteria from the solution to the glass surface in the whole experimental time. n_{trans} was approximated by applying the solution to convection-diffusion equation (eq. 3):

21
$$n_{trans} = A_s \frac{A_{132}}{9\pi\eta a_b^2 \upsilon} \frac{a_b^{1.875}}{a_s} + 0.00338A_s \frac{2a_b^2(\rho_b - \rho_l)g}{9\eta\upsilon} \frac{a_b^{1.2}}{a_s} + 4A_s^{0.33} \frac{12\upsilon a_s\pi\eta a_b^{-0.67}}{kt}$$
(3)

22
$$A_{s} = \frac{2(1 - (1 - \varepsilon)^{1.67})}{2 - 3(1 - \varepsilon) + 3(1 - \varepsilon)^{1.67} - 2(1 - \varepsilon)^{2}}$$
(4)

with ε being the porosity of column (0.41), a_b and a_s are the radii of bacteria ($a_b = 10^{-6}$ m) and the glass beads ($a_s = 5 \times 10^{-5}$ m), respectively, η and ρ_l are the absolute viscosity ($\eta = 3.19$ kg m⁻¹ h⁻¹) and density of buffer solution ($\rho = 1000 \text{ kg m}^3$), v is the approach velocity (1.1×10^{-4} m s⁻¹), g is the gravitational acceleration (9.81 ms⁻²), k is the Bolzmann constant (1.38 × 10⁻²³ J K⁻¹), t is the room temperature of 293K. ρ_b is the density of the bacteria solution, ($\rho_b = 1090$ kg m³) and A₁₃₂ is the Hamaker constant ² as described by eq. 5⁻³

29
$$A_{132} = (\sqrt{A_{11}} - \sqrt{A_{33}})(\sqrt{A_{22}} - \sqrt{A_{33}})$$
(5)

Here, A_{ii} denotes the individual Hamaker constant of bacteria (A_{11}) , glass (A_{22}) and water (A_{33}), respectively. A_{33} was taken from literature ⁴ whereas A_{11} and A_{22} were obtained by eq. 6 ⁵.

33
$$A_{ii} = 6\pi l_0^2 \gamma_i^{LW}$$
 (6)

According to Fowkes ⁵, the value of $6\pi l_0^2$ equals 1.44×10^{-18} m², with l_0 being the minimum distance between the outermost cell surface and the glass bead (0.157 nm) ⁶. Thus, the individual and effective Hamaker constants in media were assessed in Table S2. Derick et al. have reported that Hamaker constant (A₁₃₂) values range from 0.28 to 3.46×10^{-21} J for quartz surface ⁶. For the interaction of cellulose with SiO₂, the Hamaker constant was in the range of 0.32 - 0.38⁷. The value of the Hamaker constant used in our study is consistent with these values.

41

42 Calculations of surface coverage and the fraction of bacteria retained

Assuming that the entire glass surface allows for irreversible adhesion, the fraction ofbacterial coverage on the surface can be described by eq. 7:

$$\theta = \frac{N_b \pi a_b^2}{N_s 4 \pi a_s^2} \tag{7}$$

46 where N_s and N_b are the numbers of collectors and bacteria in the column and a_b and a_s the 47 radii of bacteria and the collectors, respectively ⁸.

48 The fraction of bacteria retained in the column, R is calculated by eq. 8:

49
$$R = \int (1 - \frac{C}{C_0}) \cdot dV \tag{8}$$

where C and C₀ are the effluent and influent cell concentrations of the column, and V the flow of the cell suspension ($V = 19 \text{ ml h}^{-1}$) through the column ^{9, 10}.

53 Calculation of XDLVO interaction energy of bacterial adhesion

According to the extended DLVO theory ¹¹, the XDLVO interaction energy of bacterial adhesion (G_{XDLVO}) is composed of the acid-base (G_{AB}) interaction energy, the electrostatic repulsion (G_{EDL}), and the Lifshitz-van der Waals (G_{LW}) energy (eq. 9) ¹¹:

57
$$G_{XDLVO} = G_{AB} + G_{EDL} + G_{LW}$$
(9)

58 *Acid-base interaction energy* (G_{AB}). The acid-base interaction energy (G_{AB}) depends on the 59 Gibbs free energy of the bacteria and the glass as given by eq. 10, in which a_b is the radius of 60 bacteria (1 µm), and h is the separation distance between the bacterium and the surface. The λ 61 is the characteristic decay length of AB interaction in water (estimated 0.6nm)¹¹.

62
$$G_{AB} = 2\pi a_b \Delta G^{AB} \lambda \exp(\frac{l_0 - h}{\lambda})$$
(10)

63 ΔG^{AB} is the acid-base component of the free energy interaction at contact given by eq. 11^{12,13}

64
$$\Delta G^{AB} = 2 \begin{bmatrix} (\sqrt{\gamma_b^+} - \sqrt{\gamma_s^+})(\sqrt{\gamma_b^-} - \sqrt{\gamma_s^-}) - (\sqrt{\gamma_b^+} - \sqrt{\gamma_l^+})(\sqrt{\gamma_b^-} - \sqrt{\gamma_l^-}) \\ -(\sqrt{\gamma_s^+} - \sqrt{\gamma_l^+})(\sqrt{\gamma_s^-} - \sqrt{\gamma_l^-}) \end{bmatrix}$$
(11)

65

The surface Gibbs free energies of bacteria γ_b and the glass surface γ_s (mJ m⁻²) were calculated based on measured contact angles (θ) of microbial lawns, membrane filters and glass surfaces using water, formamide and methylene iodide as liquids using the Young equation according to eq. 12:

70
$$Cos(\theta) = -1 + 2\frac{\sqrt{\gamma_b^{LW}\gamma_l^{LW}}}{\gamma_l^{total}} + 2\frac{\sqrt{\gamma_b^+\gamma_l^-}}{\gamma_l^{total}} + 2\frac{\sqrt{\gamma_b^-\gamma_l^+}}{\gamma_l^{total}}$$
(12)

The total surface Gibbs free energies (γ^{total}) thereby were separated in a Lifshitz-van der Waals (γ^{LW}) and an acid-base component (γ^{AB}) (eq. 13) with γ^+ and γ^- as the electron acceptor and the electron donor components of acid-base surface energy (eqs. 13 & 14).

$$\gamma^{total} = \gamma^{AB} + \gamma^{LW} \tag{13}$$

$$\gamma_i^{AB} = 2\sqrt{\gamma_i^+ \gamma_i^-} \tag{14}$$

Using literature data ¹⁴ of γ , γ^{LW} , γ^+ , γ^- values for water, formamide and methyleneiodide, the parameters γ_b , γ_b^{LW} , γ_b^+ , γ_b^- of bacteria were calculated as proposed by van Oss et al¹⁵, and the data from literature taken for assessing the free energy of the glass surface ¹⁶.

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80 Electrostatic repulsion energy, (G_{EDL}). The electrostatic repulsion energy between bacteria 81 and the glass surface was calculated by eq. 15¹¹:

82
$$G_{EDL} = \pi \varepsilon_0 \varepsilon_r a_b \left\{ 2\xi_b \xi_s \ln \left[\frac{1 + \exp(-\kappa h)}{1 - \exp(-\kappa h)} \right] + (\xi_b^2 + \xi_s^2) \ln \left[1 - \exp(-2\kappa h) \right] \right\}$$
(15)

where κ^{-1} is the thickness of electrical double layer (EDL, nm) as calculated by the Guoy-Chapman theory with *C* and z being the molar bulk concentration and the charge number of the electrolytes¹⁴ (eq. 16).

86

$$\kappa^{-1} = \left[3.29z C^{1/2} \right]^{-1} \tag{16}$$

For a 10 mM and a 100 mM buffer solution, a κ^{-1} of 2.15 nm (10 mM buffer) and κ^{-1} of 0.65 nm (100 mM buffer) were calculated.

89

90 Lifshitz-van der Waals interaction energy (G_{LW}). With given values of the effective 91 Hamaker constant, the Lifshitz-van der Waals interaction energy can be calculated by eq. 17 92 ^{13-15, 17}

93
$$G_{LW} = -\frac{A_{132}}{6} \left[\frac{2a_b(h+a_b)}{h(h+2a_b)} - \ln(\frac{h+2a_b}{h}) \right]$$
(17)

95 Tables

	Contact angle (<i>O</i>)			Surface free energy γ (mJ m ⁻²) ¹				
	Θ _w	Θ_f	Θ _m	۲	γ⁺	γ^{AB}	۲ ^۲ ۳	γ^{Tot}
Water				25.5	25.5	51	21.8	72.8
Formamide				39.6	2.3	19	39	58
Methyleneiodide				<0.1	<0.1	≈0	50.8	50.8
P. fluorescens Lp6a	16.1	35.1	54.4	61.7	0.9	14.8	31.7	46.5
Glass	23	16	53	50.8	3	24.8	32.4	57.2

- **Table S1.** Overview of the surface free energy (γ) and the contact angles of water θ_{w} ,
- 99 methylene iodide θ_m and formamide θ_f of glass and bacterial lawns of *P. fluorescens* Lp6a.

100 ¹ Data for water, formamide, methyleneiodide and glass taken from: $^{6, 18}$.

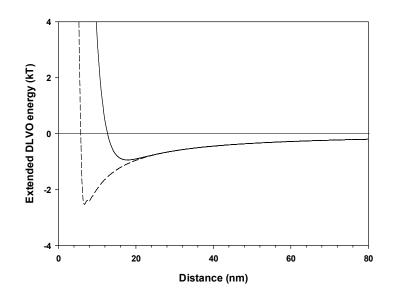
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105	Table S2. Overview of the individual Hamaker constants (A_{ii}) of the bacteria (A_{11}) , glass (A_{22}) ,
106	and water (A_{33}), respectively. The calculated effective Hamaker constant is denoted by A_{123} .

	A ₁₁	A ₂₂	A ₃₃	A ₁₃₂
P. fluorescens Lp6a (×10 ⁻²¹ J)	45.6	46.7	37	0.5

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 temperature-programmed desorption studies of the adsorption and desorption of amorphous
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Figure S1. Profile of the extended XDLVO interaction energy $(1 \text{ kT} = 4.0 \times 10^{-21} \text{ J})$ as a function of the distance for *P. fluorescens* Lp6a cell on glass surface in 10 mM (solid line) and 100 mM (dashed line) buffer solution.

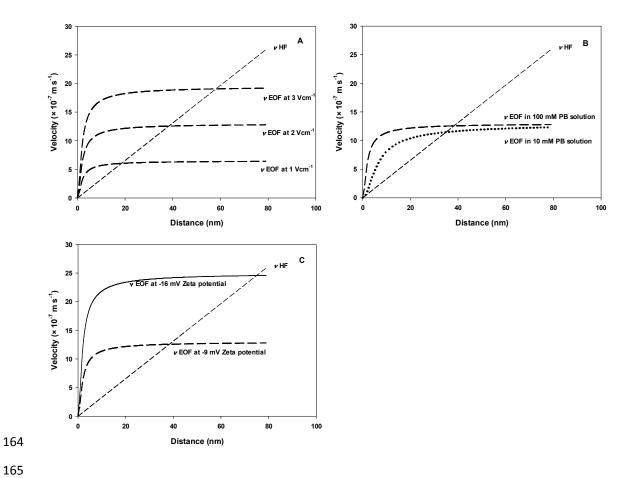


Figure S2. Calculated velocity profiles of the electroosmotic (v_{EOF} ; dashed lines) and the 167 hydraulic flow (v_{HF} ; fine dashed line) as a function of the distance to a glass surface at 168 varying electric field strengths, ionic strengths and zeta potentials of the glass surfaces. Figure 169 S2A: $\zeta = -9 \text{ mV}$; 100 mM buffer, X = 1, 2, or 3 V cm⁻¹; Figure S2B: $\zeta = -9 \text{ mV}$; 10 and 100 170 mM buffer, $X = 2 \text{ V cm}^{-1}$; Figure S2C: $\zeta = -9$ and -16 mV; 100 mM buffer, $X = 2 \text{ V cm}^{-1}$. 171

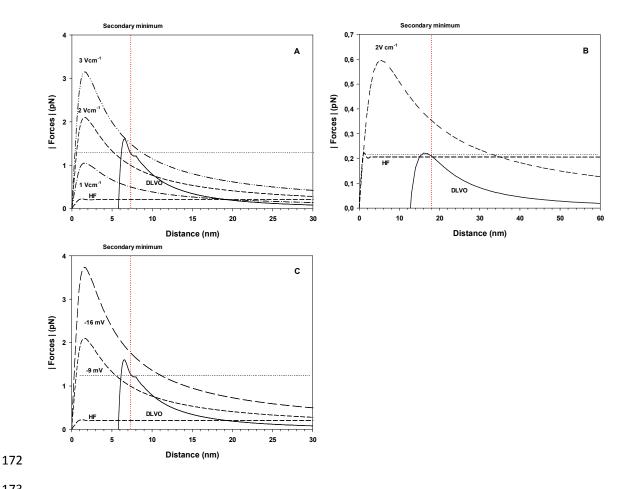
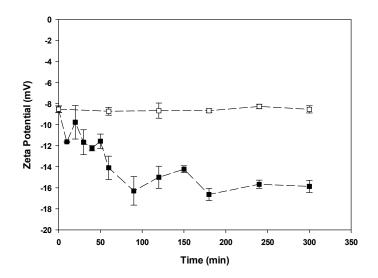


Figure S3. Calculated profiles of the shear forces induced by the electroosmotic (big dashed 174 lines) and the hydraulic flow (short dashed line) acting on P. fluorescens Lp6a cell. Please 175 note that the change of ζ from -9 mV to -16 mV did not result in printable (i.e. minimal) 176 177 changes of the XDLVO force and hence is not further detailed in the graph. The solid line represents the calculated profile of the absolute value of the calculated XDLVO maximum 178 179 attractive force acting on a P. fluorescens Lp6a cell. Dotted vertical and horizontal lines 180 represent the calculated distance of the secondary minimum and the absolute value of the maximum XDLVO attractive force, respectively. Figure S3A: $\zeta = -9$ mV; 100 mM buffer, X = 181 1, 2, or 3 V cm⁻¹; Figure S3B: $\zeta = -9$ mV; 10 mM buffer, X = 2 V cm⁻¹; Figure S3C: $\zeta = -9$ and 182 -16 mV; 100 mM buffer, $X = 2 V \text{ cm}^{-1}$. 183



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Figure S4. Effect of time (300 minutes) on the zeta potential of glass beads (squares) during exposure of to a bacterial suspension ($OD_{578} = 0.3$; filled squares) and a cell free control (open squares).

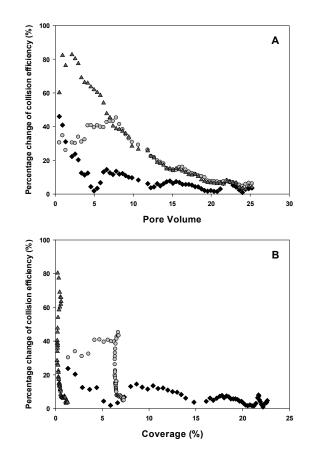
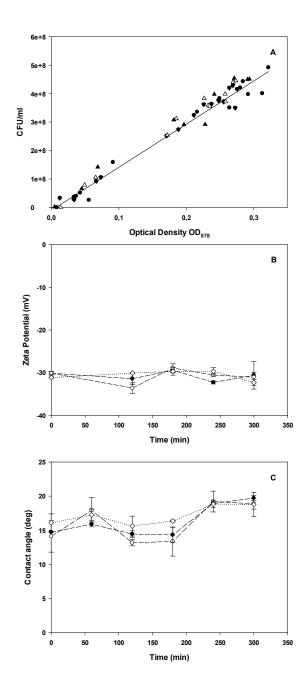


Figure S5. The reduction of Collision efficiency was changing as a function of the pore volume (Fig. S5A) and bacterial coverage (Fig. S5B): Triangles refer to X = 3 V cm⁻¹, circles to X = 2 V cm⁻¹ and diamonds to X = 1 V cm⁻¹.



198 Figure S6. Effect of the electrokinetic treatment on the viability, zeta potential and water contact angle of P. fluorescens Lp6a cells at the outflow of percolation columns filled with 199 glass beads the absence (empty symbols) and presence (filled symbols) of an DC electric field 200 of X = 1 V cm⁻¹ (filled triangles) and X = 2 V cm⁻¹ (filled circles) over time. Figure S5A: 201 202 Comparison of the optical density (578 nm) and the colony forming units on LB agar plates 203 (cfu) of strain Lp6a in the outflow of the columns; Figure S5B: Zeta potential of outflow cell vs time; dotted line represents the zeta potential of the inflowing cells; Figure S5C: Water 204 205 contact angle of outflowing cells over time; dotted line represents the water contact angle of the inflowing cells. 206

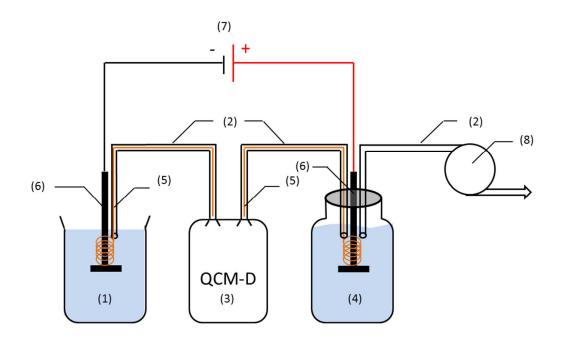
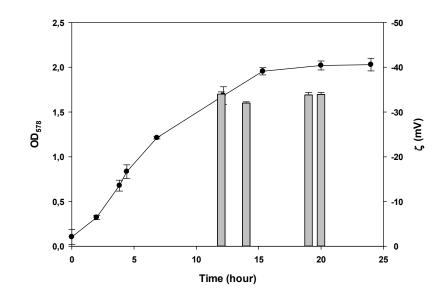


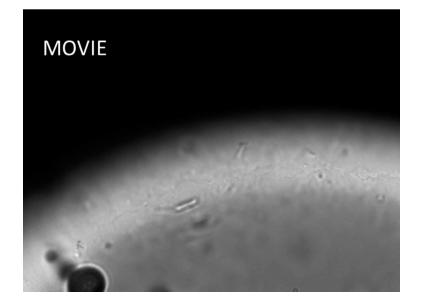
Figure S7. Schematic graph of the quartz crystal microbalance with dissipation measurement (QCM-D) under applied DC electric field: By using a peristaltic pump (8) a bacterial suspension was withdrawn by underpressure from a reservoir (1) and pumped through the QCM-D sensor chamber (3) into a recipient container (4). Disk-shaped Ti/Li electrodes (6) were connected to two copper wires (5) that extended electrodes through the Teflon tubing (2) to the QCM chamber. A power pack (7) was used to apply a constant DC electric field as indicated in the figure.



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Figure S8. The *LP6a* bacteria growths curve (left) and measured zeta potential ζ (bar, right)

218 as function of time



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Movie 1. A 30 s time-lapse video showing the movement of P. fluorescens Lp6a cells 224 attached to glass beads, in the presence and absence of a 2 Vcm⁻¹ electric field can be found at 225 http://pubs.acs.org. The surface of the glass beads is visible at the bottom of the picture. The 226 rod-shaped bacteria attached to the surface, is highlighted as red torus. Initially, no electrical 227 field is applied to the solution. After 10 sec, the electric field was switched on and negatively 228 charged cell is attracted by the anode. Meanwhile, the induced the EOF moves in the opposite 229 direction, from anode to the cathode. Prior to the microscopy experiment, a pre-culture of the 230 bacteria was grown to an $OD_{578} = 0.3$ and used to inoculate a culture with sterile glass beads 231 (0.1 - 0.25 mm diameter) in mineral media with 1 gL⁻¹ glucose in a flask. This culture was 232 stationary incubated for 3 days at room temperature to allow cell attachment on the glass 233 234 surface. The glass beads were subsequently picked out cautiously and transferred to a glass 235 bottom dish (50mm μ-Dish, Ibidi GmBH, Munich, Germany) using 1 mL pipette. Glass beads were rinsed with 3 mL potassium phosphate buffer for three times to wash away non-attached 236 cells and gently resuspended in buffer solution. The anode and cathode grid electrodes were 237 238 applied on the right and left side of petri dish respectively. Attached bacterial cells were visualized by light microscopy on an Axio Observer.Z1 inverted microscope, using a Plan-239 240 Apochromat 100x/1.4 objective (both Carl Zeiss AG, Oberkochen, Germany) and a frame rate of 5 fps. 241

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