

SUPPORTING INFORMATION

Thermoresponsive Supramolecular Hydrogels with High Fracture Toughness

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Part 1: Video of pure shear test for notched NF10 hydrogel.

Part 2: Calculation of crosslink density of the NFx hydrogels.

An effective crosslink density of the supramolecular hydrogels was calculated from the phantom network model¹ for rubber elasticity using the tensile modulus data, assuming a Poisson ratio of 0.5 and using the volume of the swollen hydrogel as the reference volume.

$$G = \frac{E}{3} = \left(1 - \frac{2}{f}\right) \nu_e RT \phi_2^{\frac{1}{3}} \quad (S1)$$

where G is the shear modulus, ν_e is the crosslink density, f is the functionality of the crosslinks and ϕ_2 is the volume fraction of polymer in the fully swollen hydrogel,

$$\phi_2 = \left[1 + \frac{(q-1)\rho}{d}\right]^{-1} \quad (S2)$$

Where q is the swelling ratio (mass of hydrogel/mass of dry polymer), d is the solvent (water) density ($1.00 \text{ g}\cdot\text{cm}^{-3}$) and ρ is the density of the dry NFx copolymers ($1.21 \text{ g}\cdot\text{cm}^{-3}$, $1.25 \text{ g}\cdot\text{cm}^{-3}$, $1.28 \text{ g}\cdot\text{cm}^{-3}$ and $1.34 \text{ g}\cdot\text{cm}^{-3}$ for NF5, NF8, NF10 and NF14, respectively).

Each FOSA group is attached to two NIPAM chains, so each FOSA—FOSA supramolecular bond produces four network chains. Thus the functionality, f , of a nanodomain crosslinks is twice the number of FOSA groups within the nanodomain (N_{agg}). Values for N_{agg} , determined by small angle neutron scattering² for NF5, NF10 and NF10 hydrogels at temperatures

between 9°C and 13°C vary from ~29 – 59, values of f for the NFx hydrogels used in the present study were estimated to be $f = 2N_{agg} \sim 60 - 120$. Thus, the $2/f$ term in Equation (1) is essentially negligible and

$$\nu_e \approx \frac{E}{3RT\phi_2^{1/3}} \quad (S3)$$

Part 3: Tensile tests of samples with various notch sizes (crack lengths)

Pure shear tests following the method described by Rivlin and Thomas³ and using the same type of specimen used for the pure shear tests described in the paper, except that the crack length, c , was varied were used to calculate the fracture energy of the NF10 hydrogel. Figure S1 shows the measured tensile force, F , vs. strain for NF10 specimens with initial crack lengths of 1 – 9 mm. The work, W , required to deform that sample to a specific strain, ϵ_L , is the area under the F - ϵ curves integrated to $\epsilon = \epsilon_L$. Figure S2 shows the initial crack length dependence on W measured at a constant strain of $\epsilon_L = 476\%$, which was the fracture strain for the sample with the 9 mm notch. The W - c data were fit with a linear least squares regression, solid line in Figure S2, and the slope of the line was $\left(\frac{\partial U}{\partial c}\right)_{\epsilon_L} = -(4.62 \pm 0.76) \text{ J/m}$. The fracture energy is given by equation (S4)³.

$$\Gamma = -\frac{1}{t} \left(\frac{\partial U}{\partial c}\right)_{\epsilon_L} \quad (S4)$$

where t = specimen film thickness. In this case $\Gamma = 6.3 \pm 1.0) \text{ kJ/m}^2$, which is comparable to the value determined from the pure shear analysis of Suo et al.⁴ of $\Gamma = 7.8 \pm 1.1) \text{ kJ/m}^2$.

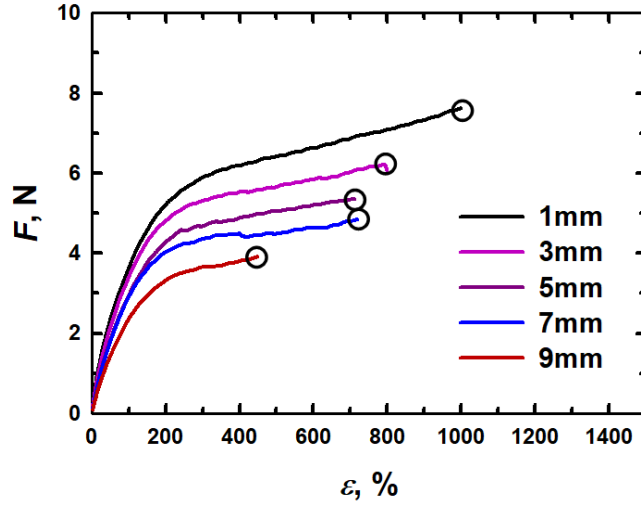


Figure S1. F versus strain curves at 5°C for NF10 hydrogel samples with various notch length. The circles indicate the strain at which the notch began to propagate.

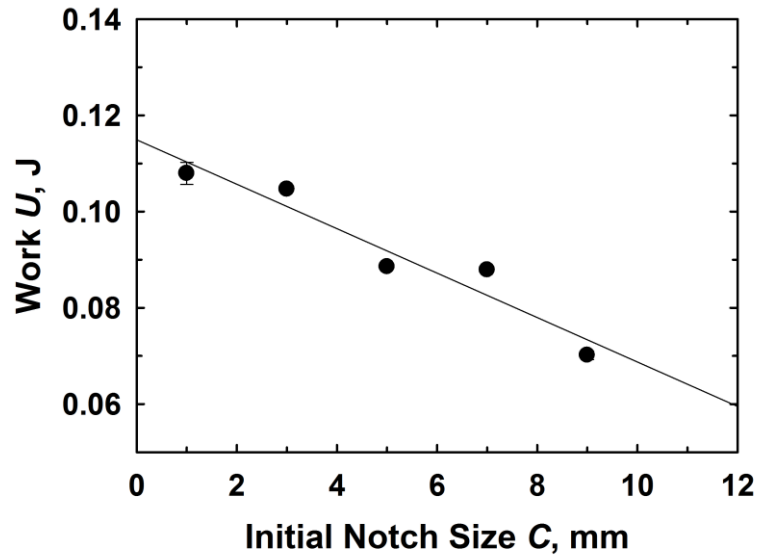


Figure S2. Work U versus initial notch size C for the NF10 hydrogel at 5°C. A linear least squares fit is shown. The slope is $\left(\frac{\partial U}{\partial c}\right)_{\epsilon_L} = -(4.62 \pm 0.76) \text{ J/m}$.

References

1. Treloar, L. R. G. *The Physics of Rubber Elasticity*; Oxford University Press, 1975.
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3. Rivlin, R. S.; Thomas, A. G. Rupture of rubber. I. Characteristic energy for tearing. *J. Polym. Sci.* 1953, *10*, 291.
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