

Supplementary data for

## **CO<sub>2</sub> pretreatment to aerated concrete with high-volume industry wastes enables a sustainable precast concrete industry**

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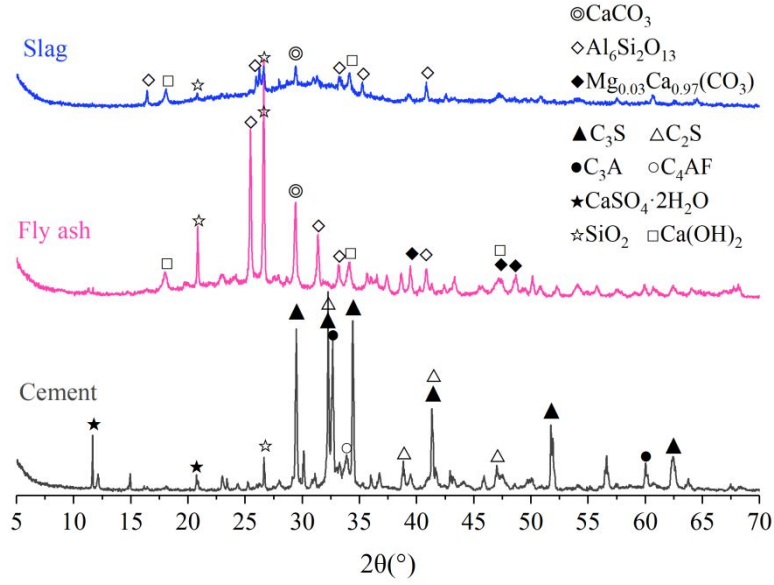
### **1. Raw Materials Characterization**

The chemical and mineral compositions of the cement, fly ash and GGBS as received were characterized by XRF and XRD. Table S1 shows the oxides of these raw materials. It is clear that the cement and fly ash contain high contents of CaO, while the fly ash and GGBS contain high mass fractions of SiO<sub>2</sub> and Al<sub>2</sub>O<sub>3</sub>. Moreover, MgO occupies more than 7% mass of the GGBS (Table S1).

**Table S1. Chemical composition of materials (wt%)**

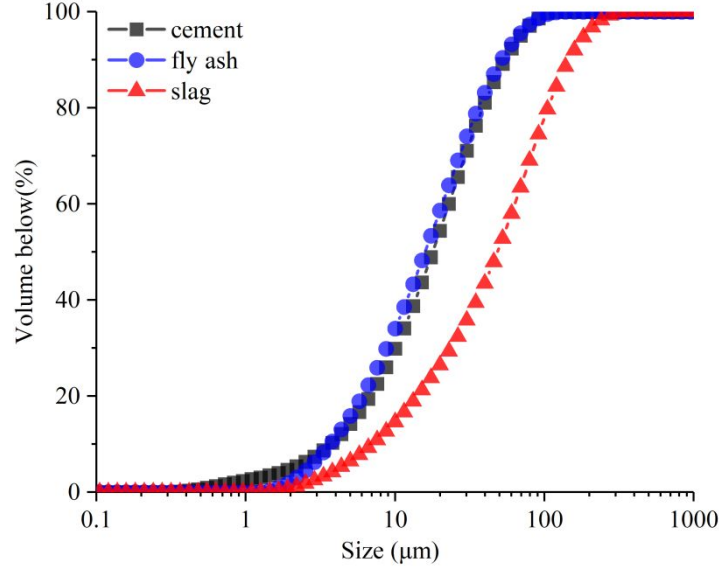
	CaO	SiO <sub>2</sub>	Al <sub>2</sub> O <sub>3</sub>	SO <sub>3</sub>	Fe <sub>2</sub> O <sub>3</sub>	MgO	K <sub>2</sub> O	TiO <sub>2</sub>	Others
<b>Cement</b>	57.61	12.03	5.15	3.46	3.01	1.46	1.21	0.26	15.81
<b>Slag</b>	33.83	18.60	15.98	1.01	0.98	7.74	0.39	1.40	20.08
<b>Fly ash</b>	17.58	39.87	28.25	5.07	4.44	1.24	0.70	1.11	1.74

Figure S1 demonstrates the crystalline phases of the solid materials tested by XRD. The cement mainly contains  $C_3S$ ,  $C_2S$ ,  $C_3A$ ,  $C_4FA$  and gypsum. The slag and fly ash share the crystals of mullite, quartz, calcium carbonate and calcium hydroxide, but the former also contains a certain amount of magnesium calcite (Fig. S1).



**Fig. S1.** XRD patterns of cement, fly ash and GGBFS used in this study.

The particle size distribution of the materials is shown in Fig. S2. The cement and fly ash share the similar particle size distribution with the 50% volume size of 17  $\mu m$ , while the GGBS has the coarser particle sizes with the 50% volume size of 49  $\mu m$ .



**Fig. S2.** Particle size distribution of cement, fly ash and GGBFS

## 2. Estimation process of absorption mass of CO<sub>2</sub> in AC blocks

The mass loss between 550~800 °C from the TG curve was considered as the mass of CO<sub>2</sub> absorbed by AC blocks (Fig. 4f). In order to calculate the mass of CO<sub>2</sub> absorbed by a AC block with the side length of 100 mm, we assumed that the CO<sub>2</sub> absorption decreased linearly with depth, and the calculation diagram was shown in Fig. S3. We took the carbonation data of AC blocks cured at 0.1 MPa as an example. CO<sub>2</sub> mass in the C0.1 sample was estimated as follows:

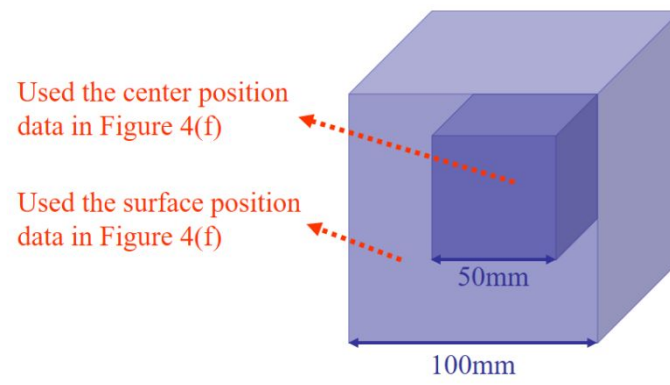
$$m_{CO_2}(C0.1) = \frac{5^3}{10^3} \times 2.02 + \left(1 - \frac{5^3}{10^3}\right) \times 9.17 = 8.27625g$$

CO<sub>2</sub> mass in the Ref. sample was estimated as:

$$m_{CO_2}(Ref.) = \frac{5^3}{10^3} \times 1.64 + \left(1 - \frac{5^3}{10^3}\right) \times 3.05 = 2.87375g$$

So, the neat CO<sub>2</sub> absorption capacity of the C0.1 block was:

$$m_{absorbed\ CO_2} = 8.27625 - 2.87375 \approx 5.4g$$



**Fig. S3.** Calculation of CO<sub>2</sub> absorption ratio in an AC block