# Supporting Information

# Boosting Toluene Combustion by Engineering Co-O Strength in Cobalt Oxide Catalysts

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## CHARACTERIZATIONS

X-ray diffraction (XRD) patterns were recorded using 3KW D/MAX-2500 X-ray diffractometer equipped with Cu Ka$\alpha$ radiation at 40 kV and 140 mA at a scanning rate of 8° min$^{-1}$. Thermogravimetric analysis (TGA) was conducted on a Thermogravimetric Analyzer (SHIMADZU DTG-60H), at a rate of 10 °C min$^{-1}$ under air flow. Raman measurements were carried out at room temperature, and the signals were recorded by FT-Raman spectrophotometer (LabRAM HR Evolution, Bruker). An Nd:YAG laser 633 nm line was used as the excitation source. The obtained XPS spectra were recorded with a resolution of approximately 1.5. X-ray photoelectron spectrum (XPS) analysis was conducted with a VG SCIENTA R3000 X-ray photoelectron spectroscope equipped with Al K$\alpha$ radiation, and the binding energy was calibrated by the C 1s peak (284.8 eV) of contamination carbon. Specific surface area ($S_{BET}$) was calculated based on $N_2$ adsorption/desorption isotherms recorded on a ASAP 2460 Surface Area and Porosity Analyzer (Micrometrics, USA), at 77 K, all samples were outgassed under vacuum at 300 °C for 12 h. SIGMA-300 field emission electron microscope (FESEM) was used to observe the morphology and particle size of the synthesized catalyst. HR-TEM observations were carried out by a high-resolution TEM (HRTEM, JEOL JEM-2100F) at 200 kV. The EPR test was conducted using the Bruker A300 at low temperature.

$H_2$ temperature programmed reduction ($H_2$-TPR) was performed on an AutoChem II 2920 adsorption apparatus (Micromeritics, USA) equipped with TCD detector. Prior to $H_2$-TPR experiment, 30 mg of catalysts was pretreated with He with a total flow rate of 30 mL·min$^{-1}$ at 300 °C for 0.5 h, then cooled down to room

90 temperature in the He atmosphere. Finally, the reactor temperature was raised to 600 °C

91 at a constant heating rate of 10 °C·$min^{-1}$ in a flow of $H_2$ (10 vol %)/He (30 mL·$min^{-1}$).

92 The $H_2$ consumption during the experiment was monitored by a TCD.

93 Temperature programmed desorption of $O_2$ ($O_2$-TPD) was conducted on the

94 TP2920 AutoChem adsorption analyzer. 30 mg sample was pretreated under the He

95 atmosphere (30 mL·$min^{-1}$) at 300 °C for 30 min and cooled down to 30 °C at the same

96 airstream condition. After the catalyst was in $O_2$(2 vol %)/He (30 mL·$min^{-1}$) at 300 °C

97 for 0.5 h, the treated catalyst was heated from 30 °C to 800 °C with a rate of 10 °C·$min^{-1}$

98 in a He flow (30 mL·$min^{-1}$).

99 Toluene TPD-MS was tested using a TP 5080 (Xianquan, Tianjin, China)

100 chemical adsorption instrument and an OMNISTAR (Pufa, Shanghai, China)

101 spectrometer. 30 mg sample was pretreated at 300 °C for 0.5 hours in the He atmosphere

102 (30 mL · $min^{-1}$), and cool to 30 °C under the same airflow conditions. After the catalyst

103 was treated in toluene (1000ppm) / He (50 mL · $min^{-1}$) for 1 hour, it was purged with

104 He gas for 0.5 hours. Then the treated catalyst was heated from 30 °C to 600 °C in He

105 gas (30 mL · $min^{-1}$) at a rate of 5 °C.

106 FTIR and operando/ in-situ DRIFTS experiments were carried out on a Nicolet

107 is50 spectrometer (Thermo Fisher, USA) equipped with a Harrick DRIFTS cell and an

108 MCT/A detector.

109

**CATALYTIC ACTIVITY TEST**

111    300 mg of the sample with 40-60 mesh was used to evaluate the catalytic oxidation

112   of toluene in a continuous flow fixed-bed tube microreactor ($\Phi$ = 6.0 mm). The toluene

113   vapor was generated and injected using a bubbler in a thermostatic bath at 0 °C, which

114   passed through a container filled with liquid toluene. The reactant mixture (volumetric

115   composition) consisted of 1000 ppm toluene and 20% $O_2$ balanced in $N_2$ with a total

116   flow of 200 mL/min, corresponding to WHSV of 40,000 mL $g^{-1}$ $h^{-1}$. At the beginning

117   of each test, the catalyst was pretreated in the real reactant mixture for 1 h in order to

118   overcome the over-estimation of toluene catalytic combustion conversion caused by

119   adsorption of toluene. The performances at steady states (typically after 0.5 h for every

120   10 °C) were used for discussion. The concentrations of the reactants and the generation

121   of the catalytic oxidation products were monitored in real time by a GC machine

122   (Shimadzu 2014C) equipped with double flame ionization detectors (FID), where $CO_2$

123   was detected by $CO_2$ detector.

124    The toluene conversion ($X_{Toluene}$) and reaction rate r (mol $g^{-1}$ $s^{-1}$) was calculated

125   using the following equations:

126   $X_{Toluene}(\%) = (([C_7H_8]_{in} - [C_7H_8]_{out}/[C_7H_8]_{in}) \times 100\%$              (1)

127   $r = [C_7H_8]_{in} \times X\%/m_{cat} = WHSV \times X \times 1.240079 \times 10^{-13}$              (2)

128    where [$C_7H_8$]in and [$C_7H_8$]out denoted the inlet and outlet concentrations of

129   toluene, respectively. where $c_{CO_2}$ is the outlet gas $CO_2$ concentration.

130   $X_{CO2} = [CO_2]_{out}/(7[C_7H_8]_{in}) \times 100\%$              (3)

131    where $[CO_2]_{out}$ is the outlet gas $CO_2$ concentration. This equation is based on the molar

132    ratio of toluene ($C_7H_8$) to $CO_2$ is 1: 7.

133

## COMPUTATIONAL METHODS

134     

135      Our spin-polarized DFT calculations have been carried out with the Vienna *Ab*

136      *initio* Simulation Package ) VASP( [1] using the Perdew-Burke-Ernzerhof ) PBE(

137      functional [2] and the projector augmented wave )PAW( method [3]. For all calculations,

138      a plane wave energy cutoff of 400 eV was used and the Brillouin zone integration was

139      performed using Monkhorst-Pack scheme with $2 \times 2 \times 1$ k-points [4]. For geometry

140      optimizations, the force and energy convergences were $0.025$ eV/Å and $10^{-6}$ eV,

141      respectively. The DFT + U was applied to address the on-site Coulomb interaction with

142      the U-J parameters of 3.3. eV for Co 3d [5]. To account for van der Waals ) vdW(

143      interaction, the DFT-D3 method of Grimme was utilized [6].

144      In this work, the $Co_3O_4$ (311) $(1 \times 1)$ slab surface containing 96 Co and 128 O

145      atoms was employed. During geometry optimizations, the bottom 3 Co layers are fixed

146      to their bulk positions and all the rest atoms are fully relaxed. A vacuum space of 15 Å

147      was added in the direction perpendicular to the surface to prevent interactions between

148      periodic images.

149      The O- and Co-vacancy formation energies ($E_{vac}$) were calculated as: $E_{vac} = E_{slap}$

150      $- E_{slap-vac} - E_{removed}$ where $E_{slap}$ is the energy of (311) surface without vacancy site and

151      $E_{slap-vac}$ and $E_{removed}$ are the energy of (311) surface with O- or Co-vacancy site and the

152      energy of $\frac{1}{2}(O_2)$ for O vacancy or the energy of Co atom for Co vacancy, respectively.

153      And the adsorption energy ($E_{ads}$) of $O_2$ on the $Co_3O_4$ (311) surface with O- and Co-

154      vacancy site were defined by $E_{ads} = E_{O2/slap-vac} - E_{slap-vac} - E_{O2}$. Here, $E_{O2/slap-vac}$ is the

155      energy of adsorption complex and $E_{slap-vac}$ and $E_{O2}$ are the energy of corresponding slap

156     surface and isolated oxygen molecule, respectively.

157

158     **Table S1.** $H_2$ consumption from $H_2$-TPR and catalytic properties of $Co_3O_4$-HA, $Co_3O_4$-

159     MA, and $Co_3O_4$-LA.

| 160 | $H_2$ consumption (mmol/g) | | | | $T_{50\%}$/℃ | $T_{90\%}$/℃ | Ea/(kJ/mol) |
|---|---|---|---|---|---|---|---|
| | $C_{Tmin}$ | $C_{Tmax}$ | $C_{Total}$ | $C_{Tmin/Tmax}$(%) | | | |
| $Co_3O_4$-HA | 3.4 | 12.2 | 15.6 | 38.6 | 232 | 240 | 35.35 |
| $Co_3O_4$-MA | 3.5 | 8.8 | 12.3 | 66.0 | 242 | 251 | 40.41 |
| $Co_3O_4$-LA | 5.6 | 11.3 | 16.9 | 98.2 | 250 | 260 | 44.74 |

161

162     **Table S2.** Catalytic performance parameters reported on toluene over related catalysts.

| Catalysts | Surface area $(m^2 \cdot g^{-1})$ | VOC conc. (ppm) | GHSV $(mL \cdot g_{cat}^{-1} \cdot h^{-1})$ | $T_{50\%}$ (°C) | $T_{90\%}$ (°C) | References |
|---|---|---|---|---|---|---|
| Co$_3$O$_4$-HA | 19.4 | 1000 | 40000 | 232 | 240 | This work |
| Pt/KBeta-SDS | 299 | 1000 | 60000 | 142 | 150 ($T_{98}$) | J. Mater. Chem. A. 2015, 3, 5556. |
| 3D hierarchical Co$_3$O$_4$ | 26.7 | 500 | 60000 | 234 | >245 | Appl. Surf. Sci. 2020, 507, 145. |
| Co$_3$O$_4$-cube | 83.1 | 1000 | 48000 | 240 | 248 | J. Mater. Chem. A. 2018, 6, 498. |
| 0.99Au/3DOM Co$_3$O$_4$ | 36.2 | 1000 | 40000 | 268 | 275 | J. Catal. 2015, 322, 38. |
| 6.4Au/bulk Co$_3$O$_4$ | 8.7 | 1000 | 20000 | 244 | 277 | J. Catal. 2014, 309, 408. |
| Co$_3$O$_4$-HT | 41.9 | 1000 | 20000 | 241 | 260 | ACS Catal. 2014, 4, 2753. |

163

164 **Table S3.** Summary of the physicochemical properties of $Co_3O_4$-HA, $Co_3O_4$-MA, and

165 $Co_3O_4$-LA.

| Catalysts | Crystalline/% | Lattice para-meter/Å | BET surface area (m$^2$g$^{-1}$) | $O_{ads}/(O_{ads}+O_{latt})$ (%) | $Co^{3+}/Co^{2+}$ (%) |
|---|---|---|---|---|---|
| $Co_3O_4$-HA | 58.59 | a=b=c=8.067 | 19.4 | 36.6 | 34.0 |
| $Co_3O_4$-MA | 69.07 | a=b=c=8.080 | 14.8 | 32.4 | 40.9 |
| $Co_3O_4$-LA | 73.73 | a=b=c=8.077 | 8.0 | 32.3 | 46.5 |

166

167 **Table S4.** Quantitative data of toluene TPD-MS of $Co_3O_4$-HA, $Co_3O_4$-MA, and $Co_3O_4$-

168 LA.

|  | $Co_3O_4$-HA | $Co_3O_4$-MA | $Co_3O_4$-LA |
|---|---|---|---|
| T(Toluene)/□ | 73 | 64 | 58 |
| T($CO_2$)/□ | 339 | 341 | 340 |

169

170 **Table S5.** Infrared vibration information of toluene related to intermediate species
171 adsorbed on the catalyst.

| Wavenumber($cm^{-1}$) | Vibration mode | References |
|---|---|---|
| 1025 $cm^{-1}$ | The C-O stretching vibration of benzyl alcohol | Appl. Surf. Sci. 2014, 311, 690. |
| 1155 $cm^{-1}$ | | Appl. Catal., B. 2016, 181, 236. |
| 1177 $cm^{-1}$ | | Chem. Eng. J. 2020, 125192. |
| 1599 $cm^{-1}$ | The benzene ring vibration | Chem. Eng. J. 2015, 270, 58. |
| 1305 $cm^{-1}$ | The vibrational peak of maleic anhydride | Chem. Eng. J. 2018, 334, 768. Appl. Catal., B 2019, 256, 117814. ACS Appl. Mater. Interfaces 2019, 11, 730. |
| 1408 $cm^{-1}$ | C-O symmetric stretching vibration peak attributed to benzoate | Appl. Catal., B 2019, 245, 502. ACS Catal. 2019, 9, 6698. J. Mater. Chem. A 2019, 7, 3366. |
| 1520 $cm^{-1}$ | The anti-symmetric vibration of the COO- group of the benzoate | |
| 1447 $cm^{-1}$ | The vibration of the skeleton C-C bond derived from the benzene ring of benzaldehyde | ACS Catal. 2019, 9, 6698. Chem. Eng. J. 2018, 344, 469. Appl. Catal., B 2018, 224, 705. |
| 1468 $cm^{-1}$ | The C=O vibration peak subordinate to benzaldehyde | |
| 1654 $cm^{-1}$ | | |
| 1753 $cm^{-1}$ | | |
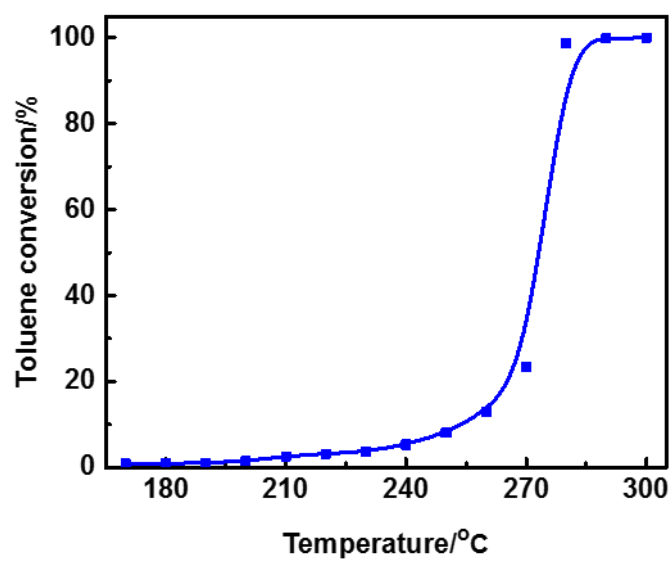
172

173 **Figure S1.** Plots of toluene conversion versus temperature over $Co_3O_4$-600.
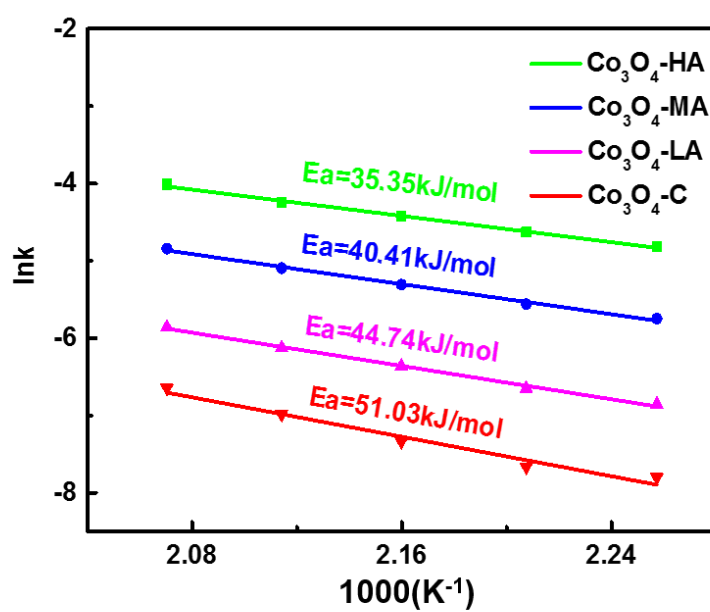
174

175 **Figure S2.** Arrhenius plots for toluene oxidation over $Co_3O_4$-HA, $Co_3O_4$-MA, $Co_3O_4$-

176 LA, and $Co_3O_4$-C.

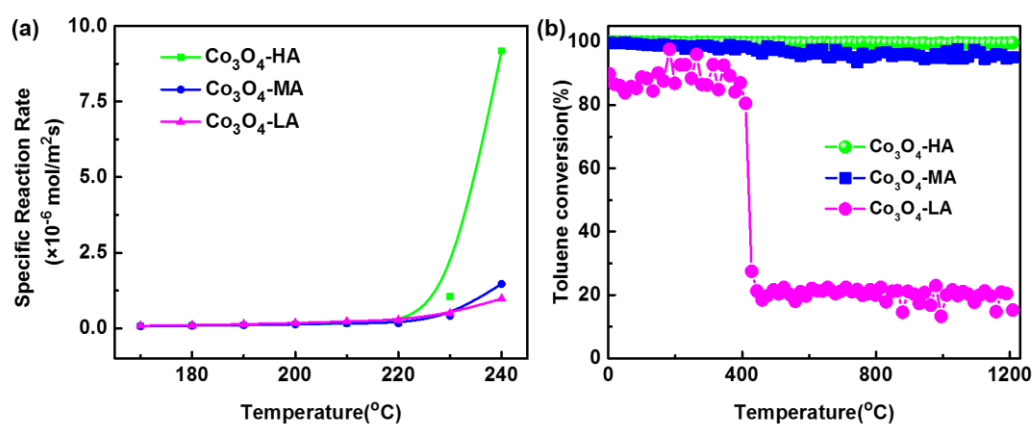**Figure S3.** (a) Plots of specific reaction rate of different samples normalized by specific surface area, and (b) catalytic stability (under 250°C for 20h) of $Co_3O_4$-HA, $Co_3O_4$-MA, and $Co_3O_4$-LA.
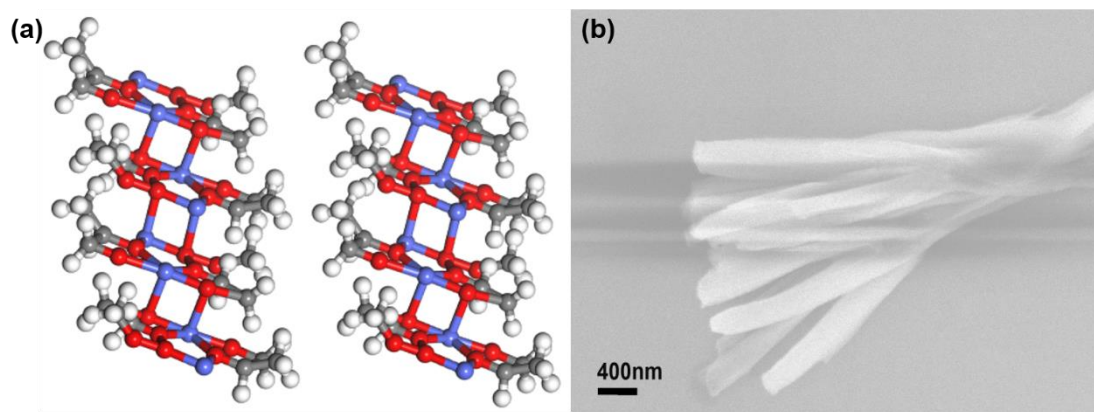
181
182      **Figure S4.** (a) Crystal structure and (b) SEM image of $Co_3O_4$ precursor.
183
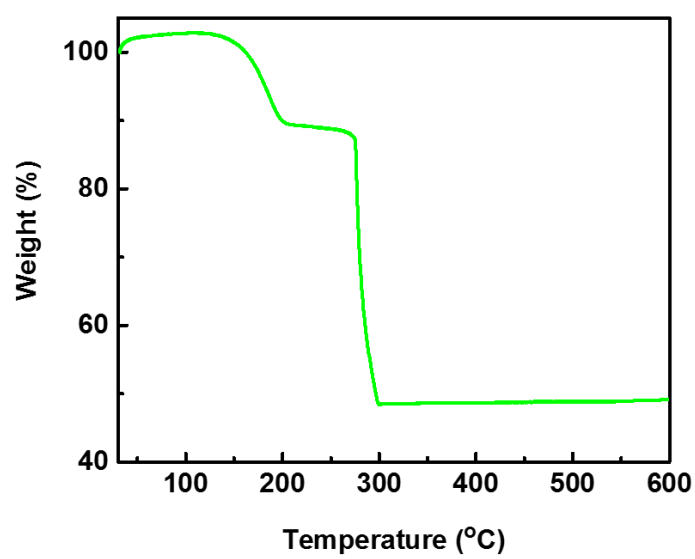
**Figure S5.** TG profiles of CoGly (precursor).
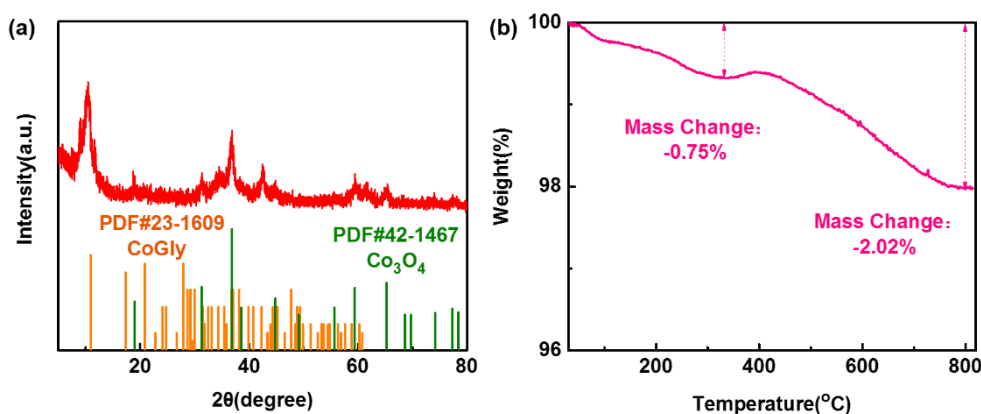
**Figure S6.** (a) XRD patterns and (b) TG profiles of $Co_3O_4$-C.

**Note:** $Co_3O_4$-C is a mixed phase of carbon and cobalt oxide; the crystal plane index is not good to be directly marked on the XRD pattern. However, combined with the synthesis method in the article, as shown in Figure S6a, two PDF cards can explain the XRD pattern of $Co_3O_4$-C. CoGly (PDF#23-1609)[7] is a precursor to synthetic catalysts and contains cobalt and glycerin. $Co_3O_4$ (PDF#42-1467) is the product after calcination. These indicate that, CoGly has not been completely calcined under air calcination at 270 °C, and the product contains part of GoGly and $Co_3O_4$. The thermogravimetric experiment was carried out over $Co_3O_4$-C to prove the amount of $Co_3O_4$ in $Co_3O_4$-C catalyst. It can be seen from Figure S6b that the curve has a small platform in the temperature range of 300-400°C, and the mass loss is 0.75% at this time. This loss is due to the consumption of carbon species in $Co_3O_4$-C. The mass loss (1.27%) after 400 °C may be regarded as the oxygen released during the sintering of small particles into large particles. It can be concluded that the loading of $Co_3O_4$ in $Co_3O_4$-C is around 99.18%.
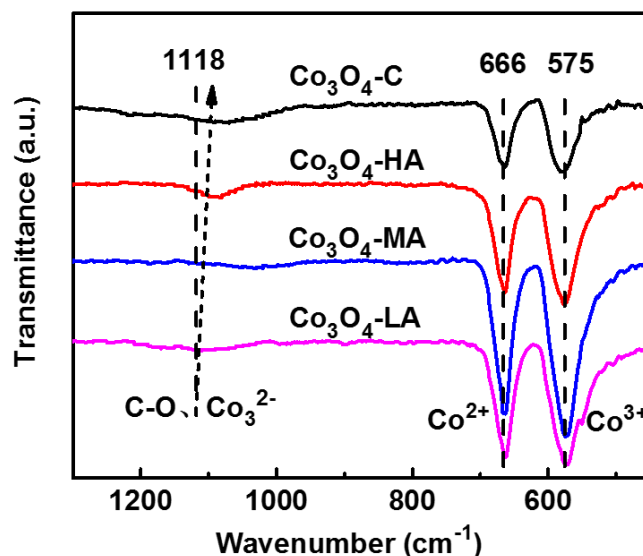
202

**Figure S7.** FTIR spectra of $Co_3O_4$-C, $Co_3O_4$-HA, $Co_3O_4$-MA, and $Co_3O_4$-LA.

**Note:** The peak at 575 cm$^{-1}$ is regarded as the peak of $Co^{3+}$, the peak at 666 cm$^{-1}$ is classified as the peak of $Co^{2+}$, and the peak at 1118 cm$^{-1}$ is attributed to the vibration of C-O and $CO_3^{2-}$.[8] Obviously, all samples have peaks related to $Co^{3+}$ and $Co^{2+}$ species, which indicates that all samples contain the crystal phase of $Co_3O_4$. Although all samples have peaks at 1118cm$^{-1}$, the attribution varies. The presence of this peak in $Co_3O_4$-C is attributed to the relatively uniform distribution of carbon species in $Co_3O_4$-C (XRD and Raman of $Co_3O_4$-C can be proven again.), while the remaining samples containing this peak is considered to be a little $CO_3^{2-}$ remaining on the sample when the precursor is calcined.
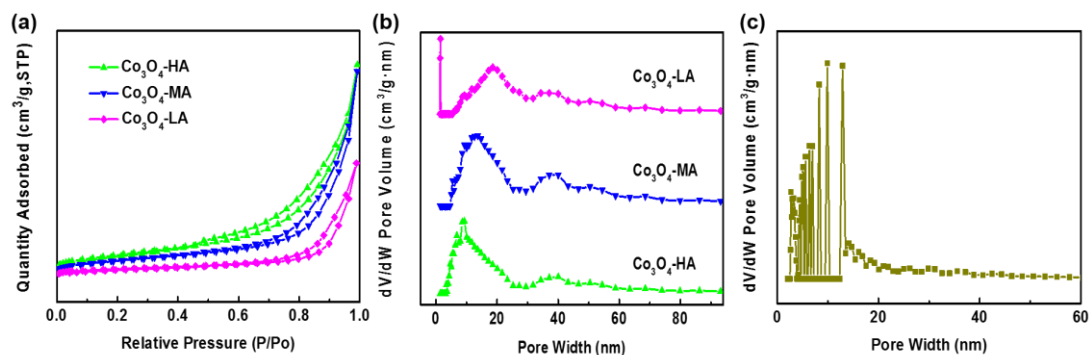
213

**Figure S8.** (a) N$_2$ adsorption-desorption isotherms, and (b) pore size distribution
profiles of Co$_3$O$_4$-HA, Co$_3$O$_4$-MA, and Co$_3$O$_4$-LA. (c) The pore size distribution profile
of Co$_3$O$_4$-C.
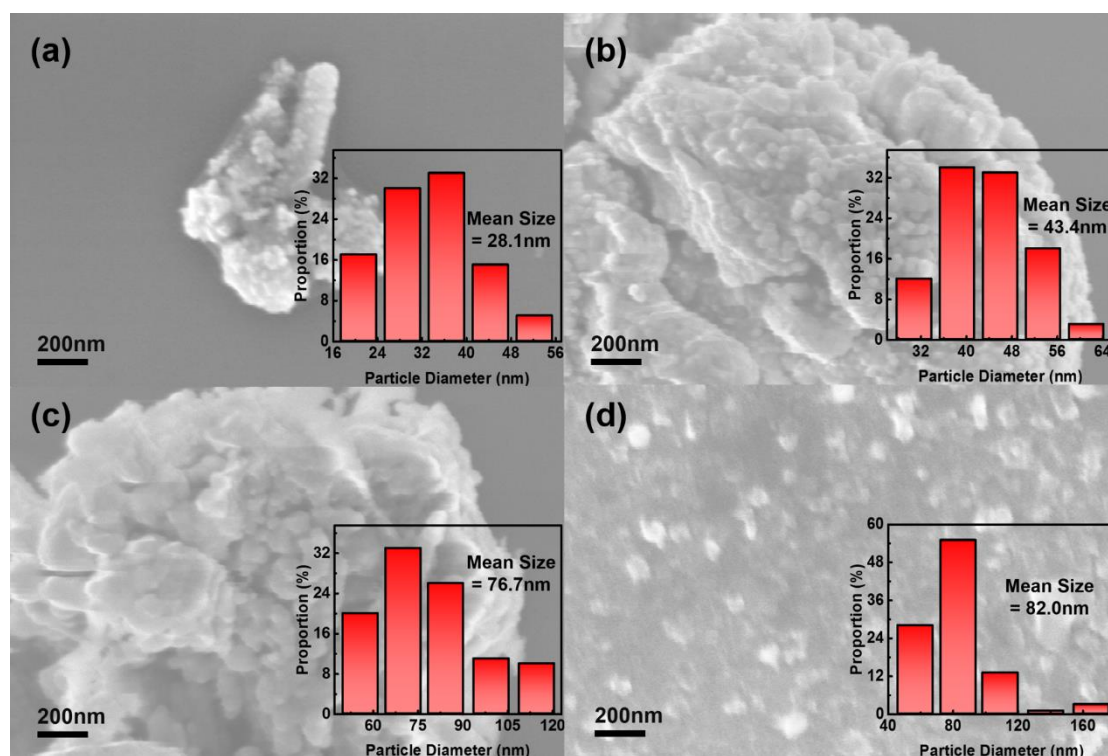
**Figure S9.** SEM images of (a) $Co_3O_4$-HA, (b) $Co_3O_4$-MA, (c) $Co_3O_4$-LA, and (d) $Co_3O_4$-C.
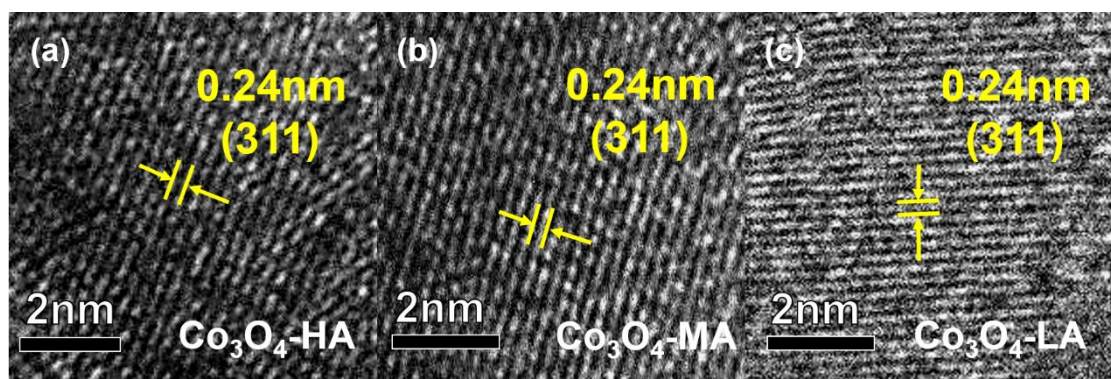
**Figure S10.** HRTEM images of (a) $Co_3O_4$-HA, (b) $Co_3O_4$-MA, and (c) $Co_3O_4$-LA.

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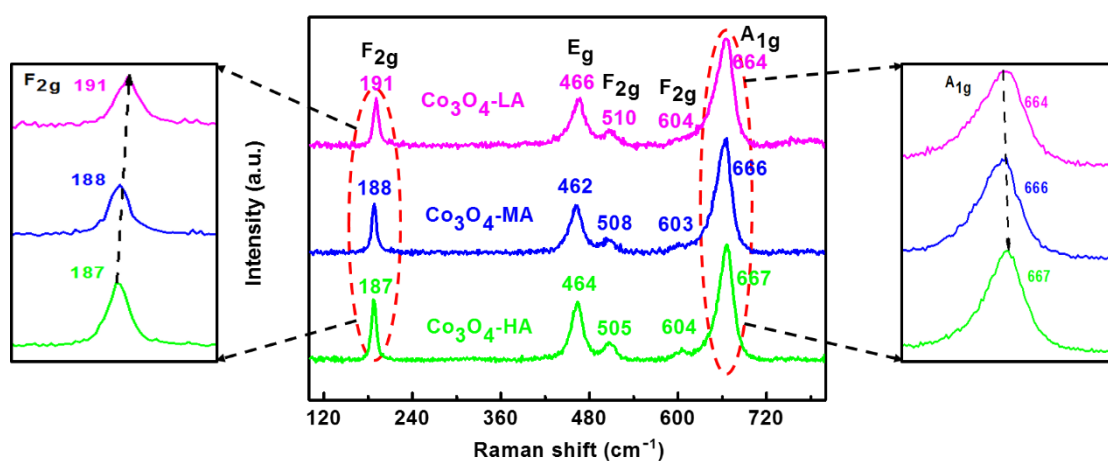
223 **Figure S11.** Raman spectra of the $Co_3O_4$-HA, $Co_3O_4$-MA, and $Co_3O_4$-LA.

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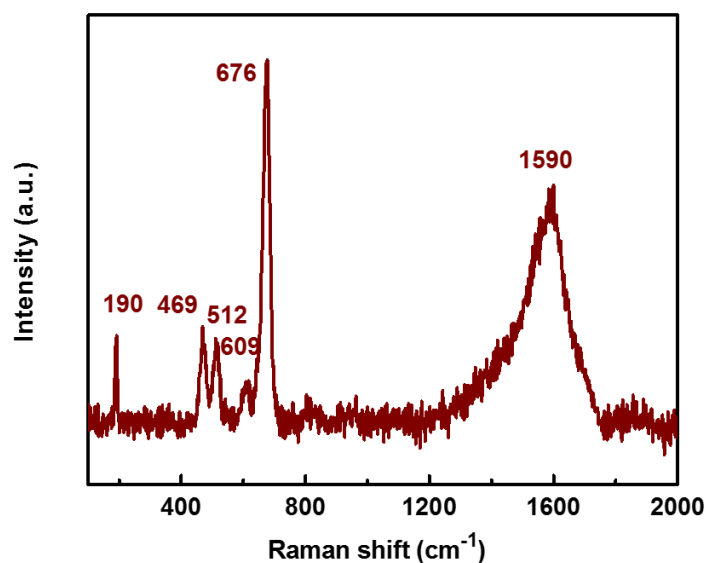
**Figure S12.** Raman spectra of $Co_3O_4$-C.

**Note:** As shown in Figure S12, the peaks at $190 cm^{-1}$ ($F_{2g}$), $469$ $cm^{-1}$, ($E_g$), $512$ $cm^{-1}$ ($F_{2g}$), $609$ $cm^{-1}$ ($F_{2g}$), and $676$ $cm^{-1}$ ($A_{1g}$) are assigned to the Raman active vibration mode of $Co_3O_4$.[9] The peak at $190 cm^{-1}$ is attributed to four-coordinated Co ($CoO_4$), and the peak at $676 cm^{-1}$ is attributed to six-coordinated Co ($CoO_6$). In addition, the peak at $1590$ $cm^{-1}$ is assigned to the G-band peak of the carbon peak. In summary, $Co_3O_4$-270 is a mixed-phase catalyst containing a part of $Co_3O_4$ crystal phase and carbon species.

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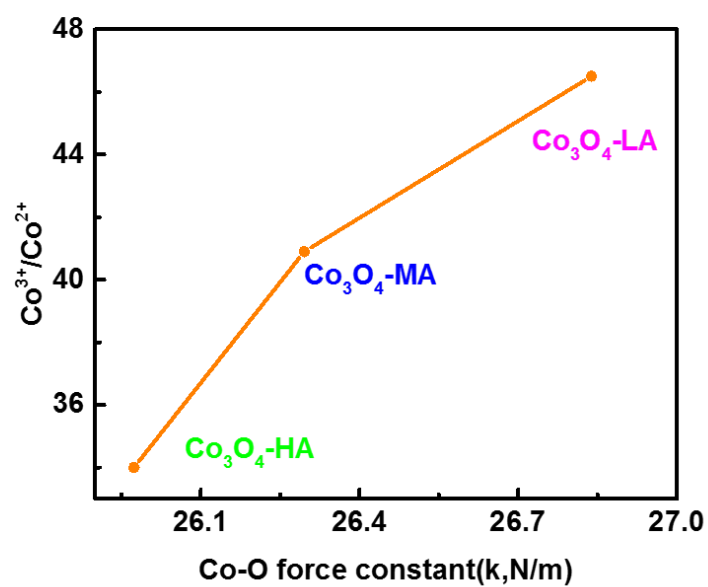
**Figure S13.** The trend profile of the relationship between the ratio of $Co^{3+}$ to $Co^{2+}$ from XPS results and the Co−O bond force constant from Raman results of the catalysts.
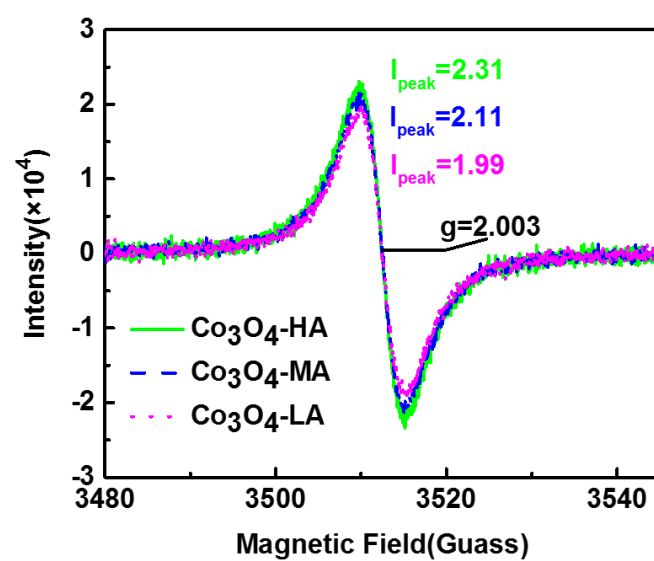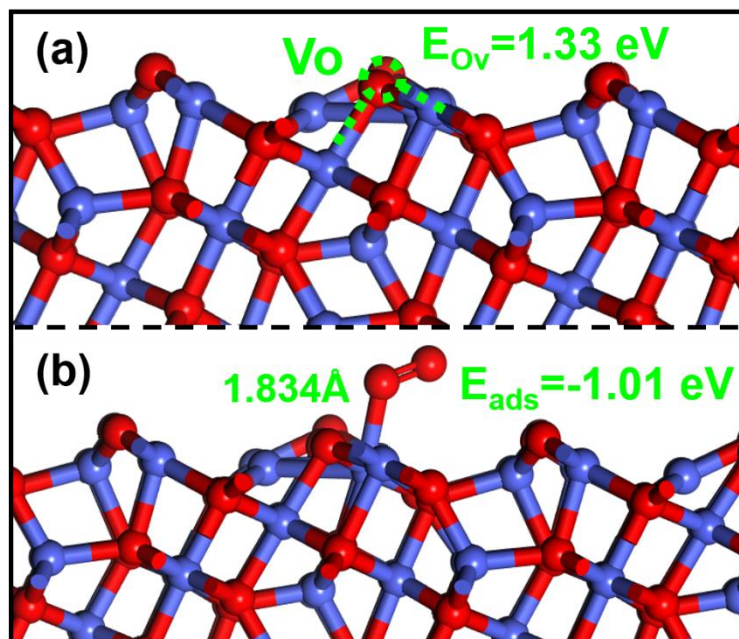
236

237        **Figure S14.** EPR spectra of the $Co_3O_4$-HA, $Co_3O_4$-MA, and $Co_3O_4$-LA.

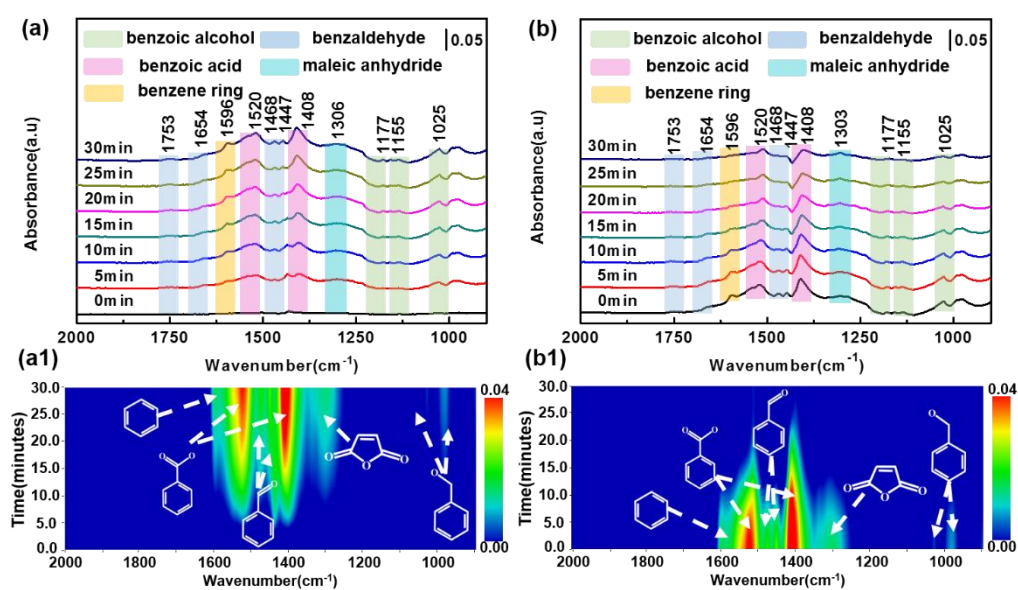**Figure S15.** Optimized structures of (a) oxygen vacancy and (b) $O_2$ adsorption on low

activated $Co_3O_4$.

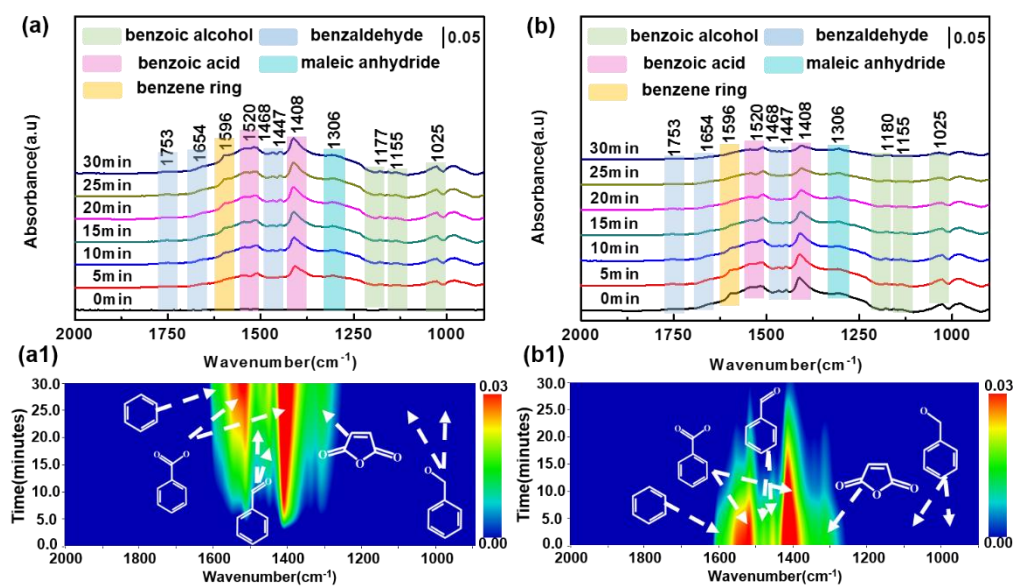**Figure S16.** In situ DRIFTS spectra of toluene (a, a1) adsorption and (b, b1) oxidation on $Co_3O_4$-MA at 240 $^oC$.

**Figure S17.** In situ DRIFTS spectra of toluene (a, a1) adsorption and (b, b1) oxidation on $Co_3O_4$-LA at 240 $^o$C.
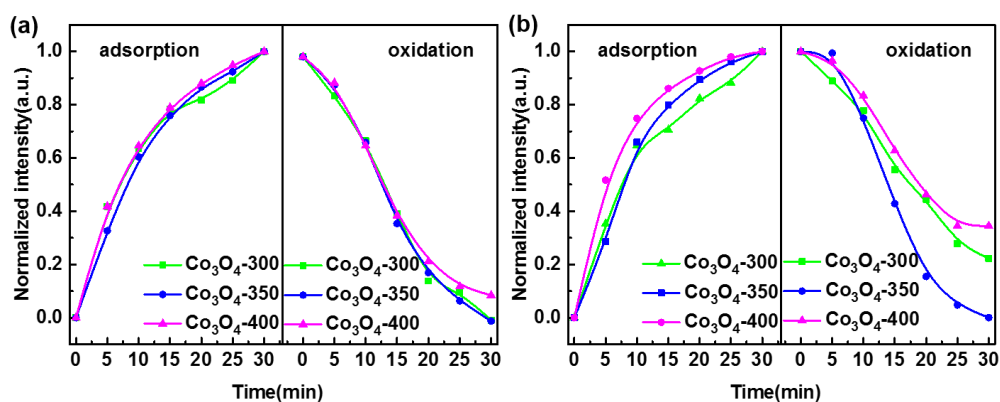
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**Figure S18.** Accumulation and consumption of (a) benzyl alcohol and (b) benzaldehyde

upon passing air stream over the $Co_3O_4$ catalysts after the catalysts absorbed toluene
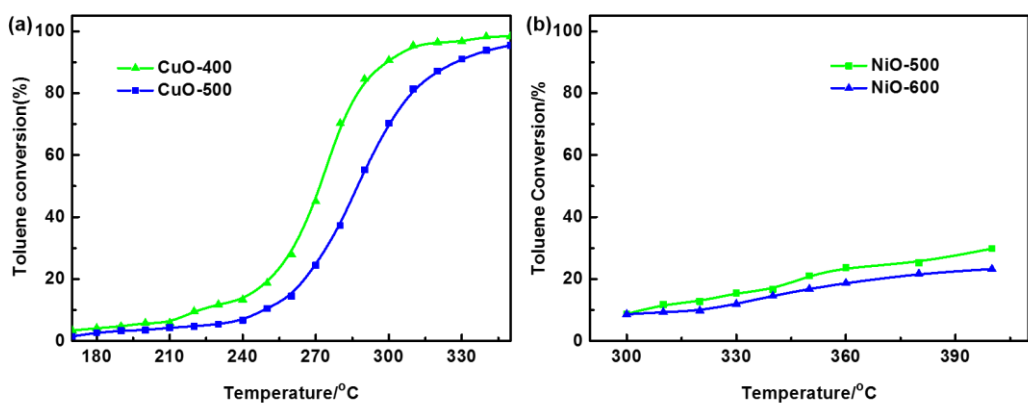
for 30 min.

**Figure S19.** Plots of toluene conversion versus temperature over (a) CuO and (b) NiO catalysts. (The number represents the processing temperature.)

**Note:** CuO and NiO have better toluene degradation performance at lower pyrolysis temperature. The bond strength between CuO and NiO metal and oxygen needs to be further explored in future work.

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282    for Highly Efficient Oxygen Evolution. *Adv. Energy Materials*. 2017, 7, (1), 1601492.