Supporting Information

Trace Cr(VI) Removal: Evidence of redox-active ion exchange by a weak base anion exchanger

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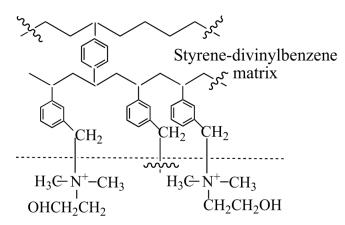
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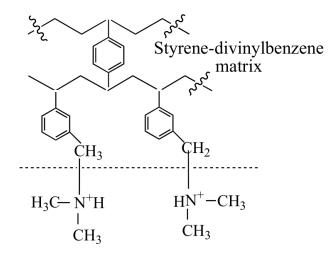
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- 1. Chemical structures of ion exchange resins used in the study
- a) INDION 820



b) INDION 860



c) Amberlite IRA 67

IUPAC Name: 1,2-bis(ethenyl)benzene,4-[(E)-2-[(E)-2-but-3-enoxyethenoxy]ethenoxy]but-1-ene,N-[3-(dimethylamino)propyl]prop-2-enamide

Molecular Formula: C₃₀H₄₄N₂O₄

polyacrylate matrix KKKKK HN⁺-CH₃ H₃C-H CH₃ CH₃

d) Duolite A7

Chemical Name: Formaldehyde, polymer with N,N'-bis(2-aminoethyl)-1,2-ethanediamine and phenol

Molecular Formula: C₁₃H₂₆N₄O₂

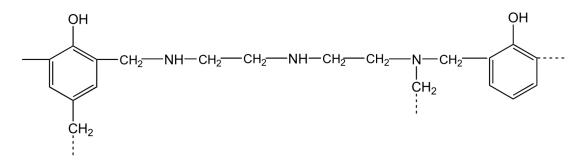


Figure S1. Chemical structures of ion exchange resins used in the study.

2. Experimental setup in the laboratory

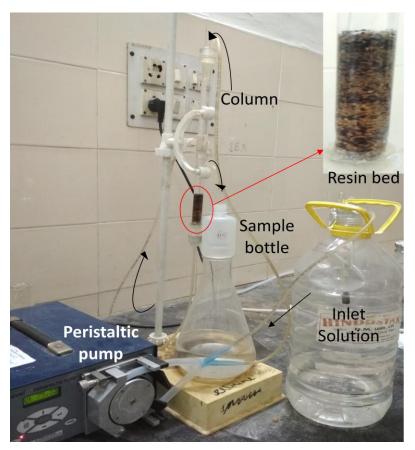


Figure S2. Experimental setup in the laboratory; Cr(VI) concentration in the synthetic raw water kept as 200 μ g/L with a background concentration of competing anions like sulphate, chloride and bicarbonate as 100 mg/L each.

3. Column performances of different ion exchange resins for trace Cr(VI) removal at influent pH 7

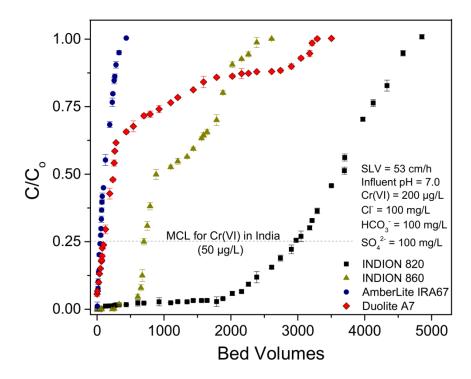


Figure S3. Chromium breakthrough profiles of column runs of strong base anion exchange resin (INDION 820) and weak base anion exchange resins (INDION 860, Amberlite IRA 67, and Duolite A7) with synthetic influent containing Cr(VI) anions in presence of competing background anions.

4. Speciation diagram of aqueous Cr(VI) species

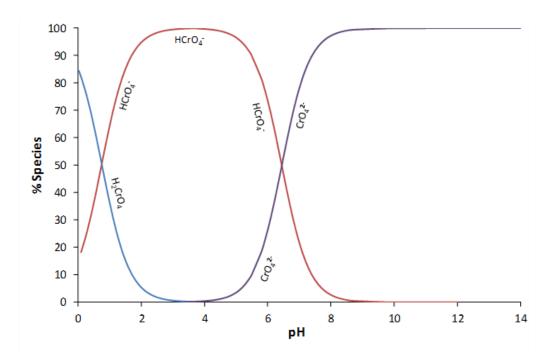


Figure S4. Speciation diagram of aqueous Cr(VI) species for Cr (VI) concentration less than 0.01M.

The diagram was drawn using the following equilibrium equations.¹

$H_2CrO_4 \leftrightarrow H_2$	$H^+ + HCrO_4^-$	$\log K = -0.8$
$HCrO_4^- \leftrightarrow H$	$H^{+} + CrO_{4}^{2-}$	log K = -6.5

5. Speciation diagram of aqueous chromium

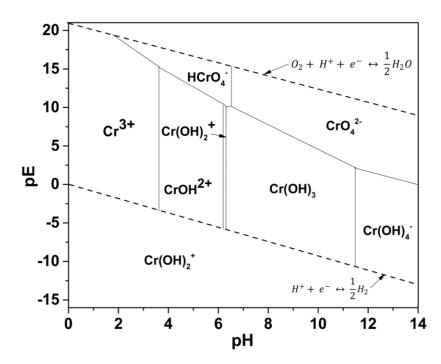


Figure S5. Speciation diagram of aqueous Chromium.

The diagram was drawn using the following equilibrium equations.²

$$\frac{1}{3}HCrO_{4}^{-} + \frac{7}{3}H^{+} + e^{-} \leftrightarrow \frac{1}{3}Cr^{3+} + \frac{4}{3}H_{2}O \qquad \log K = +20.2$$

$$HCrO_{4}^{-} \leftrightarrow H^{+} + CrO_{4}^{2-} \qquad \log K = -6.5$$

$$Cr^{3+} + H_{2}O \leftrightarrow CrOH^{2+} + H^{+} \qquad \log K = -4.0$$

$$Cr^{3+} + 2H_{2}O \leftrightarrow Cr(OH)_{2}^{+} + 2H^{+} \qquad \log K = -9.7$$

$$Cr^{3+} + 3H_{2}O \leftrightarrow Cr(OH)_{3} + 3H^{+} \qquad \log K = -18.0$$

$$Cr^{3+} + 4H_{2}O \leftrightarrow Cr(OH)_{4}^{-} + 4H^{+} \qquad \log K = -27.4$$

$$O_{2} + H^{+} + e^{-} \leftrightarrow \frac{1}{2}H_{2}O \qquad pE^{\circ} = +20.75$$

$$H^{+} + e^{-} \leftrightarrow \frac{1}{2}H_{2} \qquad pE^{\circ} = 0.0$$

6. Thermal analysis

Thermo Gravimetric/Differential Thermal Analysis (TG/DTA) was performed using EXSTAR Model SII 6300, under inert (nitrogen) atmosphere with temperature ranging from 35 to 650°C at 10°C/min heating rate. Thermogravimetric analysis (TGA) is performed to study the variation in weight of a sample with temperature in a controlled atmosphere, which is then used to obtain information like phase changes, kinetics, or ash content of the sample.

For virgin resin, the first loss stage is observed at 30-120°C which is due to evaporation of water that is chemically adsorbed in the porous network and release of low molecular weight compounds. The second loss stage occurred at 130-360°C due to formaldehyde release from dimethylene ether bridges that are transformed into methylene bridges.^{3,4} The weight loss above the temperature of 360°C is attributed to the rupture of methylene bridges and degradation of the phenolic network.^{3,4} It is also depicted by the primary decomposition peak at 397°C of the DTG curve. About 49% is left as a solid residue which shows that the resin has good thermal stability. DTA curve showed that exothermic reactions took place throughout the process but there was no rapid reaction and the negligible thermal effect was observed after 450°C. After Cr(VI) loading, the first loss stage was observed at 30-200°C and similar behavior has been reported in previous studies.⁵ DTA curve shows a significant three-stage weight loss of the sample observed at 245, 333, and 501°C. All these reactions are exothermic in nature. The peaks at 245 and 333°C can be attributed to formaldehyde release from dimethylene ether bridges that are transformed into methylene bridges.³ The peak at 501°C is due to thermo-oxidation of resin, i.e., breakage of aromatic rings releasing gaseous products like CH₄, CO₂, CO, etc. In the case of exhausted resin, only 4% residue is left. These results indicate that chromium might have interacted with the matrix of the resin and formed complexes that have altered the thermal behavior of the resin.

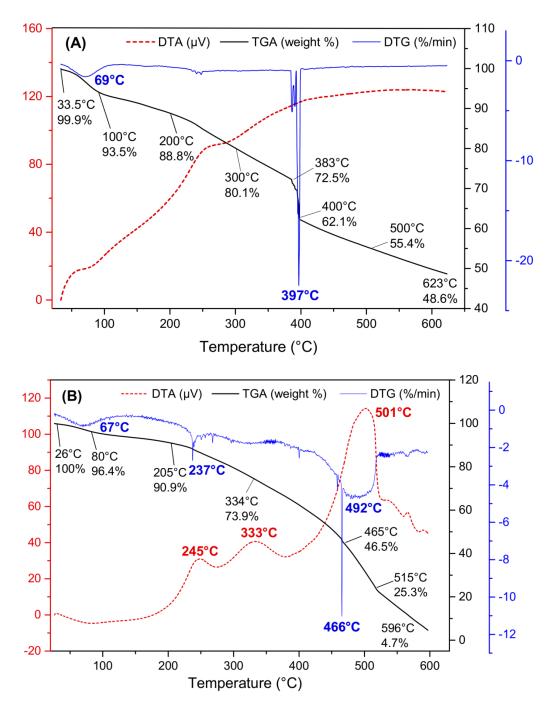


Figure S6. Thermal curves of (A) virgin Duolite A7 resin and (B) exhausted Duolite A7 resin collected from column running at influent pH 7, under nitrogen atmosphere.

References

- 1. Sengupta, A. K.; Clifford, D. Important Process Variables in Chromate Ion Exchange. *Environ. Sci. Technol.* **1986**, 20, 149-155.
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