

SUPPORTING INFORMATION

Singlet Oxygen Photogeneration in Coastal Seawater: Prospect of Large-Scale Modelling in Seawater Surface and its Environmental Significance.

Michael O. Sunday^{a,b}, Kazuhiko Takeda^a, Hiroshi Sakugawa^{a*}

^aGraduate School of Biosphere Science, Hiroshima University, 1-7-1, Kagamiyama, Higashi-Hiroshima, 739-8521 Japan.

^bDepartment of Chemistry, Federal University of Technology, Akure, P.M.B 704, Ondo State, Nigeria. E-mail: omsunday@futa.edu.ng

**Corresponding Author*

Hiroshi Sakugawa

Graduate School of Biosphere Science, Hiroshima University, 1-7-1, Kagamiyama, Higashi-Hiroshima, 739-8521 Japan. Tel: +81-82424-6504; E-mail: hsakuga@hiroshima-u.ac.jp

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CONTENTS

S1: CDOM absorption characteristics

Absorption coefficient (a_{300})

The absorbance due to CDOM in the samples was monitored using an UV-visible spectrophotometer (UV-2400, Shimadzu, Japan). Samples were placed in a 5 cm pathlength (l) quartz cuvette and absorbance readings at 300 nm (A_{300}) were obtained. Prior to sample measurement, MilliQ water was used to obtain baseline values and was intermittently analyzed during sample measurements to check for consistency and correction where necessary. The A_{300} was then converted to the Napierian absorption coefficient (a_{300} , m^{-1}) according to equation (S1.1).¹

$$a_{300} = \frac{2.303A_{300}}{l} \quad (S1.1)$$

Spectra slope

The slope of the CDOM absorption spectra, which is known as the spectra slope (S), was determined by fitting the absorption coefficient values (a_{λ}) from 300–550 nm to the exponential function in equation S1.2 using a non-linear least square regression routine.^{1,2}

$$a_{\lambda} = (a_{\lambda_0} - K)e^{-S(\lambda - \lambda_0)} + K \quad (S1.2)$$

where S is the spectra slope (μm^{-1}), a_{λ} is the absorption coefficient at wavelength λ , a_{λ_0} is the absorption coefficient at reference wavelength λ_0 (300 nm) and K is a constant to account for baseline offset.

Carbon-specific absorption (a_{300})

The carbon-specific absorption or specific absorption coefficient (a_{300}) is defined as the absorption coefficient (a_{300}) normalized to DOC concentration (mg C/L) of the sample.³ The units are $\text{m}^2 \text{g}^{-1} \text{C}$. This variable also provides information regarding variations in CDOM composition as it shows how “chromophoric” the DOC content of a sample is. Additionally, this variable has been shown to have a positive correlation with aromatic content and molecular size of DOC.⁴

S2: Photoirradiation experiments

Laboratory irradiation under a solar simulator

Solutions to be irradiated (7 mL) were contained in an 8.8 mL quartz cell and irradiated under a solar simulator. The device consisted of a lamp housing (WACOM Co., HX-500) equipped with a 500 W Xe lamp (WACOM Co., KXL-500F) and an optical filter (HOYA Co., UV-31) with a transmission wavelength limit of 310 nm. The quartz cell was placed in an air-conditioned compartment of the simulator that maintained the temperature of the sample at 20°C during irradiation. A detailed description of the solar simulator has been reported by Nakatani et al.⁵ Aliquots were withdrawn at intervals for HPLC analysis.

S3. Analytical determinations

S3A. Singlet oxygen

$^1\text{O}_2$ was determined using FFA as a chemical probe. Samples were spiked with FFA (final concentration; 100 μM) and irradiated under a solar simulator or sunlight accordingly. At intervals, aliquots of the reaction mixture were withdrawn and analyzed for FFA and 6-HP-one simultaneously

by HPLC. The isocratic HPLC system consisted of a pump (Prominence LC-20AD, Shimadzu, Kyoto) that delivered *eluent* (0.1% H₃PO₄: ACN (90:10)) at a flow rate of 1 mL/min, as well as an injection valve equipped with a 20 µL sample loop for sample injection. FFA and 6-HP-one were separated on a C₁₈ column (Cosmosil, MS-II, 250 mm x 4.6 mm, 5 µm) and detected on a UV-Visible detector (Prominence LC-20AD, Shimadzu, Kyoto, Japan) at 219 nm.

Kinetic data treatment

Generation of ¹O₂ using FFA as a probe was determined by monitoring: (i) FFA degradation (HH method) and (ii) 6-HP-one formation (ZM method) adopting the approach used by Zhou and Mopper.⁶

HH method

FFA reacts with ¹O₂ resulting in a pseudo first order degradation rate constant, *k*, of FFA. As shown in Fig. S4, the degradation of FFA in this study also followed first order kinetics. Therefore, [¹O₂]_{ss} was determined from equation S3.1 by dividing the observed first order degradation rate constant (*k*) of FFA in the irradiated solution by the reaction rate constant of FFA with ¹O₂ (*k*_{FFA,¹O₂}), which is given as 1.09 × 10⁸ M⁻¹s⁻¹.⁷ The *k*_{FFA,¹O₂} used for each sample was corrected for the effect of salinity on the rate constant as recommended by Appiani et al.⁸

$$[{}^1O_2]_{ss} = K/k_{FFA,{}^1O_2} \quad (S3.1)$$

The photoformation rate (*R*¹O₂) was calculated using equation S3.2:

$$R{}^1O_2 = [{}^1O_2]_{ss} \times k_d \quad (S3.2)$$

where *k_d* is the dissociation rate constant of ¹O₂ in water given as 2.5 × 10⁵ s⁻¹.⁹ Water is the main scavenger of ¹O₂; hence, the scavenging capacity of other potential scavengers in natural waters are negligible.

78

79 *ZM method*

80 The photoformation rate of $^1\text{O}_2$ ($R^1\text{O}_2$) was also investigated using the approach described by Zhou
 81 and Mopper⁶ by monitoring 6-HP-one formation. It was determined using equation S3.3, where
 82 $R_{6\text{-HP}}$ is the formation rate of 6-HP-one from the reaction of FFA and $^1\text{O}_2$; $Y_{6\text{-HP}}$ is the yield of 6-
 83 HP-one defined as the amount of 6-HP-one formed for each mole of FFA that reacts with $^1\text{O}_2$ and
 84 F is the fraction of $^1\text{O}_2$ that reacts with FFA. $Y_{6\text{-HP}}$ was determined using equation S3.4.

$$85 \quad R^1\text{O}_2 = \frac{R_{6\text{-HP}}}{Y_{6\text{-HP}} \times F} \quad (\text{S3.3})$$

$$86 \quad Y_{6\text{-HP}} = \frac{\text{photoformation rate of 6-HP-one}}{\text{degradation rate of FFA}} \quad (\text{S3.4})$$

87 The reaction of FFA and $^1\text{O}_2$ in the sample is in competition with the deactivation or quenching of
 88 $^1\text{O}_2$ by water as the main quencher of $^1\text{O}_2$. Therefore, the fraction, F , which is the fraction of $^1\text{O}_2$
 89 that reacts with FFA, compared to physical quenching by H_2O molecules was obtained using
 90 equation S3.5:

$$91 \quad F = \frac{k_{\text{FFA},^1\text{O}_2} [\text{FFA}]}{k_d + k_{\text{FFA},^1\text{O}_2} [\text{FFA}]} \quad (\text{S3.5})$$

92 The value of F varied slightly between 0.0368–0.0372 due to the salinity correction applied to the
 93 $k_{\text{FFA},^1\text{O}_2}$.

94 **S3B. $\cdot\text{OH}$ determination**

95 $\cdot\text{OH}$ photoformed in the seawater sample was measured using benzene as a chemical probe.^{10,11}
 96 Briefly, 7 mL samples were spiked with a final concentration of 1.2 mM benzene and irradiated

using the solar simulator described above. The same quartz cell used for the $^1\text{O}_2$ irradiation experiment above was also used here. The irradiation lasted for about 40 mins, during which time aliquots were obtained at 10 min intervals for phenol determination using an HPLC.

The HPLC system used for this determination consisted of a pump (LC-10Ai, Shimadzu, Kyoto, Japan) that delivered eluent (acetonitrile:MQ (60:40)) at a flow rate of 1 mL/min. An injection valve equipped with a 50 μL sample loop was used to inject samples into the system. Phenol was separated on a C_{18} column (Cosmosil, MS-II, 250 mm x 4.6 mm, 5 μm) and detected using a fluorescence detector (LC-20AD, Shimadzu, Kyoto, Japan) set at excitation/emission wavelengths of 270/298 nm.

The photoformation rate of $\cdot\text{OH}$ (ROH) was determined using equation S3.6:

$$R_{\text{OH}} = \frac{R_{\text{phenol}}}{Y_{\text{phenol}} \times F_{\text{benzene-OH}}} \quad (\text{S3.6})$$

where R_{phenol} is the photoformation rate of phenol in each irradiated sample; Y_{phenol} is the yield of phenol formed in the reaction between benzene and $\cdot\text{OH}$, and $F_{\text{benzene-OH}}$ is the fraction of $\cdot\text{OH}$ that reacts with benzene during the irradiation of benzene-spiked samples. A Y_{phenol} of 0.75 reported by Arakaki & Faust¹⁰ and an $F_{\text{benzene-OH}}$ value of 0.68 reported in Seto inland seawater by Takeda et al.¹¹ were used for all calculations.

The generated $\cdot\text{OH}$ will be scavenged by both benzene and the group of all other potential scavengers such as DOM and Br^- , in seawater. Hence, it is important to determine the scavenging rate constant (SRC) of these scavengers in the seawater sample. The SRC is the sum of the reaction rates (rate constant of scavenger with $\cdot\text{OH}$ ($k_{s,\text{OH}}$) x [Scavengers]) given as $\sum_i^j (k_{si,\text{OH}})[s]$ of all

other scavengers present in the seawater sample that compete with benzene for the photoformed $\cdot\text{OH}$.

The SRC was determined using equation S3.7, which expresses the fraction ($F_{benzene-OH}$) of $\cdot\text{OH}$ that reacts with benzene.

$$F_{benzene-OH} = \frac{k_{benzene-OH} [benzene]}{k_{benzene-OH} [benzene] + \sum_i^j (k_{si,OH})[s]} \quad (S3.7)$$

where $k_{benzene-OH}$ is the reaction rate constant of benzene with $\cdot\text{OH}$ given as $7.8 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$.¹²

By substituting equation S3.7 for $F_{benzene-OH}$ in equation S3.6 and making R_{phenol} the subject of the formula, the following equation was obtained:

$$\frac{1}{R_{phenol}} = \frac{1}{R_{OH}Y_{OH}} + \frac{\sum_i^j (k_{si,OH})[s]}{R_{OH}Y_{OH}k_{benzene-OH}} \times \frac{1}{[Benzene]} \quad (S3.8)$$

Therefore, a plot of $1/R_{phenol}$ against $1/[Benzene]$ gives a straight-line graph with:

$$Intercept = \frac{1}{R_{OH}Y_{OH}} ; Slope = \frac{\sum_i^j (k_{si,OH})[s]}{k_{benzene-OH}} \times Intercept$$

$$Hence, SRC (\sum_i^j (k_{si,OH})[s]) = \frac{Slope \times k_{benzene-OH}}{Intercept} \quad (S3.9)$$

To determine SRC experimentally, seawater samples were treated with varying concentrations of benzene (25, 50, 75 and 100 μM) and irradiated, after which their corresponding R_{phenol} values were obtained. A plot of $1/R_{phenol}$ against $1/[Benzene]$ gave a straight-line graph as expected from equation S3.8. The slope and intercept obtained in addition to $k_{benzene-OH}$ were then used in equation S3.9 to obtain the SRC for the sample.

The steady state concentration $[\cdot\text{OH}]_{ss}$ was determined using equation (S3.10)

$$[\cdot OH]_{ss} = \frac{\text{Photoformation rate, } R_{OH}}{\text{Scavenging rate constant}} \quad (S3.10)$$

Having initially obtained ROH, the steady state concentration was obtained after determining the SRC in each sample.

S4. Other measurements

Nitrite was determined according to the method described by Strickland and Parsons.¹³ This procedure is based on the reaction of nitrite with sulfanilamide in an acid solution to form a diazonium compound, which is then coupled to N-(1-Naphthyl)-ethylenediamine dihydrochloride to form a colored azo dye. The absorbance of the azo dye is then read spectrophotometrically at 540 nm. Sample concentrations were determined from a calibration curve obtained using standard solutions of nitrite ion.

Dissolved organic carbon (DOC) was analyzed using a TOC-VCSH analyzer (Shimadzu, Kyoto, Japan). Potassium hydrogen phthalate was used as the standard to obtain the calibration curve for DOC measurement.

S5. Effect of azide on ¹O₂ determination

NaN₃ is an effective quencher of ¹O₂; therefore, irradiation of FFA-spiked samples in the presence of NaN₃ is expected to result in a corresponding decrease in the rate of FFA degradation (R_{FFA}) and 6-HP-one formation (R_{6-HP}). To investigate this, the S11 seawater sample, which had the highest CDOM abundance, was spiked with FFA and irradiated in the absence and presence of 0.5 mM NaN₃. The R_{FFA} was monitored in both experiments. As shown in Fig. S4, R_{FFA} was reduced in the presence of azide compared with its absence.

155 Mathematically, R_{FFA} can be expressed as:

$$156 \quad R_{FFA} = R_{1O_2} \times \text{Fraction (F)} \quad (S5.1)$$

157 In the absence of azide, F is obtained from equation S5.2 as shown below.

$$158 \quad F = \frac{k_{FFA, 1O_2} [FFA]}{k_d + k_{FFA, 1O_2} [FFA]} \quad (S5.2)$$

$$159 \quad F = \frac{1.09 \times 10^8 \times 1 \times 10^{-4}}{2.76 \times 10^5 + (1.09 \times 10^8 \times 1 \times 10^{-4})}$$

$$160 \quad F = 0.038$$

161 However, in the presence of azide, F can be expressed as equation S5.3:

$$162 \quad F = \frac{k_{FFA, 1O_2} [FFA]}{k_d + k_{FFA, 1O_2} [FFA] + k_{NaN_3, 1O_2} [NaN_3]} \quad (S5.3)$$

$$163 \quad F = \frac{1.09 \times 10^8 \times 1 \times 10^{-4}}{2.76 \times 10^5 + (1.09 \times 10^8 \times 1 \times 10^{-4}) + (7.8 \times 10^8 \times 5 \times 10^{-4})}$$

$$164 \quad F = 0.0163$$

165 where $k_{NaN_3, 1O_2}$ is the reaction rate constant between azide and 1O_2 was given as $7.8 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$.

166 F in the presence of azide was 0.0163, which represents a 43% reduction from the value of 0.038

167 obtained in the absence of azide. According to equation S5.1, R_{1O_2} was assumed to be constant in

168 both experiments with and without azide; therefore, R_{FFA} is dependent on F. Hence, R_{FFA} in the

169 presence of azide was expected to be reduced by 43% based on the % reduction in F.

170 Experimentally, the R_{FFA} obtained in the absence of azide was $0.0288 \mu\text{M}/\text{min}$, while that obtained

171 in the presence of azide was $0.0126 \mu\text{M}/\text{min}$. This represents a 44% reduction in R_{FFA} in the

172 presence of azide, which agrees with kinetic estimations of 43%. These findings confirm that the

degradation of FFA in this study was mediated by $^1\text{O}_2$ photoformed in the irradiated seawater sample.

The effects of azide on $\text{R}_{6\text{-HP}}$ were also investigated. R^1O_2 determined based on $\text{R}_{6\text{-HP}}$ can be expressed as equation X4:

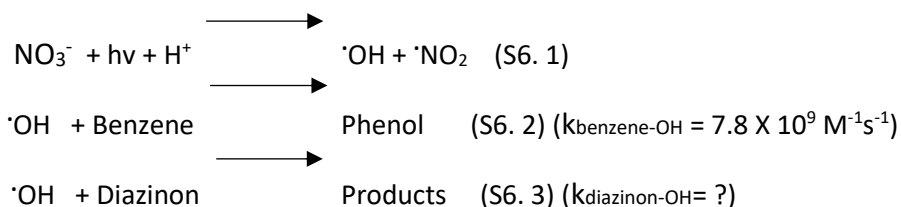
$$R_{1\text{O}_2} = \frac{R_{6\text{-HP}}}{Y_{6\text{-HP}} \times F} \quad (\text{X4})$$

Assuming R^1O_2 and $Y_{6\text{-HP}}$ are constant in both experiments with and without azide, $\text{R}_{6\text{-HP}}$ will be dependent on F and is expected to follow a manner dependent on % reduction in F (43 %). The $\text{R}_{6\text{-HP}}$ in the absence of azide was $0.029 \mu\text{M}/\text{min}$, while it was $0.014 \mu\text{M}/\text{min}$ in the presence of azide. This represents a 48% reduction in agreement with kinetic estimations based on the % reduction in F. This also shows that formation of 6-HP-one arose from the reaction between FFA and $^1\text{O}_2$.

S6. Reaction rate constants of diazinon with ROS ($^1\text{O}_2$ and $\cdot\text{OH}$)

• Reaction rate constant of diazinon with $\cdot\text{OH}$

The reaction rate constant of diazinon with $\cdot\text{OH}$ was investigated by the competition kinetics method using benzene as a reference compound and 1 mM NO_3^- as the photochemical source of $\cdot\text{OH}$ generation in MQ.¹⁴ Benzene reacts with $\cdot\text{OH}$ to form phenol, which has a known reaction rate constant of $7.8 \times 10^9 \text{ M}^{-1} \text{ s}^{-1}$.¹²



When a solution containing NO_3^- and benzene in MQ is irradiated in the absence of diazinon, all of the generated $\cdot\text{OH}$ reacts with benzene (S6.2) to give phenol product. However, in the presence of diazinon, the generated $\cdot\text{OH}$ reacts with both benzene and diazinon. In this case, the observed phenol product is expected to be lower. This reduction is because of competition of the reaction of diazinon with the generated $\cdot\text{OH}$.

The relationship between phenol produced in the absence and presence of diazinon can be expressed according to equation S6.4 below:

$$\frac{R_{\text{phenol}}}{R'_{\text{phenol}}} = 1 + \frac{k_{\text{diazinon-OH}}[\text{diazinon}]}{k_{\text{benzene-OH}}[\text{benzene}]} \quad (\text{S6.4})$$

where R_{phenol} and R'_{phenol} are the phenol signals in the absence and presence of diazinon, respectively, and $k_{\text{benzene-OH}}$ and $k_{\text{diazinon-OH}}$ are the reaction rate constants of benzene with $\cdot\text{OH}$ and diazinon with $\cdot\text{OH}$, respectively.

Based on equation S6.4, a plot of $R_{\text{phenol}}/R'_{\text{phenol}}$ against $[\text{diazinon}]/[\text{benzene}]$ should give a straight line with an intercept of 1 and a slope = $k_{\text{diazinon-OH}}/k_{\text{benzene-OH}}$. Experimentally, the rate of phenol production in the absence of diazinon and its rate in the presence of varying concentrations of diazinon was obtained and plotted against the $[\text{diazinon}]/[\text{benzene}]$ ratio.

Procedure

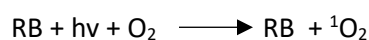
A stock solution of 30 mg/L (98.6 μM) diazinon was prepared by dissolving in MQ. The solubility limit of diazinon in water according to the literature is 40 mg/L. A solution containing 200 μM benzene and 1 mM NO_3^- (as the photochemical source of $\cdot\text{OH}$ generation) was irradiated in the absence of diazinon for 20 min. The phenol signal obtained was taken as R_{phenol} . Subsequently, a

solution containing the same concentration of benzene and NO_3^- was irradiated in the presence of varying concentrations of diazinon (5, 10, 30 and 50 μM). The phenol signal here was taken as R'_{phenol} . The concentrations of benzene and diazinon were selected such that the $[\text{diazinon}]/[\text{benzene}]$ ratio was ≤ 1 . The phenol produced from the irradiated solutions was determined by HPLC. A plot of $R_{\text{phenol}}/R'_{\text{phenol}}$ against $[\text{diazinon}]/[\text{benzene}]$ is shown in Fig. S6.

The HPLC system used in the determination of phenol consisted of a pump (LC-10Ai, Shimadzu, Kyoto, Japan) that delivered eluent (acetonitrile:MQ (60:40)) at a flow rate of 1 mL/min. An injection valve equipped with a 50 μL sample loop was used to inject samples into the system. Phenol was separated on a C_{18} column (Cosmosil, MS-II, 250 mm x 4.6 mm, 5 μm) and detected using a fluorescence detector (RF-10AXL, Shimadzu, Kyoto, Japan) set at excitation/emission wavelengths of 270/298 nm.

• Reaction rate constant of diazinon with $^1\text{O}_2$

The reaction rate constant of $^1\text{O}_2$ with diazinon was determined by monitoring the degradation rate of diazinon as it reacted with excessively high $[^1\text{O}_2]$ generated using Rose Bengal as a sensitizer.^{15,16}



$$\text{Rate of diazinon degradation } (R_{\text{deg}}) = k_{\text{diazinon}-^1\text{O}_2} [\text{diazinon}] [^1\text{O}_2] \quad (\text{S6.5})$$

where $k_{\text{diazinon}-^1\text{O}_2}$ is the reaction rate constant of diazinon with $^1\text{O}_2$. At constant $[^1\text{O}_2]$, R_{deg} was directly proportional to the $[\text{diazinon}]$. Therefore, as $[\text{diazinon}]$ increases, R_{deg} was expected to increase.

Moreover, when diazinon reacted with $^1\text{O}_2$, R_{deg} could be expressed as the product of rate of $^1\text{O}_2$ generation ($R^1\text{O}_2$) and fraction (F) of $^1\text{O}_2$ that reacts with diazinon as shown in equation S6.6 below.

$$R_{\text{deg}} = R^1\text{O}_2 \times \text{Fraction (F)} \quad (\text{S6.6})$$

$$F = \frac{k_{\text{diazinon-}^1\text{O}_2} [\text{diazinon}]}{k_d + k_{\text{diazinon-}^1\text{O}_2} [\text{diazinon}]} \quad (\text{S6.7})$$

where k_d is the dissociation rate constant of $^1\text{O}_2$ in water = $2.5 \times 10^5 \text{ s}^{-1}$.⁹

$$R_{\text{deg}} = R^1\text{O}_2 \times \frac{k_{\text{diazinon-}^1\text{O}_2} [\text{diazinon}]}{k_d + k_{\text{diazinon-}^1\text{O}_2} [\text{diazinon}]} \quad (\text{S6.8})$$

At low concentrations of diazinon (μM range), $k_{\text{diazinon-}^1\text{O}_2} [\text{diazinon}] \ll k_d$, giving rise to equation (S6.9):

$$R_{\text{deg}} = R^1\text{O}_2 k_d^{-1} k_{\text{diazinon-}^1\text{O}_2} [\text{diazinon}] \quad (\text{S6.9})$$

Therefore, from equation S6.9, obtaining a plot of R_{deg} against $[\text{diazinon}]$ at constant $^1\text{O}_2$ generation ($R^1\text{O}_2$) will give a slope = $R^1\text{O}_2 k_d^{-1} k_{\text{diazinon-}^1\text{O}_2}$. Since k_d is known, $R^1\text{O}_2$ can be obtained using FFA under the same experimental conditions. A plot of R_{deg} against $[\text{diazinon}]$ where the slope = $R^1\text{O}_2 k_d^{-1} k_{\text{diazinon-}^1\text{O}_2}$ is shown in Fig. S7.

$R^1\text{O}_2$ was determined from the initial degradation rate of FFA (R_{FFA}) by equation S6.10:

$$R_{\text{FFA}} = R^1\text{O}_2 \times \frac{k_{\text{FFA-}^1\text{O}_2} [\text{FFA}]}{k_d + k_{\text{FFA-}^1\text{O}_2} [\text{FFA}]} \quad (\text{S6.10})$$

where $k_{\text{FFA-}^1\text{O}_2}$ is the reaction rate constant between FFA and $^1\text{O}_2$ given as $1.09 \times 10^8 \text{ M}^{-1} \text{ s}^{-1}$.⁷

Procedure

Mixtures of 10 μM Rose Bengal (as a $^1\text{O}_2$ photosensitizer) and varying concentrations of diazinon (5, 10, 25 and 50 μM) were irradiated for about 4–6 hours using the solar simulator described above. At intervals, aliquots of reaction mixture were obtained and analyzed for diazinon on HPLC to monitor diazinon degradation. The HPLC system used consists of a pump (Prominence LC-20AD, Shimadzu, Kyoto) that delivered eluent (ACN:MQ (80:20)) at a flow rate of 1 mL/min, as well as an injection valve equipped with a 100 μL sample loop for sample injection. Diazinon was separated on a C_{18} column (Cosmosil, MS-II, 250 mm x 4.6 mm, 5 μm) and detected on a UV-Visible detector (Prominence LC-20AD, Shimadzu, Kyoto, Japan) at 247 nm.

Subsequently, the rate of $^1\text{O}_2$ generation (R^1O_2) from the irradiation of 10 μM RB as photosensitizer was determined using FFA (100 μM) as a probe. The degradation of FFA because of reaction with $^1\text{O}_2$ was monitored using HPLC. The HPLC system has been described earlier in S3A.

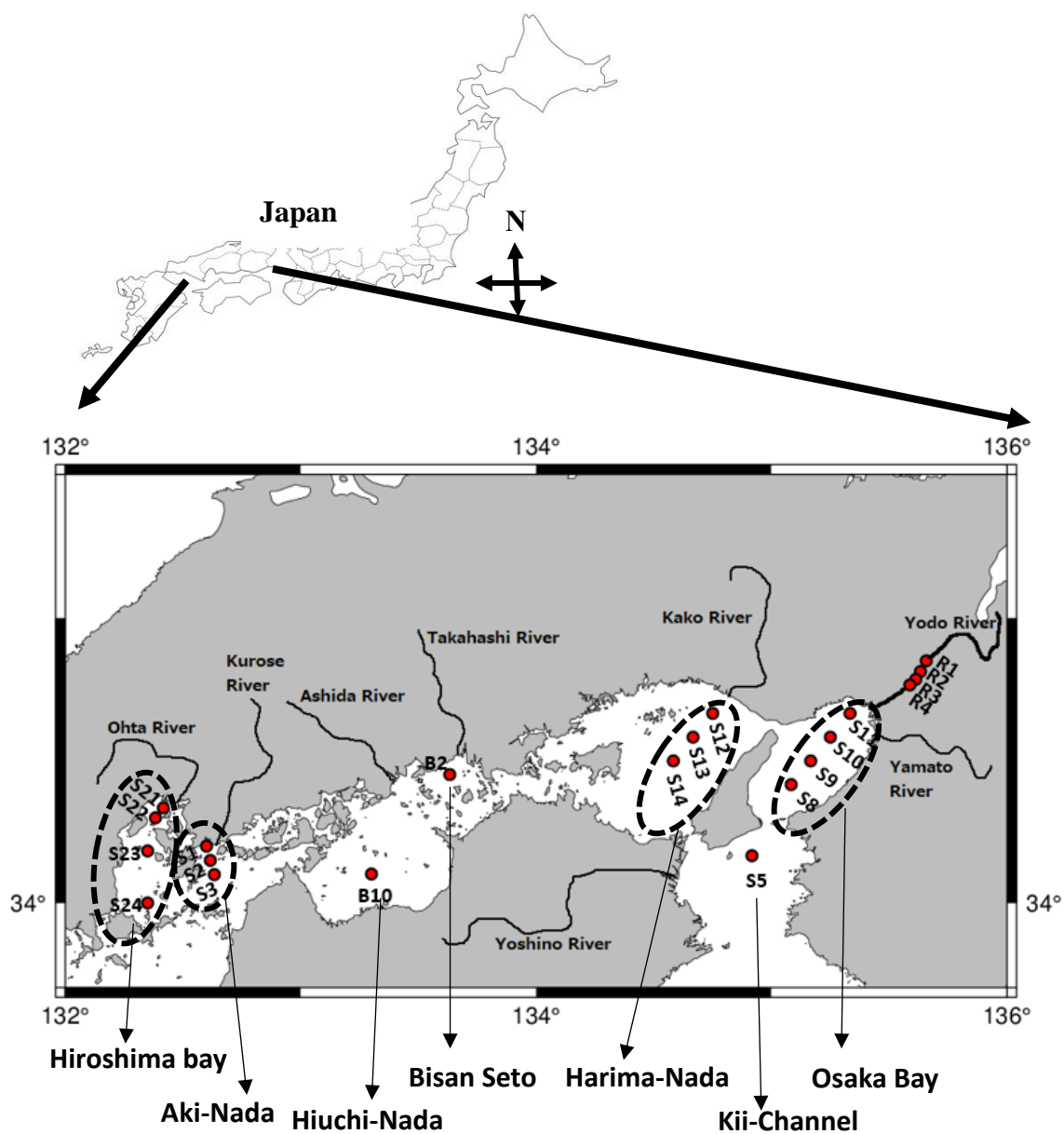
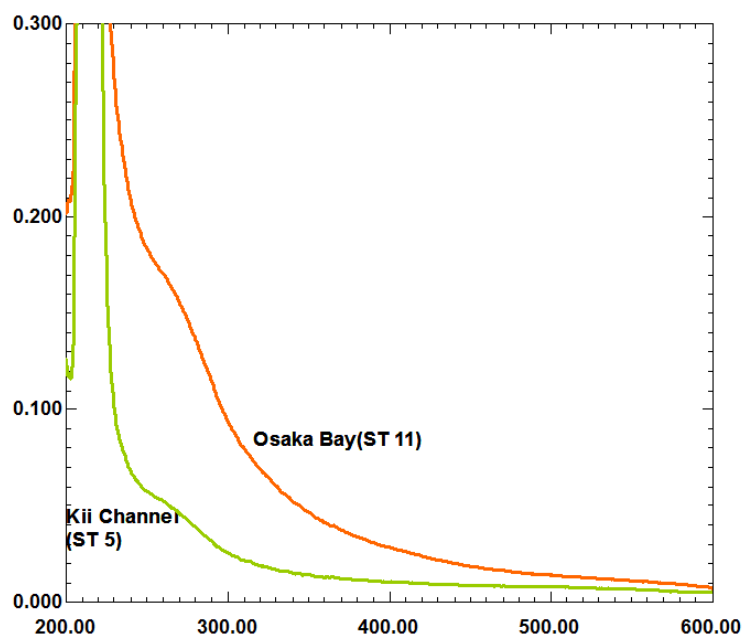


Figure S1: Map showing sampling stations in Seto Inland Sea and Yodo river.

289 CDOM absorption



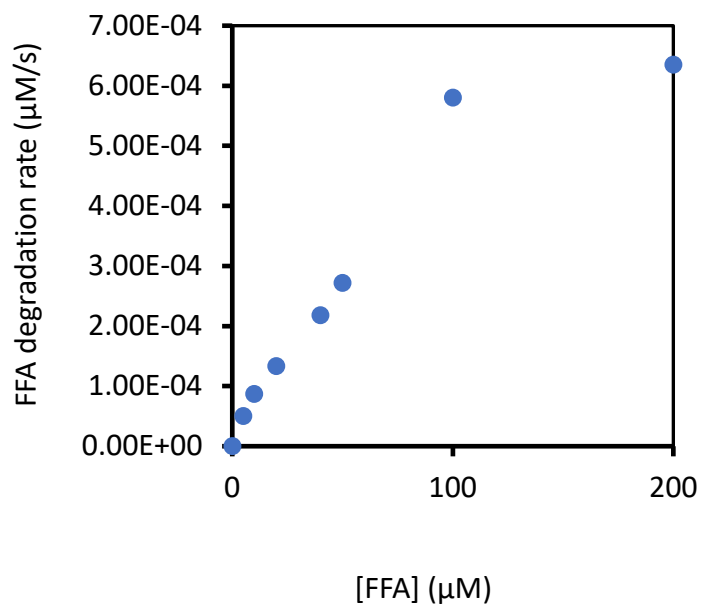
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291 Figure S2: Absorption spectra of Kii Channel and Osaka Bay seawater sample.

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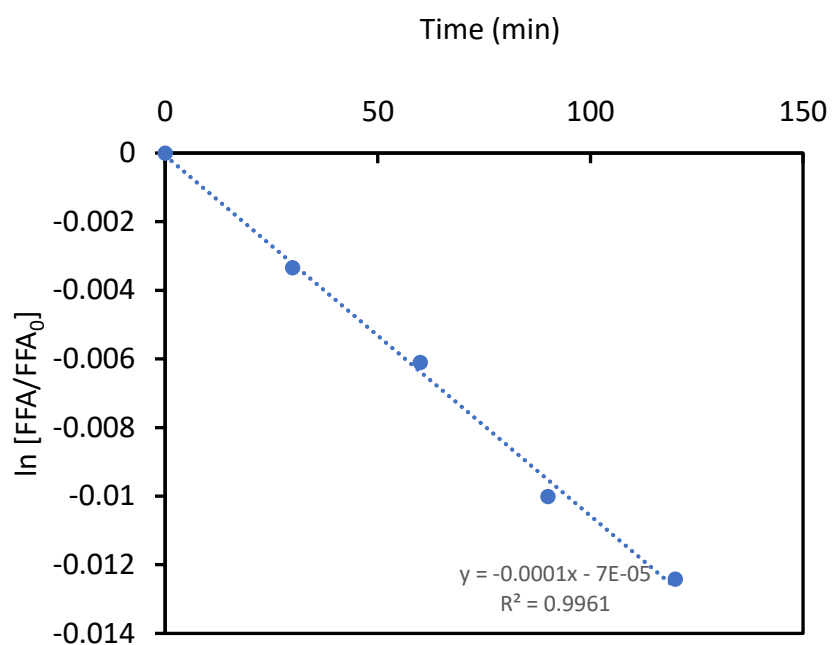
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296 Figure S3: Plot of FFA degradation rate at varying [FFA] upon irradiation in seawater.

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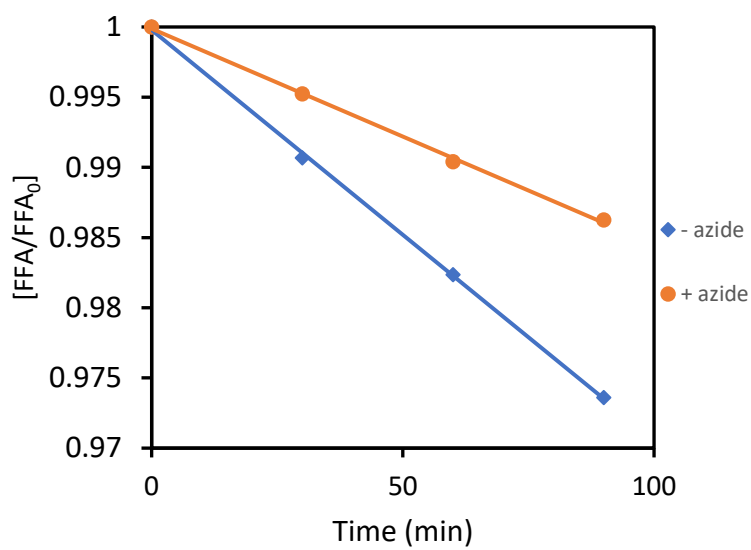


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301 Figure S4: A typical first order degradation plot of FFA in an irradiated seawater sample

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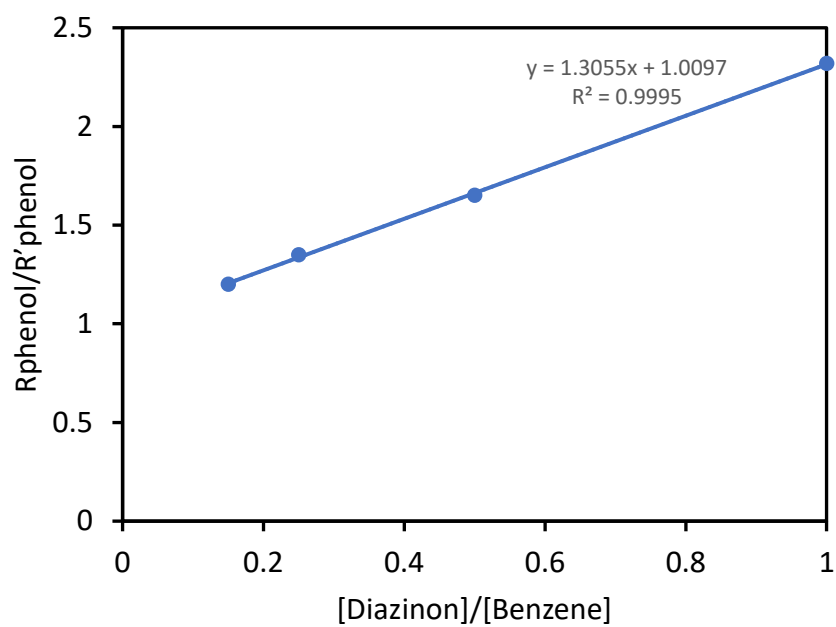


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305 Figure S5: Effect of NaN_3 on FFA degradation

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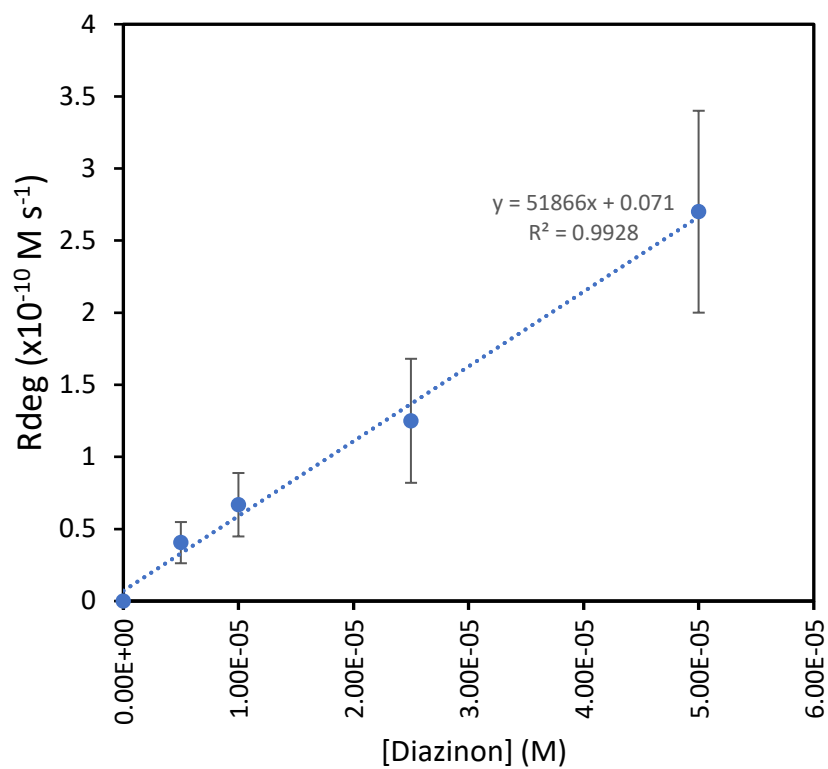
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309 Figure S6: Plot of Rphenol/R'phenol at varying ratios of [diazinon]/[benzene].

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314 Figure S7: Plot of degradation rate (R_{deg}) of diazinon at varying $[diazinon]$.

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Table S1: CDOM and spectra slopes reported in this and previous studies

Study Area	CDOM (m^{-1})	*Spectra slope ($S, \mu\text{m}^{-1}$)	Wavelength range of S	Method to Obtain S	Reference
Seto Inland Sea	a300 (0.6-3.8)	14.8-25	300-550	NLF	This study
Carribean Sea and	Sea: a300 (0.93-2.09).	I. 11-16	I. 400-500	LF	17
Orinoco River plume	River/River impacted: a300 (2.81-9.03)	II. 14-22 III. 13-20	II. 290-DL III. 290-DL		
Lake Superior	a300: Open lake (0.9-1.9) River-impacted (2-9.9) Riverine (10-150)	All samples: 16 - 26	300 – 600	NLF	1
Seto Inland Sea	a355 (0.14-1.57)			NLF + B	This study
South Pacific Ocean	a355 (0.117-0.326)	Avg. 17.3		Calculated	18
Gulf of Mexico: Open Ocean					
Spring	a355 (0.19)	15	290-DL	LF	19
Fall	(0.17)	24	290-DL		

Delaware Bay Mouth (August)	a355 (0.85)	Avg. 16	290-DL	LF	20
Tyrrhenian Sea				LF	
Coastal	a355 (0.57)	12.5	270 – DL		21
Offshore	(0.19)	25.6			
Seto Inland Sea	a375 (0.1-1.2)			NLF + B	This study
North Sea: Surface					2
Coastal	a375 (0.26-1.51)	Avg. 18.8	300 – 650	NLF + B	
Danish Fjords					
(Salinty 0-27)	a375 (0.75 – 4.5)	Avg. 19	300 - 650	NLF + B	2
Arabian Sea: Surface	a375 (0.022-0.288)	ND	ND		22

*Spectra slope comparison may be somewhat difficult because it depends on the wavelength range used, as well as the method used to obtain S-
either LF or NLF. LF: linear least square fit, NLF: non-linear least square fit

Table S2: CDOM absorption coefficient, spectra slope and DOC at surface(S), middle(M) and bottom (B) depth at the various sampling stations during the July, 2017 sampling exercise

Parameter	Depth	Aki-Nada			Kii Channel S5	Osaka Bay				Harima-Nada			Hiuchi- Nada B10	Bisan- Seto B2
		S1	S2	S3		S8	S9	S10	S11	S12	S13	S14		
a₃₀₀ (m⁻¹)	S	1.06	0.88	0.78	0.64	0.92	1.2	2.21	3.82	2.0	1.2	1.01	0.92	1.61
	M	0.92	0.74	0.64	0.64	0.92	0.92	1.34	1.61	1.57	1.06	0.98	0.83	1.20
	B	0.78	0.69	0.55	0.28	0.74	0.92	1.11	1.29	1.15	1.06	1.01	1.01	1.52
DOC (mg C/L)	S	0.74	0.65	0.64	0.80	0.8	0.96	1.23	1.85	1.25	1.63	1.28	1.42	1.8
	M	0.74	0.56	0.46	0.68	1.21	0.9	0.97	1.17	1.17	1.30	1.48	nd	nd
	B	0.67	0.6	0.46	0.58	0.76	0.86	0.87	1.00	1.21	1.28	nd	nd	nd
S₃₀₀₋₅₀₀ (μm⁻¹)	S	14.7	14.5	16.4	21.7	15.8	16.8	16	13.4	18.8	23.7	25.2	24.3	18.1
	M	18.2	20.3	16.2	14.3	14.4	16.6	15.4	13.8	20.4	25.1	26.6	21.6	22.4
	B	20.8	20	17.5	14.4	14.7	17.6	16	15.6	24.5	26	26	20.7	21.3

*nd: not determined

Table S3: CDOM absorption parameter and experimentally-determined $[^1\text{O}_2]_{\text{ss}}$ for seawater samples (Hiroshima Bay, S21-S24) and Yodo River water sampled in August and November 2019 respectively.

Seawater (S21-24) & Yodo River (R1-4)	Depth	a_{300} (m^{-1})	Experimentally- determined $[^1\text{O}_2]_{\text{ss}}$ (10^{-14} M)
ST 21	S	1.93	4.01
	M	1.47	3.34
	B	1.34	2.86
ST 22	S	1.34	3.04
	M	1.34	3.42
	B	1.24	2.71
ST 23	S	1.11	2.5
	M	1.01	2.18
	B	1.06	2.65
ST 24	S	1.11	2.19
	M	1.11	2.31
	B	0.98	2.29
Yodo River	R 1	4.59	6.9
	R 2	4.81	7.2
	R3	5.07	7.59
	R 4	4.88	7.34

Table S4: Half-lives ($t_{1/2}$) of compounds in seawater mediated by $^1\text{O}_2$ and $\cdot\text{OH}$

Compound	$k_{\text{rxn}, ^1\text{O}_2}$ ($\text{M}^{-1} \text{s}^{-1}$)	$k_{\text{rxn}, \text{OH}}$ ($\text{M}^{-1} \text{s}^{-1}$)	* $t_{1/2, ^1\text{O}_2}$ (days)	$t_{1/2, \text{OH}}$ (days)	Reference for k values
Diazinon	$7.29 \pm 0.3 \times 10^4$	$1.01 \pm 0.18 \times 10^{10}$	3185	80.6	This study
Methyl mercury	1.90×10^6	1.90×10^9	122	428	24
TBBPA	3.90×10^8	4.80×10^9	0.63	186	23,25

* $t_{1/2, ^1\text{O}_2}$ and $t_{1/2, \text{OH}}$ are half-lives calculated based on the average $[^1\text{O}_2]_{\text{ss}}$ of $3.28 \times 10^{-14} \text{ M}$ and $[\cdot\text{OH}]_{\text{ss}}$ of $8.96 \times 10^{-18} \text{ M}$, respectively, obtained in this study.

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