

# Supporting Information

## Control of Droplet Evaporation on Oil-Coated Surfaces for the Synthesis of Asymmetric Supraparticles

*Aiting Gao,<sup>†</sup> Jie Liu,<sup>\*,†</sup> Lijun Ye,<sup>†</sup> Clarissa Schönecker,<sup>†,‡</sup> Michael Kappl,<sup>†</sup> Hans- Jürgen Butt<sup>†</sup>  
and Werner Steffen<sup>\*,†</sup>*

<sup>†</sup>Max Planck Institute for Polymer Research, Ackermannweg 10, D-55128, Mainz, Germany

<sup>‡</sup>TU Kaiserslautern, Group for Micro Fluid Mechanics, Gottlieb-Daimler-Straße 49, 67663  
Kaiserslautern, Germany

\* Correspondence and requests for materials should be addressed to J. L. and W. S. (E-mail:  
liujie@mpip-mainz.mpg.de; steffen@mpip-mainz.mpg.de)

Pages: 11

Figures: 8

## 1. Evaporation on oil-coated substrate

For a droplet with a defined volume depositing on the substrate, the evaporation rate can be obtained from the loss of volume through a liquid-air interface:<sup>1-3</sup>

$$\frac{dV}{dt} = -\frac{D}{\rho} \int \nabla C \cdot dS \quad (S1)$$

Here,  $D$  is the diffusion coefficient of the vapour and  $\rho$  is the density of liquid. On oil-coated hydrophobic surface, we assume the evaporation process of the sessile droplet in a constant contact angle mode:

$$\frac{dV}{dt} = -\frac{\pi R D (c_s - c_\infty)}{\rho} \frac{g(\theta)}{(1 + \cos \theta)^2} \quad (S2)$$

$(c_s - c_\infty)/R$  is the vapour concentration gradient from the droplet to the atmosphere through the liquid-air interface of the droplet.  $\theta$  is the contact angle at the droplet base line.  $g(\theta)$  is defined by

$$g(\theta) = (1 + \cos \theta)^2 \left\{ \tan \frac{\theta}{2} + 8 \int_0^\infty \frac{\cosh^2 \theta \tau}{\sinh 2\pi \tau} \tanh[\tau(\pi - \theta)] d\tau \right\}.$$

$$\frac{dV}{dt} = -\lambda h(z) f(\theta_z) \quad (S3)$$

$$\text{Here, } \lambda = \pi D (c_s - c_\infty) / \rho, f(\theta) = \frac{g(\theta_z)}{(1 - \cos \theta_z)(1 + \cos \theta_z)^2}, h(z) = R(1 - \cos \theta_z).$$

Jian *et al.*<sup>2</sup> have reported on slippery liquid-infused surface (SLIPS), the droplet evaporation meet the equation of (the constant contact angle):

$$\frac{dV}{dt} = -\lambda h_0 \quad (S4)$$

Here,  $h_0 = h(z = 0)$ , and  $h_0$  is the initial height of the sitting droplet. For droplet evaporation on an oil-coated hydrophobic substrate, oil forms a wetting ridge around the droplet. As the evaporation only happens above the height of wetting ridge ( $h_s$ ), the evaporation of droplet on the oil-coated surface was reduced with a factor of  $[1 - h_s/h_0]$ ,

$$\frac{dV}{dt} = -\lambda h_0 \left[1 - \frac{h_s}{h_0}\right] \quad (\text{S5})$$

Equation 4 can be rewritten as

$$\frac{dV}{dt} = -\lambda h_s f(\theta_s) \quad (\text{S6})$$

$$V(t)^{2/3} \approx V_i^{2/3} - \frac{4\lambda}{3} \left[ \frac{3}{\pi \beta(\theta_0)} \right]^{1/3} f(\theta_s) t \quad (\text{S7})$$

Here,  $V(z) = \frac{\pi}{3} R^3 \beta(\theta_z)$ ,  $\beta(\theta_z) = (1 - \cos \theta_z)^2 (2 + \cos \theta_z)$ .

In Figure S2b, the evaporation curves of droplets evaporate on oil-coated surface shows a largely delay compared with that on bare glass surface, indicating the evaporation is reduced by the oil film;  $V(t)^{2/3}$  varies linearly with the evaporation time  $t$  on both oil-coated substrate and glass substrate.

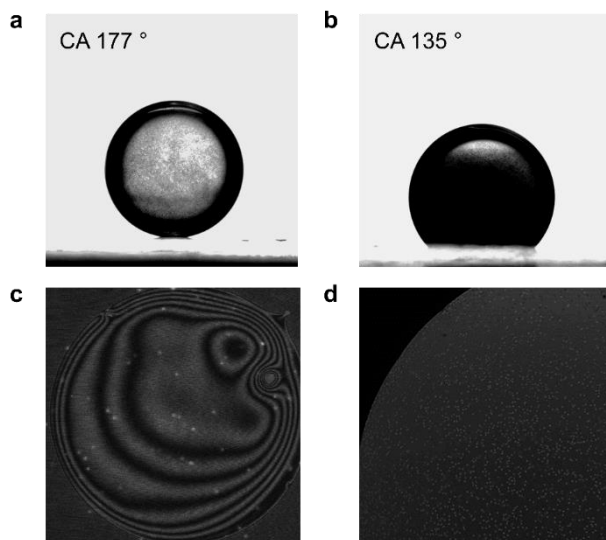
## 2. Enrichment of particles at the interface and the apparent CLLA

One interesting point is, the colloids prefer to accumulate at the apparent liquid-air interface rather than escape to the bulk liquid. This is determined by two factors: The particles were captured by the liquid-air interface. The particles trapped by the interface hardly escaped because of the strong binding energy  $\Delta E$  between particles and the liquid-air interface. (1) Suspended particles were driven to the liquid-air interface, as an upward flow generated inside droplet and captured by the descending liquid-air interface during evaporation; (2) Particles trapped by the interface were

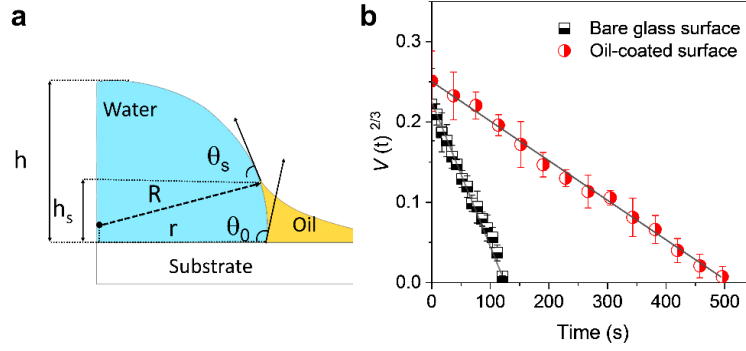
in a thermodynamically stable state because of the strong binding energy  $\Delta E$  between particles and the liquid-air interface. For each particle trapped at the liquid-air interface, the liquid-air interface is reduced by a radius of  $R$ , the corresponding energy for particle is  $\Delta E = -\pi R^2 \gamma_0 (1 - (\gamma_2 - \gamma_1)/\gamma_0)^2$  where  $\gamma_0, \gamma_1, \gamma_2$  is the interfacial tension of liquid-air, particle-liquid and particle-air interface, respectively.<sup>4,5</sup> We assume that the particle was nearly equal affinity for water and air. For micro-sized particles, the binding energy  $\Delta E \approx 10^{-10}$  mN·m, larger than the Brownian motion of particles  $\varepsilon = k_B T \approx 10^{-21}$  mN·m. Here,  $k_B$  is the Boltzmann's constant and  $T$  is the absolute temperature,  $T = 298$  K. Consequently, particles trapped at the liquid-air interface were more likely to stay at the interface to keep their thermodynamic stability, as well as nano-sized particles ( $\Delta E \approx 10^{-16}$  mN·m  $> 10^{-21}$  mN·m).

In addition, the dispersed particles were more likely to flow to the apparent CLLA, which indicates a higher evaporation flux shown at the CLLA. According to Deegan *et al.* and Gelderblom *et al.*,<sup>6,7</sup> a higher evaporation happens near the contact line, as the evaporation flux  $J \sim A(\theta) \frac{D(c_s - c_\infty)}{R} \left( \frac{R-r}{R \cos \theta} \right)^\lambda$ . Here,  $r \rightarrow R$ ,  $\lambda = \frac{2\theta - \pi}{2\pi - 2\theta}$ . For a droplet evaporates on the oil-coated substrate, we consider the evaporation near the oil ridge are the same situation. A higher evaporation occurs at the CLLA. One thing to note, we have neglected the particle-particle interactions at the liquid-air interface in this study.

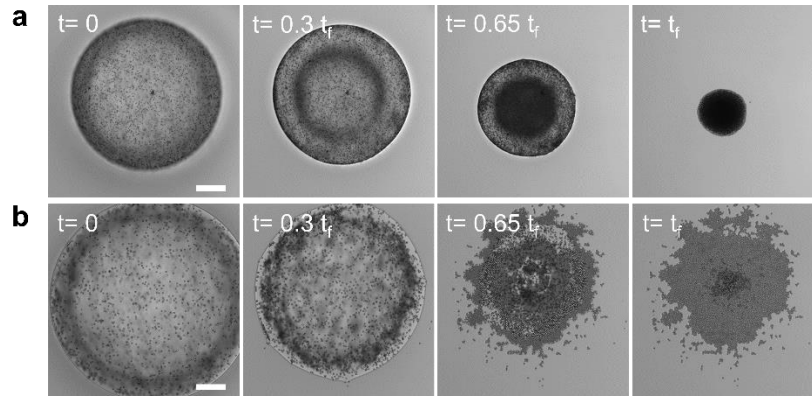
### 3. Supplementary figures



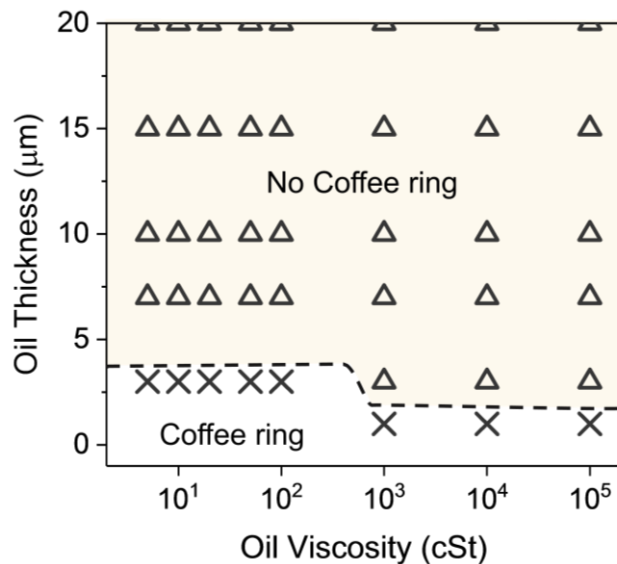
**Figure S1.** Surface wettability determines the behavior of sitting droplets and the oil film underneath the droplets. Optical images of colloidal droplets (10  $\mu\text{L}$ ) on the (a) hydrophilic and (b) hydrophobic substrates in silicon oil atmosphere (silicon oil with a viscosity of 100 cSt). An interference pattern captured by the reflection light through the pinhole from confocal microscope ( $\lambda = 458 \text{ nm}$ , 20 $\times$  oil-immersion objective) on oil-coated hydrophobic surface(c) while no interference pattern observed on oil-coated hydrophilic surface (d). (Bright spots: Fluorescent PS particles, 2.5  $\mu\text{m}$ ).



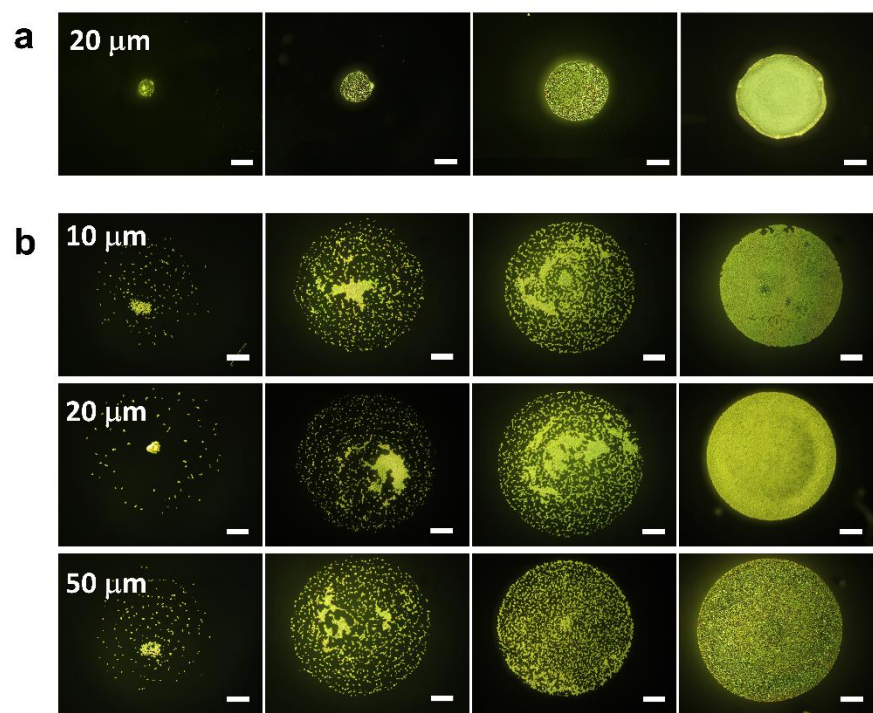
**Figure S2.** Droplet evaporation on oil-coated surface. (a) A schematic of the cross-section of droplet on an oil-coated surface. An “oil wetting ridge” formed at the base of droplet. (b) The evolution of  $0.1 \mu\text{L}$  droplets evaporating on a glass substrate and oil-coated surface. The fit curves show the volume of droplets ( $V(t)^{2/3}$ ) with the function of time. Colloidal solution ( $3.0 \mu\text{m}$  PS, 0.15 vol%) were deposited on surfaces to study the evaporation behaviors. The oil coated on surface has a viscosity of 100 cSt and the initial thickness is  $20 \mu\text{m}$ .



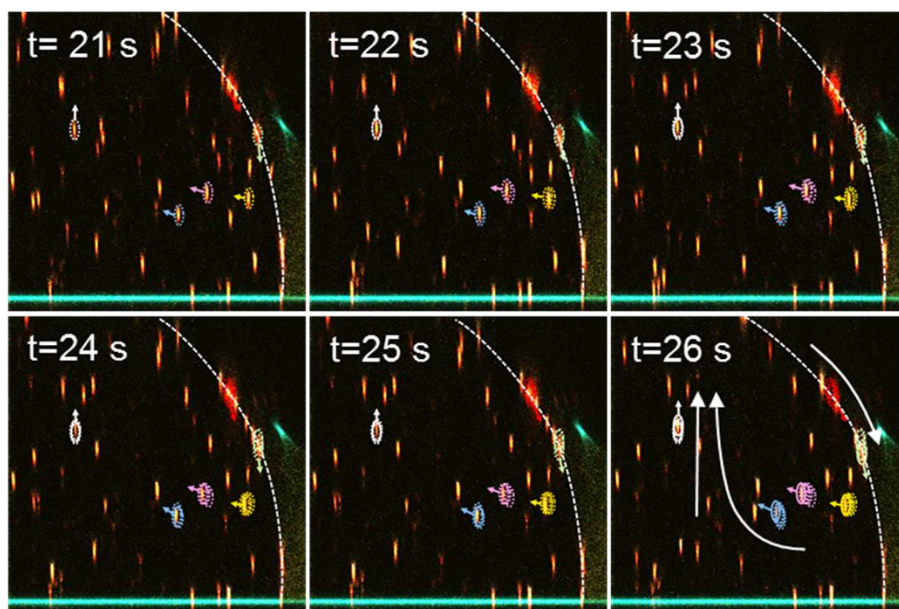
**Figure S3.** Snapshots of  $0.2 \mu\text{L}$  droplets of colloids dispersion (0.15 vol%) evaporate on (a) oil-coated hydrophobic and (b) oil-coated hydrophilic surfaces, captured by the inverted confocal microscope from the bottom.  $t_f$ : the total evaporation time.



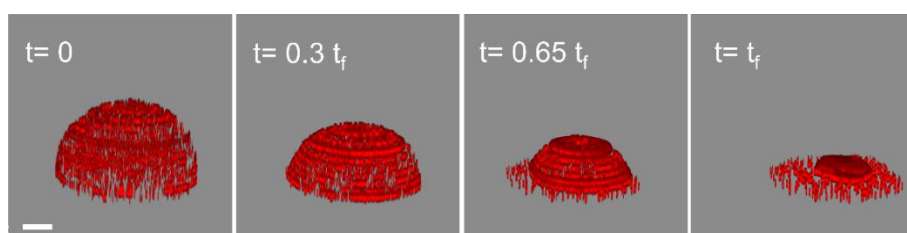
**Figure S4.** “Phase” diagram of the suppression of coffee-ring effect on oil-coated hydrophilic surface, depending on the thickness of oil film and the viscosity of oil. Uniform depositions are marked as hollow triangles ( $\Delta$ ); Coffee ring patterns are represented with crosses ( $\times$ ). Dashed black lines represent the critical oil thickness.



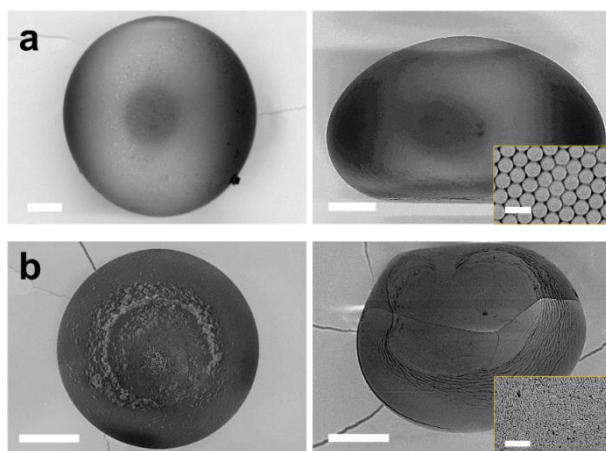
**Figure S5.** Deposition features of droplets dispersed with polystyrene particles ( $3\ \mu\text{m}$ ,  $0.2\ \mu\text{L}$ ) on oil-coated surfaces. a) Depositions on oil-coated HB surface (initial oil thickness:  $20\ \mu\text{m}$ ). Initial concentration of the dispersed particles from left to right are 0.015, 0.1, 0.3 to 1.5 vol%, respectively. b) Depositions on oil-coated HL surface. Columns increasing thickness of oil film (from 3 to  $50\ \mu\text{m}$ ); Rows present the initial concentrations of the dispersion increases from 0.015 to 1.5 vol%. Scale bars:  $100\ \mu\text{m}$ .



**Figure S6.** Transportation of particles in an evaporating droplet. Different particles are marked in different colors. Small arrows illustrate the direction of particles motion. Color scheme: Orange: Fluorescent polystyrene particles; Yellow: oil phase; Cyan: reflection of interfaces. Upward arrows: Upward flow pattern generated inside the droplet.



**Figure S7.** The 3D reconstruction of particle assembly inside the evaporating droplet on oil-coated HL surface. (Initial droplet volume:  $0.05\text{ }\mu\text{L}$ ; initial concentration is  $0.1\text{ vol\%}$ .  $t_f$ : The final drying time. Imaged by inverted confocal microscope, with a  $20\times$  multi-immersion objective).



**Figure S8.** Fabrication of pill-like supraparticles by evaporating polystyrene solutions with different sizes on oil-coated hydrophobic surface. a) 486 nm, 0.1 vol%; b) 68 nm, 0.1 vol%. Left and right images show the top and side view of the supraparticles, respectively. Insets: the magnified images of the surface of supraparticles. Scale bars: 100  $\mu\text{m}$ ; Insets: 1  $\mu\text{m}$ .

**Video S1:** 3D laser scanning confocal video sequence of droplet change due to evaporation. The upward movement of the tracer particles (PS, 2.5  $\mu\text{m}$  fluorescently labelled, see main text) due to the evaporation at the air-liquid interface is clearly visible. The oil viscosity: 100 cSt; oil thickness: 20  $\mu\text{m}$ . The initial volume of the droplet: 0.05  $\mu\text{L}$ . Observed with a 20 $\times$  multi-immersion objective, in xzt mode.

## References

1. Picknett, R.; Bexon, R., The Evaporation of Sessile or Pendant Drops in Still Air. *J. Colloid Interface Sci.* **1977**, *61*, 336-350.
2. Guan, J. H.; Wells, G. G.; Xu, B.; McHale, G.; Wood, D.; Martin, J.; Stuart-Cole, S., Evaporation of Sessile Droplets on Slippery Liquid-Infused Porous Surfaces (slips). *Langmuir* **2015**, *31*, 11781-11789.

3. Stauber, J. M.; Wilson, S. K.; Duffy, B. R.; Sefiane, K., Evaporation of Droplets on Strongly Hydrophobic Substrates. *Langmuir* **2015**, *31*, 3653-3660.
4. Pieranski, P., Two-Dimensional Interfacial Colloidal Crystals. *Phys. Rev. Lett.* **1980**, *45*, 569-572.
5. Du, K.; Glogowski, E.; Emrick, T.; Russell, T. P.; Dinsmore, A. D., Adsorption Energy of Nano- and Microparticles at Liquid-Liquid Interfaces. *Langmuir* **2010**, *26*, 12518-12522.
6. Yunker, P. J.; Still, T.; Lohr, M. A.; Yodh, A. G., Suppression of The Coffee-Ring Effect by Shape-Dependent Capillary Interactions. *Nature* **2011**, *476*, 308-311.
7. Gelderblom, H.; Bloemen, O.; Snoeijer, J. H., Stokes Flow Near the Contact Line of An Evaporating Drop. *J. Fluid Mech.* **2012**, *709*, 69-84.