

## **Supporting Information**

### **Microporous metal-organic frameworks with hydrophilic and hydrophobic pores for efficient separation of CH<sub>4</sub>/N<sub>2</sub> mixture**

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## S1. Calculation of the SSP

Sorbent selection parameter (*SSP*) can be calculated as:

$$SSP = \frac{(S_{i/j}^{ads})^2}{(S_{i/j}^{des})} \times \frac{(N_i^{ads} - N_i^{des})}{(N_j^{ads} - N_j^{des})}$$

where  $S_{i/j}^{ads}$  and  $S_{i/j}^{des}$  are the selectivities of  $i$  and  $j$  components,  $N^{ads}$  and  $N^{des}$  are the adsorption capacity. The superscripts of “*ads*” and “*des*” represent the adsorption and desorption process, respectively.

## S2. Calculations of IAST and Henry's law ideal selectivity

The pure single component isotherms of CH<sub>4</sub> and N<sub>2</sub> (CH<sub>4</sub> /N<sub>2</sub> (50/50, v/v)) at 298 K were fitted to the dual-site Langmuir equation:

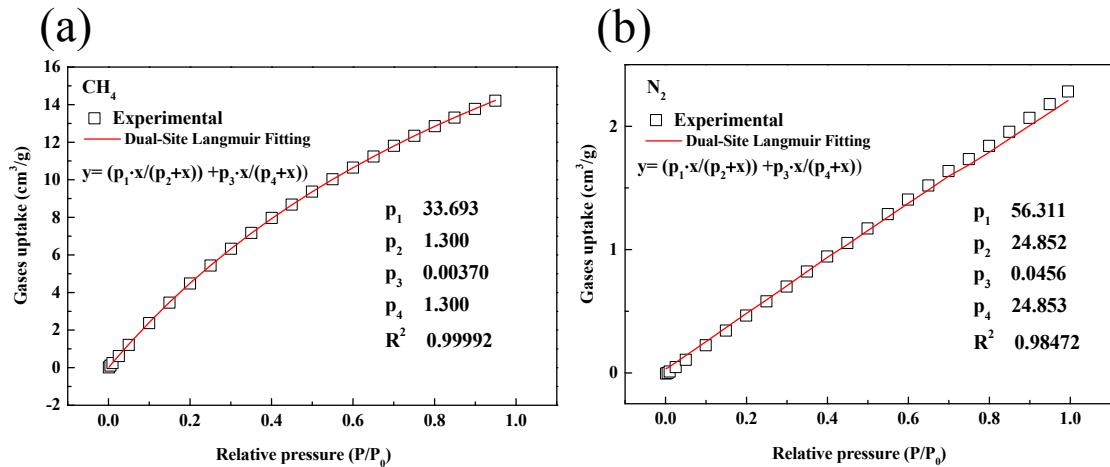
$$y = (p_1 \times x/p_2 + x) + (p_3 \times x/p_4 + x)$$

The equilibrium composition of the CH<sub>4</sub> /N<sub>2</sub> mixture is 9.14: 0.85. The calculated IAST selectivities are about 10.8-11.5 and 10.8 at the range of tested pressures and 1.0 bar, respectively.

**Table S1.** The fitted parameters by using the dual-site Langmuir model based on the pure single-

component isotherms data of CH<sub>4</sub> and N<sub>2</sub> in Cu-MOF at 298 K.

parameters	298 K	
	CH <sub>4</sub>	N <sub>2</sub>
P <sub>1</sub>	33.693	56.311
P <sub>2</sub>	1.300	24.852
P <sub>3</sub>	0.00370	0.0456
P <sub>4</sub>	1.300	24.853
R <sup>2</sup>	0.99992	0.98472



**Figure S1.** Fitting of the CH<sub>4</sub> (a) and N<sub>2</sub> (b) adsorption data of Cu-MOF at 298 K using dual-site Langmuir model

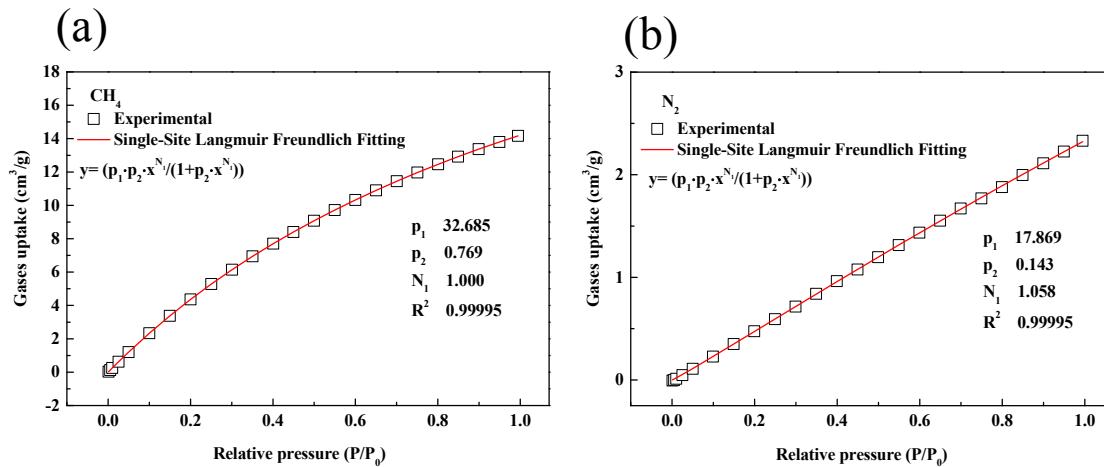
The pure single component isotherms of CH<sub>4</sub> and N<sub>2</sub> (CH<sub>4</sub> /N<sub>2</sub> (50/50, v/v)) at 298 K were fitted to the single-site Langmuir Freundlich equation:

$$y = (p_1 \times p_2 \times x^{N_1} / (1 + p_2 \times x^{N_1}))$$

The equilibrium composition of the CH<sub>4</sub> /N<sub>2</sub> mixture is 8.79: 0.7864. The calculated IAST selectivities are about 10.67-12.66 and 11.18 at the range of tested pressures and 1.0 bar, respectively.

**Table S2.** The fitted parameters by using the single-site Langmuir Freundlich model based on the pure single-component isotherms data of CH<sub>4</sub> and N<sub>2</sub> in Cu-MOF at 298 K.

parameters	298 K	
	CH <sub>4</sub>	N <sub>2</sub>
P <sub>1</sub>	32.685	17.869
P <sub>2</sub>	0.769	0.143
N <sub>1</sub>	1.000	1.058
R <sup>2</sup>	0.99995	0.99995



**Figure S2.** Fitting of the CH<sub>4</sub> (a) and N<sub>2</sub> (b) adsorption data of Cu-MOF at 298 K using single-site Langmuir Freundlich model.

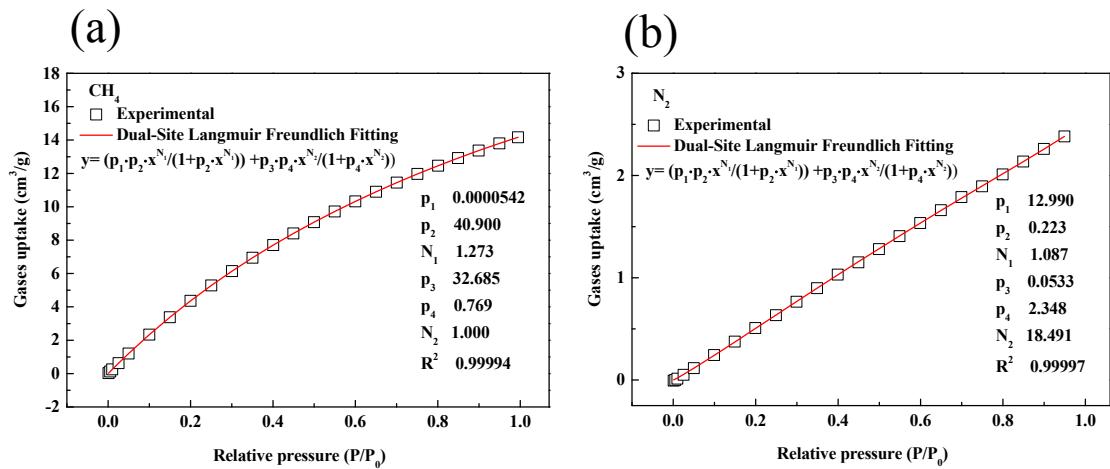
The pure single component isotherms of CH<sub>4</sub> and N<sub>2</sub> (CH<sub>4</sub> /N<sub>2</sub> (50/50, v/v)) at 298 K were fitted to the dual-site Langmuir Freundlich equation:

$$y = (p_1 \times p_2 \times x^{N_1} / (1 + p_2 \times x^{N_1})) + p_3 \times p_4 \times x^{N_2} / (1 + p_4 \times x^{N_2})$$

The equilibrium composition of the CH<sub>4</sub> /N<sub>2</sub> mixture is 8.7132: 0.7819. The calculated IAST selectivities are about 10.00-12.67 and 11.14 at the range of tested pressures and 1.0 bar, respectively.

**Table S3.** The fitted parameters by using the dual-site Langmuir Freundlich model based on the pure single-component isotherms data of CH<sub>4</sub> and N<sub>2</sub> in Cu-MOF at 298 K.

parameters	298 K	
	CH <sub>4</sub>	N <sub>2</sub>
P <sub>1</sub>	0.0000542	12.990
P <sub>2</sub>	40.900	0.223
N <sub>1</sub>	1.273	1.087
P <sub>3</sub>	32.685	0.0533
P <sub>4</sub>	0.769	2.348
N <sub>2</sub>	1.000	18.491
R <sup>2</sup>	0.99994	0.99997



**Figure S3.** Fitting of the CH<sub>4</sub> (a) and N<sub>2</sub> (b) adsorption data of Cu-MOF at 298 K using dual-site Langmuir Freundlich model.

The pure single component isotherms of CH<sub>4</sub> and N<sub>2</sub> (CH<sub>4</sub> /N<sub>2</sub> (50/50, v/v)) at 298 K were fitted to the Toth equation:

$$y = N_{max} \times p_1 \times x / 1 + ((p_1 \times x^{p_2})^{1/p_2})$$

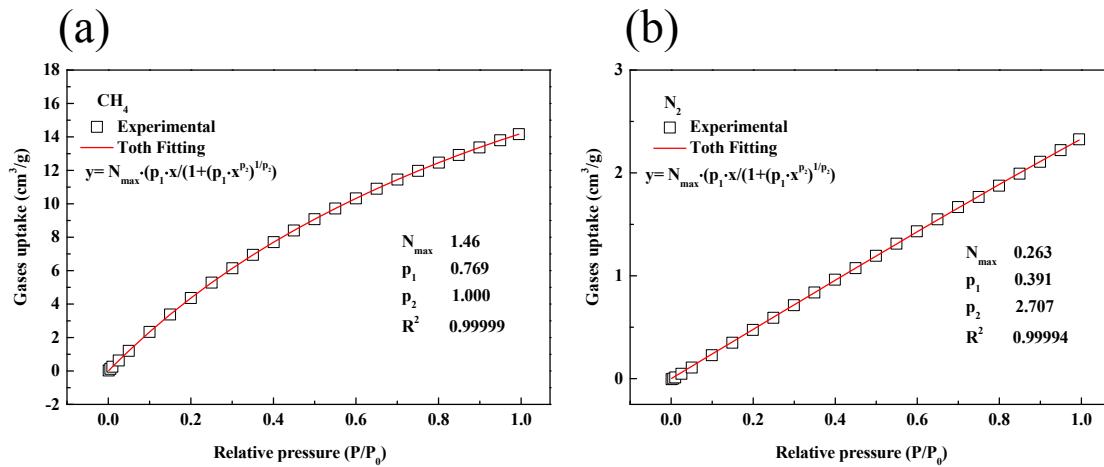
$$K_H = N_{max} \times P_1$$

$$S_{i,j} = K_{H,i} / K_{H,j}$$

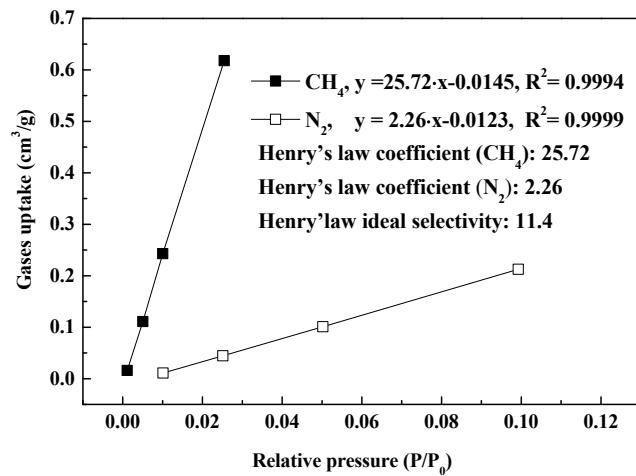
The ideal selectivity is about 10.94.

**Table S4.** The fitted parameters by using the Toth model based on the pure single-component isotherms data of CH<sub>4</sub> and N<sub>2</sub> in Cu-MOF at 298 K.

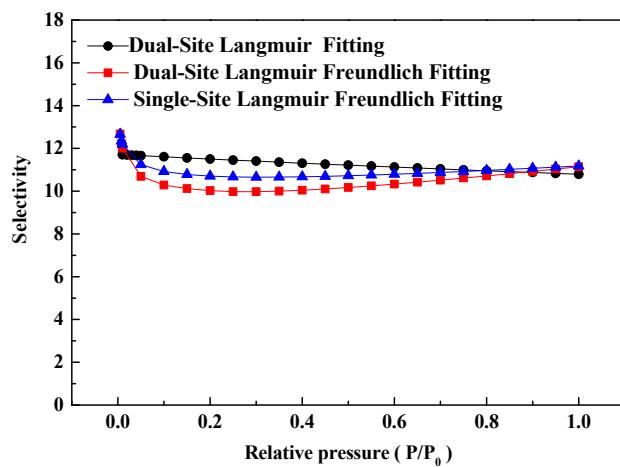
	298 K	
parameters	CH <sub>4</sub>	N <sub>2</sub>
N <sub>max</sub>	1.46	0.263
P <sub>1</sub>	0.769	0.391
P <sub>2</sub>	1.000	2.707
R <sup>2</sup>	0.99999	0.99994



**Figure S4.** Fitting of the CH<sub>4</sub> (a) and N<sub>2</sub> (b) adsorption data of Cu-MOF at 298 K using Toth model.

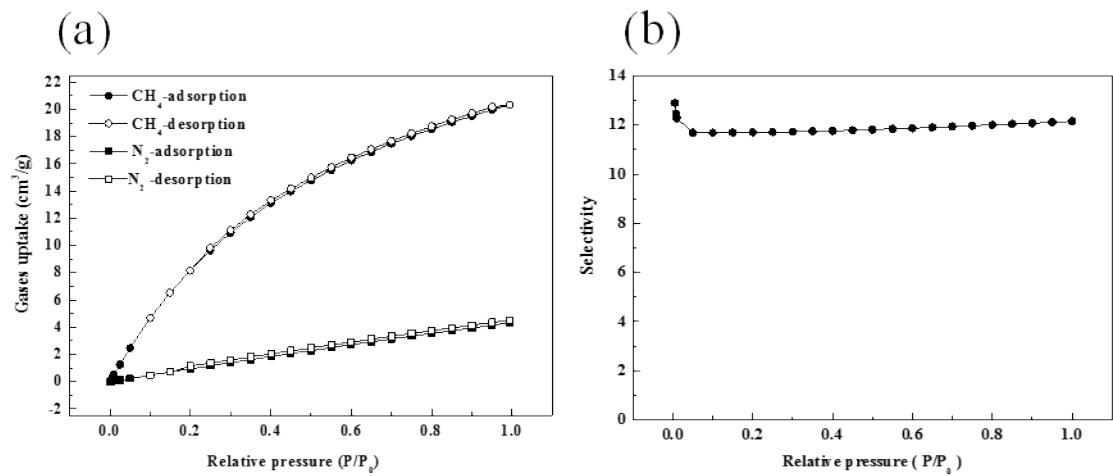


**Figure S5.** CH<sub>4</sub> and N<sub>2</sub> Henry's law coefficients and Henry's law ideal selectivity of Cu-MOF.

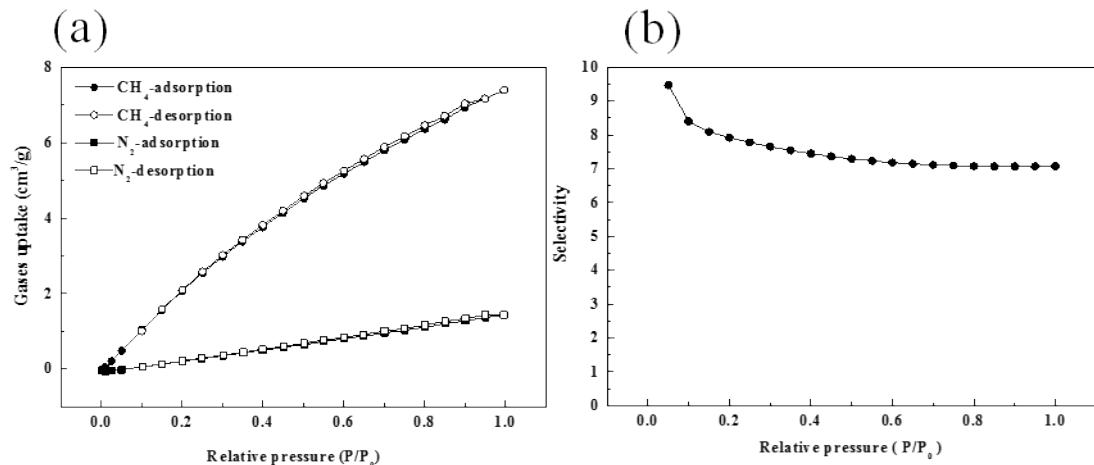


**Figure S6.** IAST-predicted selectivities using different fitting models.

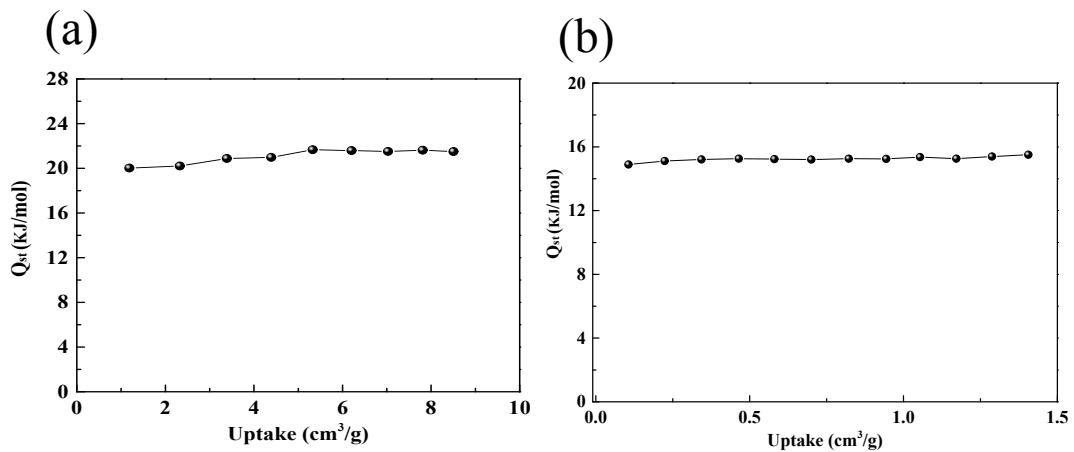
### S3. Characterization of MOFs



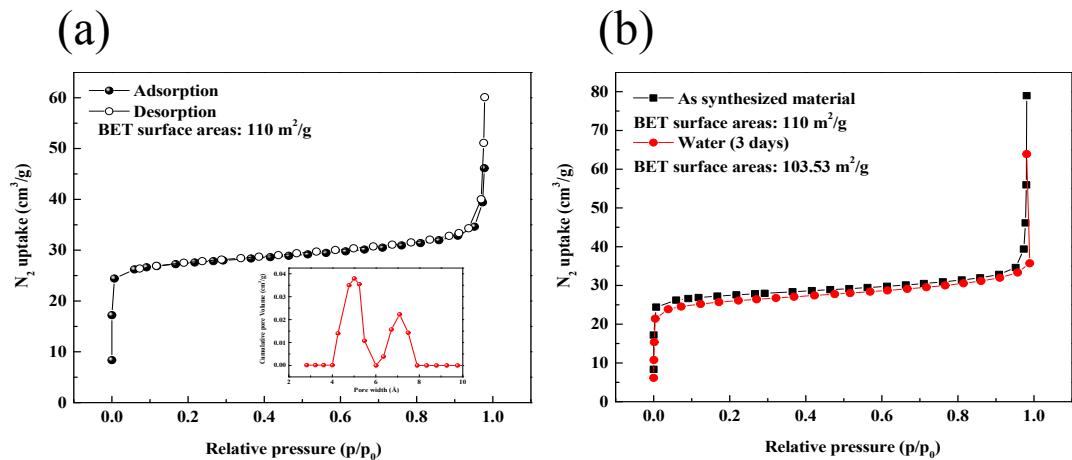
**Figure S7.** (a) Single component adsorption isotherms of  $\text{CH}_4$  and  $\text{N}_2$  in Cu-MOF at 273 K; (b) IAST selectivity of  $\text{CH}_4$  and  $\text{N}_2$  with equimolar mixture ( $\text{CH}_4 : \text{N}_2 = 0.5 : 0.5$ ) at 273 K using dual-site Langmuir Freundlich model.



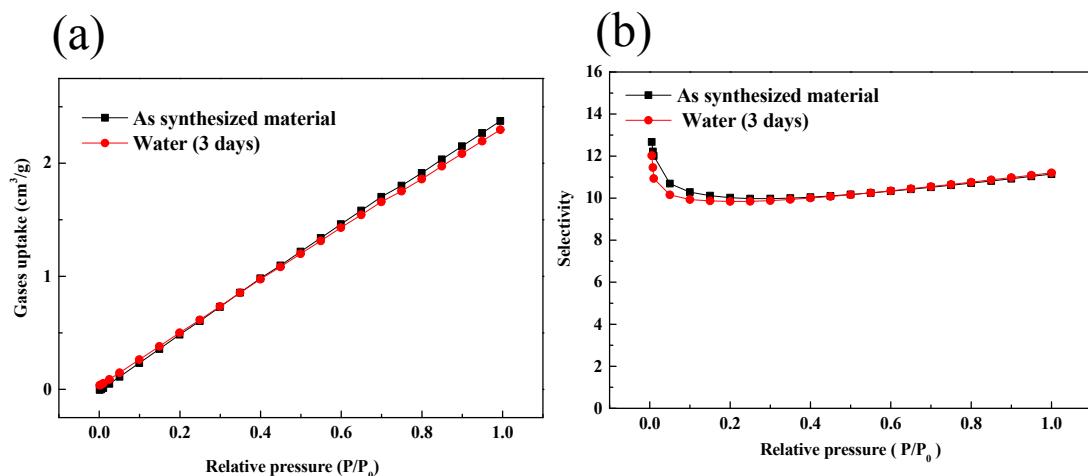
**Figure S8.** (a) Single component adsorption isotherms of  $\text{CH}_4$  and  $\text{N}_2$  in Cu-MOF at 323 K; (b) IAST predicted selectivity of equimolar  $\text{CH}_4/\text{N}_2$  mixture at 323 K using dual-site Langmuir Freundlich model.



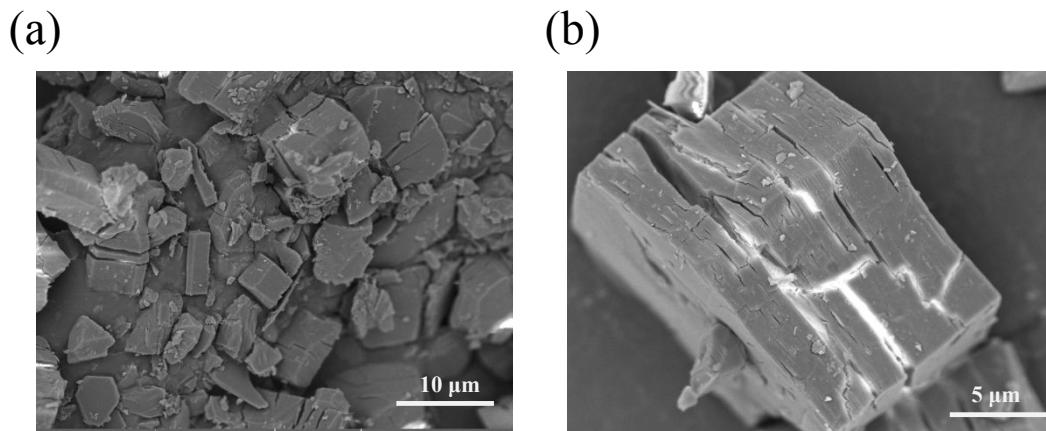
**Figure S9.** Adsorption heats of  $\text{CH}_4$  (a) and  $\text{N}_2$  (b) in Cu-MOF.



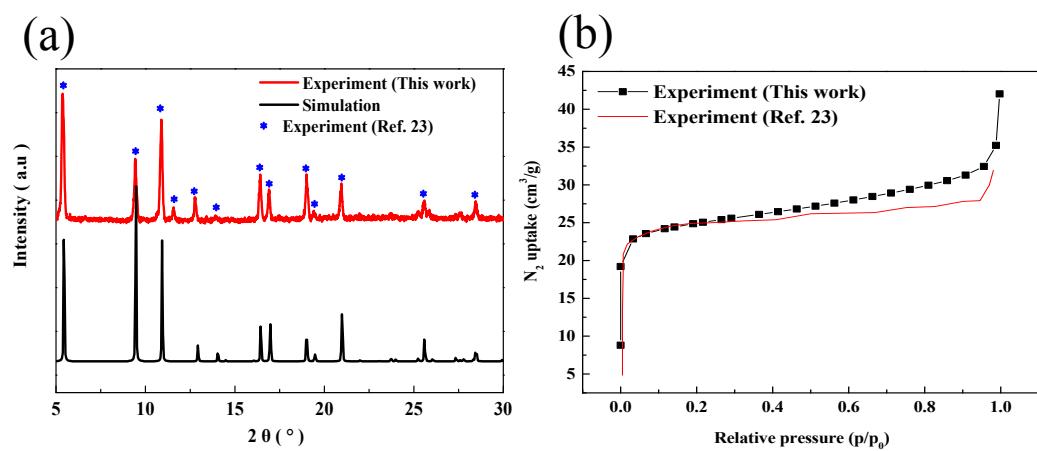
**Figure S10.**  $\text{N}_2$  adsorption-desorption isotherm at 77 K (Inset: the pore size distribution) (a) and the BET surface areas after the treatment of the material using water (b) of Cu-MOF.



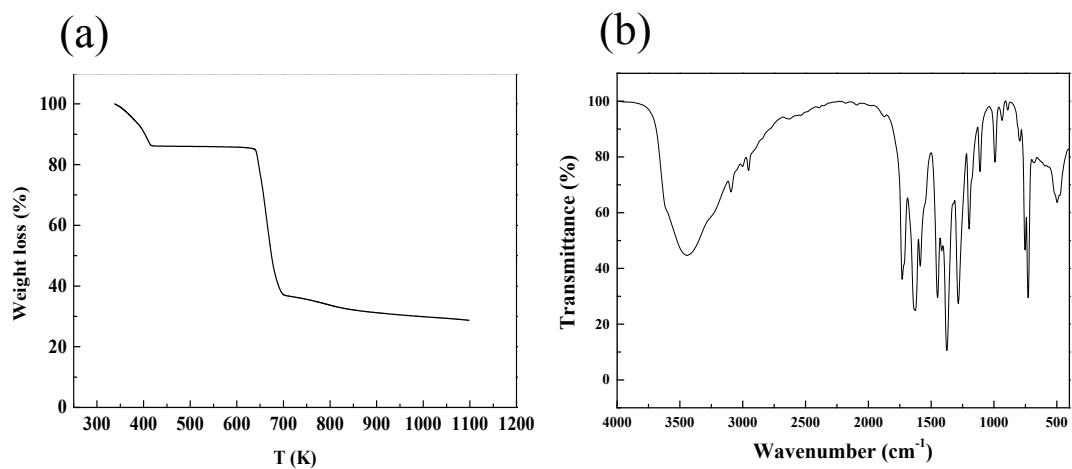
**Figure S11.** Adsorption capacity of  $\text{N}_2$  after the treatment of the material using water (a) and the corresponding IAST selectivity of Cu-MOF using dual-site Langmuir Freundlich model (b).



**Figure S12.** SEM pictures of Cu-MOF.



**Figure S13.** Power X-ray diffraction patterns (a) and  $N_2$  adsorption-desorption isotherms at 77 K (b) of Cu-MOF.



**Figure S14.** TGA curve (a) and FT-IR spectra (b) of Cu-MOF.

## S4. Comparison with other porous materials

**Table S5.** Selectivity and adsorption heat of CH<sub>4</sub> and N<sub>2</sub> in different materials at 298 K and 1 bar.

Adsorbents	Selectivity				Refs.	
	for 50/50	$Q_{st}$ for CH <sub>4</sub>	$Q_{st}$ for N <sub>2</sub>	mixture		
	CH <sub>4</sub> /N <sub>2</sub>	(kJ/mol)	(kJ/mol)			
Co-MOF	12.5 <sup>a</sup>	25.13	18.12		1	
CTF-650	8.6 <sup>a</sup>	27			2	
Na-SAPO-34	2.6 <sup>b</sup>	12.18	22.03		3	
[Ni <sub>3</sub> (HCOO) <sub>6</sub> ]	6.1 <sup>c</sup>	24.82	19.33		4	
[Co <sub>3</sub> (HCOO) <sub>6</sub> ]	5.1 <sup>c</sup>	23.03	19.7		4	
Cu-BTC	3.69 <sup>c</sup>	16.6	13.9		4	
[Cu(Me-4py-trz-ia)]	4.2 <sup>a</sup>	18	12		5	
Basolite A100	3.7 <sup>a</sup>	19	15.9		5	
MOF-888	8.38 <sup>a</sup>	26	22		6	
MOF-889	6.41 <sup>a</sup>	22	19		6	
MOF-890	7 <sup>a</sup>	23	19		6	
MOF-891	7.78 <sup>a</sup>	22	21		6	
MOF-5	1.13 <sup>c</sup>	12.2			7	
MOF-177	4 <sup>c</sup>	11.74			7	
Cu(OTf) <sub>2</sub>	4.8 <sup>a</sup>	19.6	16		8	
ZIF-68	3.5 <sup>a</sup>	15.7 <sup>f</sup>	11.9 <sup>f</sup>		9	
ZIF-69	3 <sup>a</sup>	16.2 <sup>f</sup>	12.8 <sup>f</sup>		9	
Ni-FA	6 <sup>a</sup>	22.2	18		10	
ZIF-8	2.8 <sup>d</sup>	12.4 <sup>f</sup>	9.8 <sup>f</sup>		11	
MIL-101-Cr	2.65 <sup>a</sup> (293 K)	15 (293 K)	12 (293 K)		12	
Cu(MOF)	6.9 <sup>a</sup>	24	20		13	
[Cu(INA) <sub>2</sub> ]	8.34 <sup>c</sup>	17.52			14	
Al-BDC	3.56 <sup>c</sup>	18.74			14	

Ni-HKUST-1	5.1 <sup>a</sup>		15
Boron nitride	10 <sup>a</sup>		16
[Ni <sub>3</sub> (HCOO) <sub>6</sub> ]	6.18 <sup>c</sup>		17
ATC-Cu	9.7 <sup>a</sup>	26.8	16
ACF@[Ni <sub>3</sub> (HCOO) <sub>6</sub> ]	6.22 <sup>c</sup>		19
[Cu(dhbc) <sub>2</sub> (bpy)]	2.2 <sup>e</sup>		20
ZIF-68	3.89 <sup>c</sup> (10 bar)	18.06 (10 bar)	14.58 (10 bar)
Cu-MOF	11.4 <sup>c</sup>		This work
Cu-MOF	10.00-12.67 <sup>a</sup>	20.02	15.04
			This work

<sup>a</sup> Predicted by IAST.

<sup>b</sup> Mixture selectivity.

<sup>c</sup> Henry's law ideal selectivity.

<sup>d</sup> Calculated by theoretical calculations.

<sup>e</sup> the ratio of maximum uptake capacity.

<sup>f</sup> Obtained from calculations.

Co-MOF is Co<sub>3</sub>(C<sub>4</sub>O<sub>4</sub>)(OH)<sub>2</sub>.

Cu-BTC is Cu<sub>3</sub>(BTC)<sub>2</sub>, where BTC is 1,3,5-benzene tricarboxylate.

[Cu(Me-4py-trz-ia)], where Me-4py-trz-ia is 5-(3-methyl-5-(pyridin-4-yl)-4H-1,2,4-triazol-4-yl) isophthalate.

MOF-888, MOF-889, MOF-890 and MOF-891 are [Ni<sub>2</sub>(CPB)], [Mg<sub>2</sub>(CPB)(DEF)<sub>0.5</sub>], [Cu<sub>3</sub>(CPB)(DMF)<sub>0.5</sub>] and [Cu<sub>3</sub>(CPB)(DEF)<sub>0.4</sub>], respectively, where CPB, DEF and DMF are 1',2',3',4',5',6'-Hexakis(4-carboxyphenyl)benzene, N, N-Dimethylformamide and N, N-Diethylformamide, respectively.

MOF-5 is [Zn<sub>4</sub>O(BDC)]<sub>n</sub>, where BDC is 1,4-benzenedicarboxylate.

MOF-177 is [Zn<sub>4</sub>O(BTB)]<sub>n</sub>, where BTB is benzene tribenzoate.

Cu(OTf)<sub>2</sub>, where OTf is trifluoromethanesulfonate.

ZIF-68 is [Zn(bIM)<sub>x</sub>(nIM)<sub>y</sub>]<sub>n</sub>, where bIM and nIM are benzimidazole and 2-nitroimidazole, respectively.

ZIF-69 is  $[Zn(cbIM)_x(nIM)_y]_n$ , where cbIM and nIM are 5-chlorobenzimidazole and 2-nitroimidazole, respectively.

Ni-FA is  $[Ni_3(HCOO)_6]$ .

ZIF-8 is  $[Zn(2-MI)]_n$ , where 2-MI is 2-methylimidazole.

MIL-101-Cr is  $[Cr_3F(H_2O)_2O[BDC]_3 \cdot nH_2O]_n$ .

Cu(MOF) is  $Cu(hfipbb)(H_2hfipbb)_{0.5}$ , where  $H_2hfipbb$  is 4, 4'-*(hexafluoroisopropylidene)bis(benzoic acid)*.

$[Cu(INA)_2]_n$ , where INA is isonicotinate.

Al-BDC is  $[Al(BDC)(OH)]_n$ .

Ni-HKUST-1 is  $Ni_3(BTC)_2$ .

ATC-Cu is  $Cu_2(ATC)$ , where ATC is 1, 3, 5, 7-adamantanetetracarboxylate.

$[Cu(dhbc)_2(bpy)]$ , where dhbc and bpy are 2, 5-dihydroxybenzoic acid and 4, 4'-bipyridine, respectively.

**Table S6.** Uptake capacity, working capacity, ratio of working capacity and *SSP* values in different materials at 298 K and 1 bar.

Adsorbents	Uptake capacity of CH <sub>4</sub> (cm <sup>3</sup> /g)	Working capacity of CH <sub>4</sub> (cm <sup>3</sup> /g)	Ratio of working capacity	SSP values	Refs
Co-MOF	9.03	1.51	0.506	6.32 <sup>a</sup>	1
CTF-650	32.88	28.3	3.87	33 <sup>a</sup>	2
Na-SAPO-34	13.44	11.2	1.95	5.08 <sup>b</sup>	3
[Ni <sub>3</sub> (HCOO) <sub>6</sub> ]	17.71	15.47	4.58	27.6 <sup>c</sup>	4
[Co <sub>3</sub> (HCOO) <sub>6</sub> ]	10.98	9.7	4.04	20.6 <sup>c</sup>	4
Cu-BTC	20.41	17.38	2.48	9.16 <sup>a</sup>	4
[Cu(Me-4py-trz-ia)]	25.09	21.05	3.57	15 <sup>a</sup>	5
Baselite A100	16.58	13.21	3.84	14.21 <sup>a</sup>	5
MOF-888	10.09	8.31	4.77	37.85 <sup>a</sup>	6
MOF-889	25.98	22.30	4.85	31.15 <sup>a</sup>	6
MOF-890	23.97	20.17	3.89	27.2 <sup>a</sup>	6
MOF-891	29.99	24.72	4.42	32.41 <sup>a</sup>	6
MOF-5	2.91	1.80	0.94	1.05 <sup>c</sup>	7
MOF-177	12.61	8.81	3.78	15.12 <sup>c</sup>	7
[Cu(OTf) <sub>2</sub> ]	5.69	5.10	2.01	9.6 <sup>a</sup>	8
ZIF-68	8.96	8.02	2.91	10.2 <sup>a</sup>	9
ZIF-69	11.2	10.10	3.36	10.08 <sup>a</sup>	9
Ni-FA	17.92	18.9	4.42	26.56 <sup>a</sup>	10
ZIF-8	4.48				11
MIL-101- Cr	14.56 (293 K)	10.6 (293K)	5.47(293K)	36.65 <sup>a</sup> (293K)	12
Cu(MOF)	10.53	8.5	3.27	22.57 <sup>a</sup>	13
[Cu(INA) <sub>2</sub> ]	17.90	15.80	5.5	40.16 <sup>c</sup>	14
Al-BDC	16.31	14.50	3.34	11.9 <sup>c</sup>	14
Ni-HKUST-1	37.49	31.49	4.03	20.56 <sup>a</sup>	15
Boron nitride	14.78	13.90	3.2	32 <sup>a</sup>	16
[Ni <sub>3</sub> (HCOO) <sub>6</sub> ]	18.37	16.13	4.86	30.9 <sup>c</sup>	17
ATC-Cu	64.96	47.28	3.04	40.9 <sup>a</sup>	18
ACF@[Ni <sub>3</sub> (HCOO) <sub>6</sub> ]	24.64	17.25	5.13	37 <sup>c</sup>	19
[Cu(dhbc) <sub>2</sub> (bpy)]	1.1				20
ZIF-68					21
Cu-MOF	14.17	11.4	5.90	65.73 <sup>a</sup>	This work

<sup>a</sup> Calculated using IAST selectivity.

<sup>b</sup> Calculated using mixture selectivity.

<sup>c</sup> Calculated using Henry's law ideal selectivity.

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