

## Supporting Information

### The subchalcogenides $\text{Ir}_2\text{In}_8\text{Q}$ ( $\text{Q} = \text{S}, \text{Se}, \text{Te}$ ): Dirac semimetal candidates with re-entrant structural modulation

Jason F. Khouri<sup>1</sup>, Alexander J. E. Rettie<sup>2,3</sup>, Iñigo Robredo<sup>4,5</sup>, Matthew J. Krogstad<sup>2</sup>, Christos D. Malliakas<sup>1</sup>, Aitor Bergara<sup>4,5,6</sup>, Maia G. Vergniory<sup>5,7</sup>, Raymond Osborn<sup>2</sup>, Stephan Rosenkranz<sup>2</sup>, Duck Young Chung<sup>2</sup>, and Mercouri G. Kanatzidis<sup>1,2\*</sup>

<sup>1</sup>*Department of Chemistry, Northwestern University, Evanston, Illinois 60208, United States*

<sup>2</sup>*Materials Science Division, Argonne National Laboratory, Lemont, Illinois 60439, United States*

<sup>3</sup>*Electrochemical Innovation Lab, Department of Chemical Engineering, University College London, London WC1E 7JE, United Kingdom*

<sup>4</sup>*Donostia International Physics Center, Paseo Manuel de Lardizabal 4, 20018 Donostia-San Sebastian, Spain*

<sup>5</sup>*Condensed Matter Physics Department, University of the Basque Country UPV/EHU, 48080 Bilbao, Spain*

<sup>6</sup>*Centro de Física de Materiales, Centro Mixto CSIC-UPV/EHU, 20018 Donostia, Spain*

<sup>7</sup>*Ikerbasque, Basque Foundation for Science, E-48011 Bilbao, Spain*

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### Refinement Details of Modulated Structure

The displacive distortion of a given atomic position  $x_4$  in the subcell can be expressed by a periodic modulation function  $p(x_4)$  in a form of a Fourier expansion:

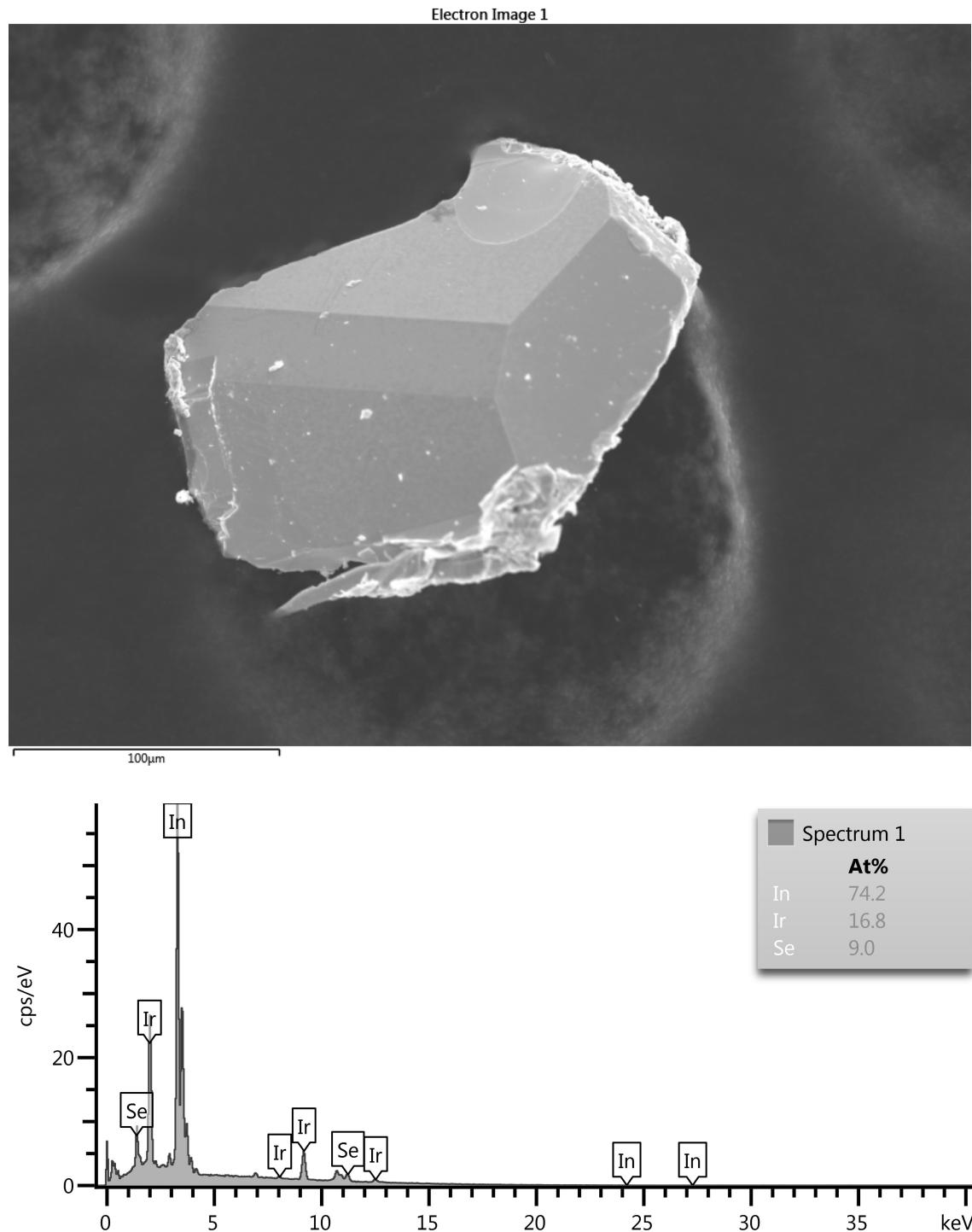
$$p(k + x_4) = \sum_{n=1}^m A_{sn} \sin[2\pi\bar{q}_n(k + x_4)] + \sum_{n=1}^m A_{cn} \cos[2\pi\bar{q}_n(k + x_4)]$$

in which  $A_{sn}$  is the sinusoidal coefficient of the given Fourier term,  $A_{cn}$  is the cosine coefficient,  $n$  is the number of modulation waves used for the refinement and  $k$  is the lattice translation.  $\bar{q}_n = \sum_{i=1}^d \alpha_{ni} q_i$  where  $\alpha_{ni}$  integer numbers for the linear combination of the incommensurate modulation vectors  $q_i$ .<sup>1-2</sup> A useful coordinate  $t$  that characterizes and describes the real three-dimensional structure constructed as a perpendicular intersection with the fourth dimensional axis is defined as

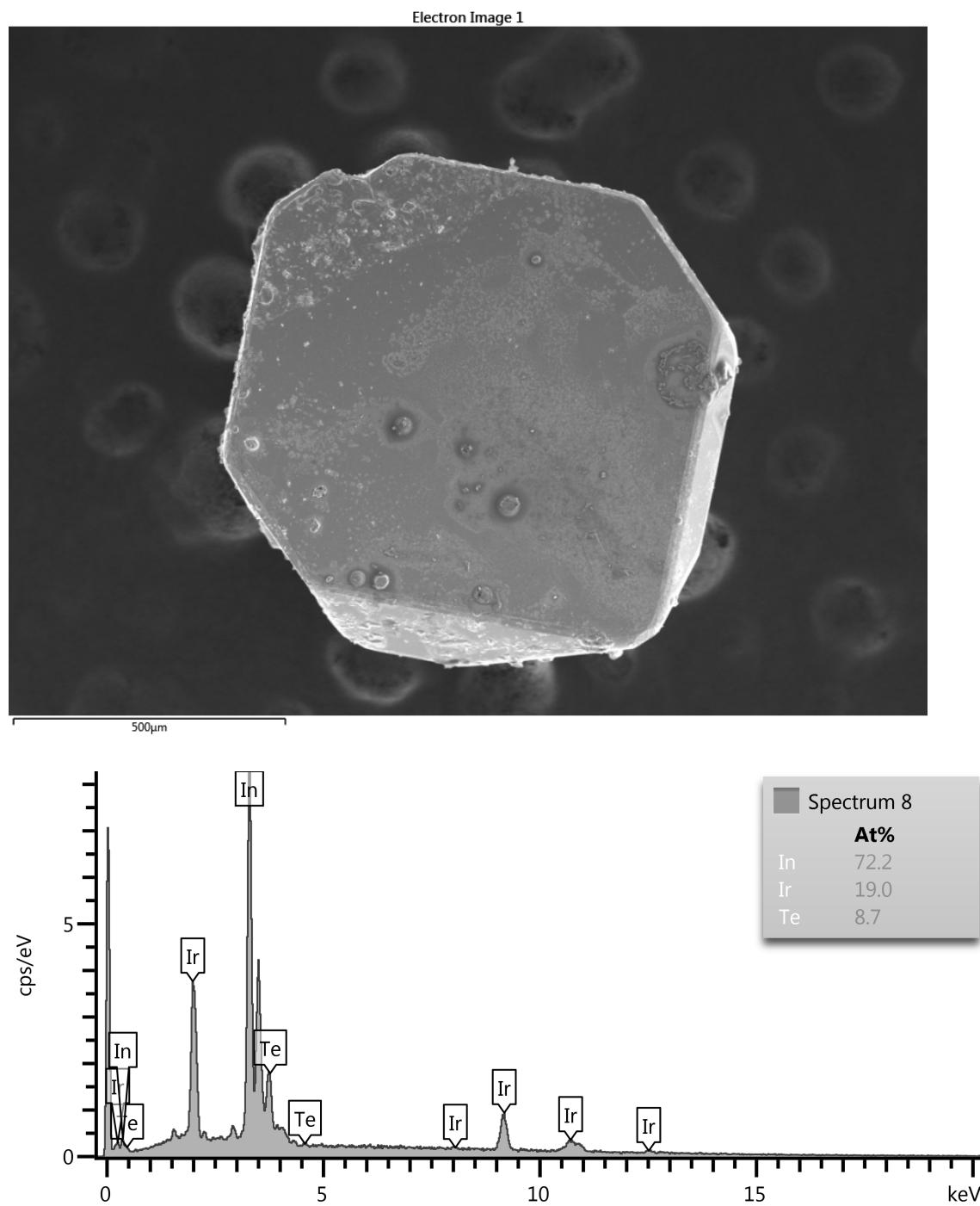
$$t = x_4 - q \cdot r$$

where  $r$  is a vector in the real three-dimensional reciprocal space.<sup>1-2</sup>

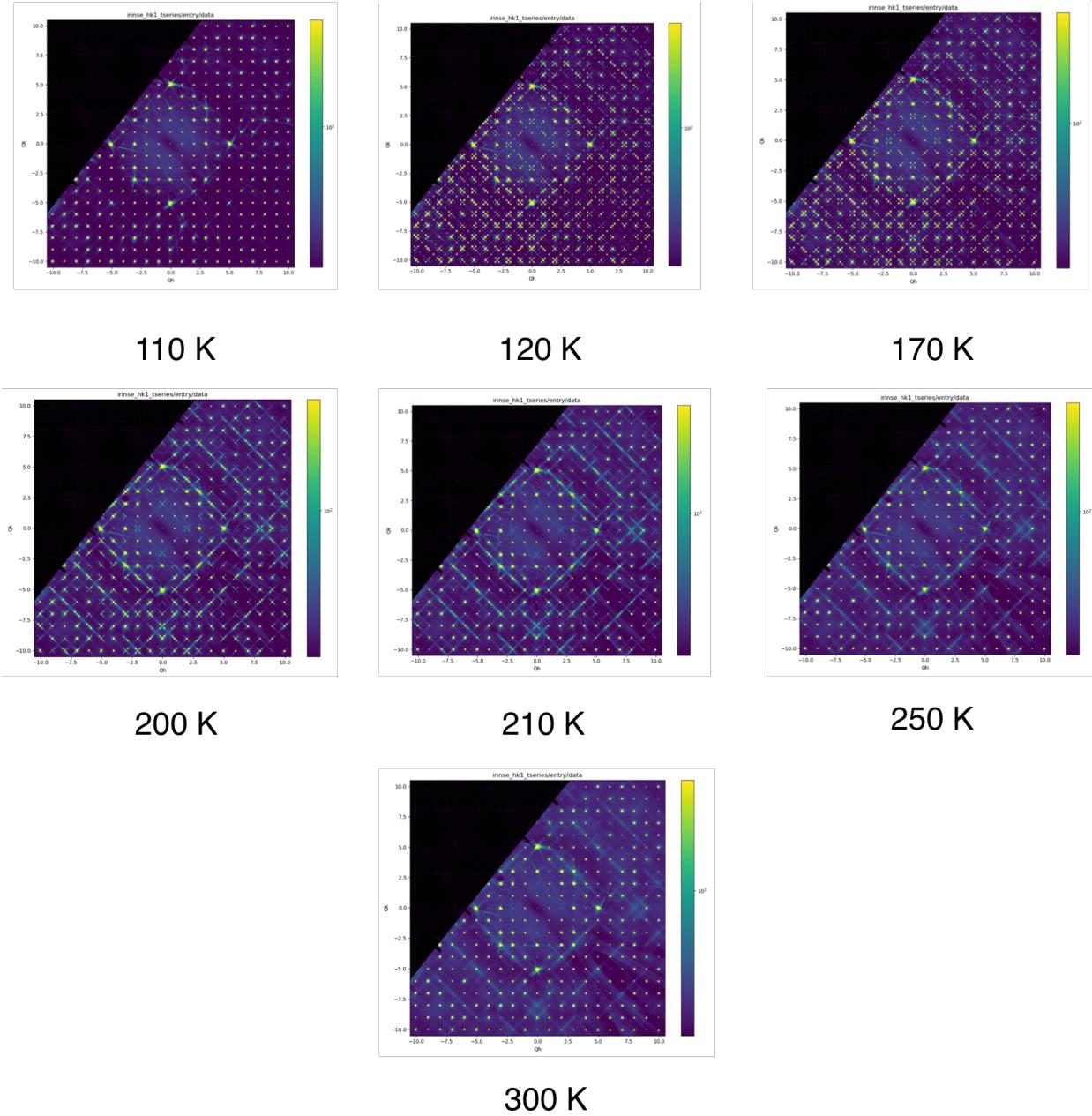
The superspace approach includes all methods for solution and refinement of aperiodic crystals. It enables the use of the tools used in structure analysis of regular crystals such as direct methods, Fourier maps, least squares, distance and angle calculations, bond valence summations, maximum entropy method, *etc.* so that they can be used in a similar way like in standard crystallography.



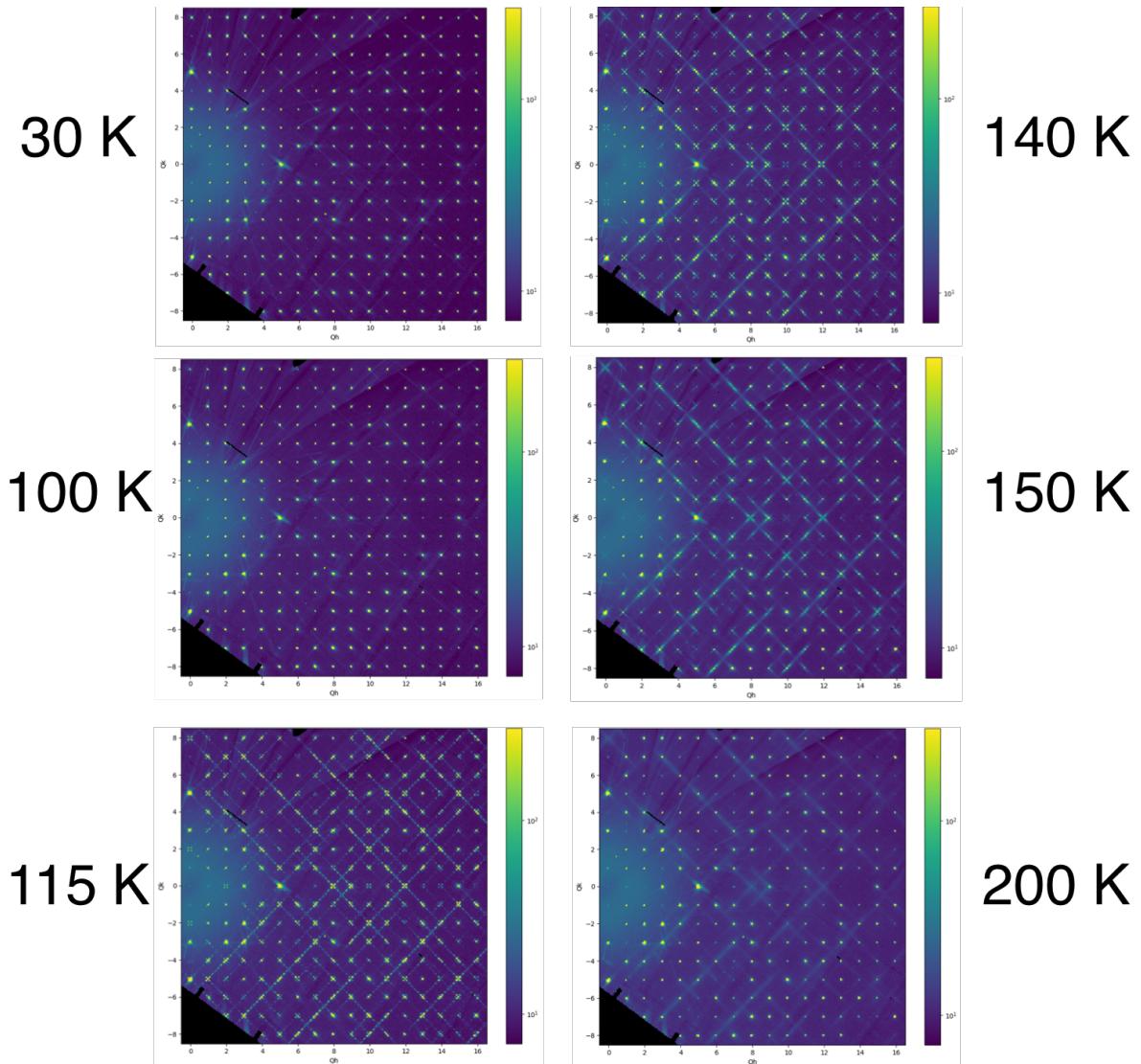
**Figure S1:** SEM (top) and EDS (bottom) for a single crystal of  $\text{Ir}_2\text{In}_8\text{Se}$ . The approximate composition from EDS is  $\text{Ir}_{1.86}\text{In}_{8.24}\text{Se}$ .



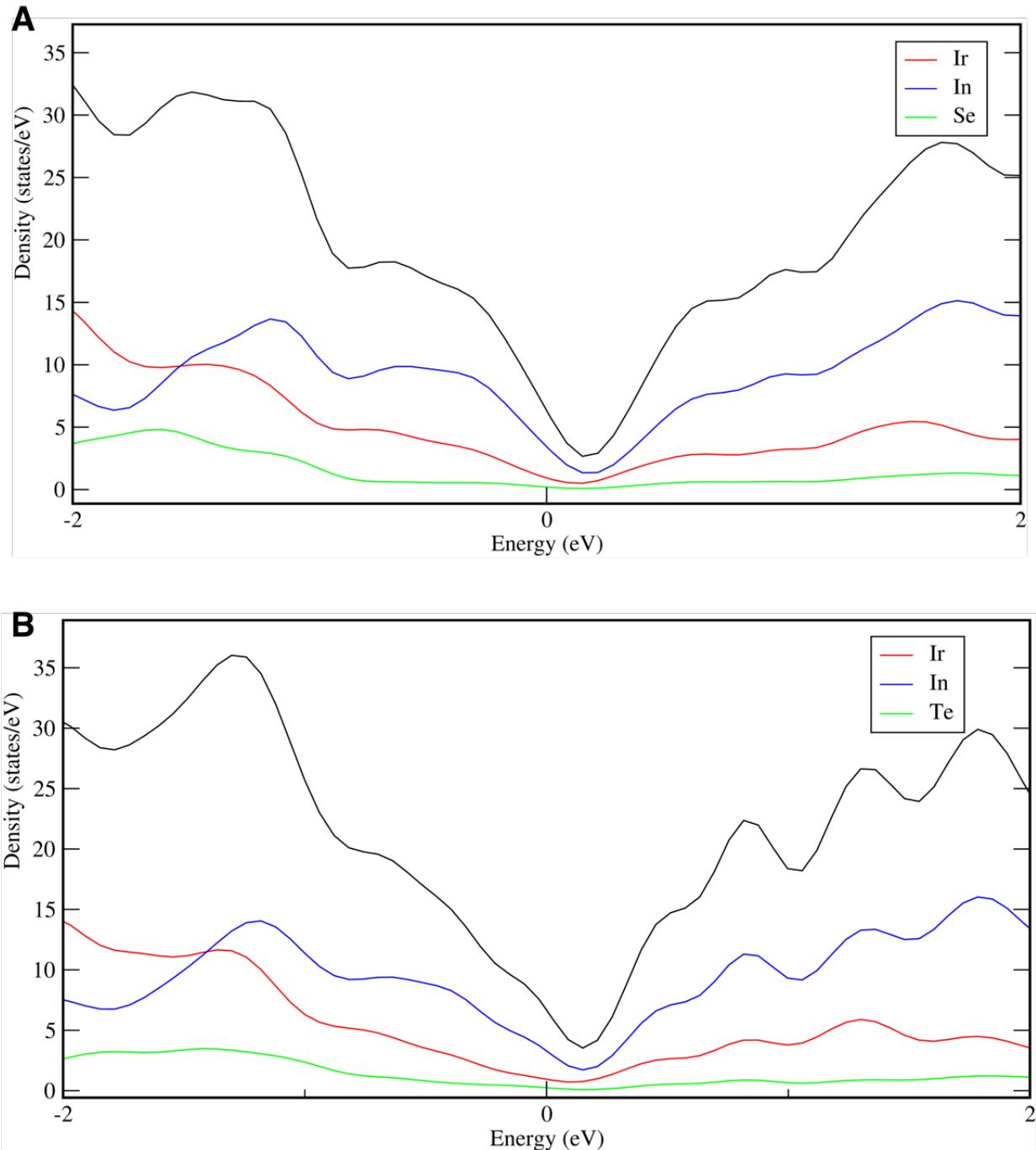
**Figure S2:** SEM (top) and EDS (bottom) for a single crystal of  $\text{Ir}_2\text{In}_8\text{Te}$ . The approximate composition from EDS is  $\text{Ir}_{2.18}\text{In}_{8.29}\text{Te}$ .



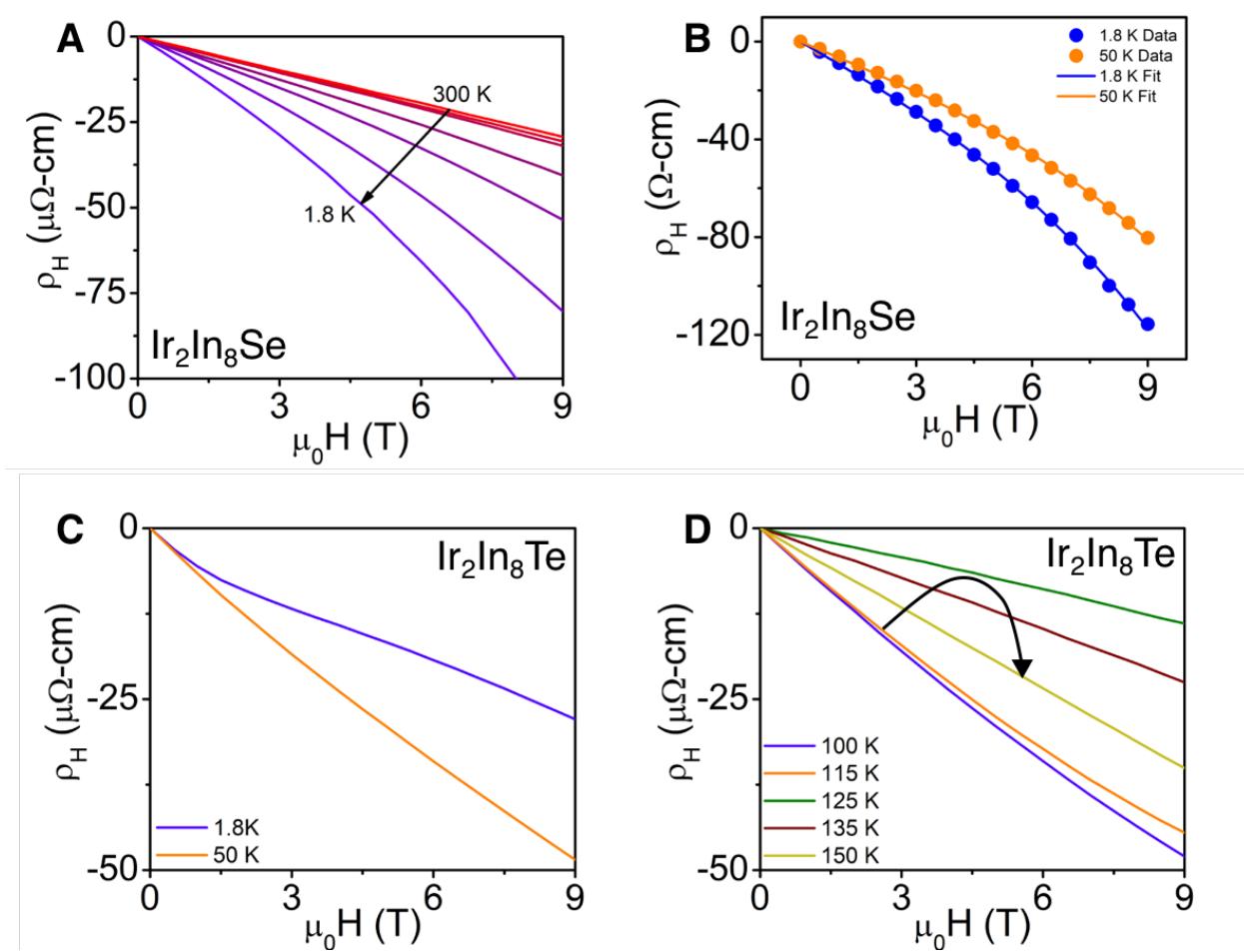
**Figure S3:** Extended single crystal synchrotron diffraction images of  $\text{Ir}_2\text{In}_8\text{Se}$  from 110 – 300 K. The higher temperature regimes show rods of diffuse scattering, the temperatures below the transition temperature (203 K) show supercell ordering, and the temperatures below the second transition temperature (120 K) revert to the original sub-cell with no diffuse scattering.



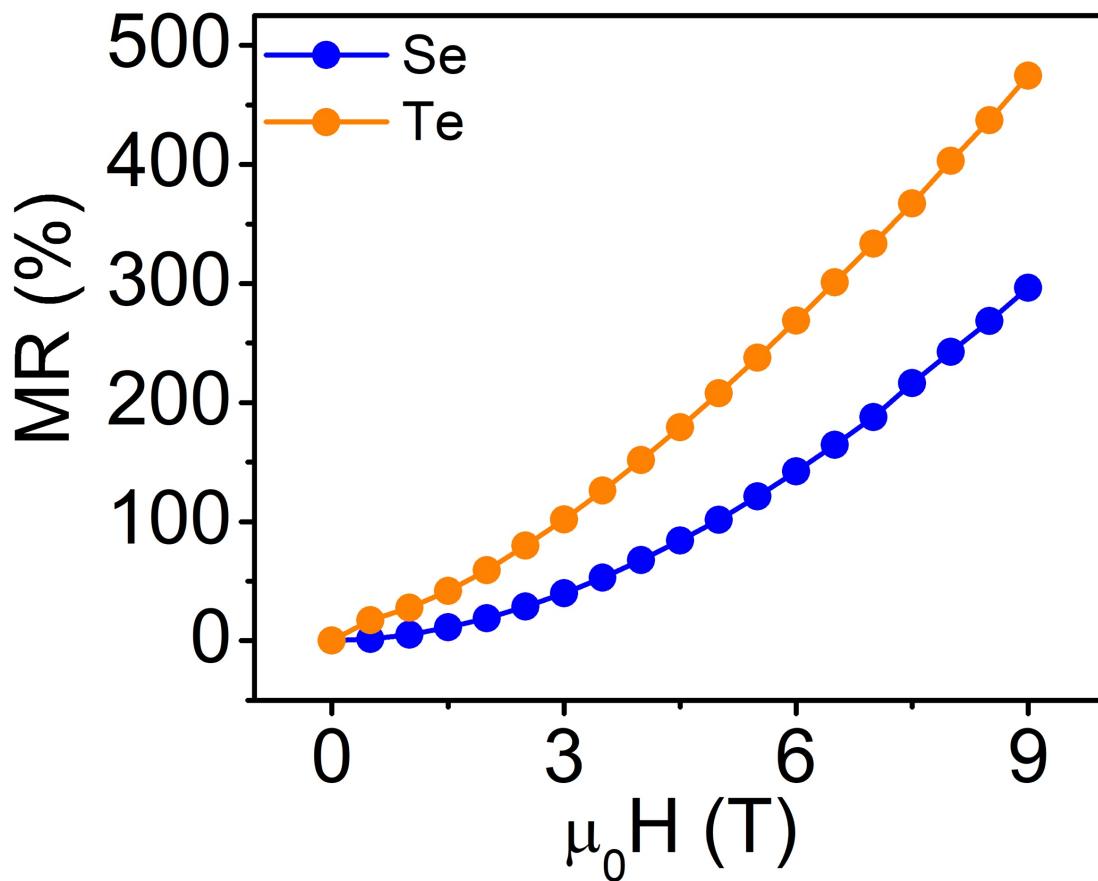
**Figure S4:** Extended single crystal synchrotron diffraction images of  $\text{Ir}_2\text{In}_8\text{Te}$ . The supercell ordering starts to come in below 150 K and reverts to the original sub-cell by 100 K.



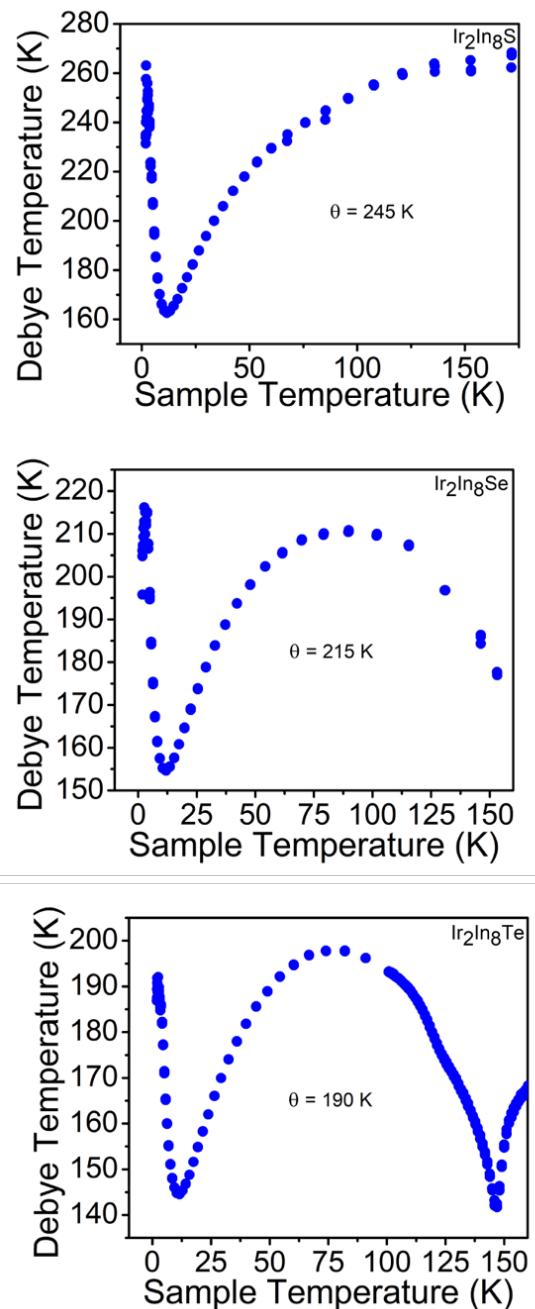
**Figure S5:** Partial density of states (PDOS) for  $\text{Ir}_2\text{In}_8\text{Se}$  (A) and  $\text{Ir}_2\text{In}_8\text{Te}$  (B), with the total DOS in black. In both cases, In and Ir orbital contributions are the main contributors to the band structure with minimal contribution from the Q atoms.



**Figure S6:** Variable temperature Hall resistivity data for  $\text{Ir}_2\text{In}_8\text{Se}$  (A, B) and  $\text{Ir}_2\text{In}_8\text{Te}$  (C, D). The multi-band fits in (B) show both electron and hole contribution at low temperatures in  $\text{Ir}_2\text{In}_8\text{Se}$ , while the telluride analogue does not fit to a multi-band model. The hole carrier concentration and mobility values are  $\sim 900 \text{ cm}^2/\text{Vs}$  and  $5 \times 10^{19} \text{ cm}^{-3}$  at 1.8 K and  $\sim 700 \text{ cm}^2/\text{Vs}$  and  $7 \times 10^{18} \text{ cm}^{-3}$  at 50 K.



**Figure S7:** Magnetoresistance data for Ir<sub>2</sub>In<sub>8</sub>Se and Ir<sub>2</sub>In<sub>8</sub>Te. Orange and blue lines are guides to the eye.



**Figure S8:** Debye temperature plots and estimated Debye temperature values of  $\text{Ir}_2\text{In}_8\text{Q}$ .  $\text{Ir}_2\text{In}_8\text{S}$  has the highest Debye temperature due to the more ionic behavior of the sulfide anion, and  $\text{Ir}_2\text{In}_8\text{Te}$  has the lowest value due to the softer, more covalent nature of the telluride anion.

**Table S1.** Atomic coordinates ( $\times 10^4$ ) and equivalent isotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{S}$  at 299 K with estimated standard deviations in parentheses.

Label	x	y	z	Occupancy	$U_{eq}^*$
Ir(1)	6876(1)	6876(1)	7399(1)	1	3(1)
In(1)	5957(1)	5957(1)	5000	1	10(1)
In(2)	5000	5000	8340(1)	1	12(1)
In(3)	9478(1)	7009(1)	8046(1)	1	13(1)
In(4)	6841(1)	6841(1)	10000	1	18(1)
In(5)	8003(1)	8003(1)	5000	1	39(1)
S(1)	10000	5000	10000	1	43(2)

\*  $U_{eq}$  is defined as one third of the trace of the orthogonalized  $U_{ij}$  tensor.

**Table S2.** Anisotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{S}$  at 299 K with estimated standard deviations in parentheses.

Label	$U_{11}$	$U_{22}$	$U_{33}$	$U_{12}$	$U_{13}$	$U_{23}$
Ir(1)	2(1)	2(1)	6(1)	0(1)	0(1)	0(1)
In(1)	11(1)	11(1)	7(1)	-6(1)	0	0
In(2)	11(1)	11(1)	14(1)	-8(1)	0	0
In(3)	2(1)	12(1)	24(1)	-3(1)	0(1)	-2(1)
In(4)	24(1)	24(1)	6(1)	-13(1)	0	0
In(5)	55(1)	55(1)	9(1)	-51(1)	0	0
S(1)	104(5)	13(2)	13(2)	22(2)	0	0

The anisotropic displacement factor exponent takes the form:  $-2\pi^2[h^2a^{*2}U_{11} + \dots + 2hka^*b^*U_{12}]$ .

**Table S3.** Bond lengths [ $\text{\AA}$ ] for  $\text{Ir}_2\text{In}_8\text{S}$  at 299 K with estimated standard deviations in parentheses.

Label	Distances
Ir(1)-In(1)	2.7532(7)
Ir(1)-In(2)	2.7993(6)
Ir(1)-In(3)	2.6668(6)
Ir(1)-In(3)#1	2.6618(6)
Ir(1)-In(3)#2	2.6668(6)
Ir(1)-In(3)#3	2.6618(6)
Ir(1)-In(4)	2.6379(6)
Ir(1)-In(5)	2.9016(8)
In(1)-Ir(1)#4	2.7531(7)
In(1)-In(1)#5	2.6843(19)
In(1)-In(3)#3	3.1858(6)
In(1)-In(3)#6	3.1858(6)
In(1)-In(3)#1	3.1858(6)
In(1)-In(3)#7	3.1858(6)
In(1)-In(5)	2.8711(15)
In(2)-Ir(1)#8	2.7992(6)
In(2)-In(2)#9	3.366(2)
In(2)-In(3)#3	3.3239(8)
In(2)-In(3)#10	3.3239(8)
In(2)-In(3)#11	3.3239(8)
In(2)-In(3)#1	3.3239(8)
In(2)-In(4)	3.0829(11)
In(2)-In(4)#9	3.0829(11)
In(2)-In(5)#11	3.2679(12)
In(2)-In(5)#12	3.2679(12)
In(3)-Ir(1)#13	2.6618(6)
In(3)-In(1)#13	3.1857(6)
In(3)-In(2)#13	3.3239(8)
In(3)-In(3)#1	3.1156(9)
In(3)-In(3)#13	3.1155(9)
In(3)-In(4)	3.2855(9)
In(3)-S(1)	2.8574(6)
In(4)-Ir(1)#14	2.6379(6)

In(4)-In(2)#9	3.0829(11)
In(4)-In(3)#2	3.2855(9)
In(4)-In(3)#14	3.2855(9)
In(4)-In(3)#15	3.2855(9)
In(5)-Ir(1)#4	2.9016(8)
In(5)-In(2)#13	3.2680(12)
In(5)-In(2)#16	3.2680(12)
S(1)-In(3)#17	2.8574(6)
S(1)-In(3)#18	2.8574(6)
S(1)-In(3)#14	2.8574(6)

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Symmetry transformations used to generate equivalent atoms:

(1)  $x-1/2, -y+3/2, -z+3/2$  (2)  $-y+3/2, x-1/2, -z+3/2$  (3)  $y, x, z$  (4)  $x, y, -z+1$  (5)  $-x+1, -y+1, -z+1$  (6)  $-y+3/2, x-1/2, z-1/2$  (7)  $x-1/2, -y+3/2, z-1/2$  (8)  $-x+1, -y+1, z$  (9)  $-x+1, -y+1, -z+2$  (10)  $y-1/2, -x+3/2, -z+3/2$  (11)  $-x+3/2, y-1/2, -z+3/2$  (12)  $-y+3/2, x-1/2, z+1/2$  (13)  $y+1/2, -x+3/2, -z+3/2$  (14)  $x, y, -z+2$  (15)  $y, x, -z+2$  (16)  $-y+3/2, x+1/2, z-1/2$  (17)  $-x+2, -y+1, -z+2$  (18)  $-x+2, -y+1, z$

**Table S4.** Bond angles [°] for Ir<sub>2</sub>In<sub>8</sub>S at 299 K with estimated standard deviations in parentheses.

Label	Angles
In(1)-Ir(1)-In(2)	82.01(3)
In(1)-Ir(1)-In(5)	60.96(3)
In(2)-Ir(1)-In(5)	142.97(3)
In(3)#3-Ir(1)-In(1)	72.054(14)
In(3)-Ir(1)-In(1)	123.670(18)
In(3)#2-Ir(1)-In(1)	123.670(18)
In(3)#1-Ir(1)-In(1)	72.054(14)
In(3)#2-Ir(1)-In(2)	126.332(19)
In(3)-Ir(1)-In(2)	126.332(19)
In(3)#1-Ir(1)-In(2)	74.937(14)
In(3)#3-Ir(1)-In(2)	74.937(14)
In(3)#1-Ir(1)-In(3)#2	152.389(11)
In(3)#1-Ir(1)-In(3)	71.56(2)
In(3)#3-Ir(1)-In(3)#1	135.56(3)
In(3)#2-Ir(1)-In(3)	81.00(2)
In(3)#3-Ir(1)-In(3)	152.389(11)
In(3)#3-Ir(1)-In(3)#2	71.56(2)
In(3)#2-Ir(1)-In(5)	79.29(2)
In(3)#3-Ir(1)-In(5)	92.410(16)
In(3)-Ir(1)-In(5)	79.29(2)
In(3)#1-Ir(1)-In(5)	92.410(16)
In(4)-Ir(1)-In(1)	151.02(3)
In(4)-Ir(1)-In(2)	69.01(3)
In(4)-Ir(1)-In(3)#1	99.402(17)
In(4)-Ir(1)-In(3)	76.54(2)
In(4)-Ir(1)-In(3)#2	76.54(2)
In(4)-Ir(1)-In(3)#3	99.402(17)
In(4)-Ir(1)-In(5)	148.02(3)
Ir(1)#4-In(1)-Ir(1)	124.15(4)
Ir(1)-In(1)-In(3)#1	52.645(12)
Ir(1)#4-In(1)-In(3)#1	119.48(2)
Ir(1)#4-In(1)-In(3)#6	52.645(12)
Ir(1)#4-In(1)-In(3)#3	119.48(2)
Ir(1)#4-In(1)-In(3)#7	52.645(12)

Ir(1)-In(1)-In(3)#7	119.48(2)
Ir(1)-In(1)-In(3)#6	119.48(2)
Ir(1)-In(1)-In(3)#3	52.645(12)
Ir(1)#4-In(1)-In(5)	62.074(19)
Ir(1)-In(1)-In(5)	62.074(19)
In(1)#5-In(1)-Ir(1)	117.926(19)
In(1)#5-In(1)-Ir(1)#4	117.926(19)
In(1)#5-In(1)-In(3)#6	97.028(19)
In(1)#5-In(1)-In(3)#3	97.028(19)
In(1)#5-In(1)-In(3)#7	97.028(19)
In(1)#5-In(1)-In(3)#1	97.028(19)
In(1)#5-In(1)-In(5)	180.00(4)
In(3)#3-In(1)-In(3)#7	165.94(4)
In(3)#1-In(1)-In(3)#6	165.94(4)
In(3)#7-In(1)-In(3)#6	101.34(2)
In(3)#3-In(1)-In(3)#1	101.34(2)
In(3)#3-In(1)-In(3)#6	76.91(2)
In(3)#1-In(1)-In(3)#7	76.91(2)
In(5)-In(1)-In(3)#3	82.972(19)
In(5)-In(1)-In(3)#1	82.972(19)
In(5)-In(1)-In(3)#6	82.972(19)
In(5)-In(1)-In(3)#7	82.972(19)
Ir(1)#8-In(2)-Ir(1)	140.13(4)
Ir(1)#8-In(2)-In(2)#9	109.94(2)
Ir(1)-In(2)-In(2)#9	109.94(2)
Ir(1)-In(2)-In(3)#10	110.22(2)
Ir(1)#8-In(2)-In(3)#10	50.651(11)
Ir(1)-In(2)-In(3)#11	110.22(2)
Ir(1)#8-In(2)-In(3)#11	50.651(11)
Ir(1)#8-In(2)-In(3)#1	110.22(2)
Ir(1)#8-In(2)-In(3)#3	110.22(2)
Ir(1)-In(2)-In(3)#1	50.651(11)
Ir(1)-In(2)-In(3)#3	50.651(11)
Ir(1)-In(2)-In(4)	53.022(17)
Ir(1)#8-In(2)-In(4)#9	53.023(17)
Ir(1)#8-In(2)-In(4)	166.85(4)

Ir(1)-In(2)-In(4)#9	166.85(4)
Ir(1)#8-In(2)-In(5)#12	100.114(8)
Ir(1)-In(2)-In(5)#11	100.113(8)
Ir(1)#8-In(2)-In(5)#11	100.114(8)
Ir(1)-In(2)-In(5)#12	100.113(8)
In(3)#1-In(2)-In(2)#9	115.022(19)
In(3)#11-In(2)-In(2)#9	115.02(2)
In(3)#10-In(2)-In(2)#9	115.022(19)
In(3)#3-In(2)-In(2)#9	115.022(19)
In(3)#11-In(2)-In(3)#10	95.69(2)
In(3)#11-In(2)-In(3)#1	129.96(4)
In(3)#10-In(2)-In(3)#3	129.96(4)
In(3)#1-In(2)-In(3)#3	95.69(2)
In(3)#11-In(2)-In(3)#3	62.805(19)
In(3)#10-In(2)-In(3)#1	62.805(19)
In(4)#9-In(2)-In(2)#9	56.91(2)
In(4)-In(2)-In(2)#9	56.91(2)
In(4)-In(2)-In(3)#3	78.131(14)
In(4)#9-In(2)-In(3)#11	78.131(14)
In(4)-In(2)-In(3)#1	78.131(14)
In(4)-In(2)-In(3)#10	131.871(10)
In(4)#9-In(2)-In(3)#3	131.871(10)
In(4)#9-In(2)-In(3)#10	78.131(14)
In(4)#9-In(2)-In(3)#1	131.871(10)
In(4)-In(2)-In(3)#11	131.871(10)
In(4)-In(2)-In(4)#9	113.83(4)
In(4)#9-In(2)-In(5)#11	73.672(17)
In(4)-In(2)-In(5)#11	73.672(17)
In(4)-In(2)-In(5)#12	73.672(17)
In(4)#9-In(2)-In(5)#12	73.672(17)
In(5)#12-In(2)-In(2)#9	59.003(19)
In(5)#11-In(2)-In(2)#9	59.003(19)
In(5)#11-In(2)-In(3)#3	65.313(16)
In(5)#12-In(2)-In(3)#11	148.574(10)
In(5)#11-In(2)-In(3)#10	148.574(10)
In(5)#11-In(2)-In(3)#11	65.313(16)

In(5)#12-In(2)-In(3)#1	65.313(15)
In(5)#11-In(2)-In(3)#1	148.573(10)
In(5)#12-In(2)-In(3)#3	148.574(10)
In(5)#12-In(2)-In(3)#10	65.313(15)
In(5)#11-In(2)-In(5)#12	118.01(4)
Ir(1)#13-In(3)-Ir(1)	147.55(2)
Ir(1)-In(3)-In(1)#13	129.06(2)
Ir(1)#13-In(3)-In(1)#13	55.301(16)
Ir(1)-In(3)-In(2)#13	95.217(17)
Ir(1)#13-In(3)-In(2)#13	54.412(11)
Ir(1)#13-In(3)-In(3)#13	54.296(18)
Ir(1)-In(3)-In(3)#1	54.145(17)
Ir(1)-In(3)-In(3)#13	132.00(2)
Ir(1)#13-In(3)-In(3)#1	134.24(2)
Ir(1)#13-In(3)-In(4)	146.59(3)
Ir(1)-In(3)-In(4)	51.336(17)
Ir(1)-In(3)-S(1)	108.149(17)
Ir(1)#13-In(3)-S(1)	104.214(18)
In(1)#13-In(3)-In(2)#13	68.03(2)
In(1)#13-In(3)-In(4)	91.36(2)
In(3)#13-In(3)-In(1)#13	98.63(3)
In(3)#1-In(3)-In(1)#13	161.73(3)
In(3)#13-In(3)-In(2)#13	98.44(2)
In(3)#1-In(3)-In(2)#13	129.99(3)
In(3)#13-In(3)-In(3)#1	82.737(14)
In(3)#13-In(3)-In(4)	146.30(2)
In(3)#1-In(3)-In(4)	78.27(2)
In(4)-In(3)-In(2)#13	115.11(2)
S(1)-In(3)-In(1)#13	85.83(2)
S(1)-In(3)-In(2)#13	152.58(2)
S(1)-In(3)-In(3)#13	76.718(16)
S(1)-In(3)-In(3)#1	76.718(16)
S(1)-In(3)-In(4)	71.993(15)
Ir(1)-In(4)-Ir(1)#14	177.89(5)
Ir(1)-In(4)-In(2)#9	124.14(4)
Ir(1)#14-In(4)-In(2)	124.14(4)

Ir(1)-In(4)-In(2)	57.97(2)
Ir(1)#14-In(4)-In(2)#9	57.97(2)
Ir(1)-In(4)-In(3)#15	126.29(3)
Ir(1)#14-In(4)-In(3)#2	126.29(3)
Ir(1)-In(4)-In(3)#2	52.128(15)
Ir(1)#14-In(4)-In(3)	126.29(3)
Ir(1)-In(4)-In(3)	52.128(15)
Ir(1)-In(4)-In(3)#14	126.29(3)
Ir(1)#14-In(4)-In(3)#15	52.129(15)
Ir(1)#14-In(4)-In(3)#14	52.129(15)
In(2)-In(4)-In(2)#9	66.17(4)
In(2)-In(4)-In(3)#15	146.186(18)
In(2)-In(4)-In(3)#14	146.186(18)
In(2)#9-In(4)-In(3)#14	99.93(2)
In(2)#9-In(4)-In(3)#15	99.93(2)
In(2)-In(4)-In(3)#2	99.93(2)
In(2)-In(4)-In(3)	99.93(2)
In(2)#9-In(4)-In(3)	146.186(18)
In(2)#9-In(4)-In(3)#2	146.186(18)
In(3)#15-In(4)-In(3)	106.44(4)
In(3)#14-In(4)-In(3)	74.17(3)
In(3)#15-In(4)-In(3)#2	74.17(3)
In(3)#15-In(4)-In(3)#14	63.63(2)
In(3)-In(4)-In(3)#2	63.62(2)
In(3)#14-In(4)-In(3)#2	106.44(4)
Ir(1)-In(5)-Ir(1)#4	113.93(4)
Ir(1)-In(5)-In(2)#16	154.03(3)
Ir(1)#4-In(5)-In(2)#16	92.04(2)
Ir(1)#4-In(5)-In(2)#13	154.03(3)
Ir(1)-In(5)-In(2)#13	92.04(2)
In(1)-In(5)-Ir(1)#4	56.97(2)
In(1)-In(5)-Ir(1)	56.97(2)
In(1)-In(5)-In(2)#13	149.00(2)
In(1)-In(5)-In(2)#16	149.00(2)
In(2)#13-In(5)-In(2)#16	61.99(4)
In(3)#14-S(1)-In(3)#18	92.21(3)

In(3)#17-S(1)-In(3)	92.21(3)
In(3)#18-S(1)-In(3)	180.0
In(3)#17-S(1)-In(3)#18	87.79(3)
In(3)#14-S(1)-In(3)#17	180.0
In(3)#14-S(1)-In(3)	87.79(3)

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Symmetry transformations used to generate equivalent atoms:

(1)  $x-1/2, -y+3/2, -z+3/2$  (2)  $-y+3/2, x-1/2, -z+3/2$  (3)  $y, x, z$  (4)  $x, y, -z+1$  (5)  $-x+1, -y+1, -z+1$  (6)  $-y+3/2, x-1/2, z-1/2$  (7)  $x-1/2, -y+3/2, z-1/2$  (8)  $-x+1, -y+1, z$  (9)  $-x+1, -y+1, -z+2$  (10)  $y-1/2, -x+3/2, -z+3/2$  (11)  $-x+3/2, y-1/2, -z+3/2$  (12)  $-y+3/2, x-1/2, z+1/2$  (13)  $y+1/2, -x+3/2, -z+3/2$  (14)  $x, y, -z+2$  (15)  $y, x, -z+2$  (16)  $-y+3/2, x+1/2, z-1/2$  (17)  $-x+2, -y+1, -z+2$  (18)  $-x+2, -y+1, z$

**Table S5.** Atomic coordinates ( $\times 10^4$ ) and equivalent isotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{Se}$  at 299 K with estimated standard deviations in parentheses.

Label	x	y	z	Occupancy	$U_{eq}^*$
Ir(1)	6863(1)	6863(1)	2405(1)	1	4(1)
In(1)	5953(1)	5953(1)	0	1	13(1)
In(2)	5000	5000	3367(1)	1	12(1)
In(3)	4463(1)	7948(1)	2025(1)	1	15(1)
In(4)	6877(1)	6877(1)	5000	1	19(1)
In(5)	7986(1)	7986(1)	0	1	34(1)
Se(1)	5000	10000	0	1	34(1)

\*  $U_{eq}$  is defined as one third of the trace of the orthogonalized  $U_{ij}$  tensor.

**Table S6.** Anisotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{Se}$  at 299 K with estimated standard deviations in parentheses.

Label	$U_{11}$	$U_{22}$	$U_{33}$	$U_{12}$	$U_{13}$	$U_{23}$
Ir(1)	5(1)	5(1)	4(1)	0(1)	0(1)	0(1)
In(1)	17(1)	17(1)	5(1)	-8(1)	0	0
In(2)	12(1)	12(1)	12(1)	-6(1)	0	0
In(3)	5(1)	15(1)	24(1)	3(1)	1(1)	2(1)
In(4)	28(1)	28(1)	3(1)	-13(1)	0	0
In(5)	47(1)	47(1)	6(1)	-39(1)	0	0
Se(1)	81(2)	12(1)	9(1)	-15(1)	0	0

The anisotropic displacement factor exponent takes the form:  $-2\pi^2[h^2a^2U_{11} + \dots + 2hka^*b^*U_{12}]$ .

**Table S7.** Bond lengths [ $\text{\AA}$ ] for  $\text{Ir}_2\text{In}_8\text{Se}$  at 299 K with estimated standard deviations in parentheses.

Label	Distances
Ir(1)-In(1)	2.7478(6)
Ir(1)-In(2)	2.7947(5)
Ir(1)-In(3)#1	2.6558(6)
Ir(1)-In(3)#2	2.6472(5)
Ir(1)-In(3)	2.6472(5)
Ir(1)-In(3)#3	2.6558(6)
Ir(1)-In(4)	2.6230(4)
Ir(1)-In(5)	2.8997(7)
In(1)-Ir(1)#4	2.7478(6)
In(1)-In(1)#5	2.6806(18)
In(1)-In(3)#4	3.2131(6)
In(1)-In(3)#2	3.2131(6)
In(1)-In(3)#6	3.2131(6)
In(1)-In(3)	3.2131(6)
In(1)-In(5)	2.8594(14)
In(2)-Ir(1)#7	2.7947(5)
In(2)-In(2)#8	3.3008(19)
In(2)-In(3)	3.2744(7)
In(2)-In(3)#2	3.2744(7)
In(2)-In(3)#9	3.2744(7)
In(2)-In(3)#7	3.2744(7)
In(2)-In(4)	3.1133(10)
In(2)-In(4)#8	3.1133(10)
In(2)-In(5)#10	3.2781(11)
In(2)-In(5)#11	3.2781(11)
In(3)-Ir(1)#11	2.6559(6)
In(3)-In(3)#1	3.1332(8)
In(3)-In(3)#11	3.1333(8)
In(3)-In(4)#11	3.2919(8)
In(3)-Se(1)	2.9394(6)
In(4)-Ir(1)#12	2.6230(4)
In(4)-In(2)#8	3.1133(10)
In(4)-In(3)#13	3.2919(8)

In(4)-In(3)#1	3.2919(8)
In(4)-In(3)#14	3.2919(8)
In(4)-In(3)#3	3.2919(8)
In(5)-Ir(1)#4	2.8997(7)
In(5)-In(2)#15	3.2780(11)
In(5)-In(2)#16	3.2780(11)
Se(1)-In(3)#4	2.9394(6)
Se(1)-In(3)#17	2.9394(6)
Se(1)-In(3)#18	2.9394(6)

Symmetry transformations used to generate equivalent atoms:

(1) y,x,z (2) x+1/2,-y+3/2,-z+1/2 (3) -y+3/2,x+1/2,-z+1/2 (4) x,y,-z (5) -x+1,-y+1,-z (6) y,x,-z  
 (7) -x+1,-y+1,z (8) -x+1,-y+1,-z+1 (9) -y+1,-x+1,z (10) -y+3/2,x-1/2,z+1/2 (11) y-1/2,-x+3/2,-z+1/2  
 (12) x,y,-z+1 (13) x+1/2,-y+3/2,z+1/2 (14) -y+3/2,x+1/2,z+1/2 (15) y+1/2,-x+3/2,-z+1/2  
 (16) -y+3/2,x+1/2,z-1/2 (17) -x+1,-y+2,-z (18) -x+1,-y+2,z

**Table S8.** Bond angles [°] for Ir<sub>2</sub>In<sub>8</sub>Se at 299 K with estimated standard deviations in parentheses.

Label	Angles
In(1)-Ir(1)-In(2)	82.61(3)
In(1)-Ir(1)-In(5)	60.77(3)
In(2)-Ir(1)-In(5)	143.37(3)
In(3)#2-Ir(1)-In(1)	73.080(13)
In(3)#3-Ir(1)-In(1)	122.390(17)
In(3)#1-Ir(1)-In(1)	122.390(17)
In(3)-Ir(1)-In(1)	73.080(13)
In(3)#1-Ir(1)-In(2)	128.092(17)
In(3)-Ir(1)-In(2)	73.929(13)
In(3)#3-Ir(1)-In(2)	128.092(17)
In(3)#2-Ir(1)-In(2)	73.929(13)
In(3)-Ir(1)-In(3)#2	135.57(2)
In(3)#2-Ir(1)-In(3)#1	151.690(10)
In(3)-Ir(1)-In(3)#1	72.43(2)
In(3)#1-Ir(1)-In(3)#3	79.36(2)
In(3)#2-Ir(1)-In(3)#3	72.43(2)
In(3)-Ir(1)-In(3)#3	151.690(10)
In(3)#3-Ir(1)-In(5)	77.256(19)
In(3)#2-Ir(1)-In(5)	93.928(15)
In(3)#1-Ir(1)-In(5)	77.256(19)
In(3)-Ir(1)-In(5)	93.928(15)
In(4)-Ir(1)-In(1)	152.68(3)
In(4)-Ir(1)-In(2)	70.07(3)
In(4)-Ir(1)-In(3)	98.497(15)
In(4)-Ir(1)-In(3)#2	98.497(15)
In(4)-Ir(1)-In(3)#3	77.16(2)
In(4)-Ir(1)-In(3)#1	77.16(2)
In(4)-Ir(1)-In(5)	146.56(3)
Ir(1)#4-In(1)-Ir(1)	124.49(4)
Ir(1)-In(1)-In(3)#4	120.82(2)
Ir(1)#4-In(1)-In(3)#2	120.82(2)
Ir(1)-In(1)-In(3)	52.018(11)
Ir(1)#4-In(1)-In(3)#4	52.018(11)

Ir(1)-In(1)-In(3)#2	52.018(11)
Ir(1)-In(1)-In(3)#6	120.82(2)
Ir(1)#4-In(1)-In(3)	120.82(2)
Ir(1)#4-In(1)-In(3)#6	52.018(11)
Ir(1)#4-In(1)-In(5)	62.243(18)
Ir(1)-In(1)-In(5)	62.243(18)
In(1)#5-In(1)-Ir(1)	117.757(18)
In(1)#5-In(1)-Ir(1)#4	117.757(18)
In(1)#5-In(1)-In(3)#4	96.351(18)
In(1)#5-In(1)-In(3)#6	96.351(18)
In(1)#5-In(1)-In(3)	96.352(18)
In(1)#5-In(1)-In(3)#2	96.351(18)
In(1)#5-In(1)-In(5)	180.00(4)
In(3)#2-In(1)-In(3)#4	167.30(4)
In(3)-In(1)-In(3)#4	79.17(2)
In(3)#2-In(1)-In(3)#6	79.17(2)
In(3)-In(1)-In(3)#6	167.30(4)
In(3)-In(1)-In(3)#2	99.41(2)
In(3)#4-In(1)-In(3)#6	99.41(2)
In(5)-In(1)-In(3)	83.648(18)
In(5)-In(1)-In(3)#6	83.649(18)
In(5)-In(1)-In(3)#2	83.649(18)
In(5)-In(1)-In(3)#4	83.649(18)
Ir(1)#7-In(2)-Ir(1)	139.27(4)
Ir(1)-In(2)-In(2)#8	110.365(19)
Ir(1)#7-In(2)-In(2)#8	110.365(18)
Ir(1)-In(2)-In(3)#2	50.973(10)
Ir(1)-In(2)-In(3)#7	109.96(2)
Ir(1)-In(2)-In(3)#9	109.96(2)
Ir(1)#7-In(2)-In(3)	109.96(2)
Ir(1)#7-In(2)-In(3)#7	50.972(10)
Ir(1)#7-In(2)-In(3)#2	109.96(2)
Ir(1)-In(2)-In(3)	50.972(10)
Ir(1)#7-In(2)-In(3)#9	50.972(10)
Ir(1)#7-In(2)-In(4)	168.35(3)
Ir(1)#7-In(2)-In(4)#8	52.377(14)

Ir(1)-In(2)-In(4)	52.377(14)
Ir(1)-In(2)-In(4)#8	168.35(3)
Ir(1)#7-In(2)-In(5)#11	100.091(7)
Ir(1)#7-In(2)-In(5)#10	100.091(6)
Ir(1)-In(2)-In(5)#10	100.090(7)
Ir(1)-In(2)-In(5)#11	100.090(7)
In(3)#2-In(2)-In(2)#8	114.478(18)
In(3)#7-In(2)-In(2)#8	114.478(18)
In(3)#9-In(2)-In(2)#8	114.478(17)
In(3)-In(2)-In(2)#8	114.478(18)
In(3)#9-In(2)-In(3)#7	96.91(2)
In(3)-In(2)-In(3)#2	96.91(2)
In(3)-In(2)-In(3)#7	131.04(4)
In(3)#9-In(2)-In(3)#2	131.04(4)
In(3)#7-In(2)-In(3)#2	62.379(17)
In(3)-In(2)-In(3)#9	62.380(17)
In(3)#2-In(2)-In(5)#10	64.021(13)
In(3)#9-In(2)-In(5)#10	148.787(9)
In(3)#2-In(2)-In(5)#11	148.787(9)
In(3)#7-In(2)-In(5)#10	64.021(13)
In(3)#9-In(2)-In(5)#11	64.021(13)
In(3)-In(2)-In(5)#10	148.787(9)
In(3)-In(2)-In(5)#11	64.021(13)
In(3)#7-In(2)-In(5)#11	148.787(9)
In(4)#8-In(2)-In(2)#8	57.988(18)
In(4)-In(2)-In(2)#8	57.988(18)
In(4)#8-In(2)-In(3)#2	131.206(9)
In(4)#8-In(2)-In(3)	131.206(9)
In(4)#8-In(2)-In(3)#7	77.321(12)
In(4)-In(2)-In(3)#2	77.322(12)
In(4)-In(2)-In(3)#9	131.206(9)
In(4)-In(2)-In(3)#7	131.206(9)
In(4)#8-In(2)-In(3)#9	77.321(12)
In(4)-In(2)-In(3)	77.321(12)
In(4)-In(2)-In(4)#8	115.98(4)
In(4)#8-In(2)-In(5)#10	74.521(15)

In(4)-In(2)-In(5)#11	74.521(15)
In(4)#8-In(2)-In(5)#11	74.521(15)
In(4)-In(2)-In(5)#10	74.521(15)
In(5)#10-In(2)-In(2)#8	59.771(17)
In(5)#11-In(2)-In(2)#8	59.771(17)
In(5)#11-In(2)-In(5)#10	119.54(3)
Ir(1)-In(3)-Ir(1)#11	151.06(2)
Ir(1)-In(3)-In(1)	54.903(14)
Ir(1)#11-In(3)-In(1)	129.10(2)
Ir(1)-In(3)-In(2)	55.099(10)
Ir(1)#11-In(3)-In(2)	97.600(16)
Ir(1)#11-In(3)-In(3)#11	53.655(16)
Ir(1)#11-In(3)-In(3)#1	134.39(2)
Ir(1)-In(3)-In(3)#11	136.39(2)
Ir(1)-In(3)-In(3)#1	53.911(17)
Ir(1)-In(3)-In(4)#11	144.70(2)
Ir(1)#11-In(3)-In(4)#11	50.974(15)
Ir(1)-In(3)-Se(1)	102.733(16)
Ir(1)#11-In(3)-Se(1)	106.180(16)
In(1)-In(3)-In(2)	68.65(2)
In(1)-In(3)-In(4)#11	89.80(2)
In(2)-In(3)-In(4)#11	115.614(19)
In(3)#1-In(3)-In(1)	96.51(2)
In(3)#11-In(3)-In(1)	157.55(3)
In(3)#11-In(3)-In(2)	133.40(3)
In(3)#1-In(3)-In(2)	99.77(2)
In(3)#1-In(3)-In(3)#11	84.617(11)
In(3)#1-In(3)-In(4)#11	143.80(2)
In(3)#11-In(3)-In(4)#11	76.79(2)
Se(1)-In(3)-In(1)	84.323(18)
Se(1)-In(3)-In(2)	151.71(2)
Se(1)-In(3)-In(3)#1	74.358(14)
Se(1)-In(3)-In(3)#11	74.357(14)
Se(1)-In(3)-In(4)#11	70.854(13)
Ir(1)-In(4)-Ir(1)#12	179.13(5)
Ir(1)-In(4)-In(2)#8	121.58(4)

Ir(1)-In(4)-In(2)	57.55(2)
Ir(1)#12-In(4)-In(2)	121.58(4)
Ir(1)#12-In(4)-In(2)#8	57.55(2)
Ir(1)-In(4)-In(3)#3	51.867(14)
Ir(1)#12-In(4)-In(3)#13	51.868(14)
Ir(1)-In(4)-In(3)#13	128.79(3)
Ir(1)#12-In(4)-In(3)#14	51.868(14)
Ir(1)-In(4)-In(3)#14	128.79(3)
Ir(1)#12-In(4)-In(3)#1	128.79(3)
Ir(1)#12-In(4)-In(3)#3	128.79(3)
Ir(1)-In(4)-In(3)#1	51.867(14)
In(2)-In(4)-In(2)#8	64.03(4)
In(2)-In(4)-In(3)#13	146.076(18)
In(2)-In(4)-In(3)#14	146.076(18)
In(2)#8-In(4)-In(3)#14	99.809(18)
In(2)#8-In(4)-In(3)#13	99.809(18)
In(2)-In(4)-In(3)#1	99.809(17)
In(2)-In(4)-In(3)#3	99.809(17)
In(2)#8-In(4)-In(3)#3	146.076(18)
In(2)#8-In(4)-In(3)#1	146.076(18)
In(3)#13-In(4)-In(3)#3	76.92(3)
In(3)#14-In(4)-In(3)#3	107.72(3)
In(3)#13-In(4)-In(3)#1	107.72(3)
In(3)#13-In(4)-In(3)#14	62.01(2)
In(3)#3-In(4)-In(3)#1	62.01(2)
In(3)#14-In(4)-In(3)#1	76.92(3)
Ir(1)-In(5)-Ir(1)#4	113.98(4)
Ir(1)-In(5)-In(2)#16	153.24(3)
Ir(1)#4-In(5)-In(2)#16	92.780(19)
Ir(1)#4-In(5)-In(2)#15	153.24(3)
Ir(1)-In(5)-In(2)#15	92.779(19)
In(1)-In(5)-Ir(1)#4	56.990(19)
In(1)-In(5)-Ir(1)	56.991(19)
In(1)-In(5)-In(2)#15	149.770(17)
In(1)-In(5)-In(2)#16	149.770(17)
In(2)#15-In(5)-In(2)#16	60.46(3)

In(3)#4-Se(1)-In(3)	88.30(2)
In(3)#17-Se(1)-In(3)#18	88.30(2)
In(3)-Se(1)-In(3)#18	180.0
In(3)#17-Se(1)-In(3)	91.70(2)
In(3)#4-Se(1)-In(3)#17	180.000(15)
In(3)#4-Se(1)-In(3)#18	91.70(2)

Symmetry transformations used to generate equivalent atoms:

(1) y,x,z (2) x+1/2,-y+3/2,-z+1/2 (3) -y+3/2,x+1/2,-z+1/2 (4) x,y,-z (5) -x+1,-y+1,-z (6) y,x,-z  
 (7) -x+1,-y+1,z (8) -x+1,-y+1,-z+1 (9) -y+1,-x+1,z (10) -y+3/2,x-1/2,z+1/2 (11) y-1/2,-x+3/2,-z+1/2  
 (12) x,y,-z+1 (13) x+1/2,-y+3/2,z+1/2 (14) -y+3/2,x+1/2,z+1/2 (15) y+1/2,-x+3/2,-z+1/2  
 (16) -y+3/2,x+1/2,z-1/2 (17) -x+1,-y+2,-z (18) -x+1,-y+2,z

**Table S9.** Atomic coordinates ( $\times 10^4$ ) and equivalent isotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{Te}$  at 299 K with estimated standard deviations in parentheses.

Label	x	y	z	Occupancy	$U_{eq}^*$
Ir(1)	6844(1)	3156(1)	7582(1)	1	5(1)
In(2)	5000	5000	6598(1)	1	12(1)
Te(1)	10000	5000	10000	1	20(1)
In(3)	7895(1)	5557(1)	7884(1)	1	16(1)
In(1)	5947(1)	4053(1)	10000	1	14(1)
In(4)	6920(1)	3080(1)	5000	1	18(1)
In(5)	7962(1)	2038(1)	10000	1	23(1)

\*  $U_{eq}$  is defined as one third of the trace of the orthogonalized  $U_{ij}$  tensor.

**Table S10.** Anisotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{Te}$  at 299 K with estimated standard deviations in parentheses.

Label	$U_{11}$	$U_{22}$	$U_{33}$	$U_{12}$	$U_{13}$	$U_{23}$
Ir(1)	4(1)	4(1)	6(1)	0(1)	0(1)	0(1)
In(2)	11(1)	11(1)	15(1)	5(1)	0	0
Te(1)	10(1)	38(1)	11(1)	7(1)	0	0
In(3)	14(1)	5(1)	28(1)	-2(1)	-4(1)	1(1)
In(1)	17(1)	17(1)	8(1)	9(1)	0	0
In(4)	23(1)	23(1)	6(1)	8(1)	0	0
In(5)	29(1)	29(1)	11(1)	21(1)	0	0

The anisotropic displacement factor exponent takes the form:  $-2\pi^2[h^2a^*{}^2U_{11} + \dots + 2hka^*b^*U_{12}]$ .

**Table S11.** Bond lengths [ $\text{\AA}$ ] for  $\text{Ir}_2\text{In}_8\text{Te}$  at 299 K with estimated standard deviations in parentheses.

Label	Distances
Ir(1)-In(2)	2.827(2)
Ir(1)-In(3)	2.672(2)
Ir(1)-In(3)#1	2.688(2)
Ir(1)-In(3)#2	2.672(2)
Ir(1)-In(3)#3	2.688(2)
Ir(1)-In(1)	2.8002(19)
Ir(1)-In(4)	2.659(2)
Ir(1)-In(5)	2.9590(19)
In(2)-Ir(1)#4	2.827(2)
In(2)-In(2)#5	3.289(3)
In(2)-In(3)	3.265(2)
In(2)-In(3)#6	3.265(2)
In(2)-In(3)#4	3.265(2)
In(2)-In(3)#2	3.265(2)
In(2)-In(4)#5	3.203(2)
In(2)-In(4)	3.203(2)
In(2)-In(5)#7	3.349(2)
In(2)-In(5)#8	3.349(2)
Te(1)-In(3)#9	3.0982(18)
Te(1)-In(3)#10	3.0982(18)
Te(1)-In(3)	3.0982(18)
Te(1)-In(3)#11	3.0982(18)
In(3)-Ir(1)#8	2.688(2)
In(3)-In(3)#8	3.215(2)
In(3)-In(3)#6	3.348(3)
In(3)-In(3)#3	3.215(2)
In(3)-In(1)	3.3091(19)
In(3)-In(4)#8	3.362(2)
In(1)-Ir(1)#9	2.8002(19)
In(1)-In(3)#2	3.3091(19)
In(1)-In(3)#12	3.3091(19)
In(1)-In(3)#9	3.3091(19)
In(1)-In(1)#13	2.712(3)

In(1)-In(5)	2.885(3)
In(4)-Ir(1)#14	2.659(2)
In(4)-In(2)#5	3.203(2)
In(4)-In(3)#15	3.362(2)
In(4)-In(3)#3	3.362(2)
In(4)-In(3)#16	3.362(2)
In(4)-In(3)#1	3.362(2)
In(5)-Ir(1)#9	2.9590(19)
In(5)-In(2)#17	3.349(2)
In(5)-In(2)#18	3.349(2)

Symmetry transformations used to generate equivalent atoms:

(1) -y+1,-x+1,z (2) -y+3/2,x-1/2,-z+3/2 (3) -x+3/2,y-1/2,-z+3/2 (4) -x+1,-y+1,z (5) -x+1,-y+1,-z+1 (6) y,x,z (7) -y+1/2,x-1/2,z-1/2 (8) y+1/2,-x+3/2,-z+3/2 (9) -x+2,-y+1,z (10) x,y,-z+2 (11) -x+2,-y+1,-z+2 (12) -y+1,-x+1,-z+2 (13) -x+1,-y+1,-z+2 (14) x,y,-z+1 (15) -y+3/2,x-1/2,z-1/2 (16) -x+3/2,y-1/2,z-1/2 (17) -y+3/2,x-1/2,z+1/2 (18) y+1/2,-x+1/2,-z+3/2

**Table S12.** Bond angles [°] for Ir<sub>2</sub>In<sub>8</sub>Te at 299 K with estimated standard deviations in parentheses.

Label	Angles
In(2)-Ir(1)-In(5)	143.74(2)
In(3)#2-Ir(1)-In(2)	72.790(14)
In(3)-Ir(1)-In(2)	72.789(14)
In(3)#3-Ir(1)-In(2)	130.34(2)
In(3)#1-Ir(1)-In(2)	130.34(2)
In(3)-Ir(1)-In(3)#1	150.733(9)
In(3)#1-Ir(1)-In(3)#3	77.05(2)
In(3)-Ir(1)-In(3)#3	73.74(2)
In(3)#2-Ir(1)-In(3)	135.36(2)
In(3)#2-Ir(1)-In(3)#3	150.732(9)
In(3)#2-Ir(1)-In(3)#1	73.74(2)
In(3)#1-Ir(1)-In(1)	120.521(18)
In(3)#3-Ir(1)-In(1)	120.521(18)
In(3)#2-Ir(1)-In(1)	74.383(12)
In(3)-Ir(1)-In(1)	74.381(12)
In(3)#2-Ir(1)-In(5)	95.61(2)
In(3)#1-Ir(1)-In(5)	74.81(4)
In(3)-Ir(1)-In(5)	95.61(2)
In(3)#3-Ir(1)-In(5)	74.81(4)
In(1)-Ir(1)-In(2)	83.69(5)
In(1)-Ir(1)-In(5)	60.05(6)
In(4)-Ir(1)-In(2)	71.35(3)
In(4)-Ir(1)-In(3)#1	77.92(2)
In(4)-Ir(1)-In(3)#2	97.528(15)
In(4)-Ir(1)-In(3)	97.529(15)
In(4)-Ir(1)-In(3)#3	77.92(2)
In(4)-Ir(1)-In(1)	155.04(4)
In(4)-Ir(1)-In(5)	144.91(4)
Ir(1)#4-In(2)-Ir(1)	138.04(5)
Ir(1)#4-In(2)-In(2)#5	110.98(3)
Ir(1)-In(2)-In(2)#5	110.98(3)
Ir(1)-In(2)-In(3)	51.404(13)
Ir(1)#4-In(2)-In(3)#4	51.403(13)

Ir(1)-In(2)-In(3)#2	51.403(13)
Ir(1)#4-In(2)-In(3)	109.48(3)
Ir(1)-In(2)-In(3)#4	109.49(3)
Ir(1)-In(2)-In(3)#6	109.49(3)
Ir(1)#4-In(2)-In(3)#6	51.403(13)
Ir(1)#4-In(2)-In(3)#2	109.49(3)
Ir(1)-In(2)-In(4)	51.88(5)
Ir(1)#4-In(2)-In(4)#5	51.88(5)
Ir(1)#4-In(2)-In(4)	170.08(3)
Ir(1)-In(2)-In(4)#5	170.08(3)
Ir(1)#4-In(2)-In(5)#8	100.13(2)
Ir(1)#4-In(2)-In(5)#7	100.13(2)
Ir(1)-In(2)-In(5)#8	100.13(2)
Ir(1)-In(2)-In(5)#7	100.13(2)
In(2)#5-In(2)-In(5)#7	60.59(3)
In(2)#5-In(2)-In(5)#8	60.59(3)
In(3)#2-In(2)-In(2)#5	113.91(3)
In(3)#4-In(2)-In(2)#5	113.91(3)
In(3)#6-In(2)-In(2)#5	113.91(3)
In(3)-In(2)-In(2)#5	113.91(3)
In(3)-In(2)-In(3)#4	132.18(6)
In(3)#6-In(2)-In(3)#2	132.18(6)
In(3)#6-In(2)-In(3)#4	98.38(3)
In(3)-In(2)-In(3)#2	98.38(3)
In(3)-In(2)-In(3)#6	61.69(2)
In(3)#4-In(2)-In(3)#2	61.69(2)
In(3)-In(2)-In(5)#7	149.134(11)
In(3)-In(2)-In(5)#8	62.59(4)
In(3)#2-In(2)-In(5)#7	62.59(4)
In(3)#4-In(2)-In(5)#8	149.133(11)
In(3)#4-In(2)-In(5)#7	62.59(4)
In(3)#6-In(2)-In(5)#8	62.59(4)
In(3)#6-In(2)-In(5)#7	149.133(11)
In(3)#2-In(2)-In(5)#8	149.133(11)
In(4)-In(2)-In(2)#5	59.10(3)
In(4)#5-In(2)-In(2)#5	59.10(3)

In(4)-In(2)-In(3)#4	130.396(15)
In(4)#5-In(2)-In(3)#2	130.396(14)
In(4)-In(2)-In(3)	76.60(4)
In(4)#5-In(2)-In(3)	130.396(15)
In(4)#5-In(2)-In(3)#4	76.60(4)
In(4)-In(2)-In(3)#6	130.396(15)
In(4)-In(2)-In(3)#2	76.60(4)
In(4)#5-In(2)-In(3)#6	76.60(4)
In(4)#5-In(2)-In(4)	118.20(6)
In(4)#5-In(2)-In(5)#8	75.39(3)
In(4)-In(2)-In(5)#7	75.39(3)
In(4)#5-In(2)-In(5)#7	75.39(3)
In(4)-In(2)-In(5)#8	75.39(3)
In(5)#7-In(2)-In(5)#8	121.18(6)
In(3)#10-Te(1)-In(3)	180.0
In(3)-Te(1)-In(3)#11	90.69(7)
In(3)#10-Te(1)-In(3)#9	90.69(7)
In(3)#9-Te(1)-In(3)#11	180.0
In(3)#10-Te(1)-In(3)#11	89.31(7)
In(3)-Te(1)-In(3)#9	89.31(7)
Ir(1)-In(3)-Ir(1)#8	155.37(2)
Ir(1)#8-In(3)-In(2)	100.653(18)
Ir(1)-In(3)-In(2)	55.807(10)
Ir(1)#8-In(3)-Te(1)	103.655(16)
Ir(1)-In(3)-Te(1)	100.969(15)
Ir(1)#8-In(3)-In(3)#3	136.77(2)
Ir(1)-In(3)-In(3)#3	53.361(16)
Ir(1)-In(3)-In(3)#8	138.47(2)
Ir(1)-In(3)-In(3)#6	111.195(11)
Ir(1)#8-In(3)-In(3)#6	51.475(10)
Ir(1)#8-In(3)-In(3)#8	52.901(16)
Ir(1)-In(3)-In(1)	54.58(4)
Ir(1)#8-In(3)-In(1)	128.79(2)
Ir(1)-In(3)-In(4)#8	142.08(3)
Ir(1)#8-In(3)-In(4)#8	50.67(4)
In(2)-In(3)-In(3)#6	59.156(10)

In(2)-In(3)-In(1)	69.64(5)
In(2)-In(3)-In(4)#8	116.34(3)
Te(1)-In(3)-In(2)	150.551(18)
Te(1)-In(3)-In(3)#3	71.65(4)
Te(1)-In(3)-In(3)#6	127.95(3)
Te(1)-In(3)-In(3)#8	71.65(4)
Te(1)-In(3)-In(1)	82.17(5)
Te(1)-In(3)-In(4)#8	69.19(4)
In(3)#8-In(3)-In(2)	137.45(4)
In(3)#3-In(3)-In(2)	101.13(2)
In(3)#8-In(3)-In(3)#3	86.533(11)
In(3)#8-In(3)-In(3)#6	104.357(10)
In(3)#3-In(3)-In(3)#6	159.562(17)
In(3)#3-In(3)-In(1)	93.82(3)
In(3)#8-In(3)-In(1)	152.31(3)
In(3)#8-In(3)-In(4)#8	75.07(4)
In(3)#3-In(3)-In(4)#8	140.248(19)
In(3)#6-In(3)-In(4)#8	60.138(18)
In(1)-In(3)-In(3)#6	84.483(16)
In(1)-In(3)-In(4)#8	87.52(6)
Ir(1)#9-In(1)-Ir(1)	125.41(6)
Ir(1)-In(1)-In(3)#9	122.73(4)
Ir(1)-In(1)-In(3)#12	122.73(4)
Ir(1)#9-In(1)-In(3)	122.73(4)
Ir(1)#9-In(1)-In(3)#2	122.73(4)
Ir(1)-In(1)-In(3)	51.03(3)
Ir(1)#9-In(1)-In(3)#9	51.03(3)
Ir(1)#9-In(1)-In(3)#12	51.03(3)
Ir(1)-In(1)-In(3)#2	51.03(3)
Ir(1)#9-In(1)-In(5)	62.71(3)
Ir(1)-In(1)-In(5)	62.71(3)
In(3)-In(1)-In(3)#12	168.97(3)
In(3)-In(1)-In(3)#9	82.30(7)
In(3)#2-In(1)-In(3)#12	82.30(7)
In(3)-In(1)-In(3)#2	96.63(6)
In(3)#9-In(1)-In(3)#12	96.63(6)

In(3)#9-In(1)-In(3)#2	168.96(3)
In(1)#13-In(1)-Ir(1)	117.29(3)
In(1)#13-In(1)-Ir(1)#9	117.29(3)
In(1)#13-In(1)-In(3)	95.518(16)
In(1)#13-In(1)-In(3)#12	95.517(16)
In(1)#13-In(1)-In(3)#9	95.518(16)
In(1)#13-In(1)-In(3)#2	95.517(16)
In(1)#13-In(1)-In(5)	180.0
In(5)-In(1)-In(3)#2	84.482(16)
In(5)-In(1)-In(3)	84.483(16)
In(5)-In(1)-In(3)#12	84.482(16)
In(5)-In(1)-In(3)#9	84.482(16)
Ir(1)-In(4)-Ir(1)#14	175.33(4)
Ir(1)#14-In(4)-In(2)	118.57(4)
Ir(1)-In(4)-In(2)	56.77(3)
Ir(1)#14-In(4)-In(2)#5	56.77(3)
Ir(1)-In(4)-In(2)#5	118.57(4)
Ir(1)#14-In(4)-In(3)#16	51.42(4)
Ir(1)#14-In(4)-In(3)#3	132.12(4)
Ir(1)#14-In(4)-In(3)#1	132.12(4)
Ir(1)-In(4)-In(3)#15	132.11(4)
Ir(1)-In(4)-In(3)#16	132.11(4)
Ir(1)-In(4)-In(3)#3	51.42(4)
Ir(1)#14-In(4)-In(3)#15	51.42(4)
Ir(1)-In(4)-In(3)#1	51.42(4)
In(2)-In(4)-In(2)#5	61.80(6)
In(2)-In(4)-In(3)#1	99.34(5)
In(2)-In(4)-In(3)#3	99.34(5)
In(2)-In(4)-In(3)#16	145.84(2)
In(2)#5-In(4)-In(3)#15	99.34(5)
In(2)#5-In(4)-In(3)#16	99.34(5)
In(2)#5-In(4)-In(3)#3	145.84(2)
In(2)-In(4)-In(3)#15	145.84(2)
In(2)#5-In(4)-In(3)#1	145.84(2)
In(3)#16-In(4)-In(3)#3	109.56(5)
In(3)#15-In(4)-In(3)#1	109.56(5)

In(3)#16-In(4)-In(3)#15	59.73(4)
In(3)#3-In(4)-In(3)#1	59.73(4)
In(3)#16-In(4)-In(3)#1	80.73(7)
In(3)#3-In(4)-In(3)#15	80.73(7)
Ir(1)#9-In(5)-Ir(1)	114.48(7)
Ir(1)-In(5)-In(2)#18	152.17(3)
Ir(1)#9-In(5)-In(2)#17	152.17(3)
Ir(1)-In(5)-In(2)#17	93.35(6)
Ir(1)#9-In(5)-In(2)#18	93.35(6)
In(2)#17-In(5)-In(2)#18	58.82(6)
In(1)-In(5)-Ir(1)#9	57.24(3)
In(1)-In(5)-Ir(1)	57.24(3)
In(1)-In(5)-In(2)#18	150.59(3)
In(1)-In(5)-In(2)#17	150.59(3)

Symmetry transformations used to generate equivalent atoms:

(1) -y+1,-x+1,z (2) -y+3/2,x-1/2,-z+3/2 (3) -x+3/2,y-1/2,-z+3/2 (4) -x+1,-y+1,z (5) -x+1,-y+1,-z+1 (6) y,x,z (7) -y+1/2,x-1/2,z-1/2 (8) y+1/2,-x+3/2,-z+3/2 (9) -x+2,-y+1,z (10) x,y,-z+2 (11) -x+2,-y+1,-z+2 (12) -y+1,-x+1,-z+2 (13) -x+1,-y+1,-z+2 (14) x,y,-z+1 (15) -y+3/2,x-1/2,z-1/2 (16) -x+3/2,y-1/2,z-1/2 (17) -y+3/2,x-1/2,z+1/2 (18) y+1/2,-x+1/2,-z+3/2

**Table S13.** Crystal data and structure refinement for Ir<sub>2</sub>In<sub>8</sub>Se at 120 K.

Empirical formula	Ir <sub>2</sub> In <sub>8</sub> Se
Formula weight	1382
Temperature	120 K
Wavelength	0.71073 Å
Crystal system	monoclinic
Space group	Pm(αβ0)0
Unit cell dimensions	a = 9.9200(6) Å, α = 90° b = 9.9262(6) Å, β = 90° c = 10.1092(6) Å, γ = 89.9995°
q-vector(1)	0.166667a* + 0.166667b* + 0.000000c*
Volume	995.43(10) Å <sup>3</sup>
Z	4
Density (calculated)	9.2213 g/cm <sup>3</sup>
Absorption coefficient	48.361 mm <sup>-1</sup>
F(000)	2320
Crystal size	0.278 x 0.246 x 0.225 mm <sup>3</sup>
θ range for data collection	3.78 to 29.98°
Index ranges	-14<=h<=12, -7<=k<=14, -14<=l<=11, -1<=m<=1
Reflections collected	13783
Independent reflections	9179 [R <sub>int</sub> = 0.095]
Completeness to θ = 22.14°	90%
Refinement method	Full-matrix least-squares on F <sup>2</sup>
Data / constrains / restraints / parameters	9179 / 3 / 0 / 669
Goodness-of-fit on F <sup>2</sup>	2.45
Final R indices [I>2σ(I)]	R <sub>obs</sub> = 0.0513, wR <sub>obs</sub> = 0.1085
R indices [all data]	R <sub>all</sub> = 0.0749, wR <sub>all</sub> = 0.1101
T <sub>min</sub> and T <sub>max</sub> coefficients	0.0927 and 0.5796
Largest diff. peak and hole	9.29 and -10.15 e·Å <sup>-3</sup>
<hr/>	
R = Σ  F <sub>o</sub>  - F <sub>c</sub>    / Σ F <sub>o</sub>  , wR = {Σ[w( F <sub>o</sub>   <sup>2</sup> -  F <sub>c</sub>   <sup>2</sup> ) <sup>2</sup> ] / Σ[w( F <sub>o</sub>   <sup>4</sup> )]} <sup>1/2</sup> and w=1/(σ <sup>2</sup> (I)+0.0004I <sup>2</sup> )	

**Table S14.** Atomic coordinates ( $\times 10^4$ ), occupancy and equivalent isotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{Se}$  at 120 K with estimated standard deviations in parentheses.

Label	x	y	z	Occupancy	$U_{eq}^*$
Ir(1)	1867(7)	1868(8)	2381(2)	1	4(1)
Ir(2)	-1865(7)	-1868(8)	-2418(2)	1	4(1)
Ir(3)	6860(7)	3138(8)	2587(2)	1	5(1)
Ir(4)	-6871(7)	-3141(8)	-2596(2)	1	6(1)
In(1)	5919(8)	4002(9)	5000	1	6(1)
In(2)	-5981(8)	-4075(9)	-5000	1	8(1)
In(3)	937(8)	933(9)	0	1	6(1)
In(4)	-979(8)	-966(9)	0	1	9(1)
In(5)	4979(7)	5003(9)	1644(2)	1	9(1)
In(6)	8169(8)	2156(9)	5000	1	12(1)
In(7)	-7814(8)	-1861(9)	-5000	1	10(1)
In(8)	2032(7)	4467(9)	2991(3)	1	8(1)
In(9)	-2063(7)	-4459(9)	-2964(2)	1	7(1)
In(10)	16(7)	10(9)	3405(2)	1	7(1)
In(11)	2949(7)	-543(9)	1955(2)	1	8(1)
In(12)	-2935(7)	538(8)	-2063(2)	1	9(1)
In(13)	4464(7)	2035(9)	2969(3)	1	9(1)
In(14)	-4458(7)	-2061(9)	-2998(3)	1	9(1)
In(15)	-522(7)	2949(9)	1970(3)	1	8(1)
In(16)	535(7)	-2949(9)	-2073(3)	1	8(1)
In(17)	1880(8)	1900(9)	5000	1	10(1)
In(18)	-1830(8)	-1876(9)	-5000	1	12(1)
In(19)	6859(8)	3118(9)	0	1	10(1)
In(20)	-6943(8)	-3183(9)	0	1	11(2)
In(21)	2968(8)	3003(9)	0	1	2(2)
In(22)	-3019(8)	-2979(10)	0	1	4(2)
Se(1)	5021(9)	-31(12)	0	1	2(2)
Se(2)	4763(9)	-42(10)	5000	1	15(2)
Se(3)	6(10)	5001(10)	0	1	1(2)
Se(4)	-72(9)	4750(11)	5000	1	14(2)

\*  $U_{eq}$  is defined as one third of the trace of the orthogonalized  $U_{ij}$  tensor.

**Table S15.** Anisotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{Se}$  at 120 K with estimated standard deviations in parentheses.

Label	U <sub>11</sub>	U <sub>22</sub>	U <sub>33</sub>	U <sub>12</sub>	U <sub>13</sub>	U <sub>23</sub>
Ir(1)	1(1)	5(1)	4(1)	7(1)	0(1)	2(1)
Ir(2)	2(1)	10(1)	2(1)	7(1)	-1(1)	1(1)
Ir(3)	3(1)	10(1)	2(1)	7(1)	0(1)	-2(1)
Ir(4)	4(1)	10(1)	4(1)	8(1)	0(1)	-1(1)
In(1)	0(2)	12(2)	6(2)	7(2)	0	0
In(2)	2(2)	12(2)	9(2)	4(2)	0	0
In(3)	9(2)	10(2)	0(2)	5(2)	0	0
In(4)	8(2)	18(2)	2(2)	-2(2)	0	0
In(5)	4(1)	15(2)	8(2)	11(1)	0(1)	-4(2)
In(6)	10(2)	23(2)	2(2)	10(2)	0	0
In(7)	9(2)	21(2)	-1(2)	8(2)	0	0
In(8)	6(2)	11(1)	9(2)	6(2)	0(1)	-1(2)
In(9)	7(2)	11(2)	4(2)	2(2)	1(1)	1(1)
In(10)	6(1)	11(2)	4(1)	6(1)	0(1)	-2(1)
In(11)	7(2)	8(1)	11(2)	8(2)	1(1)	2(1)
In(12)	5(2)	5(1)	16(2)	6(2)	0(1)	-1(1)
In(13)	1(1)	17(2)	10(2)	5(2)	-2(1)	2(2)
In(14)	0(1)	18(2)	8(2)	7(2)	1(1)	1(2)
In(15)	3(1)	11(2)	10(2)	10(1)	1(1)	2(1)
In(16)	6(1)	8(2)	11(2)	7(2)	0(1)	-2(1)
In(17)	10(2)	14(2)	5(2)	2(2)	0	0
In(18)	6(2)	12(2)	17(2)	-8(2)	0	0
In(19)	12(2)	22(2)	-5(2)	8(2)	0	0
In(20)	8(2)	21(2)	4(2)	5(2)	0	0
In(21)	-10(2)	1(2)	14(2)	6(2)	0	0
In(22)	-4(2)	8(3)	10(2)	5(2)	0	0
Se(1)	0(2)	-3(2)	8(2)	-1(2)	0	0
Se(2)	19(2)	19(3)	7(2)	12(2)	0	0
Se(3)	-13(2)	9(2)	8(2)	2(2)	0	0
Se(4)	7(2)	28(3)	6(2)	1(2)	0	0

**Table S16.** Crystal data and structure refinement for Ir<sub>2</sub>In<sub>8</sub>Te at 115 K.

Empirical formula	Ir <sub>2</sub> In <sub>8</sub> Te
Formula weight	1430.6
Temperature	115 K
Wavelength	0.71073 Å
Crystal system	monoclinic
Space group	Pm(αβ0)0
Unit cell dimensions	a = 10.005(4) Å, α = 90° b = 10.007(4) Å, β = 90° c = 10.196(4) Å, γ = 89.991(8)°
q-vector(1)	0.100000a* + -0.100000b* + 0.000000c*
Volume	1020.8(7) Å <sup>3</sup>
Z	4
Density (calculated)	9.3091 g/cm <sup>3</sup>
Absorption coefficient	46.397 mm <sup>-1</sup>
F(000)	2392
Crystal size	0.278 x 0.246 x 0.225 mm <sup>3</sup>
θ range for data collection	2 to 30.9°
Index ranges	-7<=h<=13, -8<=k<=14, -5<=l<=13, -1<=m<=1
Reflections collected	9321
Independent reflections	5402 [R <sub>int</sub> = 0.0509]
Completeness to θ = 20.59°	80%
Refinement method	Full-matrix least-squares on F <sup>2</sup>
Data / constrains / restraints / parameters	5402 / 3 / 0 / 667
Goodness-of-fit on F <sup>2</sup>	2.37
Final R indices [I>3σ(I)]	R <sub>obs</sub> = 0.0747, wR <sub>obs</sub> = 0.1218
R indices [all data]	R <sub>all</sub> = 0.1237, wR <sub>all</sub> = 0.1314
T <sub>min</sub> and T <sub>max</sub> coefficients	0.0101 and 0.1629
Largest diff. peak and hole	14.82 and -17.22 e·Å <sup>-3</sup>
$R = \Sigma   F_o -  F_c   / \Sigma  F_o , wR = \{\Sigma [w( F_o ^2 -  F_c ^2)^2] / \Sigma [w( F_o ^4)]\}^{1/2}$ and $w=1/(\sigma^2(I)+0.0004I^2)$	

**Table S17.** Atomic coordinates ( $\times 10^4$ ), occupancy and equivalent isotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{Te}$  at 115 K with estimated standard deviations in parentheses.

Label	x	y	z	Occupancy	$U_{eq}^*$
Ir(1)	83(12)	-5287(9)	2579(5)	1	13(2)
Ir(2)	-4907(13)	-6598(9)	2412(5)	1	12(2)
Ir(3)	-1222(12)	-298(10)	2422(4)	1	14(2)
Ir(4)	3771(12)	-1606(10)	2590(4)	1	13(2)
Te(1)	6884(16)	-3446(14)	0	1	4(3)
Te(2)	7040(20)	-3420(20)	5000	1	27(4)
In(1)	-5885(11)	-8993(10)	2076(8)	1	18(3)
Te(3)	1900(30)	-8445(17)	5000	1	34(4)
In(2)	6420(13)	-1324(12)	2152(7)	1	12(3)
In(3)	1957(16)	-3433(13)	1598(6)	1	16(3)
In(4)	1040(18)	-4435(16)	5000	1	16(4)
In(5)	-999(19)	-6440(17)	5000	1	27(5)
In(6)	1418(13)	-536(12)	2898(8)	1	15(3)
In(7)	-1206(17)	-369(16)	5000	1	13(4)
Te(4)	1949(19)	-8515(16)	0	1	13(3)
In(8)	4930(20)	-490(17)	5000	1	35(5)
In(9)	-4015(19)	-7519(15)	0	1	16(4)
In(10)	-3063(15)	-8435(13)	3411(6)	1	15(2)
In(11)	4892(16)	-3990(11)	2872(9)	1	17(3)
In(12)	2506(15)	-6333(13)	2906(8)	1	19(3)
In(13)	-4994(17)	-6542(16)	5000	1	11(4)
In(14)	2909(18)	-2517(15)	5000	1	12(4)
In(15)	-46(18)	-5375(16)	0	1	19(4)
In(16)	-2467(14)	-5537(13)	2073(9)	1	24(3)
In(17)	-2095(18)	-9403(16)	0	1	15(4)
In(18)	3835(18)	-1521(16)	0	1	15(4)
In(19)	13(16)	-11397(16)	0	1	14(4)
In(20)	-976(12)	-2886(13)	2880(8)	1	16(3)
In(21)	-5918(17)	-5488(16)	0	1	21(4)
In(22)	0(2000)	-10000(200)	2116(8)	1	16(3)

\* $U_{eq}$  is defined as one third of the trace of the orthogonalized  $U_{ij}$  tensor.

**Table S18.** Anisotropic displacement parameters ( $\text{\AA}^2 \times 10^3$ ) for  $\text{Ir}_2\text{In}_8\text{Te}$  at 115 K with estimated standard deviations in parentheses.

Label	U <sub>11</sub>	U <sub>22</sub>	U <sub>33</sub>	U <sub>12</sub>	U <sub>13</sub>	U <sub>23</sub>
Ir(1)	22(3)	5(3)	11(3)	10(3)	4(2)	3(2)
Ir(2)	27(4)	-2(2)	10(2)	8(2)	0(2)	0(2)
Ir(3)	23(4)	9(3)	12(3)	11(3)	2(2)	-8(2)
Ir(4)	21(3)	8(2)	11(2)	13(2)	9(2)	10(2)
Te(1)	-4(5)	5(5)	12(4)	0(4)	0	0
Te(2)	24(8)	43(8)	14(5)	-5(6)	0	0
In(1)	21(6)	11(4)	21(5)	5(5)	-4(4)	-1(4)
Te(3)	78(11)	8(6)	16(5)	-6(6)	0	0
In(2)	16(5)	6(4)	15(4)	9(4)	-1(3)	-7(3)
In(3)	29(5)	4(4)	16(4)	5(4)	6(5)	-4(4)
In(4)	23(9)	13(7)	11(6)	4(7)	0	0
In(5)	46(12)	25(8)	9(6)	-18(8)	0	0
In(6)	15(6)	9(5)	20(5)	12(4)	-2(4)	4(4)
In(7)	13(8)	1(6)	24(7)	8(6)	0	0
Te(4)	19(7)	10(6)	10(5)	2(5)	0	0
In(8)	86(13)	18(7)	2(6)	-49(8)	0	0
In(9)	31(9)	2(6)	14(6)	11(6)	0	0
In(10)	21(5)	12(4)	13(3)	6(4)	12(4)	-1(4)
In(11)	20(6)	12(5)	19(5)	6(5)	2(4)	-7(4)
In(12)	33(7)	13(5)	11(4)	9(5)	-8(4)	8(4)
In(13)	13(7)	16(7)	3(5)	4(7)	0	0
In(14)	26(9)	1(6)	10(6)	7(6)	0	0
In(15)	26(9)	12(7)	20(7)	-4(7)	0	0
In(16)	32(7)	6(4)	33(6)	7(5)	-11(5)	-4(4)
In(17)	14(8)	17(7)	13(7)	8(6)	0	0
In(18)	32(9)	10(6)	4(5)	7(7)	0	0
In(19)	16(7)	10(7)	16(6)	0(6)	0	0
In(20)	27(7)	0(4)	20(5)	6(4)	13(4)	-7(3)
In(21)	11(7)	31(9)	20(6)	2(6)	0	0
In(22)	27(6)	-3(4)	23(5)	6(4)	-11(4)	-5(3)

**Table S19.** Fermi velocity and tilt fit values for Ir<sub>2</sub>In<sub>8</sub>Se (A) and Ir<sub>2</sub>In<sub>8</sub>Te (B). All quantities are in units of 10<sup>5</sup> m/s. The reduced  $k$  coordinates denote the crossing.

<b>A</b>		Ir <sub>2</sub> In <sub>8</sub> Se	
$k = (0, 0, 0.225)$			
$\vec{w}_0$	$w_0^x$	$w_0^y$	$w_0^z$
	0.00	0.00	1.18918
$\vec{v}_F$	$v_F^x$	$v_F^y$	$v_F^z$
	0.31259	0.31259	0.86652
$k = (0, 0, 0.296)$			
$\vec{w}_0$	$w_0^x$	$w_0^y$	$w_0^z$
	0.00	0.00	1.02907
$\vec{v}_F$	$v_F^x$	$v_F^y$	$v_F^z$
	1.71689	1.71689	1.43972

<b>B</b>		Ir <sub>2</sub> In <sub>8</sub> Te	
$k = (0, 0, 0.188)$			
$\vec{w}_0$	$w_0^x$	$w_0^y$	$w_0^z$
	0.00	0.00	0.99534
$\vec{v}_F$	$v_F^x$	$v_F^y$	$v_F^z$
	0.35250	0.35250	0.61711
$k = (0, 0, 0.235)$			
$\vec{w}_0$	$w_0^x$	$w_0^y$	$w_0^z$
	0.00	0.00	2.14744
$\vec{v}_F$	$v_F^x$	$v_F^y$	$v_F^z$
	1.88943	1.88943	2.05040

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