

Supporting Information

**Selective C<sub>2+</sub> Alcohol Synthesis from Direct CO<sub>2</sub>  
Hydrogenation over a Cs-Promoted Cu-Fe-Zn  
Catalyst**

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## Experimental Section

**Catalyst preparation.** Mixed CuFeZn oxides were prepared by using a coprecipitation method. In detail, the CuFeZn precipitates were obtained by a precipitation of Cu, Zn and Fe nitrate solution ( $0.2 \text{ mol L}^{-1}$ ) using aqueous  $(\text{NH}_4)_2\text{CO}_3$  ( $0.24 \text{ mol L}^{-1}$ ) as the precipitating agent with a single-drop method at  $70 \text{ }^\circ\text{C}$  and  $\text{pH} = 9$  under stirring. The molar ratio of Cu:Fe:Zn was set at  $x:y:1$ . The products were collected by centrifugation and washed with deionized water for several times, followed by drying at  $80 \text{ }^\circ\text{C}$  for 12 h. After calcination at  $400 \text{ }^\circ\text{C}$  for 2 h, the CuFeZn ternary metal oxides were obtained. Cs modified CuFeZn catalysts were prepared by impregnating CuFeZn oxides (1 g) in a  $\text{Cs}_2\text{CO}_3$  aqueous solution, followed by drying at  $110 \text{ }^\circ\text{C}$  and calcination at  $400 \text{ }^\circ\text{C}$  for 2 h. The final catalysts are denoted as  $x\%\text{Cs-C}_y\text{F}_z\text{Z}_{1.0}$ , where  $x\%$  represents the weight percent of Cs and  $\text{C}_y\text{F}_z\text{Z}_{1.0}$  represents Cu, Fe and Zn with a molar ratio of  $y:z:1.0$ . And the weight percent of Cs is fixed at 3% if it is not marked.

**Catalyst characterization.** All samples were reduced under 10%  $\text{H}_2/\text{Ar}$  flow at  $350 \text{ }^\circ\text{C}$  prior to characterization. After cooling down to room temperature, the samples were transferred into a sample vial of liquid chromatography and we then replaced the air in the bottle with  $\text{N}_2$ . The bottle was then put into a Teflon flask containing Fe powder at the bottom and then vacuumed and filled with  $\text{N}_2$  to purge  $\text{O}_2$  in the flask.

Transmission Electron Microscopy (TEM) images were acquired on a JEM-2100F (JEOL) at 200 kV. After taken out from sample vial filled with protective  $\text{N}_2$ , the sample was dispersed in ethanol and then deposited on a carbon film. The TEM imaging was

immediately performed after ethanol volatilization. The lattice d-spacing was measured with Digital Micrograph software as follows: we first drew a line vertical to lattice fringes, and then we generally counted 10-20 units of fringes to calculate the d-spacing value. N<sub>2</sub> sorption was used to analyze Brunauer-Emmett-Teller (BET) surface area and pore volume on an ASAP 2020 (Micromeritics). Powder X-ray diffraction (PXRD) was performed on a Bruker D8 Advances with Cu K $\alpha$  radiation. The samples were scanned from 20° to 60° with a step angle of 0.02°. The crystallite size was calculated with Scherrer formula. Elemental analysis was detected by ICP-AES with a ContrAA 700 spectrometer (Analytikjena).

H<sub>2</sub> temperature-programmed reduction (TPR) experiments were performed on Micromeritics Autochem 2920. The experimental procedure is described as follows: 50 mg sample was loaded on the layer of quartz wool in a U-shaped quartz tube and then heated to 150 °C with a rate of 4 °C min<sup>-1</sup> in an Ar flow (30 mL min<sup>-1</sup>) for 0.5 hour to clean the sample. The experiment was carried out in a 5% H<sub>2</sub>/Ar flow of 30 mL min<sup>-1</sup> with heating to 600 °C at a heating rate of 10 °C min<sup>-1</sup>. The signal was recorded by a TCD detector.

H<sub>2</sub> temperature-programmed desorption (TPD) experiments were performed as follows: 100 mg sample was reduced under 5% H<sub>2</sub>/Ar flow (30 mL/min) at 350 °C for 1 h and cooled down to 50 °C. Then, the gas was switched to Ar at a flow rate of 50 mL/min to purge the residual H<sub>2</sub> for 20 min. After that, the TPD measurements were conducted from 50 °C to 600 °C with a TCD detector.

CO<sub>2</sub> temperature-programmed desorption (TPD) experiments were carried out as follows: 100 mg sample was reduced under 5% H<sub>2</sub>/Ar flow (30 mL/min) at 350 °C for 1 h. Then, the gas was switched to Ar at a flow rate of 30 mL/min to purge the residual H<sub>2</sub> and cooled down to 50 °C. After a pre-adsorption of CO<sub>2</sub> in 30 mL min<sup>-1</sup> flow at 50 °C, the gas was switched to Ar at a flow rate of 50 mL min<sup>-1</sup> to purge the residual CO<sub>2</sub>. The TPD measurements were conducted by using He as carrier from 50 °C to 600 °C with a quadrupole mass spectrometer (Hidden, QIC-20) detector.

Temperature-programmed surface reaction (TPSR) experiments were performed as follows: 50 mg sample was reduced in a 5% H<sub>2</sub>/Ar atmosphere at 350 °C for 1 hour and cooled down to 50 °C in 30 mL min<sup>-1</sup> of Ar. After a pre-adsorption of CO in 30 mL min<sup>-1</sup> flow at 50 °C, the gas was switched to Ar at a flow rate of 50 mL min<sup>-1</sup> to purge the residual CO. The TPSR experiments were begun by using 5% H<sub>2</sub>/Ar as carrier from 50 °C to 700 °C (10 °C min<sup>-1</sup>) with a quadrupole mass spectrometer (Hidden, QIC-20) detector. The m/q of desorption species are listed as follows: H<sub>2</sub> (2), H<sub>2</sub>O (18), CO<sub>2</sub> (44), CH<sub>4</sub> (16) and CO (28).

In situ diffuse reflectance Fourier transform infrared spectroscopy (DRIFTS) measurements were accomplished in an in situ reaction cell on a Bruker VERTEX 70 spectrometer with a MCT detector. The DRIFTS tests were carried out at 100 °C and 200 °C in a H<sub>2</sub>/CO<sub>2</sub> (3:1) flow of 30 mL min<sup>-1</sup> at a total pressure of 0.3 MPa. The sample was reduced at 350 °C in a 10% H<sub>2</sub>/Ar flow of 30 mL min<sup>-1</sup> for 1 h, and then purged with Ar at the same temperature for 1 h before test. The spectra were collected by 32

scans at a resolution of  $4\text{ cm}^{-1}$ . Each spectrum was referenced to the spectrum collected at the same temperature in Ar flow. The background spectra were obtained after cooling down to the desired temperature.

**Catalytic testing.** The HAS from  $\text{CO}_2$  hydrogenation was evaluated on a customized fixed-bed reactor (internal diameter of 10 mm). 0.2 g catalyst was diluted with 0.4 g quartz sand and then loaded into a stainless steel tube. Before measurement, the catalyst was reduced at  $350\text{ }^\circ\text{C}$  for 1 h in a 10%  $\text{H}_2/\text{Ar}$  flow of  $30\text{ mL min}^{-1}$ . After cooling down to room temperature, the feeding gas with a  $\text{H}_2/\text{CO}_2/\text{N}_2$  ( $\text{N}_2$  as internal standard) ratio of 72/24/4 was introduced into the reactor and then pressurized to 5 MPa. Then the gas flow was set as  $15\text{ mL min}^{-1}$  and the reaction temperature was raised up to the desired temperature with a heating rate of  $5\text{ }^\circ\text{C min}^{-1}$ . The post-reactor line and valves were maintained at  $150\text{ }^\circ\text{C}$  to avoid product condensation. The products were analyzed online by a gas chromatograph equipped with thermal conductivity detector (TCD) and flame ionization detector (FID).  $\text{CO}_2$  conversion was calculated using an internal standard method and product selectivity was calculated on a molar carbon basis. All data were obtained after the reaction lasts for 3 h at each temperature for the equilibrium of tail gas composition. Then the reaction temperature was continuously increased to higher temperatures to obtain other catalytic data with using the same catalysts. For the time on stream test, the reaction was kept at  $310\text{ }^\circ\text{C}$ . As for the referenced Cs-CxFyZ1 sample reduced by syngas, the pre-reduction treatment was performed at  $350\text{ }^\circ\text{C}$  for 5 h in 10%  $\text{H}_2/\text{Ar}$  flow of  $15\text{ mL min}^{-1}$  and 5%  $\text{CO}/\text{Ar}$  flow of  $15\text{ mL min}^{-1}$ .

The methanol steam reforming experiment was performed on another fixed-bed reactor (internal diameter of 8 mm) equipped with a high-pressure constant current pump. 0.1 g catalyst diluted with 0.4 g quartz sand was loaded into the stainless steel tube. Before measurements, the catalyst was reduced at 350 °C for 1 h in a 10% H<sub>2</sub>/Ar flow (30 mL min<sup>-1</sup>). During the test, an aqueous solution of methanol (H<sub>2</sub>O:CH<sub>3</sub>OH = 2:1) at a rate of 0.1 mL min<sup>-1</sup> was fed into a vaporizer. H<sub>2</sub> (20 mL min<sup>-1</sup>) was also introduced into the vaporizer to carry the feed vapor into the reactor at atmospheric pressure. The products were analyzed online by a gas chromatograph equipped with a TCD detector.

## Discussion on the particle size of active components

CuO and ZnO are the primary components for the fresh Cs-C<sub>y</sub>F<sub>z</sub>Z<sub>1.0</sub> catalysts (Fig. 1a). The absence of Fe<sub>2</sub>O<sub>3</sub> suggests that Fe species is highly dispersed. After H<sub>2</sub> reduction treatment, Cu and Fe<sub>3</sub>O<sub>4</sub> appear (Fig. 1b). The peak intensity trends of Cu and Fe species are consistent with their relative contents. The particle sizes of Cu and Fe<sub>3</sub>O<sub>4</sub> were obtained by XRD (see Table 1). However, the Cu particle sizes over Cs-C<sub>0.2</sub>F<sub>1.0</sub>Z<sub>1.0</sub> and Cs-C<sub>0.2</sub>F<sub>1.0</sub>Z<sub>1.0</sub> are lacking because the content of Cu is low and the diffraction peak of Cu (111) is covered by Fe<sub>3</sub>O<sub>4</sub> (400). But we can speculate the Cu size follows an order Cs-C<sub>0.2</sub>F<sub>1.0</sub>Z<sub>1.0</sub> < Cs-C<sub>0.5</sub>F<sub>1.0</sub>Z<sub>1.0</sub> < Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> according to H<sub>2</sub>-TPR results (Fig. S1).

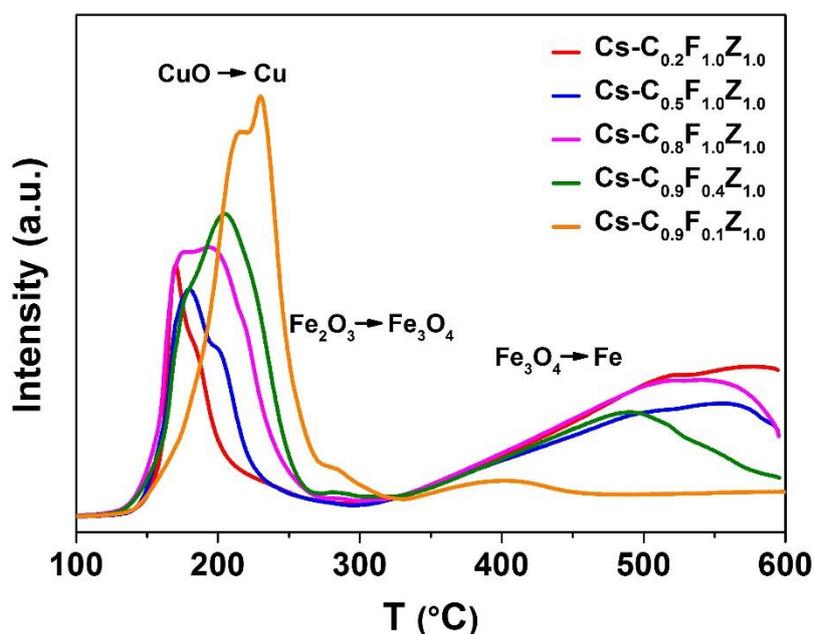
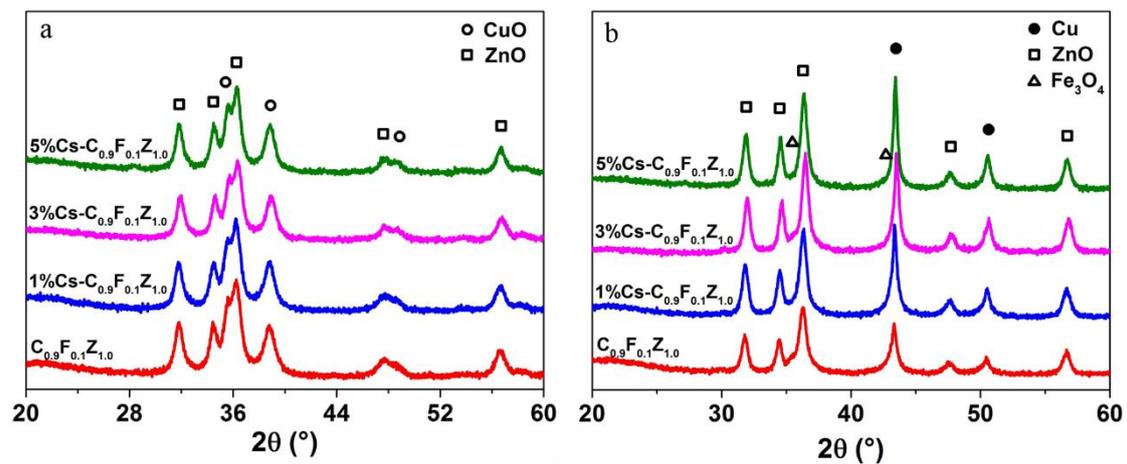
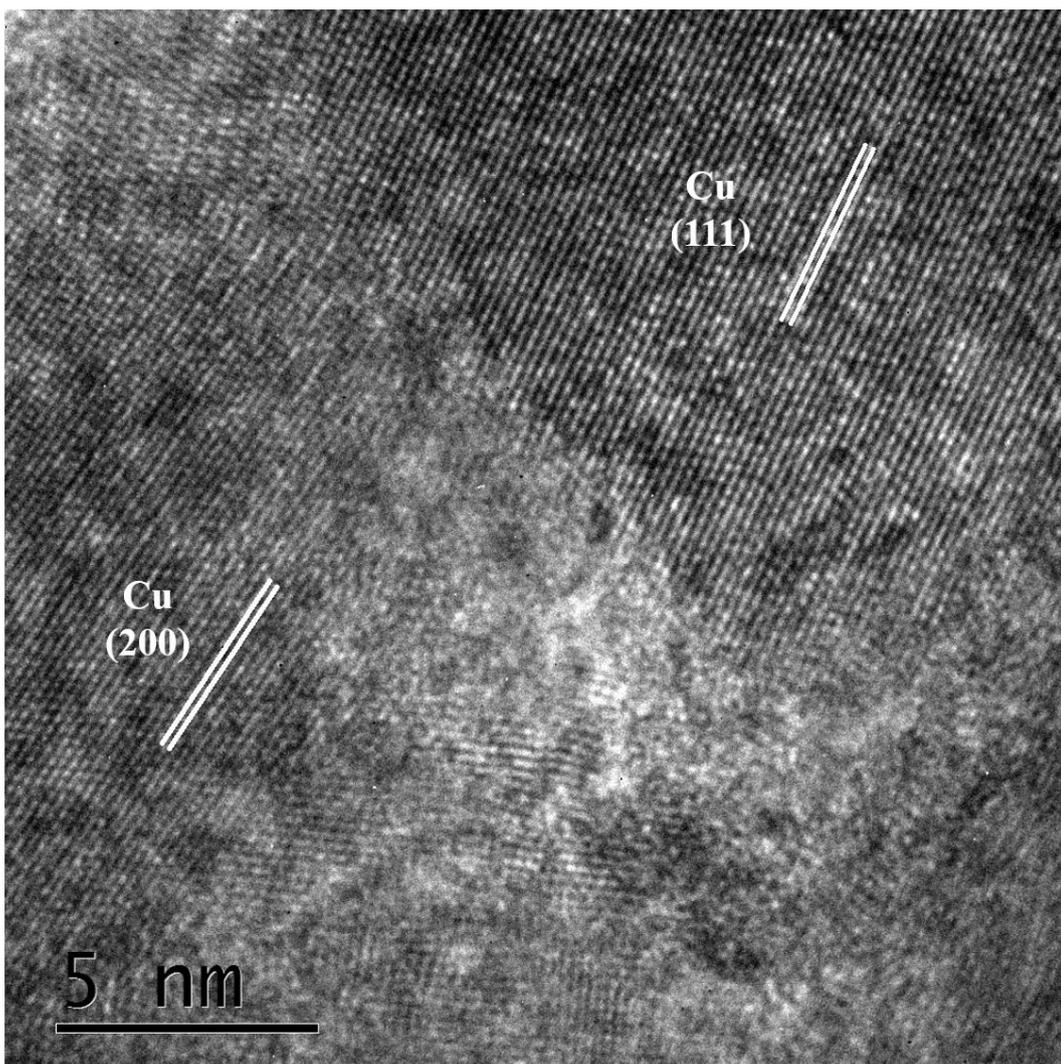


Fig. S1. H<sub>2</sub>-TPR results of fresh Cs-C<sub>y</sub>F<sub>z</sub>Z<sub>1.0</sub> catalysts.

The reduction peak in the temperature range of 150-300 °C is assigned to the reduction of CuO to metallic Cu along with Fe<sub>2</sub>O<sub>3</sub> to Fe<sub>3</sub>O<sub>4</sub>.<sup>1-4</sup> And the broad reduction peak at above 300 °C is ascribed to continuous reduction of Fe<sub>3</sub>O<sub>4</sub> to metallic Fe.<sup>1-4</sup> With the increase of Cu/Fe molar ratio, the reduction peak area of CuO goes up while that of Fe<sub>3</sub>O<sub>4</sub> decreases. Moreover, the reduction peak of CuO slightly shifts towards high temperature, verifying the increase in the particle size of CuO which is observed in the XRD patterns (Table 1).



**Fig. S2.** XRD patterns over (a) fresh and (b) reduced  $x\%Cs-C_{0.9}F_{0.1}Z_{1.0}$  catalysts. Cu PDF#85-1326, CuO PDF#45-0937, ZnO PDF#79-2205,  $Fe_3O_4$  PDF#75-1372.



**Fig. S3.** HRTEM image of reduced Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> catalyst.

**Table S1.** Particle sizes of Cu/CuO and ZnO in fresh and reduced x%Cs-C<sub>0.9</sub>F<sub>0.1</sub>Z<sub>1.0</sub> catalysts calculated by the Scherrer formula.

Catalyst	Fresh		Reduced	
	d <sub>CuO</sub> (nm)	d <sub>ZnO</sub> (nm)	d <sub>Cu</sub> (nm)	d <sub>ZnO</sub> (nm)
C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	8.7	12.3	22.6	18.1
1%Cs-C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	9.5	12.6	25.0	16.8
3%Cs-C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	10.2	13.7	28.9	18.5
5%Cs-C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	10.2	14.4	31.6	17.9

**Table S2.** The amount of H<sub>2</sub> desorption over x%Cs-C<sub>0.9</sub>F<sub>0.1</sub>Z<sub>1.0</sub> catalysts.

Sample	H <sub>2</sub> desorption (umol g <sup>-1</sup> )			Total H <sub>2</sub> desorption (umol g <sup>-1</sup> )
	$\alpha$	$\beta$	$\gamma$	
C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	25.3	101.5	60.4	187.2
1%Cs-C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	50.8	99.7	36.6	187.1
3%Cs-C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	60.6	84.1	43.1	187.8
5%Cs-C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	95.6	68.2	24.4	188.2

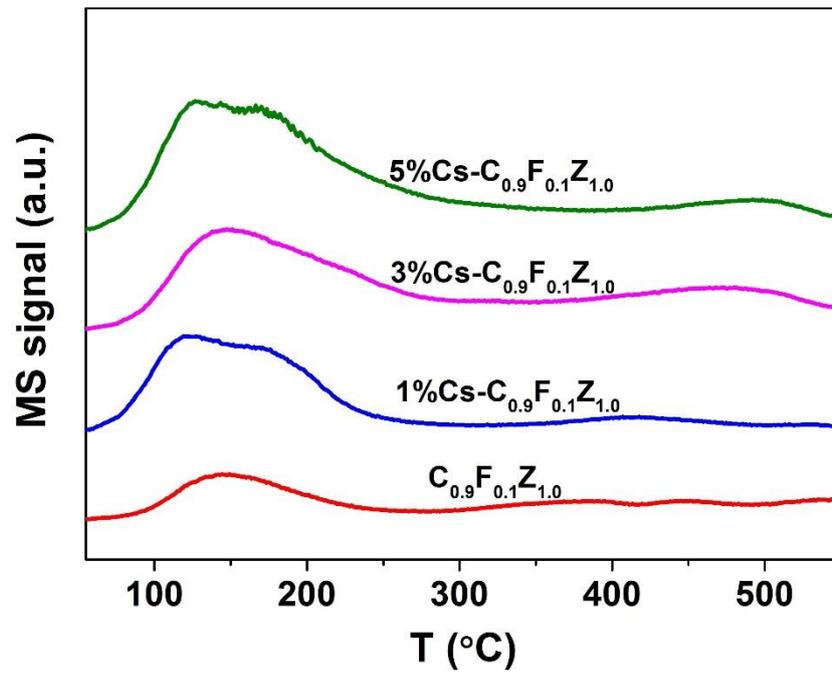
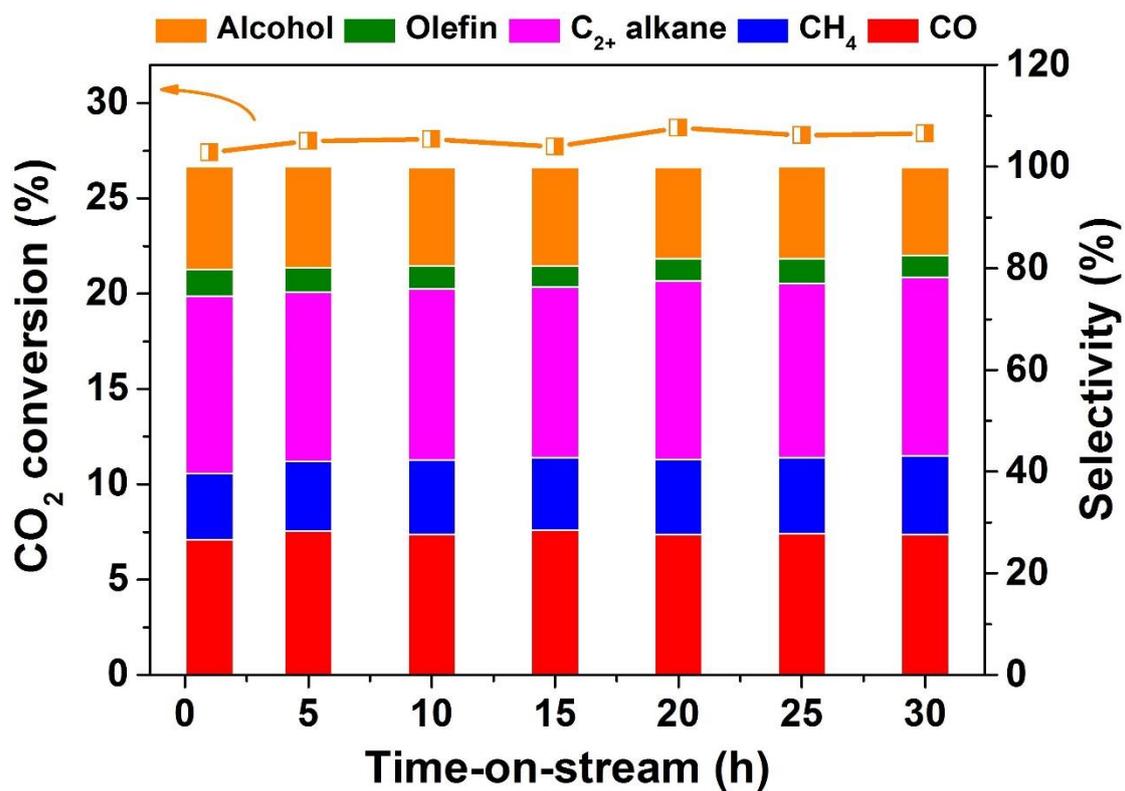


Fig. S4. CO<sub>2</sub>-TPD-MASS results over x%Cs-C<sub>0.9</sub>F<sub>0.1</sub>Z<sub>1.0</sub> catalysts.



**Fig. S5.** Time-on-stream test of the Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> catalyst in CO<sub>2</sub> hydrogenation. Reaction conditions: 200 mg catalyst diluted by 400 mg quartz sand; H<sub>2</sub>/CO<sub>2</sub> = 3:1; 5 MPa; 15 mL min<sup>-1</sup>; 310 °C.

**Table S3.** Comparison of HAS activity over Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> with some advanced catalysts in the literature in HAS from CO<sub>2</sub> hydrogenation.

Catalyst	Reactor	Reaction conditions	X <sub>CO<sub>2</sub></sub> <sup>a</sup> (%)	S <sub>HA</sub> <sup>b</sup> (%)	S <sub>VP</sub> <sup>c</sup> (%)	Y <sub>HA</sub> <sup>d</sup> (%)	STY <sub>HA</sub> (mmol g <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )	W <sub>HA</sub> <sup>e</sup> (%)	Ref.
Pt/Co <sub>3</sub> O <sub>4</sub>	Tank	20 mg, water/DMLI, 8 MPa, 200 °C	-	29.3	34.0	-	0.42	82.5	5
Pt/Co <sub>3</sub> O <sub>4</sub> -m	Fixed-bed	6000 h <sup>-1</sup> , 2 MPa, 200 °C	≈ 11	≈ 23	≈ 56	≈ 5.1	0.75	≈ 41.8	6
CoAlO <sub>x</sub>	Tank	20 mg, water, 4 MPa, 140/200 °C	-	92.1/88.9 (ethanol)	-	-	0.44/0.89 (ethanol)	-	7
CuZnFe <sub>0.5</sub> K <sub>0.15</sub>	Fixed-bed	5000 h <sup>-1</sup> , 6 MPa, 300 °C	42.3	31.9 (wt%)	-	13.5 (wt%)	0.17 (g mL <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )	87.1	1
RhFeLi-TiO <sub>2</sub>	Fixed-bed	6000 h <sup>-1</sup> , 3 MPa, 250 °C	15.7	31.3 (ethanol)	33.5	4.9 (ethanol)	1.32 (ethanol)	93.2 (ethanol)	8
Rh-0.3VO <sub>x</sub> /MCM-41	Fixed-bed	6000 h <sup>-1</sup> , 3 MPa, 250 °C	12.1	24.1 (ethanol)	41.9	2.9 (ethanol)	1.04 (ethanol)	49.4 (ethanol)	9
Cu/Co <sub>3</sub> O <sub>4</sub> -2h	Fixed-bed	36000 h <sup>-1</sup> , 3 MPa, 250 °C	13.9	15.2 (ethanol)	55.6	2.1	1.87 (ethanol)	-	10
Na-Co/SiO <sub>2</sub>	Fixed-bed	4000 h <sup>-1</sup> , 5 MPa, 250 °C	18.8	8.7	33.4	1.6	-	87.5	11
Cs-C <sub>0.8</sub> F <sub>1.0</sub> Z <sub>1.0</sub>	Fixed-bed	4500 h <sup>-1</sup> , 5 MPa, 330 °C	36.6	19.8	67.6	7.2	1.47 (ethanol 1.12)	93.8	This work

[a] CO<sub>2</sub> conversion.

[b] Alcohol selectivity.

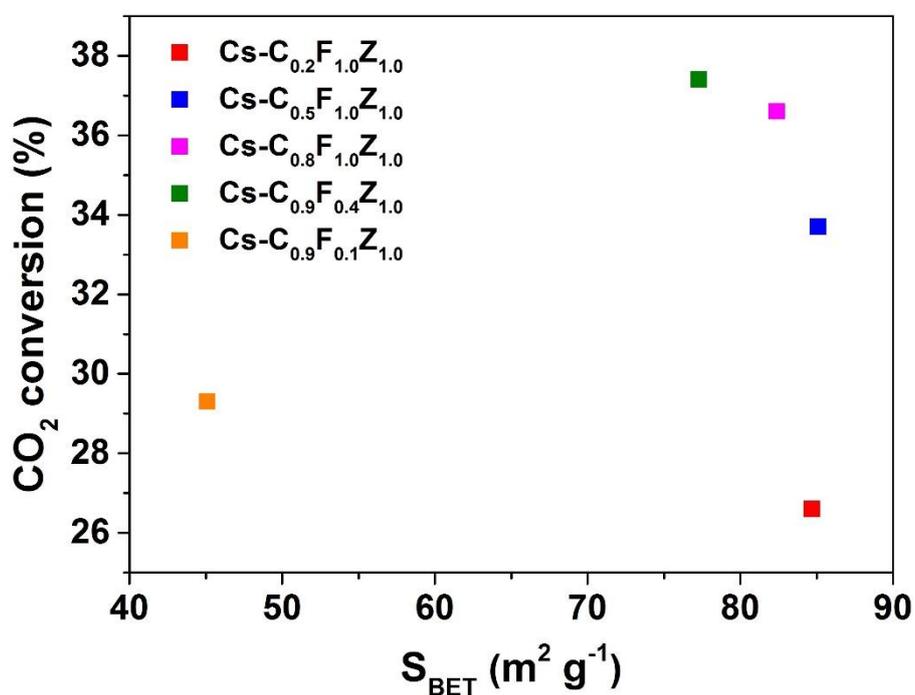
[c] Valuable products (e.g. alcohols and C<sub>2+</sub> hydrocarbons) selectivity.

[d] HA yield.

[e] Weight percent of HA in total alcohol.

### Discussion on the effect of BET surface area

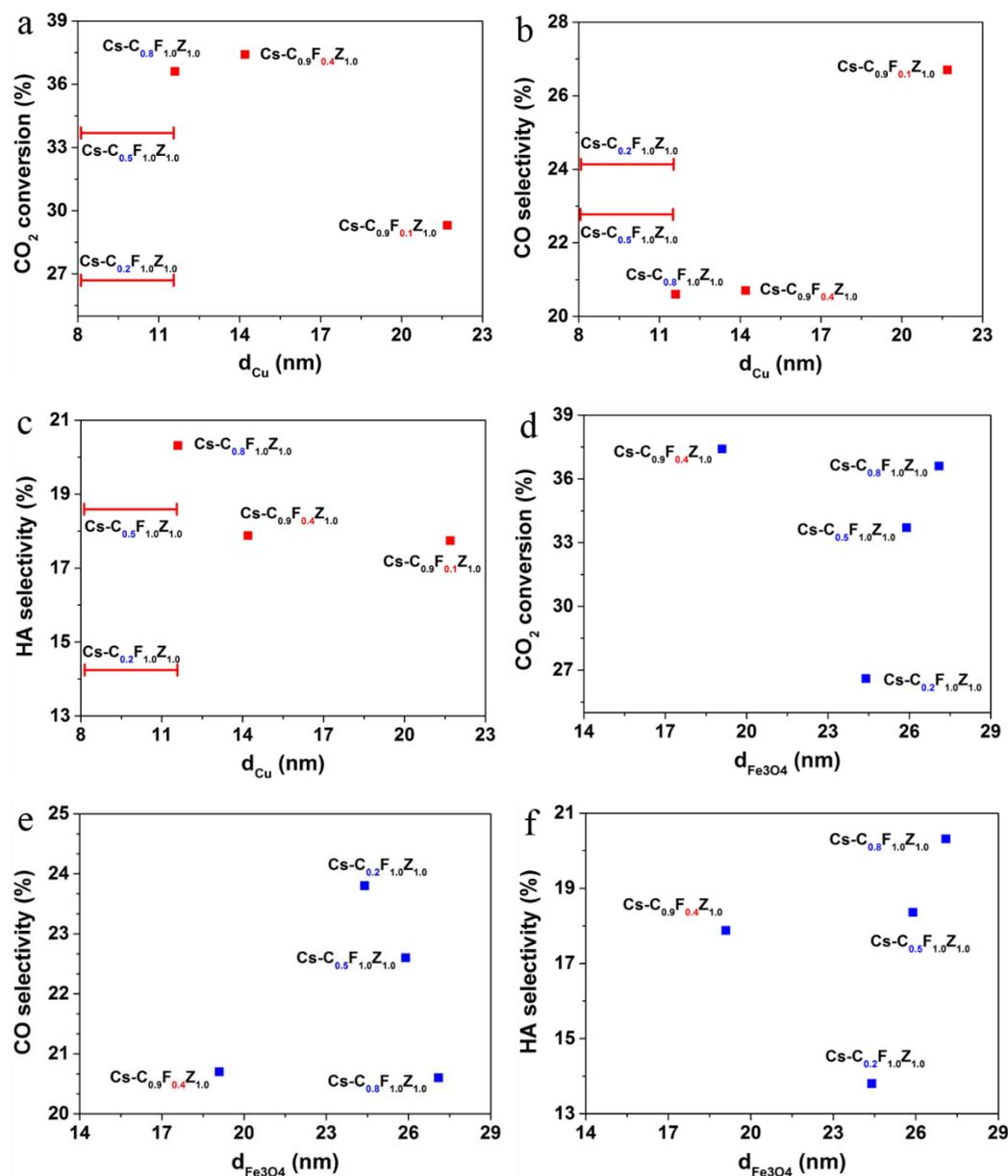
The surface area (SA) is an important factor for the activity of a catalyst. The physicochemical properties of our Cs-C<sub>y</sub>F<sub>z</sub>Z<sub>1.0</sub> catalysts are showed in Table 1. All catalysts have similar BET surface area and porosity. We then try to correlate catalytic activity with SA. From Fig. S6, there is no linear relevance between CO<sub>2</sub> conversion and BET SA. So, we can conclude that the CO<sub>2</sub> conversion is not directly determined by the surface area in our catalysis system.



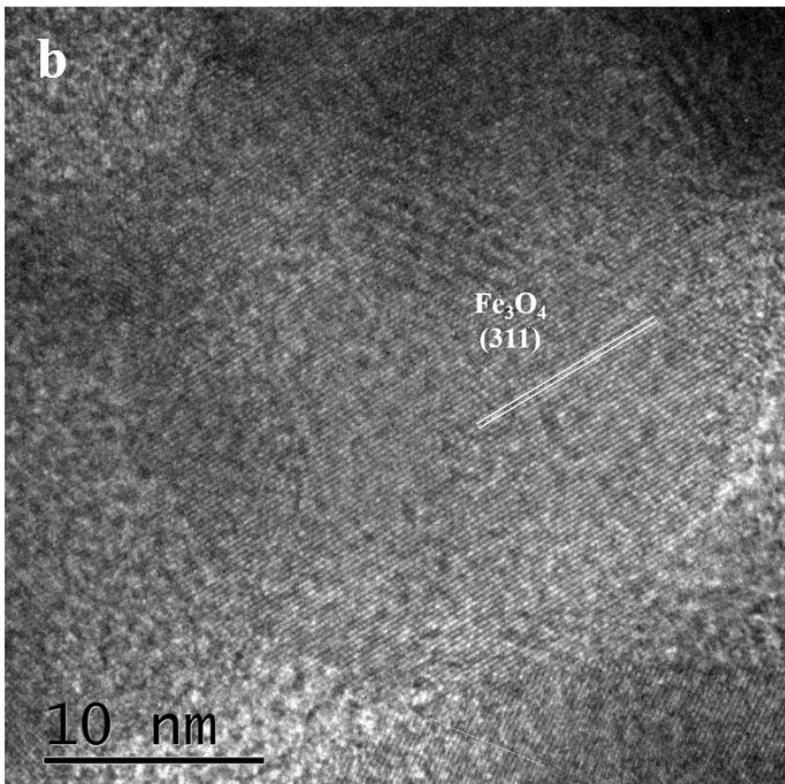
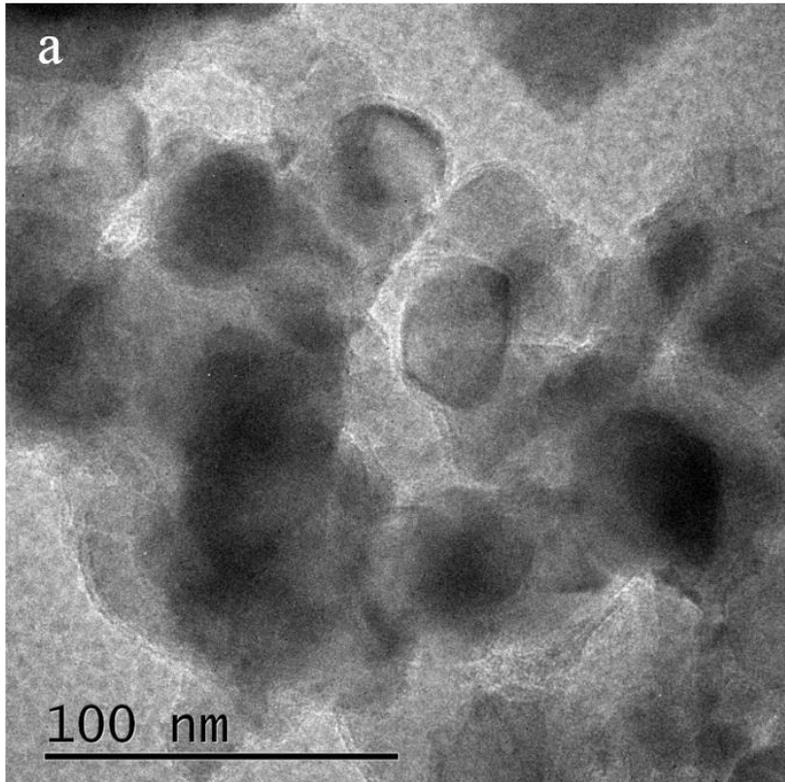
**Fig. S6.** CO<sub>2</sub> conversion at 330 °C as a function of BET surface area of Cs-C<sub>y</sub>F<sub>z</sub>Z<sub>1.0</sub> catalysts.

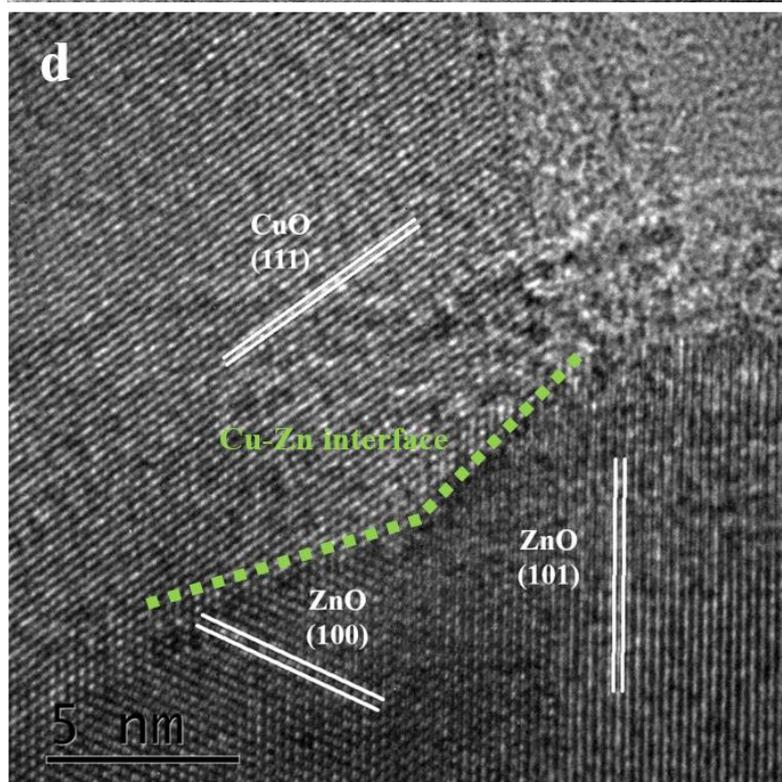
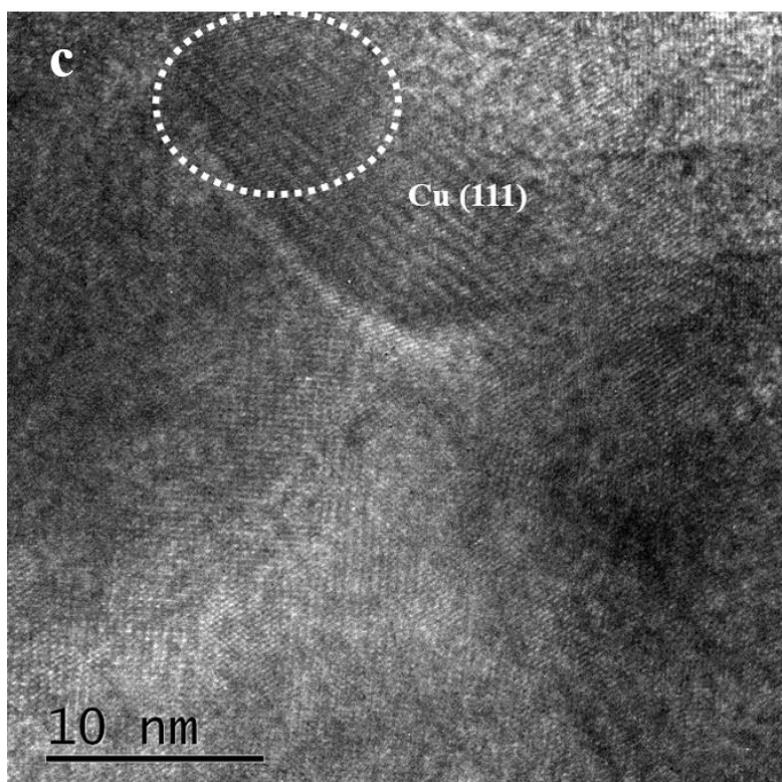
## Discussion on the effect of particle size

The particle sizes of active Cu and Fe species are also an important factor for catalytic performance. It is reported that high HA selectivity is obtainable if Cu is around 10 nm in size and Fe is moderately aggregate for CO hydrogenation over CuFe catalysts.<sup>12</sup> However, in this work, the trend of catalytic performance is not monotonous with particle size of individual species, which rules out the effect of particle size (Fig. S7).



**Fig. S7.** Correlations between catalytic performance (CO<sub>2</sub> conversion, CO and HA selectivity) at 330 °C and particle size of Cu (a, b and c) and Fe<sub>3</sub>O<sub>4</sub> (d, e and f).

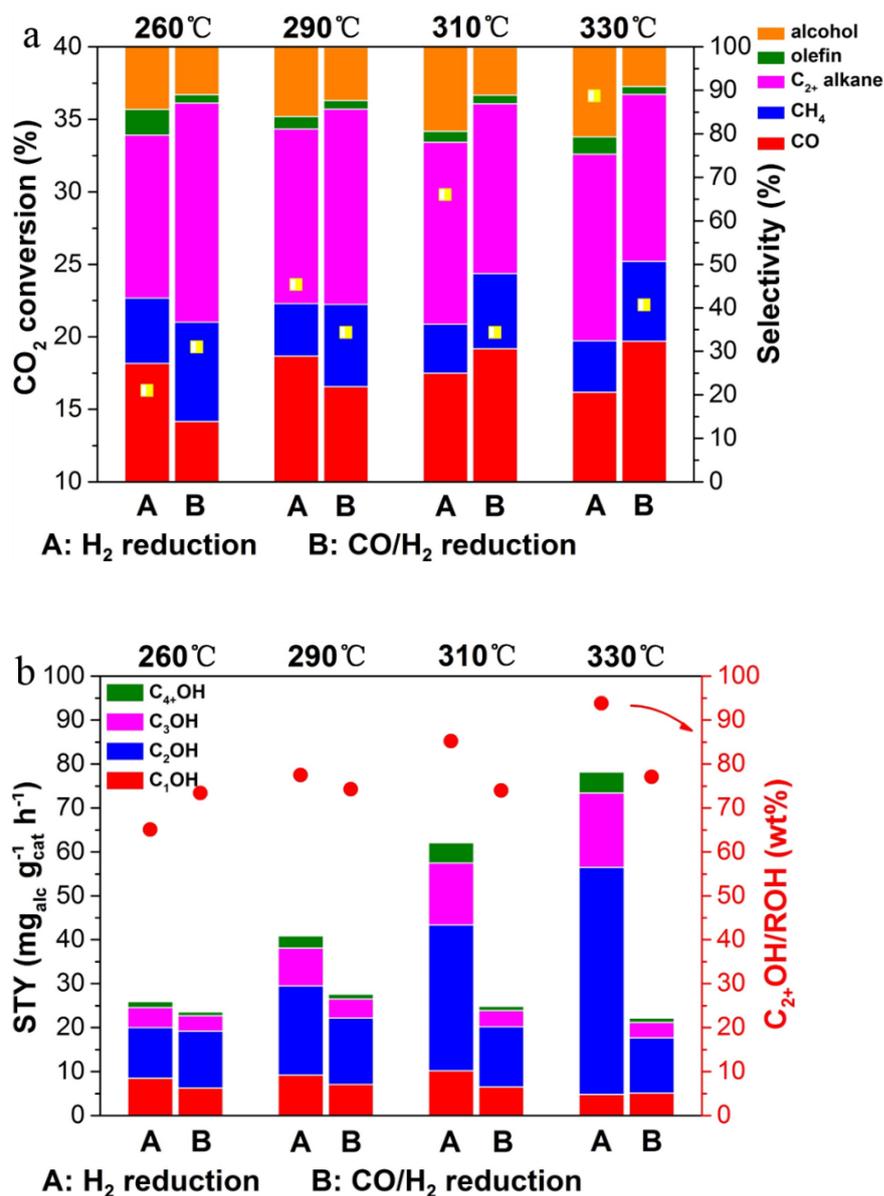




**Fig. S8.** TEM images of Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> catalyst after TOS test.

**Table S4.** Particle size of Cu, ZnO and Fe<sub>3</sub>O<sub>4</sub> in the Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> catalyst after different treatments calculated by the Scherrer formula.

Catalyst	d <sub>Cu</sub> (nm)	d <sub>ZnO</sub> (nm)	d <sub>Fe<sub>3</sub>O<sub>4</sub></sub> (nm)
Spent catalyst pre-reduced with H <sub>2</sub> /Ar	30.1	45.9	44.6
Spent catalyst pre-reduced with diluted syngas	31.2	39.4	75.4
After TOS	33.1	51.4	44.1

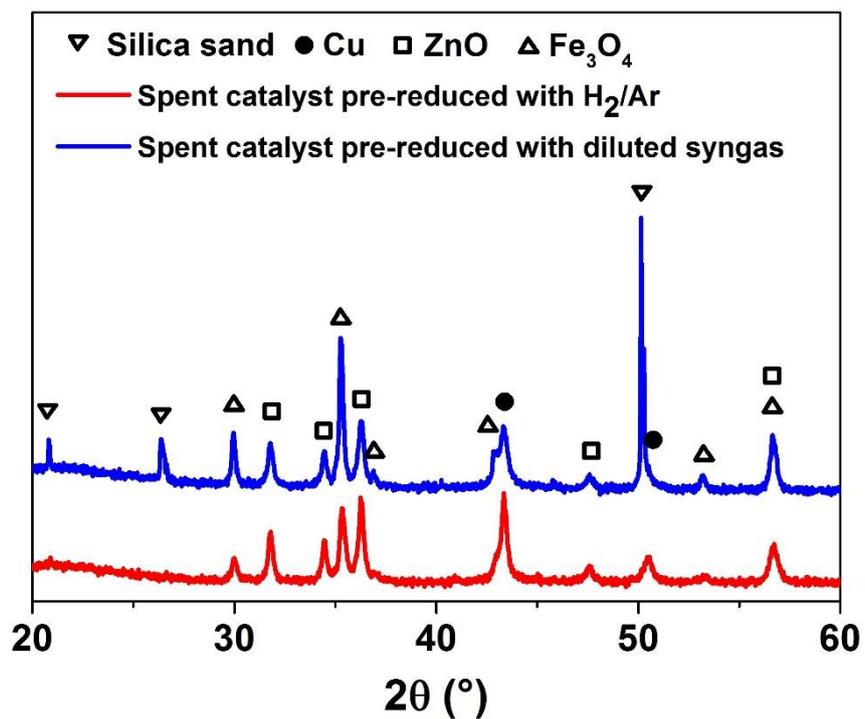


**Fig. S9.** Comparison of HAS activities over Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> reduced by different gas flows: 10% H<sub>2</sub>/Ar reduction (A) and diluted syngas reduction (B). (a) CO<sub>2</sub> conversion (yellow square) and product distribution (CO, CH<sub>4</sub>, C<sub>2+</sub> alkane, olefin and alcohol, in all carbon products); (b) STY of different alcohols and C<sub>2+</sub>OH/ROH weight contents (red circle). Reaction conditions: catalyst 200 mg and quartz sand 400 mg; H<sub>2</sub>/CO<sub>2</sub> = 3:1; 5 MPa; 15 mL min<sup>-1</sup>; 260-330 °C.

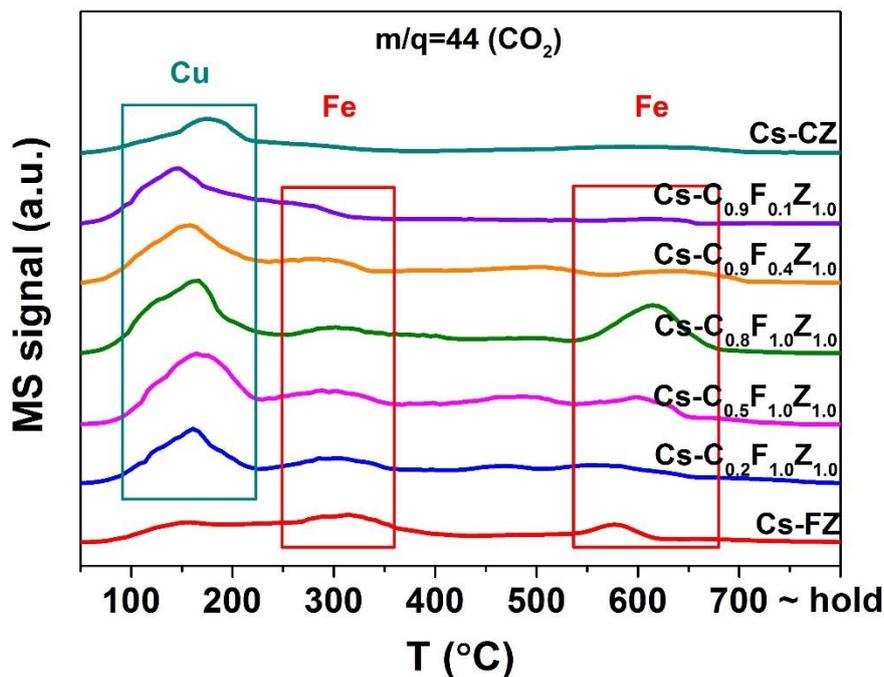
## Discussion on the effect of reduction conditions

We also investigated the influence of pre-reduction conditions on the activity of Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub>. The catalyst reduced by H<sub>2</sub>/Ar is denoted as Catalyst A. The reference catalyst was treated by diluted syngas at 350 °C for 5 h, denoted as Catalyst B. Fig. S9 shows that, as the reaction temperature is raised from 260 °C to 310 °C, the CO<sub>2</sub> conversion over Catalyst A is significantly enhanced while that over Catalyst B shows just a slight increasing trend. The selectivity and STY of total alcohols or C<sub>2+</sub>OH over Catalyst B are much lower than those over Catalyst A. This reveals that H<sub>2</sub>/Ar reduction is preferable and much better than syngas reduction for our Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> catalysts.

To rationalize the poor activity of Catalyst B, we next compared the particle size of Cu, Fe and Zn species in Catalyst A and Catalyst B. As seen in Table S4, after syngas reduction, the agglomeration of Fe<sub>3</sub>O<sub>4</sub> phase is severe (75.4 nm) when compared with that by H<sub>2</sub> reduction (44.6 nm) while ZnO and Cu are almost the same. This is probably because syngas has a stronger reducing activity than H<sub>2</sub>/Ar, which causes a severe sintering of Fe<sub>3</sub>O<sub>4</sub>. Moreover, there is still no diffraction peaks of iron carbide for the spent Catalyst B (Fig. S10). So the poor activity of Catalyst B results from severe sintering of Fe species and thus disfavoring the formation of abundant copper-iron carbide interfaces. By contrast, a mild reduction treatment (H<sub>2</sub>/Ar and the following *in-situ* reaction condition) is beneficial to the formation of copper-iron carbide interfaces as active sites for HAS.



**Fig. S10.** PXRD patterns over spent Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> catalyst pre-reduced by H<sub>2</sub>/Ar or diluted syngas. Cu PDF#85-1326, ZnO PDF#79-2205, Fe<sub>3</sub>O<sub>4</sub> PDF#75-1372.



**Fig. S11.** H<sub>2</sub>-TPSR-MS results of desorbed CO<sub>2</sub> over CO pre-adsorbed Cs-C<sub>y</sub>F<sub>z</sub>Z<sub>1.0</sub> catalyst.

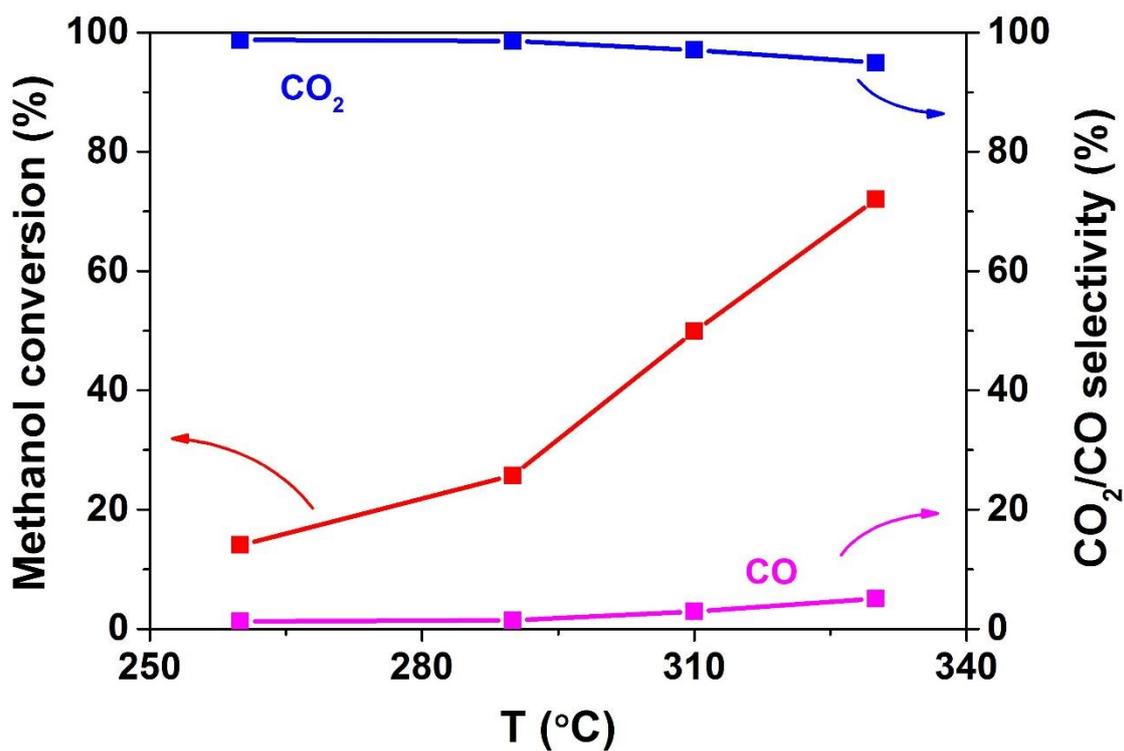
**Table S5.** Proportion (A%) of desorbed CO, CO<sub>2</sub> and CH<sub>4</sub> species in all desorbed carbon-based molecules (CO<sub>2</sub>, CO and CH<sub>4</sub>) calculated by MS peak areas and catalytic performance over different Cs-C<sub>y</sub>F<sub>z</sub>Z<sub>1.0</sub> catalysts.

Sample	A <sub>CO</sub> % <sup>a</sup> (%)	A <sub>CO<sub>2</sub></sub> % (%)	A <sub>CH<sub>4</sub></sub> % (%)	S <sub>HC</sub> <sup>b</sup> (%)	S <sub>CO</sub> (%)	S <sub>HA</sub> (%)	STY <sub>HA</sub> (mg g <sub>cat</sub> <sup>-1</sup> h <sup>-1</sup> )
Cs-C <sub>0.2</sub> F <sub>1.0</sub> Z <sub>1.0</sub>	16.9	26.7	56.4	62.4	23.8	13.8	36.2
Cs-C <sub>0.5</sub> F <sub>1.0</sub> Z <sub>1.0</sub>	22.6	32.3	45.1	58.7	22.6	17.9	64.5
Cs-C <sub>0.8</sub> F <sub>1.0</sub> Z <sub>1.0</sub>	25.7	30.3	44.0	58.7	20.6	19.8	73.4
Cs-C <sub>0.9</sub> F <sub>0.4</sub> Z <sub>1.0</sub>	34.1	28.8	37.1	61.2	20.7	17.4	65.5
Cs-C <sub>0.9</sub> F <sub>0.1</sub> Z <sub>1.0</sub>	39.5	29.5	31.0	54.7	26.7	17.2	51.7

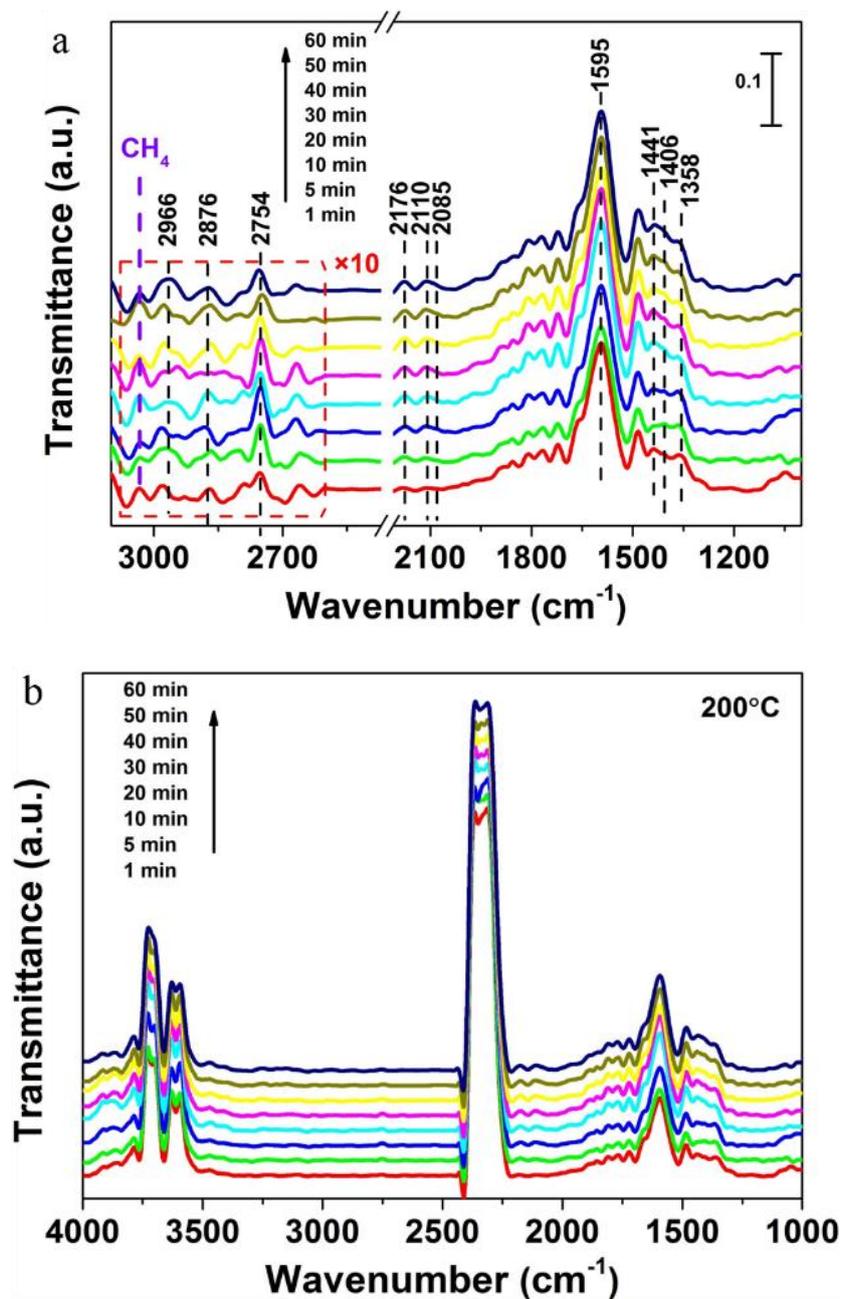
<sup>[a]</sup> A% stands for the proportion of MS peak area for specific species.

<sup>[b]</sup> Product selectivity.

As for all Cs-C<sub>y</sub>F<sub>z</sub>Z<sub>1.0</sub> catalysts, CO<sub>2</sub> desorption shows three peaks (peak  $\alpha$  at 150 °C,  $\beta$  at 300 °C and  $\gamma$  at 600 °C). As a reference, Cs-CZ (without Fe) exhibits good WGS activity at low temperature region while Cs-FZ (without Cu) shows relatively weak CO<sub>2</sub> desorption at 300 °C and 600 °C (Fig. S11). So we can conclude that Cu sites mainly contribute to  $\alpha$  while Fe species contribute to  $\beta$  and  $\gamma$ . The CO<sub>2</sub> desorption capability can reflect the RWGS ability in our real condition. With the increase in Cu/Fe molar ratio, the peak intensity of CO<sub>2</sub> increases first and then decreases (see Table S5), implying the synergistic effect between Cu and Fe species.

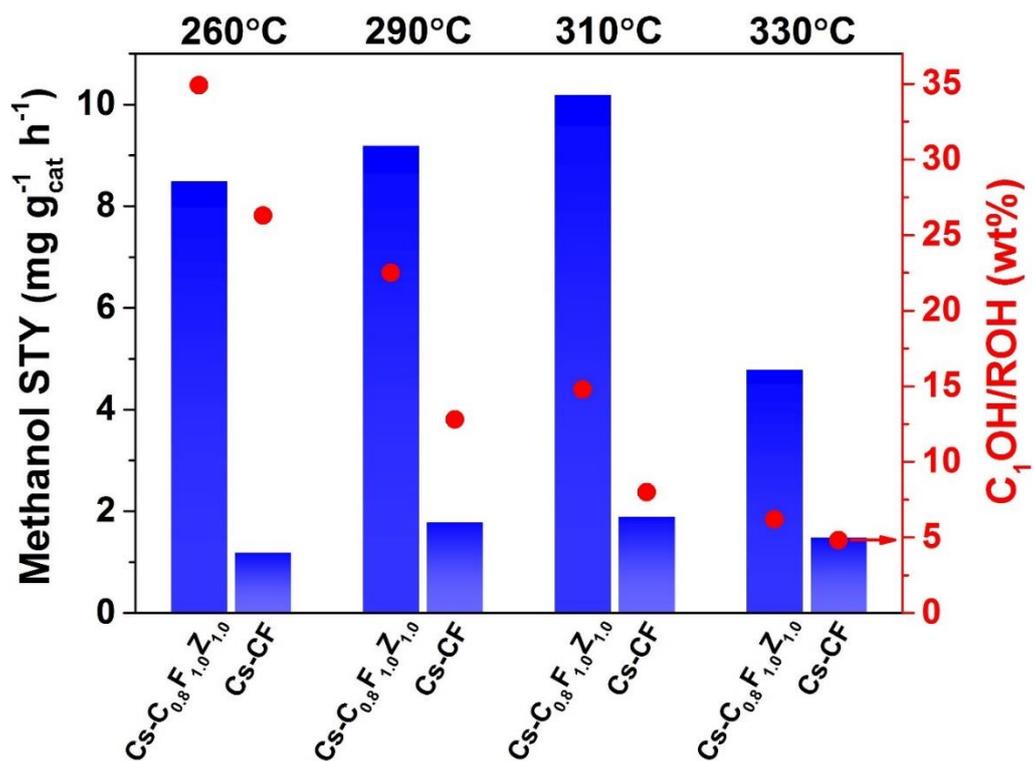


**Fig. S12.** Catalytic performance (methanol conversion and CO<sub>2</sub>/CO selectivity) of the Cs-C<sub>y</sub>F<sub>z</sub>Z<sub>1.0</sub> catalyst. Reaction conditions: 100 mg catalyst diluted by 400 mg quartz sand; methanol/water = 1:2, 0.1 mL min<sup>-1</sup>; carrier gas H<sub>2</sub> flow=20 mL min<sup>-1</sup>; 260-330 °C.



**Figure S13.** (a) In situ DRIFTS spectra and (b) full-range ( $1000 \sim 4000 \text{ cm}^{-1}$ ) spectra of the  $\text{CO}_2+\text{H}_2$  reaction over  $\text{Cs-C}_{0.5}\text{F}_{1.0}\text{Z}_{1.0}$  catalyst taken under  $0.3 \text{ MPa CO}_2/\text{H}_2$  flow at  $200 \text{ }^\circ\text{C}$ .

The characteristic band of gaseous  $\text{CH}_4$  is at  $\sim 3016 \text{ cm}^{-1}$ . Indeed, the small peak at  $3025 \text{ cm}^{-1}$  is likely assigned to gaseous  $\text{CH}_4$  (Fig. S13a). As for the other alkyl species, the characteristic bands are overlapped with carbonate and bicarbonate species in the range of  $1300\text{-}1500 \text{ cm}^{-1}$ . The bands for  $\text{CO}_2$  overtones and hydroxyl are displayed in the range of  $3100\text{-}4000 \text{ cm}^{-1}$  (Fig. S13b).



**Fig. S14.** Methanol STY (blue bar chart) and its weight percent in total alcohols (red circle) over Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> and Cs-CF catalysts.

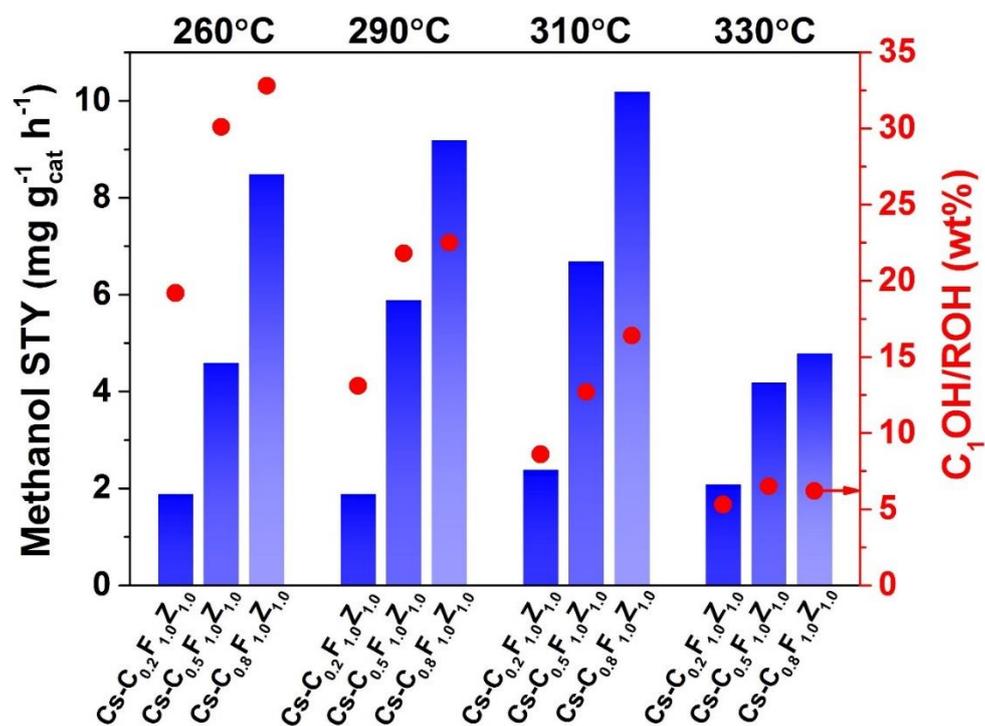
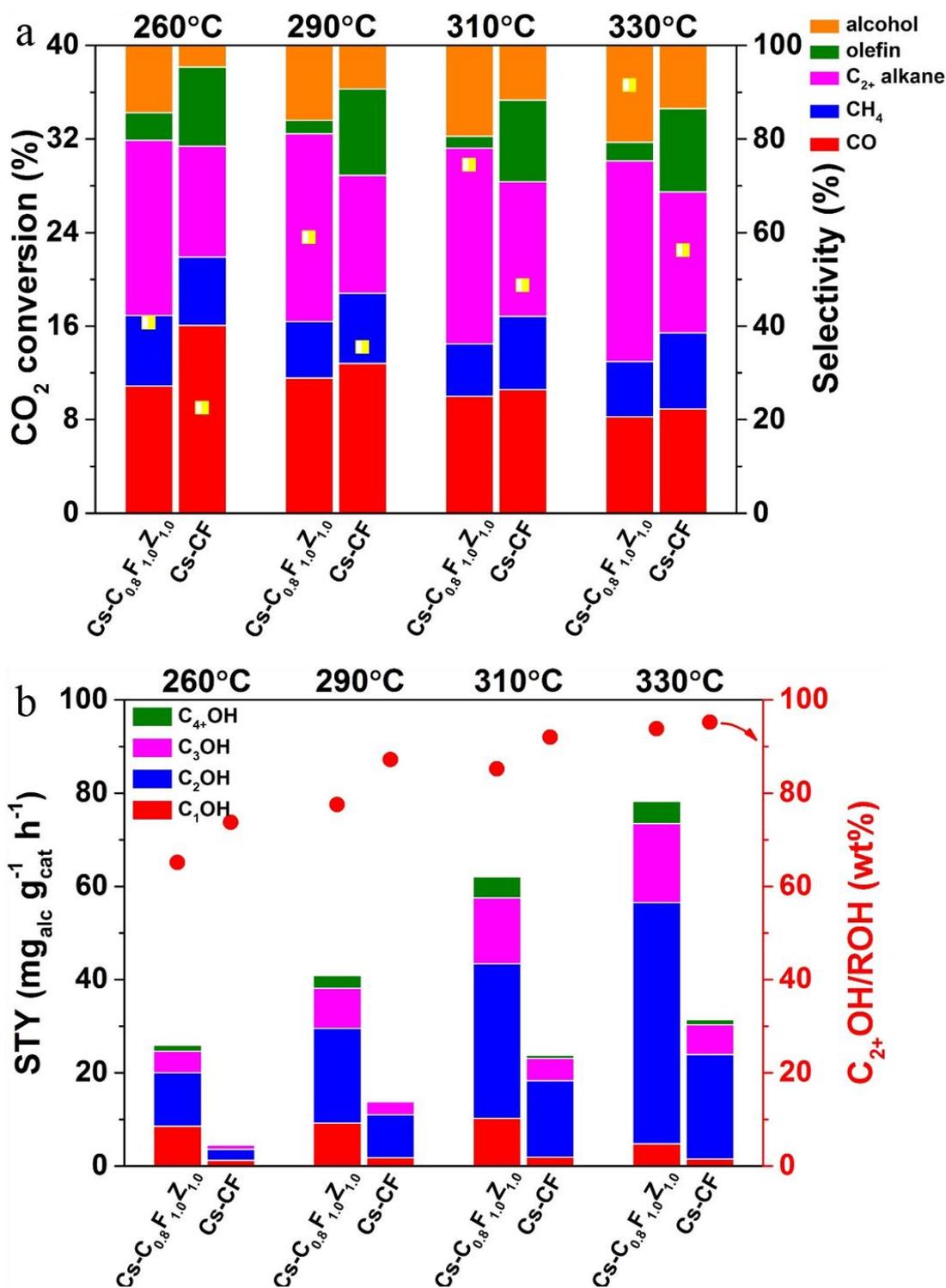


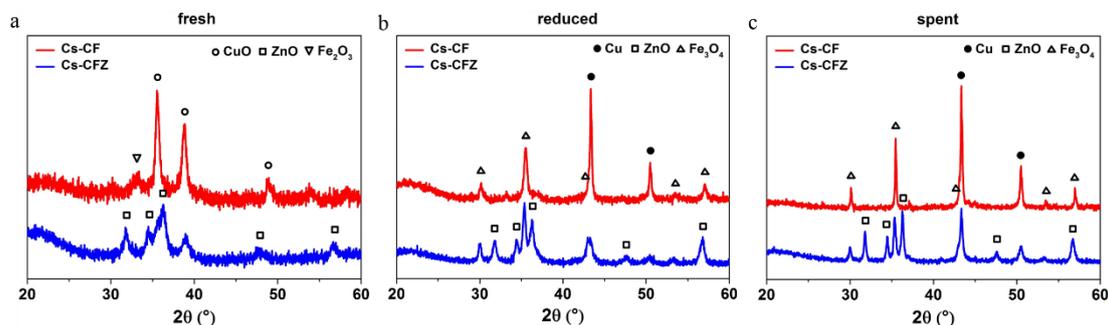
Fig. S15. Methanol STY (blue bar chart) and its weight percent in total alcohols (red circle) over Cs-C<sub>0.2</sub>F<sub>1.0</sub>Z<sub>1.0</sub>, Cs-C<sub>0.5</sub>F<sub>1.0</sub>Z<sub>1.0</sub> and Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> catalysts.



**Fig. S16.** Catalytic performance of Cs-CF and Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> catalysts. (a) CO<sub>2</sub> conversion (yellow square) and product selectivity (CO, CH<sub>4</sub>, C<sub>2+</sub> alkane, olefin and alcohol, in all carbon products), (b) STY of alcohols and C<sub>2+</sub>OH/ROH selectivity (red circle). Reaction conditions: 200 mg catalyst and 400 mg quartz sand; H<sub>2</sub>/CO<sub>2</sub> = 3:1; 5 MPa; 15 mL min<sup>-1</sup>; 260-330 °C.

## Discussion on the effect of ZnO

As showed in Fig. S17, we can clearly see that the CuO and Cu particles would grow bigger without the protection of ZnO. Fe<sub>3</sub>O<sub>4</sub> shows the similar results. Therefore, ZnO plays an important role in dispersing and stabilizing Cu and Fe species. Moreover, ZnO is a good partner to Cu. Cu-ZnO is a widely studied catalyst system for methanol synthesis as well as RWGS reaction.<sup>13-18</sup> The high RWGS activity of Cu-ZnO would provide a relatively high fraction of initial CO for tandem reaction. Theoretical calculations have shown that ZnO decoration can benefit the adsorption of O-anchored intermediates such as formate and acyl groups due to the oxophile property of Zn atoms.<sup>16</sup> In this content, Zn would promote the formation of oxy-compounds. ZnO is also a good hydrogen reservoir and hence increases the hydrogenation activity of Cu based catalysts, which can be further confirmed by the lower olefins/paraffin ratio over Cs-C<sub>0.8</sub>F<sub>1.0</sub>Z<sub>1.0</sub> (Fig. S16).<sup>18,19</sup>



**Fig. S17.** XRD patterns over (a) fresh, (b) reduced and (c) spent Cs-CF and Cs-CFZ catalysts. Cu PDF#85-1326, CuO PDF#45-0937, ZnO PDF#79-2205, Fe<sub>3</sub>O<sub>4</sub> PDF#75-1372.

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