

## Supporting Information

### **Mechanism and kinetics of Propane dehydrogenation and cracking over Ga/H-MFI prepared via vapor-phase exchange of H-MFI with GaCl<sub>3</sub>**

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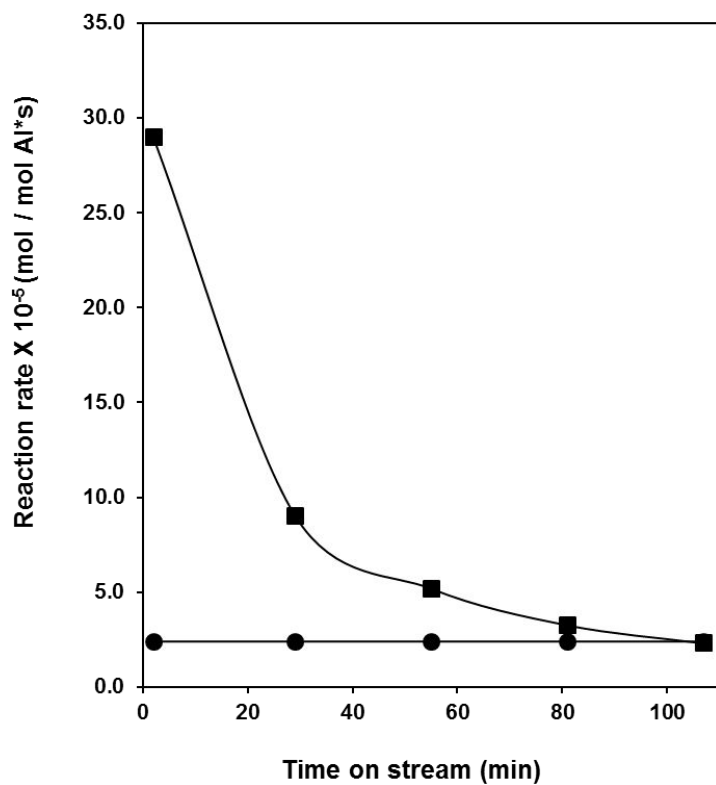
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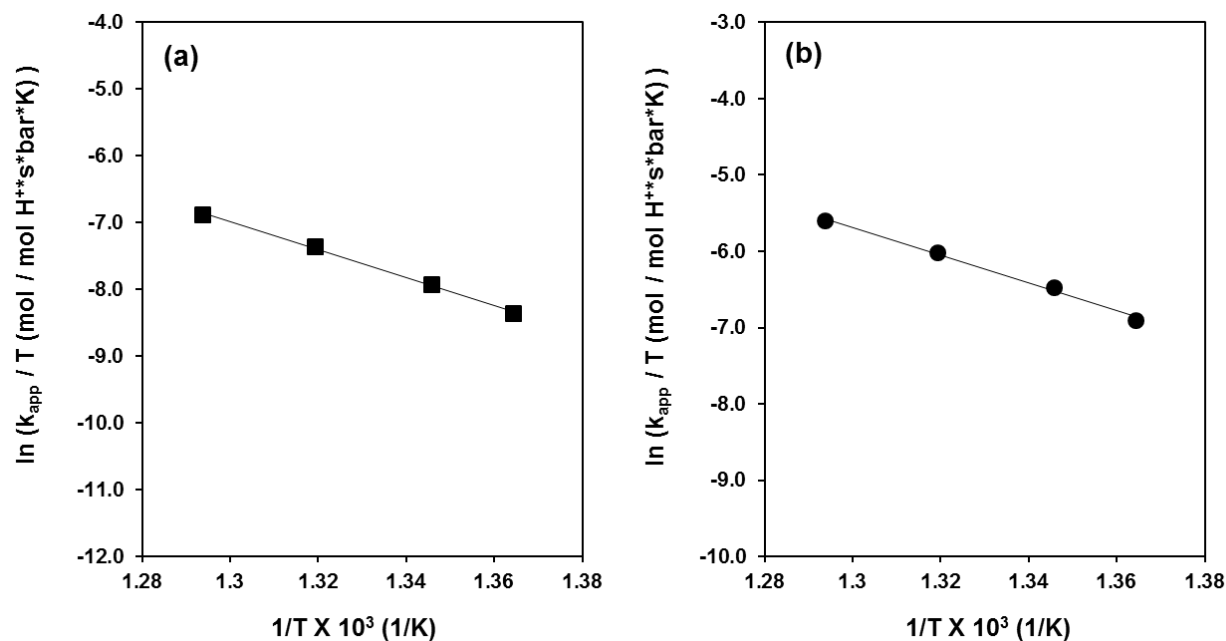
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Text S1.



**Figure S.1:** C<sub>3</sub>H<sub>8</sub> dehydrogenation rates (filled squares) and cracking rates (filled circles) as a function of time-on-stream, measured at 1.4 kPa C<sub>3</sub>H<sub>8</sub>/He and  $\tau = 10$  mol Al\*s/mol C<sub>3</sub>H<sub>8</sub> space time and 733 K. C<sub>3</sub>H<sub>8</sub> conversions were < 2 %

Text S2.

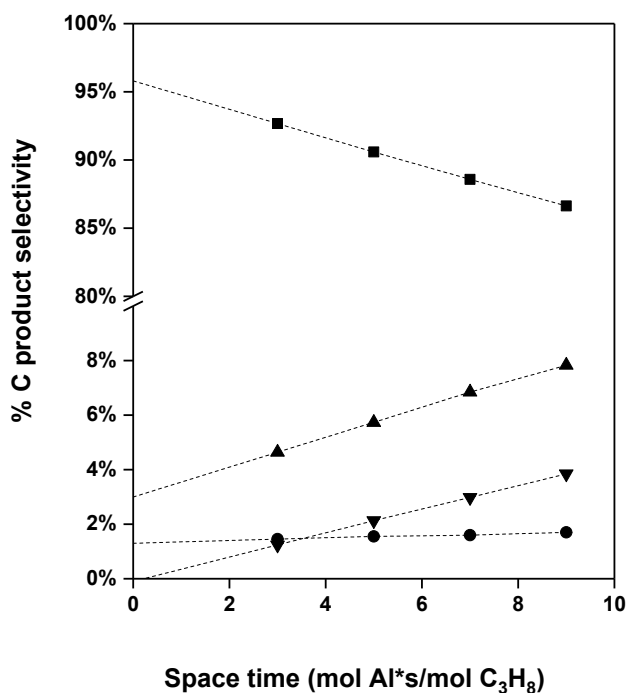


**Figure S.2:** First-order rate coefficients ( $k_{app}$ ) for  $C_3H_8$  dehydrogenation (a) and cracking (b) as a function of temperature. Rate constants were normalized to the density of Brønsted acid O-H acid groups in H-MFI, measured via  $NH_3$ -TPD ( $0.87 H^+/Al_{tot}$ ).

**Text S3. Effects of space time on steady-state product selectivities over Ga/H-MFI (Ga/Al = 0.2) during C<sub>3</sub>H<sub>8</sub> conversion**

Shown in Figure S3, are the steady-state product selectivities (shown as % of converted C in products) as a function of space time for the reaction of C<sub>3</sub>H<sub>8</sub> over Ga/H-MFI (Ga/Al = 0.2) at 733 K and 1.5kPa C<sub>3</sub>H<sub>8</sub>/He. Under the differential conversions employed during reactivity measurements (< 7% C<sub>3</sub>H<sub>8</sub> conversion), only C<sub>3</sub>H<sub>6</sub>, CH<sub>4</sub>, C<sub>2</sub>H<sub>4</sub> and aromatics (C<sub>6</sub>H<sub>6</sub> and C<sub>7</sub>H<sub>8</sub>) were detected as reaction products in the reactor effluent. All product selectivities shown in Figure S3 were also linearly extrapolated to 0 space time, as can be seen by the dotted lines in the figure. C<sub>3</sub>H<sub>6</sub> is the dominant product at all space times tested (> 85% C selectivity), but the selectivity to this product decreases with increasing space time from an extrapolated C selectivity of 96 % at 0 space time. The decrease in C<sub>3</sub>H<sub>6</sub> selectivity with increasing space time is attributed to secondary pathways that consume C<sub>3</sub>H<sub>6</sub> to form higher molecular weight products, such as aromatics. The C selectivity to C<sub>2</sub>H<sub>4</sub> is about 3% at zero space time and then increases linearly with increasing space time. By contrast the C selectivity to CH<sub>4</sub> is roughly independent of space time, with a value of approximately 1.5%. The ratio of the extrapolated C selectivities of C<sub>2</sub>H<sub>4</sub> and CH<sub>4</sub> (approximately 2) is consistent with the cracking of C<sub>3</sub>H<sub>8</sub> into C<sub>2</sub>H<sub>4</sub> and CH<sub>4</sub>. The increase in this ratio with increasing space time that additional C<sub>2</sub>H<sub>4</sub> is formed by the cracking of higher molecular weight products. This could occur, for example, via  $\beta$ -scission of larger alkenes. The C selectivity to aromatics (C<sub>6</sub>H<sub>6</sub> and C<sub>7</sub>H<sub>8</sub>) increased with increasing space time and at zero space time, extrapolated to a value close to zero, suggesting that these products form via secondary pathways from products of C<sub>3</sub>H<sub>8</sub> dehydrogenation and cracking. This trend is consistent with previous experiments studies of C<sub>3</sub>H<sub>8</sub> conversion over Ga/H-MFI.<sup>1</sup>

Measured selectivities of products (on a  $\text{C}_3\text{H}_8$  basis) together with overall  $\text{C}_3\text{H}_8$  conversion rates were used to determine the rates of  $\text{C}_3\text{H}_8$  dehydrogenation, cracking and aromatics formation. These rates are shown as a function of space time in Figure S4a-d. The rate of  $\text{C}_3\text{H}_8$  consumption (Figure S4a) decreases with increasing space time, possibly due to inhibition by the products of  $\text{C}_3\text{H}_8$  conversion. To explore this possibility, reaction rates were also measured in the presence of co-fed  $\text{H}_2$ . In the presence of 1.5kPa  $\text{H}_2$ , the rates of  $\text{C}_3\text{H}_8$  conversion (open symbols in Figure S4a) show a much weaker dependence on space time, confirming that  $\text{H}_2$  inhibits the rates.  $\text{C}_3\text{H}_8$  dehydrogenation rates (Figure S4b) and  $\text{C}_3\text{H}_8$  cracking rates (Figure S4c) also decrease with increasing space time. In the presence of 1.5kPa co-fed  $\text{H}_2$ , both rates show a much weaker dependence on space time. We note that while the inhibition of the rate of  $\text{C}_3\text{H}_8$  dehydrogenation by  $\text{H}_2$  has been reported in previously,<sup>1,2</sup> inhibition of the rate of  $\text{C}_3\text{H}_8$  cracking rate by  $\text{H}_2$  has not been reported. We note that  $\text{H}_2$  does not inhibit Brønsted acid catalyzed monomolecular dehydrogenation and cracking on H-MFI. This observation suggests that the site requirements for both the dehydrogenation and cracking reaction over Ga/H-MFI are similar i.e., both reactions may be catalyzed by  $\text{Ga}^{3+}$  sites. Both rates also exhibit a weak, but observable decrease with space time, even in the presence of 1.5kPa  $\text{H}_2$ . We speculate that this residual inhibition arises from the binding of alkene products to  $\text{Ga}^{3+}$  sites. Aromatics formation rates (Figure S4d) increased with space time, consistent with their secondary nature. The formation of aromatics was, however, strongly inhibited by  $\text{H}_2$ , suggesting that their formation also requires the participation of  $\text{Ga}^{3+}$  sites.

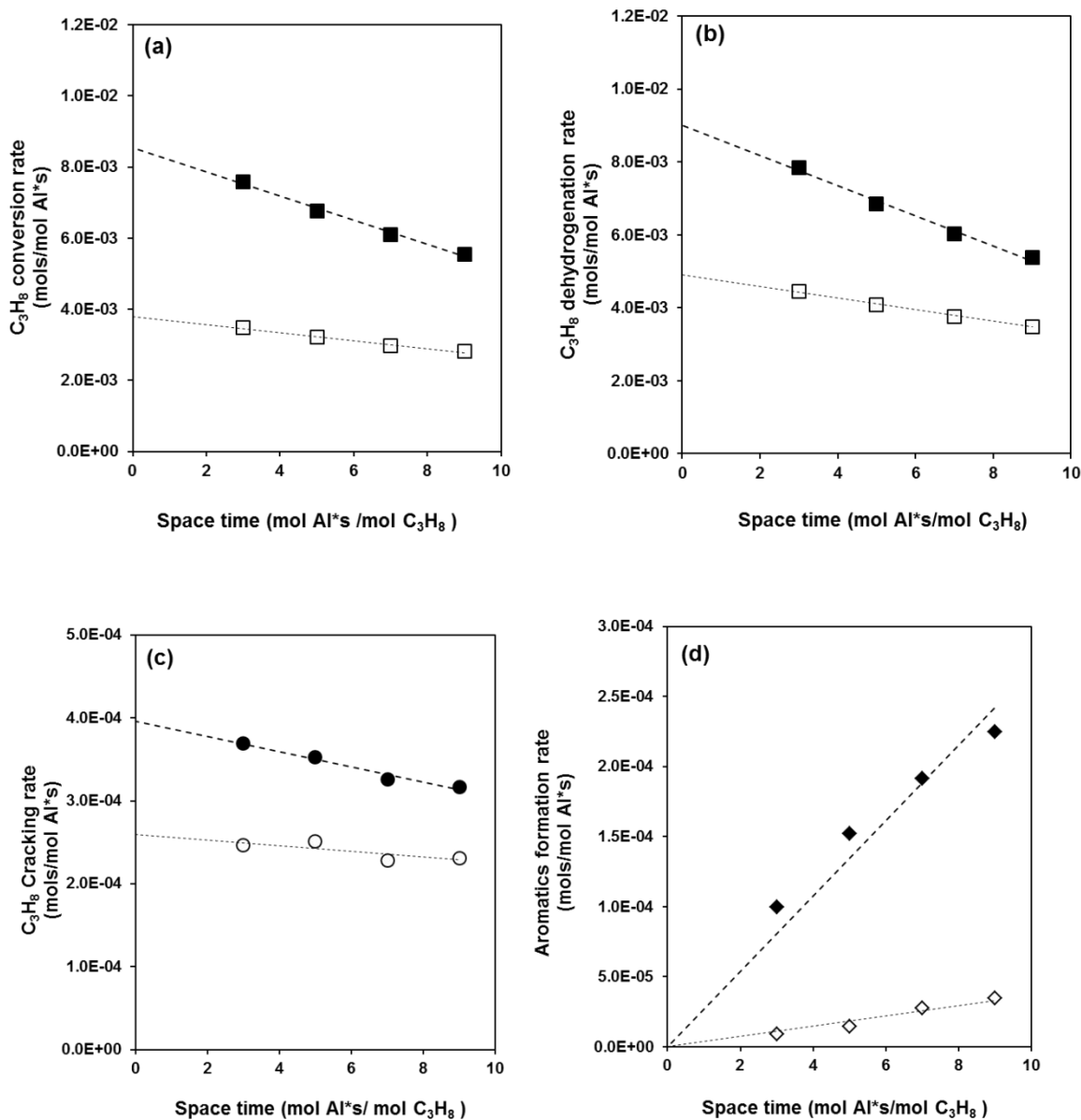


**Figure S3:** C product selectivities (% of C converted to products) as a function of space time, during C<sub>3</sub>H<sub>8</sub> conversion over Ga/H-MFI (Ga/Al = 0.2) at 1.5 kPa C<sub>3</sub>H<sub>8</sub>/He and 733 K. Ga/H-MFI was pre-treated in 2.5% H<sub>2</sub>/He at 773 K, prior to reaction. C<sub>3</sub>H<sub>8</sub> conversions were < 9 %. Filled squares (■) denote C<sub>3</sub>H<sub>6</sub>, filled triangles (▲) denote C<sub>2</sub>H<sub>4</sub>, filled inverted triangles (▼) denote aromatics (C<sub>6</sub>H<sub>6</sub> and C<sub>7</sub>H<sub>8</sub>) and filled circles (●) denote CH<sub>4</sub>. Dotted lines indicate linear extrapolations to 0 space time.

**Table S1:** Apparent reaction orders of H<sub>2</sub> for C<sub>3</sub>H<sub>8</sub> dehydrogenation and cracking at 0.9 kPa C<sub>3</sub>H<sub>8</sub> and 8 kPa C<sub>3</sub>H<sub>8</sub> measured at 733 K over Ga/Al = 0.2. Data are derived from Figure 6.

| C <sub>3</sub> H <sub>8</sub> partial pressure X 10 <sup>2</sup> (bar) | Dehydrogenation | Cracking |
|------------------------------------------------------------------------|-----------------|----------|
| 0.9                                                                    | -0.3            | -0.5     |
| 8.0                                                                    | -0.1            | -0.1     |

<sup>a</sup> Apparent reaction orders were determined using the relationship  $\text{Rate} = k[\text{H}_2]^x$  where k is a rate coefficient and x is the reaction order



**Figure S4:** (a) C<sub>3</sub>H<sub>8</sub> conversion rates (per Al<sub>tot</sub> atom) as a function of space time. (b) C<sub>3</sub>H<sub>8</sub> dehydrogenation rates (per Al<sub>tot</sub> atom) as a function of space time. (c) C<sub>3</sub>H<sub>8</sub> cracking rates (per Al<sub>tot</sub> atom) as a function of space time. (d) Aromatics (C<sub>6</sub>H<sub>6</sub> and C<sub>7</sub>H<sub>8</sub>) formation rates (per Al<sub>tot</sub> atom) as a function of space time. In all plots, closed symbols refer to 0 kPa cofed H<sub>2</sub> and open symbols refer to 1.5 kPa cofed H<sub>2</sub>. Rates were measured at 1.5 kPa C<sub>3</sub>H<sub>8</sub>/He at 733 K.

## Text S.4 Derivation of rate equations for plausible mechanisms for dehydrogenation and cracking over Ga/H-MFI.

### (a) Derivation of rate law for C<sub>3</sub>H<sub>8</sub> dehydrogenation over [GaH]<sup>2+</sup> sites via alkyl mechanism

The elementary steps outlined in Scheme 1 for C<sub>3</sub>H<sub>8</sub> dehydrogenation over [GaH]<sup>2+</sup> sites are used here to derive a rate law in terms of kinetic and thermodynamic coefficients. The steady-state hypothesis was applied to all reactive surface intermediates. On the basis of free energy and enthalpy calculations outlined in Figure S.5, the physisorption of C<sub>3</sub>H<sub>8</sub> onto [GaH]<sup>2+</sup> to form C<sub>3</sub>H<sub>8</sub>-[GaH]<sup>2+</sup> complexes (Step 1) and the dissociative adsorption of C<sub>3</sub>H<sub>8</sub>-[GaH]<sup>2+</sup> to form [C<sub>3</sub>H<sub>7</sub>-GaH]<sup>+</sup>-H<sup>+</sup> cation pairs (Step 2) are predicted to have low activation barriers ( $\leq 2$  kcal/mol) and are therefore assumed to be quasi-equilibrated. This assumption leads to the derivation of equations S1 and S2 that describe the relationship between gas-phase C<sub>3</sub>H<sub>8</sub> and C<sub>3</sub>H<sub>8</sub> derived surface intermediates.

$$K_{\text{phys}} = \frac{[\text{C}_3\text{H}_8 - [\text{GaH}]^{2+}]}{[\text{C}_3\text{H}_8][\text{GaH}]^{2+}} \quad \text{S1}$$

$$K_{\text{dis}} = \frac{[[\text{C}_3\text{H}_7 - \text{GaH}]^+ - \text{H}^+]}{[\text{C}_3\text{H}_8 - [\text{GaH}]^{2+}]} \quad \text{S2}$$

Here,  $K_{\text{phys}}$  and  $K_{\text{dis}}$  are the thermodynamic adsorption constants for C<sub>3</sub>H<sub>8</sub> physisorption at [GaH]<sup>2+</sup> and dissociation of C<sub>3</sub>H<sub>8</sub> by [GaH]<sup>2+</sup> into [C<sub>3</sub>H<sub>7</sub>Ga-H]<sup>+</sup>-H<sup>+</sup> cation pairs, respectively. Similarly, inhibition of reaction rates by H<sub>2</sub> may occur via dissociation of H<sub>2</sub> by [GaH]<sup>2+</sup> to form [GaH<sub>2</sub>]<sup>+</sup>-H<sup>+</sup> pairs as described by equation S3.

$$K_{H_2} = \frac{[[GaH_2]^+ - H^+]}{[H_2][GaH]^{2+}} \quad S3$$

Here,  $K_{H_2}$  is the equilibrium constant for  $H_2$  dissociation.

As also described in the main text, the rate-limiting step in the alkyl dehydrogenation sequence is the cyclic  $\beta$ -hydride elimination of  $C_3H_7$  fragments by the  $Ga^{3+}$  center to form  $C_3H_6$  and  $H_2$  in a concerted step (Step 3). The overall rate of dehydrogenation (per  $[GaH]^{2+}$ ) can be described by equation S4.

$$\frac{\text{Rate, D}}{[GaH]^{2+}} = k_{alk}\theta_{alk} \quad S4$$

Here, Rate, D refers to the dehydrogenation rate,  $k_{alk}$  refers to the rate coefficient for  $\beta$ -hydride elimination and  $\theta_{alk}$  refers to the surface coverage of  $[C_3H_7-GaH]^+-H^+$  cation pairs, the precursor to the rate-limiting transition state and is given by equation S5.

$$\theta_{alk} = \frac{[[C_3H_7-GaH]^+ - H^+]}{[L]} \quad S5$$

Here,  $[[C_3H_7-GaH]^+-H^+]$  refers to the surface concentration of  $[C_3H_7-GaH]^+-H^+$  cation pairs and  $[L]$  refers to the total density of active sites i.e  $[GaH]^{2+}$  sites.  $[L]$  can be described in terms of the various reactive surface intermediates via equation S6.

$$[L] = [GaH]^{2+} + [C_3H_8-[GaH]^{2+}] + [[C_3H_7-GaH]^+-H^+] + [[GaH_2]^+-H^+] \quad S6$$

Theoretical calculations suggest that the interaction of gas-phase  $C_3H_8$  with  $[GaH]^{2+}$  is expected to be weak ( $\sim -6$  kcal/mol adsorption enthalpy). Therefore the second term in equation S6 can be neglected. This leads to a reduction in equation S6 to equation S7.

$$[L] = [\text{GaH}]^{2+} + [[\text{C}_3\text{H}_7\text{-GaH}]^+ \text{-H}^+] + [[\text{GaH}_2]^+ \text{-H}^+] \quad \text{S7}$$

Solving equations S1-S7 leads to a rate expression for  $\text{C}_3\text{H}_8$  dehydrogenation, shown below as equation S8, shown in the main text as equation 3.

$$\frac{\text{Rate, D}}{[\text{GaH}]^{2+}} = \frac{k_{\text{alk}}K_{\text{dis}}K_{\text{phys}}[\text{C}_3\text{H}_8]}{1 + K_{\text{dis}}K_{\text{phys}}[\text{C}_3\text{H}_8] + K_{\text{H}_2}[\text{H}_2]} \quad \text{S8}$$

**(b) Derivation of rate law for  $\text{C}_3\text{H}_8$  dehydrogenation over  $[\text{GaH}]^{2+}$  sites via carbenium mechanism.**

The elementary steps outlined in Scheme 2 for  $\text{C}_3\text{H}_8$  dehydrogenation over  $[\text{GaH}]^{2+}$  sites are used here to derive a rate law in terms of kinetic and thermodynamic coefficients. The steady-state hypothesis was applied to all reactive surface intermediates. As discussed in Text S.4 (a), we assumed the physisorption of  $\text{C}_3\text{H}_8$  over  $[\text{GaH}]^{2+}$  sites to form  $[\text{C}_3\text{H}_8\text{-}[\text{GaH}]^{2+}]$  complexes (Step 1) is quasi-equilibrated. Theoretical calculations suggest that that rate-limiting step for the carbenium mechanism is the activation of the  $\alpha$  C-H bond in  $\text{C}_3\text{H}_8$ , resulting in a hydride transfer to the  $\text{Ga}^{3+}$  center and concomitant formation of a propyl carbenium fragment (Step 2). Accordingly, the dehydrogenation rate (per  $[\text{GaH}]^{2+}$ ) can be expressed as equation S9.

$$\frac{\text{Rate, D}}{[\text{GaH}]^{2+}} = k_{\text{carb}}\theta_{\text{phys}} \quad \text{S9}$$

Here, Rate, D refers to the dehydrogenation rate,  $k_{\text{carb}}$  refers to the rate coefficient for  $\alpha$  C-H carbenium activation and  $\theta_{\text{phys}}$  refers to the surface coverage of  $[\text{C}_3\text{H}_8\text{-}[\text{GaH}]^{2+}]$  complexes, the precursor to the rate-limiting transition state and is given by equation S10.

$$\theta_{\text{phys}} = \frac{[\text{C}_3\text{H}_8 - [\text{GaH}]^{2+}]}{[\text{L}]} \quad \text{S10}$$

Here,  $[\text{C}_3\text{H}_8 - [\text{GaH}]^{2+}]$  refers to the surface concentration of  $\text{C}_3\text{H}_8 - [\text{GaH}]^{2+}$  complexes and  $[\text{L}]$  refers to the total density of active sites i.e  $[\text{GaH}]^{2+}$  sites.  $[\text{L}]$  can be described in terms of the various reactive surface intermediates via equation S11. Inhibition by  $\text{H}_2$  can be described via the formation of  $[\text{GaH}_2]^+ - \text{H}^+$  cation pairs, as shown in equation S3.

$$[\text{L}] = [\text{GaH}]^{2+} + [\text{C}_3\text{H}_8 - [\text{GaH}]^{2+}] + [[\text{GaH}_2]^+ - \text{H}^+] \quad \text{S11}$$

Since the interaction of gas-phase  $\text{C}_3\text{H}_8$  with  $[\text{GaH}]^{2+}$  cations is predicted to be weak, the second term in equation S11 can be neglected. Together with equations S1, S9-S11, a rate law for dehydrogenation via the carbenium mechanism can be derived, shown as equation S12 here and as equation 4 in the main text.

$$\frac{\text{Rate, D}}{[\text{GaH}]^{2+}} = \frac{k_{\text{carb}}K_{\text{phys}}[\text{C}_3\text{H}_8]}{1 + K_{\text{H}_2}[\text{H}_2]} \quad \text{S12}$$

It can be seen from equation S12, that in the absence of cofed  $\text{H}_2$  at very low  $\text{H}_2$  concentrations, equation S12 reduces to equation S13, which predicts the dehydrogenation rate to bear a first-order dependence on  $\text{C}_3\text{H}_8$  at all  $\text{C}_3\text{H}_8$  partial pressures.

$$\frac{\text{Rate, D}}{[\text{GaH}]^{2+}} = \frac{k_{\text{carb}}K_{\text{phys}}[\text{C}_3\text{H}_8]}{1} \quad \text{S13}$$

**(b) Derivation of rate law for  $\text{C}_3\text{H}_8$  cracking over  $[\text{GaH}]^{2+}$  sites via alkyl mechanism.**

The elementary steps outlined in Scheme 3 for C<sub>3</sub>H<sub>8</sub> cracking over [GaH]<sup>2+</sup> sites can be used to derive a rate expression containing kinetic and thermodynamic coefficients that describes the dependence of cracking rates on C<sub>3</sub>H<sub>8</sub> and H<sub>2</sub> partial pressures. Equations S1, S2 and S3 also describe the surface intermediates relevant for C<sub>3</sub>H<sub>8</sub> cracking, as outlined in Scheme 3. Theoretical calculations predict that the rate-limiting step for C<sub>3</sub>H<sub>8</sub> cracking is the C-C bond attack of the anionic C<sub>3</sub>H<sub>7</sub> fragment by the proximate Brønsted acid O-H group that constitutes the [C<sub>3</sub>H<sub>7</sub>-GaH]<sup>+</sup>-H<sup>+</sup> cation pair (Step 3). Therefore, the rate of C<sub>3</sub>H<sub>8</sub> cracking (per [GaH]<sup>2+</sup>) can be expressed as equation S14.

$$\frac{\text{Rate, C}}{[\text{GaH}]^{2+}} = k_{\text{crack}}\theta_{\text{alk}} \quad \text{S14}$$

Here, Rate, C refers to the C<sub>3</sub>H<sub>8</sub> cracking rate,  $k_{\text{crack}}$  refers to the rate coefficient for C-C bond attack in Step 4 and  $\theta_{\text{alk}}$  refers to the surface coverage of [C<sub>3</sub>H<sub>7</sub>-GaH]<sup>+</sup>-H<sup>+</sup> cation pairs, the precursor to the cracking transition state.  $\theta_{\text{alk}}$  can be described by equations S5-S7. Together, these equations lead to a rate expression for C<sub>3</sub>H<sub>8</sub> cracking over [GaH]<sup>2+</sup> sites, in terms of C<sub>3</sub>H<sub>8</sub> and H<sub>2</sub> partial pressures, shown as equation S15 here and equation 5 in the main text.

$$\frac{\text{Rate, C}}{[\text{GaH}]^{2+}} = \frac{k_{\text{crack}}K_{\text{dis}}K_{\text{phys}}[\text{C}_3\text{H}_8]}{1 + K_{\text{dis}}K_{\text{phys}}[\text{C}_3\text{H}_8] + K_{\text{H}_2}[\text{H}_2]} \quad \text{S15}$$

### Text S.5 Derivations of equations relating experimentally measured rate coefficients to apparent and intrinsic activation enthalpies

Both dehydrogenation and cracking rates over Ga/H-MFI obey the behavior predicted by a Langmuir Hinshelwood kinetic model, shown in Equations 1 and 2 of the main text. At very low C<sub>3</sub>H<sub>8</sub> pressures, experimentally observed dehydrogenation and cracking rates bear a first-order dependence on C<sub>3</sub>H<sub>8</sub> pressure. The rate coefficient for this first order dependence ( $k_{app}$ ) bears units of (mol/ mol Al\*s\*bar) can therefore be expressed as a product of an intrinsic, zero-order rate coefficient ( $k_{int}$ ) with units of (mol/ mol Al\*s) and a thermodynamic adsorption constant ( $K_{ads}$ ) with units of (bar<sup>-1</sup>), as shown in Equation S16<sup>3</sup>

$$k_{app} = k_{int} * K_{ads} \quad S17$$

Here, the intrinsic rate coefficient  $k_{int}$  which purely reflects the dynamics between the transition state and the adsorbed state directly preceding it can be expressed with the aid of classical transition-state theory as Equation S18.<sup>4</sup>

$$k_{int} = \frac{\kappa k_B T}{h} \exp\left(-\frac{\Delta G_{int}}{RT}\right) \quad S18$$

Here,  $k_{int}$  is the intrinsic rate constant (s<sup>-1</sup>),  $\kappa$  is the transmission coefficient,  $k_B$  is the Boltzmann constant,  $h$  is the Planck constant,  $T$  is temperature (K),  $\Delta G_{int}$  is the intrinsic Gibbs free energy activation barrier,  $R$  is the gas constant.

The thermodynamic adsorption constant  $K_{ads}$  which relates gas-phase C<sub>3</sub>H<sub>8</sub> to the adsorbed state preceding the transition state can be expressed in terms of the Gibbs free energy of adsorption as Equation S19.<sup>3</sup>

$$K_{\text{ads}} = \exp\left(-\frac{\Delta G_{\text{ads}}}{RT}\right) \quad \text{S19}$$

The Gibbs free energy can be expressed in terms of enthalpy ( $\Delta H$ ) and entropy ( $\Delta S$ ), as shown in Equation S20

$$\Delta G = \Delta H - T\Delta S \quad \text{S20}$$

Combining Equations S17-S19 leads to Equation S21

$$k_{\text{app}} = \frac{k_{\text{B}}T}{h} \exp\left(-\frac{\Delta G_{\text{int}}}{RT}\right) \exp\left(-\frac{\Delta G_{\text{ads}}}{RT}\right) \quad \text{S21}$$

Further simplification of Equation S21 leads to Equation S22

$$k_{\text{app}} = \frac{k_{\text{B}}T}{h} \exp\left(-\frac{(\Delta G_{\text{int}} + \Delta G_{\text{ads}})}{RT}\right) \quad \text{S22}$$

Equations S22 suggests that the apparent first order rate coefficient reflects the the Gibbs free energy of activation with respect to gas-phase  $\text{C}_3\text{H}_8$  ( $\Delta G_{\text{app}}$ ), as also summarized in Scheme 4 of the main text. This finding can be summarized as Equation S23.

$$\Delta G_{\text{app}} = \Delta G_{\text{int}} + \Delta G_{\text{ads}} \quad \text{S23}$$

Combining Equation S20 with Equation S22 and S23, the first order rate coefficient can be expressed in terms of the apparent activation enthalpy ( $\Delta H_{\text{app}}$ ) and entropy ( $\Delta S_{\text{app}}$ ), shown here as Equation S24

$$\ln\left(\frac{k_{\text{app}}}{T}\right) = -\frac{\Delta H_{\text{app}}}{RT} + \frac{\Delta S_{\text{app}}}{R} + \ln\left(\frac{k_{\text{B}}}{h}\right) \quad \text{S24}$$

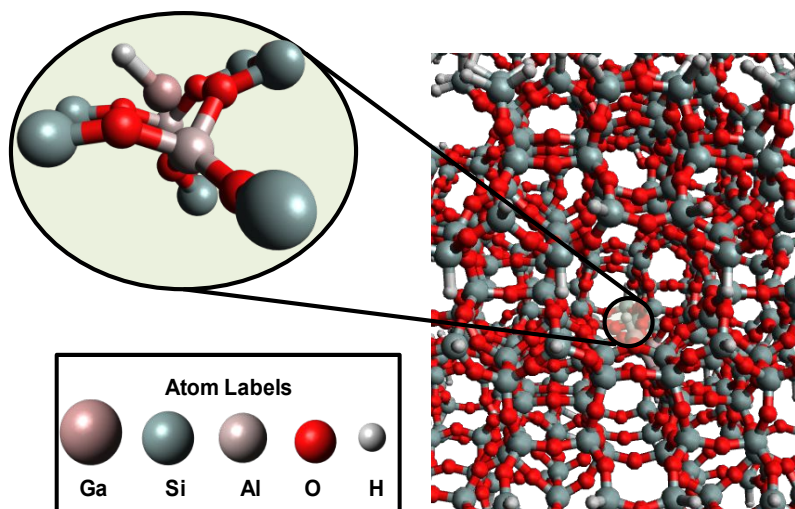
Similarly, Equation S18 together with Equation S20 can be used to express the intrinsic rate coefficient ( $k_{\text{int}}$ ) in terms of the intrinsic activation enthalpy ( $\Delta H_{\text{int}}$ ) and entropy ( $\Delta S_{\text{int}}$ ), shown here as Equation S25

$$\ln \left( \frac{k_{\text{int}}}{T} \right) = - \frac{\Delta H_{\text{int}}}{RT} + \frac{\Delta S_{\text{int}}}{R} + \ln \left( \frac{k_B}{h} \right) \quad \text{S25}$$

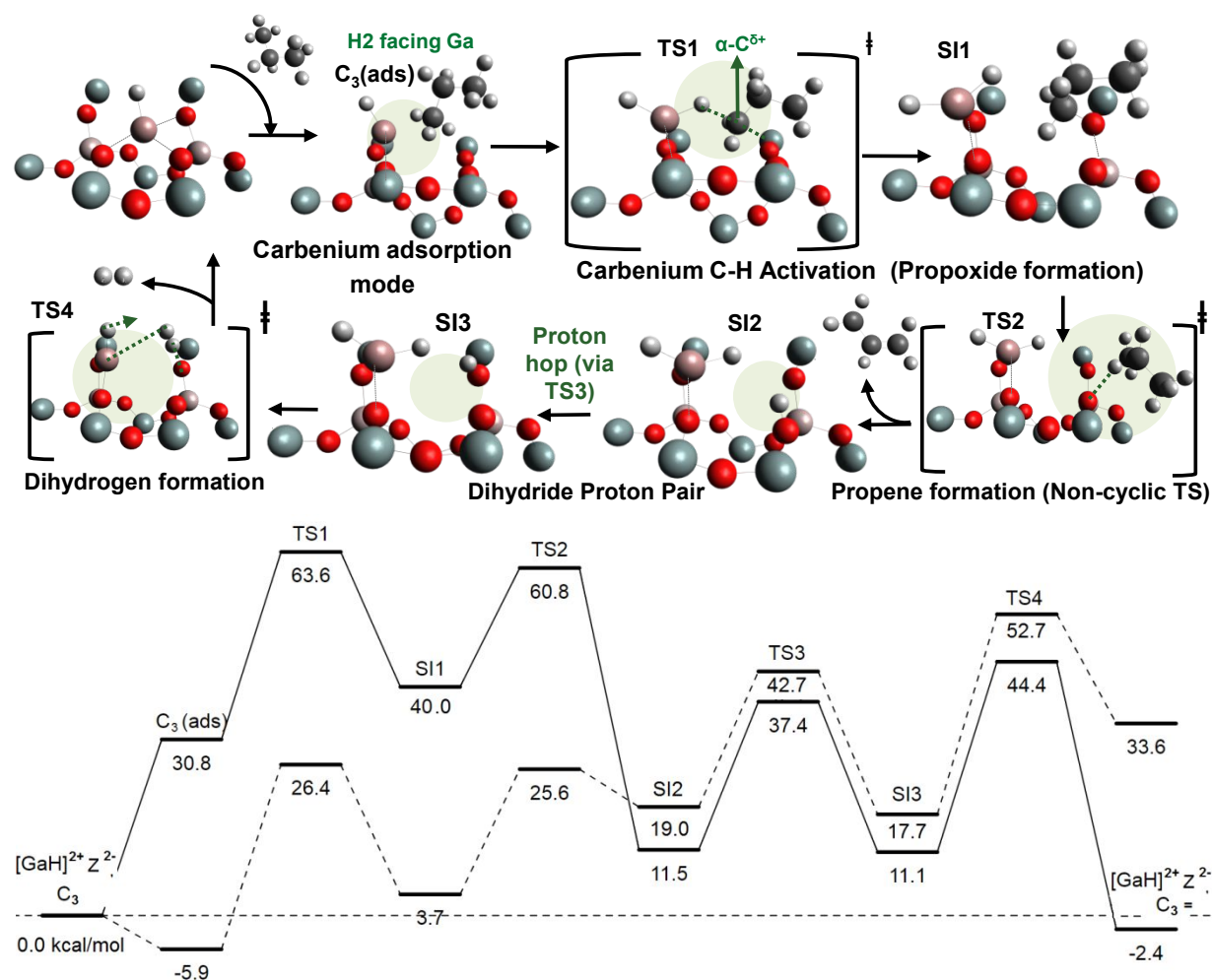
Finally, the thermodynamic adsorption constant ( $K_{\text{ads}}$ ) can be expressed in terms of the adsorption enthalpy ( $\Delta H_{\text{ads}}$ ) by combining Equation S19 and S20, shown here as Equation S26

$$\ln (K_{\text{ads}}) = - \frac{\Delta H_{\text{ads}}}{RT} + \frac{\Delta S_{\text{ads}}}{R} \quad \text{S26}$$

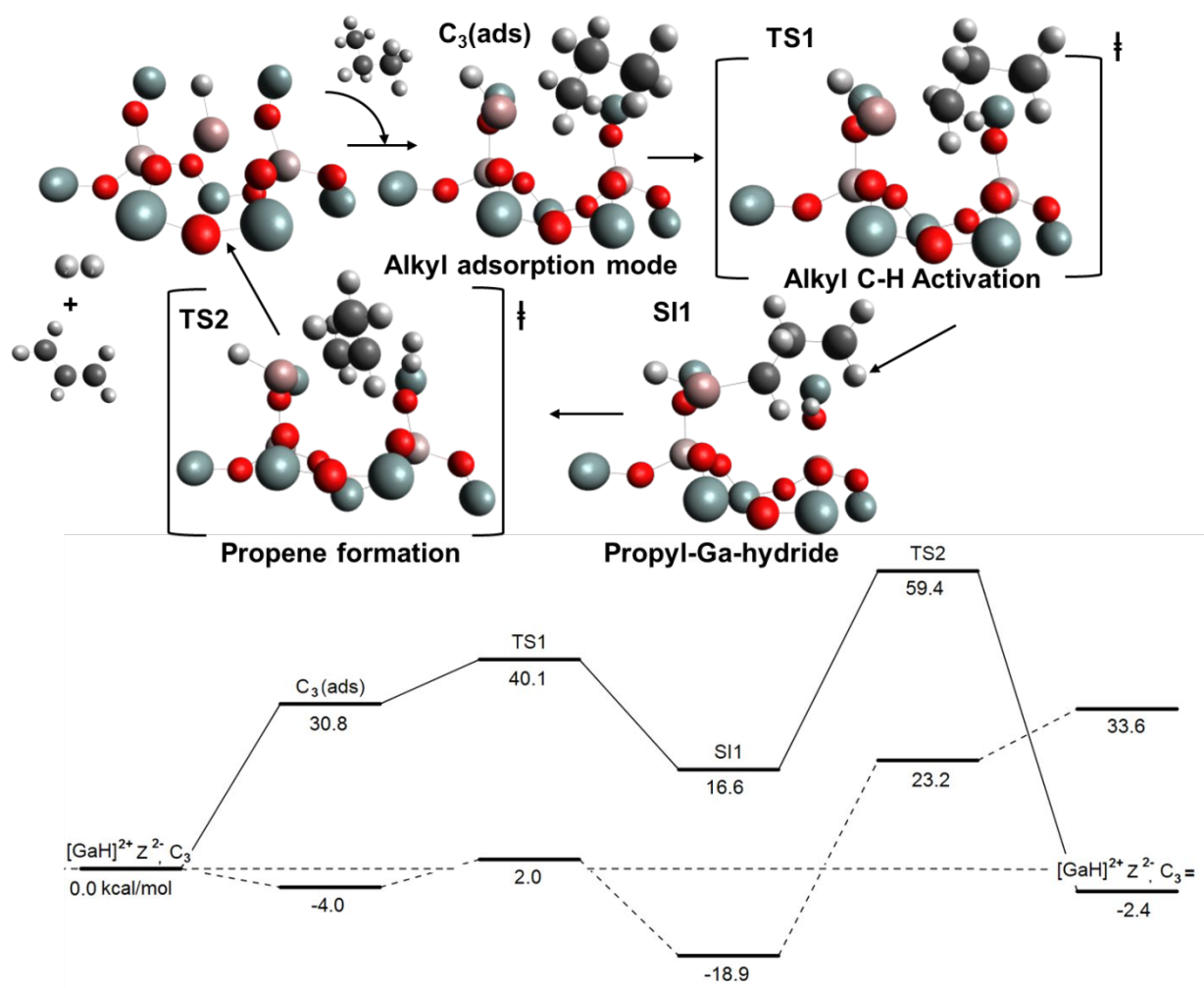
Plots of  $\ln (k_{\text{int}}/T)$  vs  $1/T$  lead to the extraction of  $\Delta H_{\text{app}}$ ,  $\Delta H_{\text{int}}$  and  $\Delta H_{\text{ads}}$  via linear regression methods. These plots are presented for dehydrogenation and cracking in Figures S10, S11 and S12.



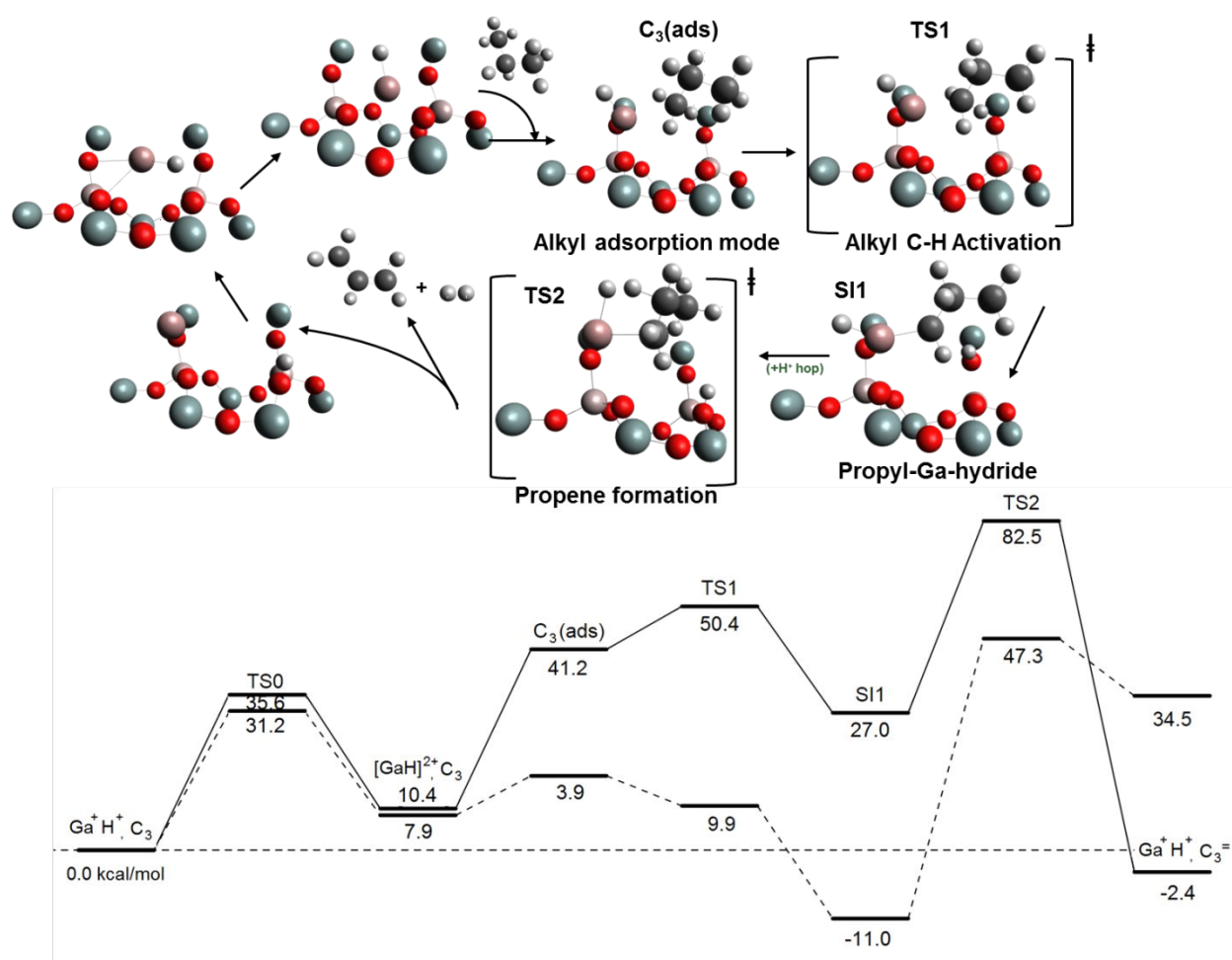
**Figure S5.** View along [100] axis of T437 atom MFI structure used to model  $[\text{GaH}]^{2+}$  sites in Ga/H-MFI. The QM region consists of a T9 model which is electrostatically embedded in an MM region



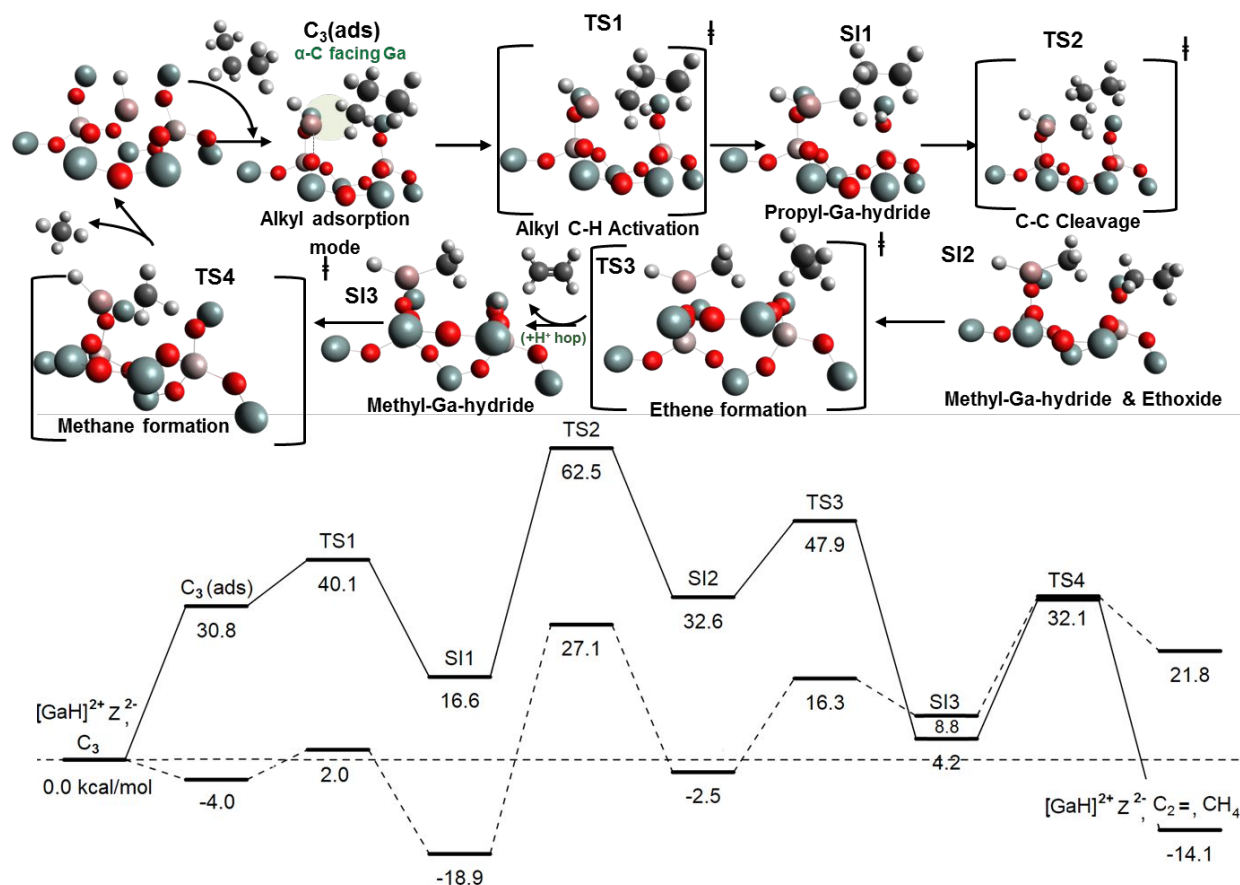
**Figure S6.** Free Energy (full lines) and enthalpy (dashed lines) landscapes for  $C_3H_8$  dehydrogenation via carbenium mechanism on  $[GaH]^{2+}$  sites, reported at 733 K, 10 kPa  $C_3H_8$ , 0.5 kPa  $C_3H_6$  and 0.5 kPa  $H_2$ . Only the QM region from the QM/MM model has been displayed here to illustrate the elementary steps in this mechanism, using the key from Figure S5.



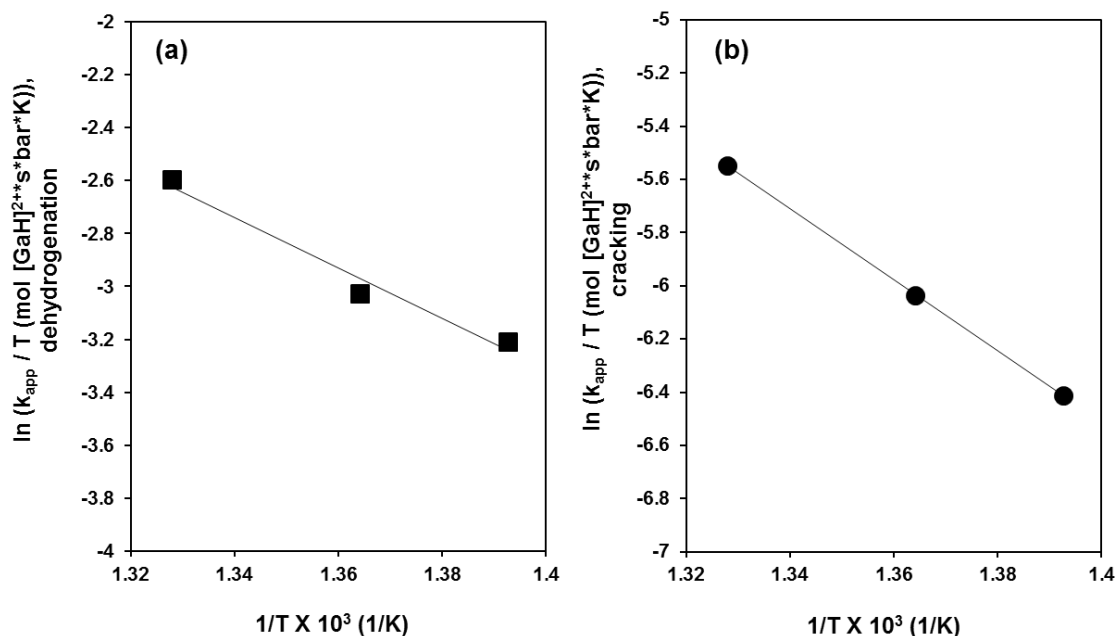
**Figure S7.** Free Energy (full lines) and enthalpy (dashed lines) landscapes for  $C_3H_8$  dehydrogenation via alkyl mechanism on  $[GaH]^{2+}$  sites, reported at 733 K, 10 kPa  $C_3H_8$ , 0.5 kPa  $C_3H_6$  and 0.5 kPa  $H_2$ . Only the QM region from the QM/MM model has been displayed here to illustrate the elementary steps in this mechanism, using the key from Figure S5.



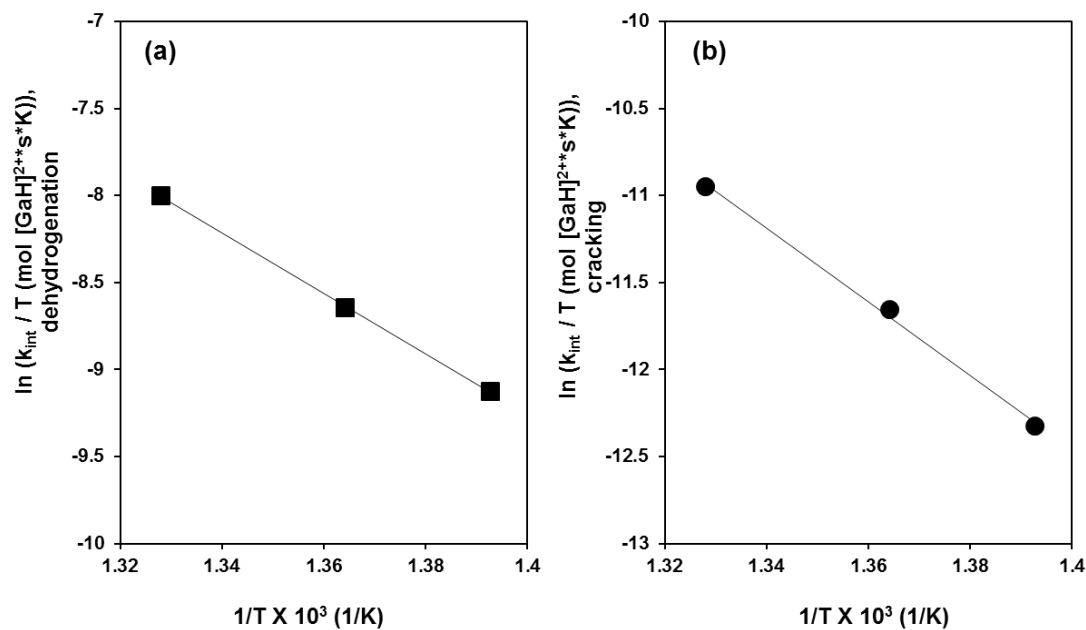
**Figure S8.** Free Energy (full lines) and enthalpy (dashed lines) landscapes for  $C_3H_8$  dehydrogenation on  $Ga^+ H^+$  sites, reported at 733 K, 10 kPa  $C_3H_8$ , 0.5 kPa  $C_3H_6$  and 0.5 kPa  $H_2$ . Only the QM region from the QM/MM model has been displayed here to illustrate the elementary steps in this mechanism, using the key from Figure S5.



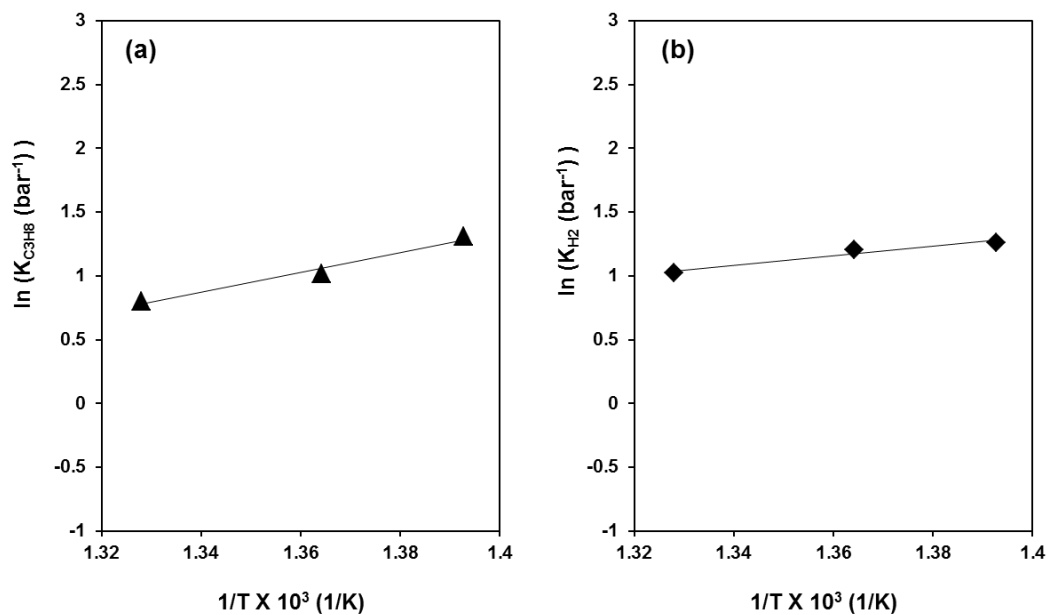
**Figure S9.** Free Energy (full lines) and enthalpy (dashed lines) landscapes for  $C_3H_8$  cracking via alkyl mechanism on  $[GaH]^{2+}$  sites, reported at 733 K, 10 kPa  $C_3H_8$ , 0.5 kPa  $C_2H_4$ , and 0.5 kPa  $CH_4$ . Only the QM region from the QM/MM model has been displayed here to illustrate the elementary steps in this mechanism, using the key from Figure S5.



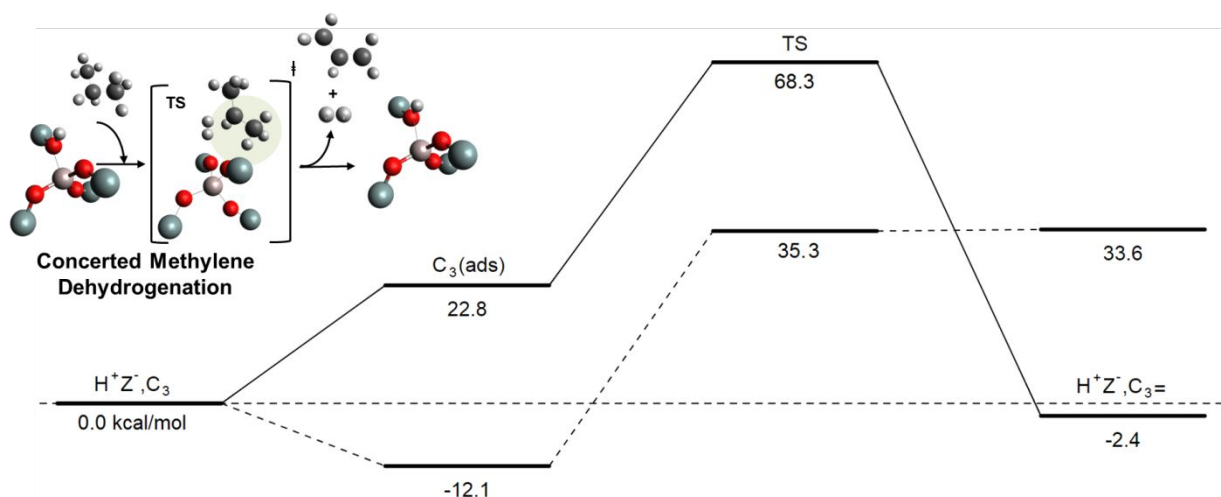
**Figure S10:** Plots of  $\ln(k_{app}/T)$  vs  $1/T$  for (a) C<sub>3</sub>H<sub>8</sub> dehydrogenation (b) C<sub>3</sub>H<sub>8</sub> cracking for the Ga/Al = 0.2 sample. Values for  $k_{app}$  (first order rate coefficients) were obtained by regression of rate data in Figures 5a-c and 6a-c to Equations 1 and 2. Rate coefficients were normalized to the fraction of [GaH]<sup>2+</sup> sites per Al<sub>tot</sub> estimated via NH<sub>3</sub>-TPD.<sup>5</sup> Solid lines reflect linear regression to Equation S24



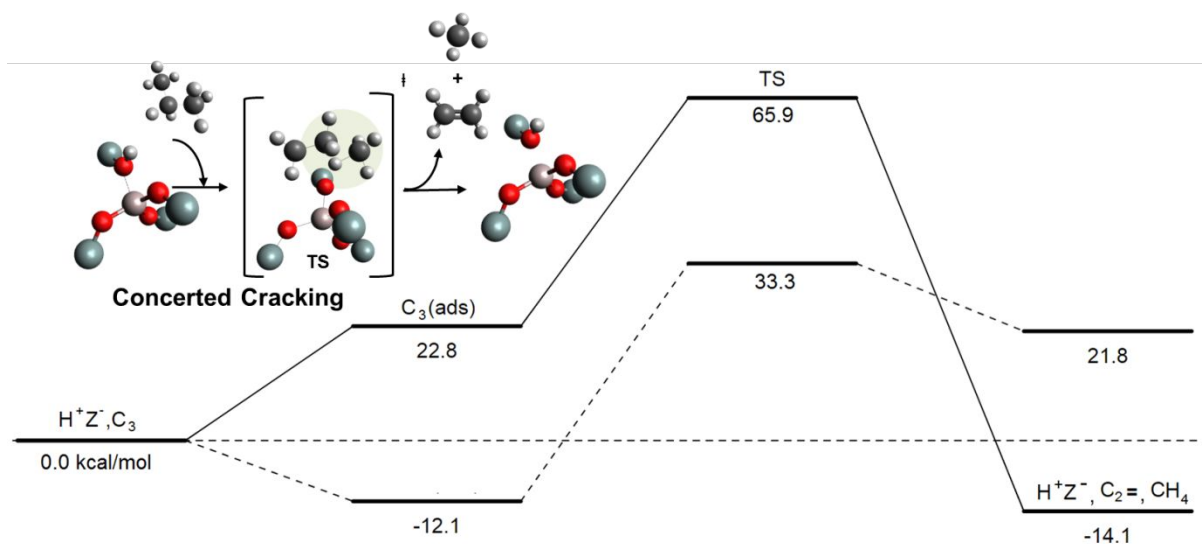
**Figure S11:** Plots of  $\ln(k_{\text{int}}/T)$  vs  $1/T$  for (a)  $\text{C}_3\text{H}_8$  dehydrogenation (b)  $\text{C}_3\text{H}_8$  cracking for the  $\text{Ga}/\text{Al} = 0.2$  sample. Values for  $k_{\text{int}}$  (zero order rate coefficients) were obtained by regression of rate data in Figures 5a-c and 6a-c to Equations 1 and 2. Rate coefficients were normalized to the fraction of  $[\text{GaH}]^{2+}$  sites per  $\text{Al}_{\text{tot}}$  estimated via  $\text{NH}_3$ -TPD.<sup>5</sup> Solid lines reflect linear regression to Equation S25.



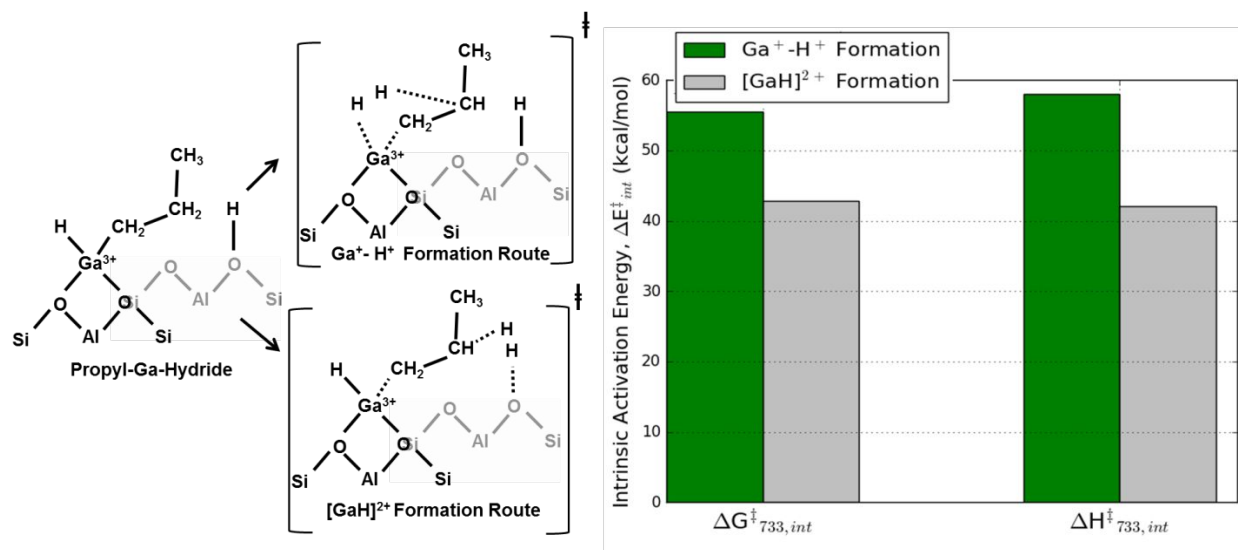
**Figure S12:** Plots of  $\ln(K_{\text{ads}})$  vs  $1/T$  for (a)  $\text{C}_3\text{H}_8$  adsorption (b)  $\text{H}_2$  adsorption for the Ga/Al = 0.2 sample. Values for  $K_{\text{ads}}$  (adsorption constants) were obtained by regression of rate data in Figures 5a-c and 6a-c to Equations 1 and 2. Solid lines reflect linear regression to Equation S26.



**Figure S13.** Free Energy (full lines) and enthalpy (dashed lines) landscapes for  $C_3H_8$  dehydrogenation (methylene) on Brønsted acid O-H groups, reported at 733 K, 10 kPa  $C_3H_8$ , 0.5 kPa  $C_3H_6$  and 0.5 kPa  $H_2$ . Only the QM region from the QM/MM model has been displayed here to illustrate the elementary steps in this mechanism, using the key from Figure S5.



**Figure S14.** Free Energy (full lines) and enthalpy (dashed lines) landscapes for  $C_3H_8$  cracking catalyzed by Brønsted acid O-H groups, reported at 733 K, 10 kPa  $C_3H_8$ , 0.5 kPa  $C_2H_4$ , and 0.5 kPa  $CH_4$ . Only the QM region from the QM/MM model has been displayed here to illustrate the elementary steps in this mechanism, using the key from Figure S5.



**Figure S15.** Free Energy and enthalpy barriers for  $C_3H_6$  formation from  $C_3H_7$ -Ga-hydride intermediates, reported at 733 K, 10 kPa  $C_3H_8$ , 0.5 kPa  $C_3H_6$ , 0.5 kPa  $C_2H_4$ , and 0.5 kPa  $CH_4$ .

### **Text S.6 Estimation of exchange stoichiometries of Ga<sup>3+</sup> species H<sub>2</sub>-reduced Ga/H-MFI via NH<sub>3</sub>-TPD and density of [GaH]<sup>2+</sup> cations in Ga/H-MFI samples**

In a recently published study, our group developed protocols for the synthesis of well-defined and isolated Ga<sup>3+</sup> cations in Ga/H-MFI via the vapor-phase exchange of dehydrated H-MFI with GaCl<sub>3</sub>.<sup>5</sup> These materials were characterized using a number of spectroscopic and chemical probes in order to elucidate the structure of Ga<sup>3+</sup> species under oxidizing and reducing conditions. These findings were also corroborated with the aid of theoretical calculations.

H<sub>2</sub> –temperature programmed reduction, infrared spectroscopy, Ga K-edge XANES (X-Ray Absorption Near Edge Spectroscopy) and EXAFS (Extended X-Ray Absorption Fine Structure) and theoretical calculations suggested that at low Ga/Al ratios and under reducing anhydrous conditions, [GaH]<sup>2+</sup> and [GaH<sub>2</sub>]<sup>+</sup>-H<sup>+</sup> cation pairs form in Ga/H-MFI.<sup>5</sup> The relative proportion of these cationic species can be determined on the basis of their exchange stoichiometry (H<sup>+</sup> exchanged per Ga<sup>3+</sup> atom) because [GaH]<sup>2+</sup> cations titrate 2 Brønsted acid O-H groups (H<sup>+</sup>) per Ga<sup>3+</sup> atom while [GaH<sub>2</sub>]<sup>+</sup> cations titrate 1 Brønsted acid O-H group (H<sup>+</sup>) per Ga<sup>3+</sup> atom. The exchange stoichiometry of Ga/H-MFI samples was determined on the basis of titration of residual Brønsted acid O-H groups in Ga/H-MFI by NH<sub>3</sub>. The quantity of NH<sub>3</sub> adsorbed was determined by means of NH<sub>3</sub> –temperature programmed desorption experiments.

These experiments were conducted over H<sub>2</sub>-reduced Ga/H-MFI samples using protocols developed by Di Iorio et al. that enable the selective titration of residual Brønsted acid O-H groups in metal-exchanged zeolites, without concomitant titration of metal cations by NH<sub>3</sub>.<sup>6</sup> The reader is referred to our characterization study of Ga/H-MFI for exact details of the experimental

procedures used here to conduct NH<sub>3</sub>-TPD experiments over Ga/H-MFI.<sup>5</sup> We find that NH<sub>3</sub>-TPD spectra conducted in this fashion show only a feature at 660 K representative of NH<sub>3</sub> desorption from Brønsted acid O-H groups.<sup>5</sup> The quantity of NH<sub>3</sub> desorbed can be estimated by integrating the area under this feature. An assumption of a 1:1 stoichiometry between NH<sub>3</sub> desorbed and H<sup>+</sup> leads to an estimate of the concentration of residual Brønsted acid O-H groups in the sample. This quantity together with the density of Brønsted acid O-H groups per Al<sub>tot</sub> present in the parent in the H-MFI sample can be used to compute the fraction of Brønsted acid O-H groups replaced per Al<sub>tot</sub> atom. When normalized by the Ga/Al ratio, the exchange stoichiometry – H<sup>+</sup> exchanged per Ga<sup>3+</sup> atom is obtained. The exchange stoichiometries for H<sub>2</sub>- reduced Ga/H-MFI samples are shown in Table S2. Since [GaH]<sup>2+</sup> cations are expected to possess an exchange stoichiometry of 2 H<sup>+</sup><sub>exch</sub> per Ga<sup>3+</sup> atom, the density of [GaH]<sup>2+</sup> /Al can be readily estimated, as shown in Table S1. This density is similar within error (H<sup>+</sup><sub>exch</sub>/Ga estimates have errors of  $\pm$  20%) to the expected density of [GaH]<sup>2+</sup> if a 100% of Ga at a Ga/Al ratio of 0.1 is [GaH]<sup>2+</sup> and if further increases in Ga/Al ratio do not lead to the formation of any additional [GaH]<sup>2+</sup>.

For the Ga/Al = 0.05 sample and 0.5 sample, errors in NH<sub>3</sub>-TPD quantification were too large to accurately determine the density of [GaH]<sup>2+</sup> cations. On the basis of the trend observed in Table S2, where the fraction of [GaH]<sup>2+</sup> is maximum at a Ga/Al ratio of 0.1, it was assumed that the close distance ( $\leq 5$  Å) proximate cation-exchange sites that have been found to be required for the formation of [GaH]<sup>2+</sup> cations in our previous work<sup>5</sup> would be saturated at a Ga/Al ratio of 0.1. For Ga/Al ratios less than 0.1 therefore, it was assumed that a sufficient concentration of such cation-exchange sites would be available for Ga<sup>3+</sup> siting and therefore a 100% of the Ga would be present at [GaH]<sup>2+</sup> cations. This analysis leads to an estimate of 0.05 [GaH]<sup>2+</sup> /Al<sub>tot</sub> for a Ga/Al ratio of 0.05. For the Ga/Al = 0.5 sample, it was assumed any

additional Ga exceeding a Ga/Al ratio of 0.1 in this sample would not form  $[\text{GaH}]^{2+}$  cations.

Therefore, a value of 0.1  $[\text{GaH}]^{2+}/\text{Al}_{\text{tot}}$  was assumed for this sample.

**Table S2:**  $\text{H}^+_{\text{exch}}/\text{H}^+_{\text{total}}$ ,  $\text{H}^+_{\text{exch}}/\text{Ga}$  and  $[\text{GaH}]^{2+}/\text{Al}_{\text{tot}}$  values measured via  $\text{NH}_3$ -TPD after  $\text{H}_2$  treatment of Ga/H-MFI samples at 823 K.

| Ga/Al | $\text{H}^+_{\text{exch}}/\text{H}^+_{\text{tot}}$ | $\text{H}^+_{\text{exch}}/\text{Ga}^{\text{a}}$ | Predicted $\text{H}^+_{\text{exch}}/\text{Ga}^{\text{b}}$ | $[\text{GaH}]^{2+}/\text{Al}_{\text{tot}}$ |
|-------|----------------------------------------------------|-------------------------------------------------|-----------------------------------------------------------|--------------------------------------------|
| 0.1   | 0.2                                                | 2.2                                             | 2.0                                                       | 0.1                                        |
| 0.2   | 0.3                                                | 1.5                                             | 1.5                                                       | 0.1                                        |
| 0.3   | 0.4                                                | 1.2                                             | 1.3                                                       | 0.1                                        |

<sup>a</sup> Obtained from  $\text{NH}_3$ -TPD profiles of  $\text{H}_2$ -treated Ga/H-MFI samples.  $\text{NH}_3/\text{Al}_{\text{tot}}$  values from these experiments were used together with eq (2) in order to estimate  $\text{H}^+_{\text{exch}}/\text{H}^+_{\text{tot}}$ . These values were then normalized by the Ga/ $\text{Al}_f$  ratio (obtained by dividing Ga/ $\text{Al}_{\text{tot}}$  values by the  $\text{Al}_f/\text{Al}_{\text{tot}}$  value for H-MFI, to reflect framework  $\text{Al}_f$  in order to obtain values of  $\text{H}^+_{\text{exch}}/\text{Ga}$ )

<sup>b</sup> Predicted values are based on the assumption that 100% of Ga at a Ga/Al ratio of 0.1 is present as  $[\text{GaH}]^{2+}$  cations and no further  $[\text{GaH}]^{2+}$  is product upon further increases in Ga content

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