## Supporting Information for

## Bipolar electric-field switching of perpendicular magnetic tunnel junctions through voltage-controlled exchange coupling

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## Supporting Information

## MATERIALS AND METHODS

## Sample preparation

The FePd SAF p-MTJ structures studied in this work were prepared on single crystal (001) MgO substrates by magnetron sputtering under an ultrahigh vacuum (base pressure < $5.0 \times 10^{-8}$ Torr) under the same conditions as in our previous work (40). The FePd (3 nm)/Ru (1.1 $\mathrm{nm}) / \mathrm{FePd}(3 \mathrm{~nm})$ perpendicular SAF stack was prepared with a $\mathrm{Cr}(15 \mathrm{~nm}) / \mathrm{Pt}(4 \mathrm{~nm})$ seed layer, keeping the substrate temperature at $350{ }^{\circ} \mathrm{C}$. The rest of the layers of the FePd SAF p-MTJ structures with a stack of $\mathrm{Ta}(0.8) / \mathrm{CFB}(1.3) / \mathrm{MgO}(2.0,2.3) / \mathrm{CFB}(1.3) / \mathrm{Ta}(0.7) /[\mathrm{Pd}(0.7) / \mathrm{Co}$ $(0.3)]_{4} / \mathrm{Pd}(5) /$ capping layer (where the numbers in parentheses are thicknesses in nanometers) were grown after the substrate was cooled to room temperature. The $15-\mathrm{nm} \mathrm{Pt}$ capping layer was deposited for the conductive atomic force microscope (C-AFM) testing. Before device patterning, the FePd SAF p-MTJ stacks were annealed at $350^{\circ} \mathrm{C}$ using rapid thermal annealing (RTA). Then the FePd SAF p-MTJ stacks were patterned into nano-pillars by e-beam lithography and Ar ion milling.

## p-MTJ device testing

The spin transport properties were tested by using C-AFM at room temperature for 100nm diameter FePd SAF p-MTJs. The C-AFM was an RHK UHV 350 with an R9 controller operating in contact mode. Si-doped AFM probe tips (Arrow-FM nanoworld) were made conducting by sputtering 200 nm of Pt onto a Ta adhesion layer (29). A Pt-coated AFM tip was used to make direct electrical contact with the top of FePd SAF p-MTJ pillars. In all the C-AFM measurements, the tip was grounded and $V_{\text {bias }}$ (positive or negative) was applied at the bottom electrode. Thus, for a positive $V_{\text {bias, }}$, the current flows from the bottom to the top, and for a negative $V_{\text {bias }}$, the current flows from the top to the bottom of FePd SAF p-MTJs. The E-field can
be calculated by dividing $V_{\text {bias }}$ by the thickness of the MgO tunnel barrier. During the testing, a sweep rate of $150 \mathrm{Oe} / \mathrm{sec}$ was used to measure the $R-H$ loops. A sweep rate of $500 \mathrm{mV} / \mathrm{sec}$ was used to measure the resistance versus bias voltage ( $R$ - $V_{\text {bias }}$ ) loops. For resistance versus time ( $R-t$ ) traces, an acquisition rate of 1 MHz was used. A variable out-of-plane magnetic field with $H_{\text {ext }}$ up to 1300 Oe was applied (29).

## DFT calculation

The IEC of the SAF structure as a function of E-field was calculated using first-principles methods based on density functional theory (DFT). As implemented in the Vienna ab initio simulation package (VASP) code (41), the generalized gradient approximation (GGA) exchangecorrelation potentials plus the projector augmented wave (PAW) method for the electron-ion interaction was used (42). Based on the experimental structure, we constructed a SAF structure with the stack of $\mathrm{MgO}(6) / \mathrm{Co}_{2} \mathrm{Fe}_{6}(8) / \mathrm{Ta}(6) / \mathrm{FePd}(11)$, as shown in Fig. 3 A in the main text, to study IEC between $\mathrm{Co}_{2} \mathrm{Fe}_{6}$ and FePd layers through a Ta spacer. The numbers indicate the atomic thickness for each layer, which corresponds to a thickness of $10.7,8.5,10.8,15.7 \AA$ for $\mathrm{MgO}, \mathrm{Co}_{2} \mathrm{Fe}_{6}, \mathrm{Ta}$, and FePd , respectively. This $\mathrm{Co}_{2} \mathrm{Fe}_{6}$ composition was used because it most closely reflects the stoichiometry after annealing the experimental sample to crystallize the MgO tunnel barrier (43). All self-consistent calculations were performed with a plane-wave cutoff of 400 eV . The geometric optimizations were carried out without any constraint until the force on each atom is less than $0.02 \mathrm{eV} / \AA$ and the change of total energy per cell is smaller than $10^{-4} \mathrm{eV}$. The Brillouin zone k-point sampling was set with a $9 \times 9 \times 1 \Gamma$-centered Monkhorst-Pack grids. A vacuum layer thicker than $15 \AA$ was applied along the $z$-direction to eliminate the interaction between slabs. The lattice constant and the atomic arrangement of the SAF structure were first relaxed without considering spin. The relaxed structure with a lattice constant of $2.92 \AA$ was then
applied to study the magnetic interaction between the $\mathrm{Co}_{2} \mathrm{Fe}_{6}$ and FePd FM layers. Spin-orbit coupling effects were considered to study the magnetic anisotropy. The IEC was calculated by comparing the energy difference between FM and AFM couplings aligned of $\mathrm{Co}_{2} \mathrm{Fe}_{6}$ and FePd layers. An electric field is applied along the $z$-direction with the dipole corrections performed to avoid interactions between the periodically repeated images.

## Section S1. Evaluation of $\boldsymbol{H}_{\mathrm{C}}, K_{\mathrm{u}, \mathrm{eff}}$, and $\xi_{\mathrm{vCMA}}$

To quantitatively evaluate the E-field effect, the mean coercivity $\left(H_{\mathrm{C}}\right)$, effective magnetic anisotropy ( $K_{\mathrm{u}, \text { eff }}$ ), and VCMA coefficiency ( $\xi_{\mathrm{vcma}}$ ) of the FePd p-SAF free layer were obtained by measuring their minor $R$ - $H$ loops and fitting the switching field distribution (SFD) (29). To obtain SFD, multiple $R$ - $H$ loops were measured at a given $V_{\text {bias. }}$. The $H_{\mathrm{C}}$ value was obtained by fitting SFD using the Kurkijärvi-Fulton-Dunkelberger equation:

$$
\begin{equation*}
\sigma=\left\{\frac{1}{\tau_{0} v} \exp \left[-K_{\text {eff }} V\left(1-\frac{H M_{s}}{2 K_{\text {eff }}}\right)^{2}\right]\right\} \times \exp \left\{-\int_{0}^{H} \frac{1}{\tau_{0} v} \exp \left[\frac{-K_{\text {eff }} V}{k_{\mathrm{B}} T}\left(1-\frac{h M_{s}}{2 K_{\text {eff }}}\right)^{2}\right] d h\right\} . \tag{S1}
\end{equation*}
$$

where $\tau_{0} \sim 10^{-9}$ second is the attempt time, $v \sim 350 \mathrm{Oe} / \mathrm{s}$ is the ramping rate of $H_{\text {ext }}, M_{\mathrm{s}} \sim 970$ $\mathrm{emu} / \mathrm{cm}^{3}$ is the saturation magnetization of the FePd SAF free layer, $k_{\mathrm{B}}$ is the Boltzmann constant, and $T=300 \mathrm{~K}$ is the testing temperature. By fitting SFD from these minor $R-H$ loops as shown in Fig. S4A, we obtained $H_{\mathrm{C}}$, and $K_{\mathrm{u}, \text { eff }}\left(\xi_{\mathrm{vcma}}\right)$, as plotted in Fig. S4C and S4D. $H_{\mathrm{C}}$ exhibits a typical linear behavior $(9,18)$ and dramatically increases from $\sim 145$ Oe to $\sim 900$ Oe when $V_{\text {bias }}$ sweeps from -0.75 V to +0.75 V . This is more than one order of magnitude larger than that of $\mathrm{CoFeB} / \mathrm{MgO} / \mathrm{CoFeB}$ p-MTJs, where $H_{\mathrm{C}}$ changes from 205 Oe to $290 \mathrm{Oe}(14,29)$. The large $H_{\mathrm{C}}$ variation is attributed to the PMA modification of the CoFeB layer as well as the
modulation of the IEC strength between the FePd and CoFeB layers via the application of Efield.

## Section S2. Evaluation of STT

To evaluate the contribution of the STT effect in our VCEC p-MTJs, we calculated the effective STT field ( $H_{\text {STT }}$ ), in terms of the scalar functions given with Eqs. (S2 and S3) $(44,45)$

$$
\begin{gather*}
g(\theta)=\left[-4+\frac{(1+\eta)^{3}(3+\cos \theta)}{4 \eta^{3 / 2}}\right]^{-1}  \tag{S2}\\
H_{\mathrm{STT}}=\frac{2 \mu_{B} J g(\theta) \sin \theta}{\gamma e t_{\text {free }} M_{\mathrm{s}}} \tag{S3}
\end{gather*}
$$

Here $\mu_{\mathrm{B}}=9.27 \times 10^{-24} \mathrm{~A} . \mathrm{m}^{2}, J_{\mathrm{c}}=1.1 \times 10^{9} \mathrm{~A} / \mathrm{m}^{2}, t_{\text {free }}=1.3 \times 10^{-9} \mathrm{~m}, e=1.6 \times 10^{-19} \mathrm{~A} . \mathrm{s}, \gamma=$ $4 \pi \times 1.6 \times 10^{4} \mathrm{~m} / \mathrm{A} . \mathrm{s}, \quad \eta=0.65$, and $M_{\mathrm{s}}=8.9 \times 10^{5} \mathrm{~A} / \mathrm{m}$ are the Bohr magneton, the switching current density, the thickness of the free layer, electron charge, gyromagnetic ratio, spin polarization, and saturation magnetization, respectively. $\theta$ is the angle between the free layer and the reference layer magnetization direction. The switching current density $\left(J_{\mathrm{c}}\right)$, the thickness of the free layer $\left(t_{\text {free }}\right)$, spin polarization $(\eta)$, and saturation magnetization $\left(M_{\mathrm{s}}\right)$ are obtained from our experimental results. Figure S 3 plots the calculated $H_{\mathrm{STT}}$ as a function of the $\theta$ values. We find that the $H_{\text {STT }}$ first gradually increases and reaches its maximum value $H_{\text {STT }} \sim 5$ Oe when $\theta \sim$ 150 degrees, then decreases with the increasing $\theta$, matching the trend in the literature (46). The $H_{\text {STT }} \sim 5 \mathrm{Oe}$ indicates that the STT effect is negligible in our experiment.

## Section S3. Modeling the voltage-controlled interlayer exchange coupling (IEC)

We modeled the voltage dependence of the IEC within Bruno's theory in the context of the effective mass approximation (38). The model system is sketched in Fig. 4A. The IEC between $\mathrm{FM}_{1}$ and $\mathrm{FM}_{2}$ describes the energetic preference for the FM or AFM coupling. The coupling strength is defined as $J_{\mathrm{ex}}=\left(E_{\mathrm{FM}}-E_{\mathrm{AFM}}\right) / 2$, where $E_{\mathrm{FM}}\left(E_{\mathrm{AFM}}\right)$ is the total energy of the system per unit area for FM (AFM) configurations, and using Bruno's formula Eq. (1) in the main text. $J_{\text {ex }}>0$ and $J_{\text {ex }}<0$ represent the AFM and FM couplings, respectively. The $\mathrm{FM}_{1}$ and $\mathrm{FM}_{2}$ layers are magnetically coupled via itinerant electrons in the NM layer through spin-dependent reflections at the $\mathrm{FM}_{(1,2)} / \mathrm{NM}$ interfaces.

In our simulations, the FM layers with finite thicknesses were treated as Fabry-Perot cavities with multiple reflections within, which generates extra contributions to the total net reflection at the $\mathrm{FM}_{2} / \mathrm{NM}$ and $\mathrm{NM} / \mathrm{FM}_{1}$ interfaces. As described in the main text, the reflection coefficients at the $\mathrm{MgO} / \mathrm{FM}_{2}, \mathrm{FM}_{2} / \mathrm{NM}$ and $\mathrm{NM} / \mathrm{FM}_{1}$ interfaces were defined as $r_{\mathrm{A}}^{\uparrow(\downarrow)}, r_{\mathrm{B}}^{\uparrow(\downarrow)}$, and $r_{\mathrm{C}}^{\uparrow(\downarrow)}$ for spin-up and spin-down electrons, respectively. Since the $\mathrm{FM}_{2}$ layer was surrounded by the different materials (the MgO tunnel barrier above and the NM layer below), we expected $r_{\mathrm{A}}^{\uparrow(\downarrow)} \neq r_{\mathrm{B}}^{\uparrow(\downarrow)}$ such that the $\mathrm{FM}_{2}$ layer acts as an asymmetric Fabry-Perot cavity, where the net reflection coefficient that enters in Bruno's expression is

$$
\begin{equation*}
r_{\mathrm{B}(\mathrm{net})}^{\uparrow(\downarrow)}=\frac{r_{\mathrm{B} \infty}^{\uparrow(\downarrow)}+r_{\mathrm{A}}^{\uparrow(\downarrow)} e^{2 i k_{\mathrm{B}}^{\uparrow(\downarrow)} t_{\mathrm{B}}}}{1+r_{\mathrm{B} \infty}^{\uparrow(\downarrow)} r_{\mathrm{A}}^{\uparrow(\downarrow)} e^{2 i k_{\mathrm{B}}^{(\uparrow)} t_{\mathrm{B}}}} \tag{S4}
\end{equation*}
$$

Here $t_{\mathrm{B}}$ is the thickness of the $\mathrm{FM}_{2}$ layer and $r_{\mathrm{B} \infty}^{\uparrow(\downarrow)}=\left(k_{\mathrm{F}}-k_{\mathrm{B}}^{\uparrow(\downarrow)}\right) /\left(k_{\mathrm{F}}+k_{\mathrm{B}}^{\uparrow(\downarrow)}\right)$ is the reflection coefficient at the $\mathrm{FM}_{2} / \mathrm{NM}$ interface if the corresponding FM layer is infinite. The wave vector inside the $\mathrm{FM}_{2}$ layer, $r_{\mathrm{B}}^{\uparrow(\downarrow)}$, is related to the Fermi wave vector of the NM layer, $k_{\mathrm{F}}$, via conservation of energy

$$
\begin{equation*}
\frac{\hbar^{2}}{2 m_{\mathrm{B}}} k_{\mathrm{B}}^{\uparrow(\downarrow), 2}+U_{\mathrm{B}}^{\uparrow(\downarrow)}=\frac{\hbar^{2}}{2 m} k_{\mathrm{F}}^{2}+U_{0} \tag{S5}
\end{equation*}
$$

where the effective masses of the $\mathrm{FM}_{2}$ layer and NM layer are $m_{\mathrm{B}}$ and $m$ respectively, and the exchange splitting inside the $\mathrm{FM}_{2}$ layer is $J_{\mathrm{ex}, \mathrm{B}}=U_{\mathrm{B}}^{\downarrow}-U_{\mathrm{B}}^{\uparrow}$. An equivalent set of equations is also valid at $\mathrm{NM} / \mathrm{FM}_{1}$ interface, giving rise to the $\mathrm{FM}_{1}$ thickness-dependence of IEC.

Equation (S4) resumes to the well-known reflection coefficient of the Fabry-Perot problem when reflections at the $\mathrm{MgO} / \mathrm{FM}_{2}$ and $\mathrm{FM}_{2} / \mathrm{NM}$ interfaces are the same (symmetric cavity).

We consider that an applied E-field causes a linear voltage drop inside the MgO tunnel barrier, as shown in Fig. 4A (bottom panel). An E-field inside the MgO tunnel barrier is given by $V_{\text {bias }} / d$, where $d$ is the thickness of the MgO tunnel barrier. The barrier height of the MgO tunnel barrier is defined as $U_{\mathrm{I}}$. The E-field inside of the MgO tunnel barrier changes the reflection coefficient at the $\mathrm{MgO} / \mathrm{FM}_{2}$ interface, leading to the voltage-dependent $J_{\text {ex }}\left(V_{\text {bias }}\right)$ via $r_{\mathrm{A}}^{\uparrow(\downarrow)}\left(V_{\text {bias }}\right)$ in Eq. (S4) and modifying the reflection coefficient $r_{\mathrm{B}}^{\uparrow(\downarrow)}$, which translates to a voltage dependence of the IEC between $\mathrm{FM}_{2}$ and $\mathrm{FM}_{1}$ layers. The reflection coefficient is computed exactly by solving the tunneling problem for a trapezoidal barrier. Finally, we obtain the voltage-dependent reflection coefficient $r_{\mathrm{A}}^{\uparrow(\downarrow)}\left(V_{\text {bias }}\right)$ :

$$
\begin{equation*}
r_{\mathrm{A}}^{\uparrow(\downarrow)}\left(V_{\text {bias }}\right)=\frac{\left.\left[i k_{\mathrm{B}}^{\uparrow(\downarrow)} A i\left(z_{0}\right)-A^{\prime} i\left(z_{0}\right)\right]\left[i k_{\mathrm{A}}^{\uparrow(\downarrow)} B i\left(z_{\mathrm{d}}\right)-B^{\prime} i\left(z_{\mathrm{d}}\right)\right]-\left[i k_{\mathrm{A}}^{\uparrow(\downarrow)} A i\left(z_{\mathrm{d}}\right)-A^{\prime} i\left(z_{\mathrm{d}}\right)\right)\right]\left[i k_{\mathrm{B}}^{\uparrow(\downarrow)} A i\left(z_{0}\right)-B^{\prime} i\left(z_{0}\right)\right]}{\left.\left[k_{\mathrm{B}}^{(\lambda)}\right)+A^{\prime} i\left(z_{0}\right)\right]\left[i i_{\mathrm{A}}^{\uparrow(\lambda)} B i\left(z_{\mathrm{d}}\right)-B^{\prime} i\left(z_{\mathrm{d}}\right)\right]-\left[i k_{\mathrm{A}}^{(\uparrow)} A i\left(z_{\mathrm{d}}\right)-A^{\prime} i\left(z_{\mathrm{d}}\right)\right]\left[k_{\mathrm{B}}^{\uparrow(\uparrow)} B i\left(z_{0}\right)+B^{\prime} i\left(z_{0}\right)\right]} \tag{S6}
\end{equation*}
$$

with Airy functions ( $A i$ and $B i$ ) and corresponding derivatives ( $A^{\prime}$ and $B^{\prime}$, where the prime symbol stands for derivative with respect to $x$, and not $z)$ evaluated at points $z_{0}=z(x=0)$ and $z_{\mathrm{d}}=z(x=d)$, where

$$
\begin{equation*}
z(x)=\left(\frac{2 m d^{2}}{\hbar^{2} V_{\text {bias }}{ }^{2}}\right)^{\frac{1}{3}}\left(U_{\mathrm{I}}-E-\frac{V_{\text {bias }}}{d} x\right) \tag{S7}
\end{equation*}
$$

Here,

$$
\begin{equation*}
\frac{\hbar^{2}}{2 m_{\mathrm{A}}} k_{\mathrm{A}}^{\uparrow(\downarrow), 2}+U_{\mathrm{A}}^{\uparrow(\downarrow)}-V_{\text {bias }}=\frac{\hbar^{2}}{2 m} k_{\mathrm{F}}^{2}+U_{0} \tag{S8}
\end{equation*}
$$

Equation (S8) shows the relation of $k_{\mathrm{A}}^{\uparrow(\downarrow)}$ and $k_{\mathrm{F}}$, where $J_{\text {ex, } \mathrm{A}}=U_{\mathrm{A}}^{\downarrow}-U_{\mathrm{A}}^{\uparrow}$ is the exchange splitting of the semi-infinite $\mathrm{FM}_{1}$ layer.

In our simulations, we considered the thicknesses of all the layers in the SAF configuration to be the same as in the experiments: $t_{\mathrm{C}}=3 \mathrm{~nm}, t_{\mathrm{B}}=1.3 \mathrm{~nm}, \mathrm{D}=0.8 \mathrm{~nm}$, and $d=2$ nm . Also, $E_{\mathrm{F}}=4 \mathrm{eV}, J_{\mathrm{A}}=J_{\mathrm{C}}=1 \mathrm{eV}, J_{\mathrm{B}}=1.93 \mathrm{eV}, U_{\mathrm{A}}=U_{\mathrm{B}}=U_{\mathrm{C}}=1 \mathrm{eV}$, with $U_{0}=0 \mathrm{eV}$ and $U_{\mathrm{I}}$ $=5.4 \mathrm{eV}$. Here, $\Delta E=2 a^{2} J_{\mathrm{ex}}$, where $a=2.92 \AA$ is the in-plane lattice constant of the SAF configuration obtained from our DFT simulations. We assumed an intrinsic build-in field in all the results. The net effect was to change the bias from 0 V to 0.786 V , as estimated from the DFT calculations.

## Section S4. Performance benchmarking of spin memories.

For STT-MRAM, our simulated results are comparable with the experimental results (47) by employing the macrospin model (48). Ref. (47) is one of the most recent papers on STT-MRAM with sub- 30 nm diameters and 3 -ns switching speed and $100 \mu \mathrm{~A}$ write current. For SOT-MRAM, the micromagnetic simulation tool OOMMF (49) was used and the results were validated by experiments (50). Ref. (50) is a recent paper that had shown low write current density ( $\sim 5.4 \times 10^{6}$ $\mathrm{A} / \mathrm{cm}^{2}$ ) and fast write speed with write pulse width as short as 2 ns . In the benchmarking simulations, $5-\mathrm{ns}$ and $10-\mathrm{ns}$ hypothetical magnetization switching times were chosen. These
values show the same magnitude as STT does and can be roughly calculated based on Bruno's model. To quantify the potential impact of this VCEC switched p-MTJ device, we employed a $1000 \times 32$ bit memory array and carry out the benchmarking simulation of VCEC-MRAM against its STT-MRAM and SOT-MRAM counterparts based on the parameters of a $15-\mathrm{nm}$ CMOS technology node (51). In the benchmarking simulation, the parameters (e.g. switching current density, switching time) used for the STT and SOT simulations are from the literature. For the VCEC-MTJ, we chose our experimental switching current density and 5-ns and 10-ns hypothetical magnetization switching times which is realistic in the experiment. The benchmarking results show that VCEC-MRAM dissipates more than an order of magnitude lower energy per write operation compared to STT-MRAM, as plotted in Fig. S9A. VCECMRAM is 2 X denser than SOT-MRAM if implemented at the $15-\mathrm{nm}$ CMOS technology node, and it will be 5.5 X denser if implemented at the $7-\mathrm{nm}$ CMOS technology node, as shown in Fig. S9B. We believe that these results (52) could be beneficial for a new generation of spin memory and logic applications.


Fig. S1. Out-of-plane magnetic hysteresis ( $\boldsymbol{M}-\boldsymbol{H}$ ) loops of FePd p-SAF structure. (A) The $M$ $H$ loop of the FePd p-SAF structure with the stack of FePd (3.0 nm)/Ru (1.1 nm)/FePd (3.0 nm); (B) The $M-H$ loop of the bottom SAF free layer by combining FePd SAF with a $\mathrm{Co}_{20} \mathrm{Fe}_{60} \mathrm{~B}_{20}$ layer. Spin-flop switching and spin-flip switching are observed at a high and low applied magnetic field, respectively.


Fig. S2. Topographic images of nano-sized FePd SAF p-MTJ pillars. (A) SEM image of the top view of the patterned FePd SAF p-MTJ pillars with diameters of $35 \mathrm{~nm} \sim 250 \mathrm{~nm}$. (B) the schematic of the C-AFM setup. In all the C-AFM measurements, the tip was grounded and $V_{\text {bias }}$ (positive or negative) was applied at the bottom electrode. Thus, for a positive $V_{\text {bias }}$ (positive Efield), the current flows from the bottom to the top, and for a negative $V_{\text {bias }}$ (negative E-field), the current flows from the top to the bottom of FePd SAF p-MTJs. (C) Topography measured by atomic force microscopy (AFM). (D) The current map measured by the conductive AFM (CAFM) at 100 mV for the FePd SAF p-MTJ pillars.


Fig. S3. STT effective field. The values of the effective STT field $\left(H_{\text {STT }}\right)$ as a function of the $\theta$ values based on our experimental results.


Fig. S4. E-field effect of FePd SAF p-MTJs. (A) The minor $R-H$ loops of $100-\mathrm{nm}$ FePd SAF pMTJ devices with the different $V_{\text {bias }}$ by varying $H_{\text {ext }}$ from -1.3 kOe to +1.3 kOe . The center of each minor $R$ - $H$ loop is labeled with the arrow. Before sweeping $H_{\text {ext }}$, we applied a large $H_{\text {ext }}$ to align the magnetization of the ferromagnetic layers. During the measurement of the $R$ - $H$ loops, the magnetization of the CoFeB layer is only switched by $H_{\text {ext }}$, as shown in the inset schematics of Fig. S4A. When $V_{\text {bias }}=-0.75 \mathrm{~V}$, the CoFeB and FePd layers prefer strong FM coupling, thus the CoFeB layer is switched under negative $H_{\text {ext. }}$. When $V_{\text {bias }}=-0.1 \mathrm{~V}$ and +0.75 V , the CoFeB and FePd layers prefer AFM coupling, thus the CoFeB layer is switched under positive $H_{\text {ext. }}$ (B) The $H_{\text {ex }}$ vs. $V_{\text {bias }}$ curve, (C) The $H_{\mathrm{C}}$ vs. $V_{\text {bias }}$ curve (red diamonds denotes FePd SAF MTJs; blue stars
presents CoFeB MTJs) and (D) $K_{\text {u,eff }}$ vs. $V_{\text {bias }}$ for the $100-\mathrm{nm}$ FePd SAF p-MTJ device. Here, the $H \mathrm{c}$ and $K_{\mathrm{u}, \text { eff }}$ values are obtained by fitting the switching field distribution (SFD) with the Kurkijärvi-Fulton-Dunkelberger equation. The $\xi_{\mathrm{VCMA}}$ for $100-\mathrm{nm}$ FePd p-SAF p-MTJ devices was obtained from the linear fit.


Fig. S5. Stray field effect. The calculated stray field $\left(H_{\text {stray }}\right)$ of three ferromagnetic layers ( $H_{\mathrm{s}, \mathrm{CoFeB}-[\mathrm{Co} / \mathrm{Pd]} \mathrm{n}}, H_{\mathrm{s}, \mathrm{FePd} 1}$, and $H_{\mathrm{s}, \text { FePd2 }}$ ). $H_{\text {stray }}$ shown here is along $z$ direction (perpendicular to the MTJ pillar plane). For the micromagnetic simulation, the thickness, magnetization of three layers are chosen from the experimental data.


Fig. S6. The Fermi level shift and local potential profile under E-fields. (A) The projected density of states (PDOS) for interfacial Fe under different E-fields, which shows a clear Fermi level shift, indicating the electron accumulation and depletion at negative and positive E-Fields, respectively. (B) The local potential profiled for the system with positive, zero, and negative Efields, where the positive E-field points upward (from bottom electrode to top electrode) and the negative E-field points downwards (from top electrode to bottom electrode). A built-in potential is induced due to the interaction at the interface between the MgO tunnel barrier and the CoFe layer.


Fig. S7. VCMA effect at the interfaces. (A) The schematic of the optimized structural configuration used for first-principles calculations. Charge differential plot showing the electron depletion and accumulation at the $\mathrm{MgO} / \mathrm{CoFe}$ and $\mathrm{FePd} /$ vacuum interface. (B) and (C) show the changes in the magnetic moment of interfacial CoFe and FePd as a function of E-field.


Fig. S8. Comparison of the interfacial and bulk electronic states. The projected density of states (PDOS) at the $\mathrm{MgO} / \mathrm{CoFe}$ interface and in the bulk for the Fe atoms ( $\mathbf{A}$ ) and (B) and the Co atoms (C) and (D). The valence band electrons of $d$-orbitals at the interface clearly shift to the Fermi level compared with the bulk.


Fig. S9. Performance benchmarking of spin memories. (A) The write performance of the VCEC-MRAM compared to STT-MRAM and SOT-MRAM under a $1000 \times 32$ bit array. In our simulation, we used p-MTJ for STT-MRAM simulation, and in-plane MTJ for SOT-MRAM simulation. The magnetization switching time of VCEC-MTJ is hypothetically assumed to be 5 ns and 10 ns. (B) The comparison of the layout area for various spin memories including VCECMRAM, STT-MRAM, and SOT-MRAM. The half-metal pitch (F) of all the devices is 30 nm corresponding to the $15-\mathrm{nm}$ CMOS technology node. For VCEC-MRAM, the case of $\mathrm{F}=18 \mathrm{~nm}$ (corresponding to the 7 -nm CMOS technology node) is also considered because of its scalability due to the high PMA and low write currents of the p-MTJ devices. For the STT-MRAM, the cases with one and two access transistors are considered.

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