The chemical mechanism of exhaust gas recirculation on polycyclic aromatic hydrocarbons formation based on LIF measurement

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1. The details of time resolved LII intensity calculation

In order to eliminate the bias caused by the evolution of LII signal. A simulation of time resolved LII signal has been performed. The well-known energy balance model for LII after energy absorption, originally formulated by Melton [1] and subsequently refined by a number of researchers over the years [2–4], includes heat addition by the laser pulse and various cooling terms in the general form:

$$\frac{\mathrm{d}U_{\rm in}}{\mathrm{d}t} = \dot{Q}_{\rm a} - \dot{Q}_{\rm s} - \dot{Q}_{\rm c} - \dot{Q}_{\rm r} \quad (1)$$

where U_{in} , \dot{Q}_a , \dot{Q}_s , \dot{Q}_c and \dot{Q}_r represent, respectively, the internal energy, the laser energy absorption rate, the sublimation rate of carbonaceous materials, the rate of heat loss via thermal conduction and the rate of heat loss via thermal radiation. The rate of change in internal energy of a spherical primary particle can be expressed as:

$$\frac{\mathrm{d}U_{\mathrm{in}}}{\mathrm{d}t} = \rho_{\mathrm{s}} c_{\mathrm{s}} \frac{\pi}{6} D^{3} \frac{\mathrm{d}T}{\mathrm{d}t} \quad (2)$$

where the values of density ρ_s and specific heat capacity c_s can be found in table 1. The absorption term \dot{Q}_a is given with Eq. (3)

$$\dot{Q}_{a} = \frac{\pi^{2} D^{3} E(m)}{\lambda_{1}} \bullet \frac{Fq(t)}{q_{\max}} (3)$$

where F is the fluence of laser beam/sheet with the unit of J/m², q(t) is the temporal profile of laser pulse, q_{max} is a constant used to normalize the integrated laser temporal profile to unity, λ_1 is the laser wavelength, and E(m) is the absorption function of soot at certain λ_1 . In the present study, the value of E(m) is problematic since λ_1 is 266 nm, which is not a normally used wavelength to conduct LII measurements. Therefore, there is few value of E(m) under this wavelength wasreported. Here we use the experimental data for E(m) of Krishnan et al. [5] and a linear fitting by Snelling et al.[6] to estimate the value at 266 nm, which is:

$$E(m) = 0.232 + \lambda \cdot (1.2546 \times 10^5 \text{ m}^{-1})$$
 (4)

The calculations of the heat loss rate via conduction \dot{Q}_{c} , sublimation \dot{Q}_{s} and radiation \dot{Q}_{r} are based on the fully constrained model summarized by Michelsen et al. [3,4] as Eqs. (5-7):

$$\dot{Q}_{\rm c} = \frac{2k_{\rm a}\pi D^2}{D + GL_{\rm MFP}} (T - T_{\rm g}) \qquad (5)$$

where T_g is the temperature of the ambient gases, k_a is the thermal conductivity of the surrounding gases, and L_{MFP} is the mean free path. The heat transfer factor G is given by $G = \frac{8f}{\alpha_T(\gamma+1)}$, where α_T is the thermal accommodation coefficient; γ is the heat capacity ratio for air; and f is the Eucken correction to the thermal conductivity given by: $f = \frac{9\gamma-5}{4}$. Sublimation is an endothermic phase transition process. Heat loss by sublimation is modeled as:

$$\dot{Q}_{\rm s} = -\frac{\Delta H_{\rm v}}{W_{\rm s}} \frac{\mathrm{d}M}{\mathrm{d}t} = \frac{\Delta H_{\rm v}}{W_{\rm s}} \frac{\pi W_{\rm v} \alpha_M P_{\rm v}}{R_{\rm g} T} \left(\frac{R_{\rm g} T}{2W_{\rm v}}\right)^{\frac{1}{2}} \quad (6)$$

where $W_{\rm s}$ is the molecular weight of solid carbon, and $\Delta H_{\rm v}$ is the enthalpy of formation of sublimed carbon clusters; α_M is the mass accommodation coefficient, which is taken as unity in the present study[1,7]; $R_{\rm g}$ is the universal gas constant; $W_{\rm v}$ is the molecule weight of C3, which is assumed as main composition of vapored cluster of carbon; $P_{\rm v}$ is the partial pressure of sublimed carbon clusters C3, and is given by the Clausius-Clapeyron equation: $P_{\rm v} = P_{\rm ref} \exp\left[-\frac{\Delta H_{\rm v}}{R_{\rm g}}\left(\frac{1}{T}-\frac{1}{T_{\rm ref}}\right)\right]$, $P_{\rm ref}$ is 1 bar and $T_{\rm ref}$ is 3915 K from fits to data by Leideret al. [8].The total power of radiation can be calculated by integrating Planck's radiation function over all wavelengths:

$$\dot{Q}_{\rm r} = \int_{0}^{\infty} \varepsilon_{\lambda_{\rm LII}} \frac{2\pi^2 D^2 h c^2}{\lambda_{\rm LII}^5 \left[\exp\left(\frac{hc}{\lambda_{\rm LII} k_B T}\right) - 1 \right]} d\lambda_{\rm LII}$$
(7)

where *h* is Planck's constant, *c* is the speed of light, and k_B is the Boltzmann constant. According to Kirchhoff's law[9,10], absorptivity equates with emissivity, and the emissivity for particles in the Rayleigh limit [3] $\varepsilon_{\lambda_{LII}}$ is assumed to be: $\varepsilon_{\lambda_{LII}} = \frac{4\pi DE(m)}{\lambda_{LII}}$

By combining Eqs. (1) to (7), the differential equation Eq. (1) can be solved numerically with certain initial condition of $D = D_0$ and $T = T_g$ to obtain T(t). The values used for all relevant variables values are collected on Table 1 :

Table 1. Values for model calculations.

	Units	Value
ΔH_{v}	J/mol	7.78×10 ⁵ at 3915 K [1]
W _s	kg/mol	0.01201
$ ho_{ m s}$	kg/m ³	$2303.1 - 7.3106 \times 10^{-5} T$ [11–13]
C _s	J/kg·K	$1878 + 0.1082 T - 151.49 T^{-2}[7]$
$lpha_{_{ m T}}$	-	0.3 [3,11]
k _a	W/m·K	$5.83 \times 10^7 (T_g / 273)^{0.82} [1]$

The LII signal S_{LII} at a specific emission wavelength λ_{LII} is calculated according to Planck's radiation function:

$$S_{\rm LII}(t) = \frac{8\pi^3 h c^2 E(m) D^3}{\lambda^6} \left[\frac{1}{\exp\left(\frac{hc}{\lambda k_B T(t)}\right) - 1} - \frac{1}{\exp\left(\frac{hc}{\lambda k_B T_g}\right) - 1} \right]$$
(8)

For a certain particle diameter distribution PDF(D), assuming that the particle number concentration n_p is constant in the probe volume V_m during a single LII event, an integration considering the particle size distribution function PDF(D) yields the total LII signal $J_{LII}(t)$ at the detector surface at time t:

$$J_{\text{LII}}(t) = C_{\text{det}} n_{\text{p}} V_{\text{m}} \int_{0}^{\infty} \text{PDF}(D) S_{\text{LII}}(t) dD \qquad (9)$$

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where C_{det} is a constant of the detection system.

Previous study shows that the decay of $J_{LII}(t)$ is dominated by Sauter mean diameters $D_{32}[14,15]$ since the surface heat conduction is the dominating term in Eq. (1). D_{32} is defined as:

$$D_{32} = \frac{\int_{0}^{0} D^{3} \text{PDF}(D) dD}{\int_{0}^{\infty} D^{2} \text{PDF}(D) dD}$$
(10)

This means the different particles distributions share a same D_{32} will produce similar $J_{LII}(t)$ decay curve. For simplicity, we use a uniform particle distribution with a certain D_{32} in Eq. (9) to replace the integration term and obtain:

$$J_1(D_{32}) = C_{det} n_p V_m S_{LII}(t, D_{32}) \qquad (11)$$

In the present study, we use the model described above to estimate the LII signal collected by ICCD cameras in the first 50 ns and second 50 ns for a group of particles with certain D_{32} , which are denoted with $J_1(D_{32})$ and $J_2(D_{32})$ respectively. Thus we have:

$$\begin{cases} J_1(D_{32}) = \int_0^{50(\text{ns})} J_{\text{LII}}(t, D_{32}) dt \\ J_2(D_{32}) = \int_{50(\text{ns})}^{100(\text{ns})} J_{\text{LII}}(t, D_{32}) dt \end{cases}$$
(12)

The value of the ratio of the $J_1(D_{32})$ and $J_2(D_{32})$ can be calculated and used to in the LIF image correction. The experimental parameters inputted into the calculation are shown in Table 2:

Parameter	Value
FWHM of laser pulse	5 ns
Laser fluenceF	450 J/m ²
Laser wavelength λ_1	266 nm
Detection wavelength λ	330, 360, 390, 525 nm
Gas temperature $T_{\rm g}$	1750 K

 Table 2. Experimental parameters inputted into the calculation.

For a given group of particle within a problem volume with a certain D_{32} =20 nm, the calculated LII signal is shown in Fig. 1.

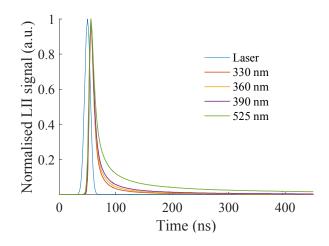


Figure 1. The calculated LII response of a given uniform soot particle distribution D_{32} =20 nm with

input parameters shown in table 1.

The correction coefficient $K(D_{32}) = J_1(D_{32}) / J_2(D_{32})$ of 330, 360, 390, 525 nm is calculate and plotted against D_{32} in Fig. 2.

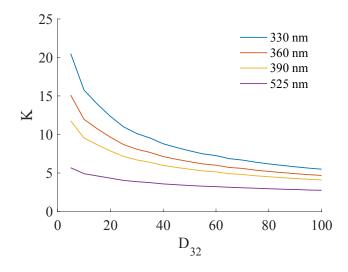


Figure 2. Calculated correction coefficient K against D₃₂.

The value of D_{32} across the tested flames can be evaluated in our previous publication [16], thus the value of *K* can then be determined with Fig. 2. Then, by using Eq. (13), the LIF signal $S_{\text{LIF,cor}}$ can be corrected.

$$S_{\text{LIF,cor}} = S_{\text{LIF}} - K \cdot J_2 \tag{13}$$

For an example, the D_{32} values is 12.84 nm at 1.2 cm, 46.08 nm at 1.3 cm, 55.3 nm at 1.4 cm, and 81.44 at 1.5 cm for the flame L1 case in [16]. The K value converges to a constant starting from 50 nm, as shown in Fig. 2. Given that the experimental signal values are abstracted from HABs = 1.4 to HABs = 2.0 cm, the D_{32} value is assumed to be 80 nm in present study.

References:

- [1] Melton LA. Soot diagnostic based on laser heating. Appl Opt 1984;23:2201–8.
- [2] Schulz C, Kock BF, Hofmann M, Michelsen H, Will S, Bougie B, et al. Laser-induced incandescence: recent trends and current questions. Appl Phys B 2006;83:333–54. doi:10.1007/s00340-006-2260-8.
- [3] Michelsen H a., Liu F, Kock BF, Bladh H, Boiarciuc a., Charwath M, et al. Modeling laser-induced incandescence of soot: a summary and comparison of LII models. Appl Phys B 2007;87:503–21.
 doi:10.1007/s00340-007-2619-5.
- [4] Michelsen H a., Schulz C, Smallwood GJ, Will S. Laser-induced incandescence: Particulate diagnostics for combustion, atmospheric, and industrial applications. Prog Energy Combust Sci 2015:1–47. doi:10.1016/j.pecs.2015.07.001.
- [5] Krishnan SS, Lin K-C, Faeth GM. Extinction and Scattering Properties of Soot Emitted From Buoyant Turbulent Diffusion Flames. J Heat Transfer 2001;123:331. doi:10.1115/1.1350823.
- [6] Snelling DR, Liu F, Smallwood GJ, Gülder ÖL. Determination of the soot absorption function and thermal accommodation coefficient using low-fluence LII in a laminar coflow ethylene diffusion flame. Combust Flame 2004;136:180–90. doi:10.1016/j.combustflame.2003.09.013.
- Kock B, Tribalet B, Schulz C, Roth P. Two-color time-resolved LII applied to soot particle sizing in the cylinder of a Diesel engine. Combust Flame 2006;147:79–92.
 doi:10.1016/j.combustflame.2006.07.009.
- [8] Leider HR, Krikorian OH, Young D a. Thermodynamic properties of carbon up to the critical point. Carbon N Y 1973;11:555–63.

- [9] De Iuliis S, Migliorini F, Cignoli F, Zizak G. Peak soot temperature in laser-induced incandescence measurements. Appl Phys B 2006;83:397–402. doi:10.1007/s00340-006-2210-5.
- [10] De Iuliis S, Migliorini F, Cignoli F, Zizak G. 2D soot volume fraction imaging in an ethylene diffusion flame by two-color laser-induced incandescence (2C-LII) technique and comparison with results from other optical diagnostics. Proc Combust Inst 2007;31:869–76. doi:10.1016/j.proci.2006.07.149.
- Bladh H, Johnsson J, Bengtsson P-E. On the dependence of the laser-induced incandescence (LII) signal on soot volume fraction for variations in particle size. Appl Phys B 2007;90:109–25.
 doi:10.1007/s00340-007-2826-0.
- Blacha T, Di Domenico M, Gerlinger P, Aigner M. Soot predictions in premixed and non-premixed laminar flames using a sectional approach for PAHs and soot. Combust Flame 2012;159:181–93. doi:10.1016/j.combustflame.2011.07.006.
- [13] Olofsson N-E, Johnsson J, Bladh H, Bengtsson P-E. Soot sublimation studies in a premixed flat flame using laser-induced incandescence (LII) and elastic light scattering (ELS). Appl Phys B 2013;112:333–42. doi:10.1007/s00340-013-5509-z.
- Sipkens T a., Mansmann R, Daun KJ, Petermann N, Titantah JT, Karttunen M, et al. In situ nanoparticle size measurements of gas-borne silicon nanoparticles by time-resolved laser-induced incandescence.
 Appl Phys B Lasers Opt 2013:1–14. doi:10.1007/s00340-013-5745-2.
- [15] Liu F, Stagg BJ, Snelling DR, Smallwood GJ. Effects of primary soot particle size distribution on the temperature of soot particles heated by a nanosecond pulsed laser in an atmospheric laminar diffusion flame. Int J Heat Mass Transf 2006;49:777–88. doi:10.1016/j.ijheatmasstransfer.2005.07.041.

[16] Gu C, Lin H, Camacho J, Lin B, Shao C, Li R, et al. Particle size distribution of nascent soot in lightly and heavily sooting premixed ethylene flames. Combust Flame 2016;165:177–87.
 doi:10.1016/j.combustflame.2015.12.002.