### **Supporting information**

# Integrated CO<sub>2</sub> Capture and Conversion as an Efficient Process for Fuels from Greenhouse Gases

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#### Supplementary Text

#### Material characterization

Due to the hygroscopic nature of the material,  $Ca(OH)_2$  is also observed in the XRD patterns of the material after calcination (Figure2e). N<sub>2</sub> physisorption measurements (FigureS9) reveal that calcined limestone has a macro-porous morphology with a type III isotherm and H3 type hysteresis loop (IUPAC classification <sup>1</sup>), a BET surface area of 16 m<sup>2</sup>/g<sub>sorbent</sub> and a BJH pore volume and pore diameter of 0.13 cm<sup>3</sup>/g<sub>sorbnet</sub> and 38.2 nm, respectively.

Turning to the dry reforming catalyst, after reduction at 800 °C (the reduction temperature was determined by H<sub>2</sub>-TPR experiments, FigureS<sub>2</sub>), Ni/MgO-Al<sub>2</sub>O<sub>3</sub> (Figure<sub>2</sub>e) contains metallic nickel and periclase phases (MgO-Al<sub>2</sub>O<sub>3</sub>). The XRD data shows that the d(200) spacing of periclase in reduced DRM catalyst (2.093 Å) is smaller than that of the pure periclase reference, MgO, (2.102 Å), indicative that Al<sup>3+</sup> cations are incorporated into the periclase structure <sup>2</sup>. N<sub>2</sub> physisorption measurements show a type IV isotherm and a H<sub>2</sub> type hysteresis loop, indicating a mesoporous morphology (BET surface area and BJH pore volume was equal to 163 m<sup>2</sup>/g<sub>catalyst</sub> and 0.91 cm<sup>3</sup>/g<sub>catalyst</sub>, respectively). Using H<sub>2</sub> chemisorption, a Ni surface area of 10.3 m<sup>2</sup>·g<sub>cat</sub><sup>-1</sup> is determined.

#### Cyclic CO<sub>2</sub> capture performance of limestone-derived CaO as determined in a TGA

To rationalize the cyclic  $CO_2$  capture capacity measured in the fluidized bed (Figure4b), the cyclic  $CO_2$  uptake of limestone-derived CaO is also evaluated in a TGA at 720 °C. Although there are appreciable difference between a TGA and a fluidized bed e.g. with regards to mass transfer characteristics, we find that  $CO_2$  capacity of limestone-derived CaO as determined in a TGA is comparable to the results obtained in a fluidized bed. This observation indicates that for the given number of cycles, attrition is a minor contributor to the decreasing  $CO_2$  uptake of limestone.

#### Regeneration of CaCO3 coupled with DRM at 900 °C

We tests the regeneration of CaCO<sub>3</sub> under pure CH<sub>4</sub> stream at 900 °C after CO<sub>2</sub> capture at 720 °C. 3 g of pre-calcined limestone is used to avoid complete calcination of CaCO<sub>3</sub> before reaching at 900 °C. The CO<sub>2</sub> molar fraction was reached to 0.49 under N<sub>2</sub> (0.2 L/min) at 900 °C, albeit very short ( $\approx$  3 min) due to limited quantity of CaCO<sub>3</sub> (FigureS8a). The coupled CO<sub>2</sub> capture and conversion reactions at 900 °C using a mixture of 3.0 g limestone and 3.0 g Ni/MgO-Al<sub>2</sub>O<sub>3</sub> is performed (FigureS8b) under pure CH<sub>4</sub> (0.2 L/min). H<sub>2</sub> mole fraction is prominently high due to CH<sub>4</sub> decomposition (t = 25 – 31 min), where CO<sub>2</sub> released from CaCO<sub>3</sub> is completely converted CO and CO mole fraction was gradually increased in accordance with CO<sub>2</sub> release profile of CaCO<sub>3</sub> depending on temperature. Only H<sub>2</sub> and CO with 1.04 of H<sub>2</sub>/CO molar ratio is observed in pre-breakthrough at 900 °C (t = 30 – 33 min), indicative of full conversion of the CO<sub>2</sub> released

via the dry reforming of methane into a synthesis. In breakthrough, CO mole fraction is steadily reduced due to the quantity of  $CO_2$  released decreased, whereas  $H_2$  mole fraction is increased due to  $CH_4$  decomposition. In the post-breakthrough stage (t > 35 min), the concentration of  $CH_4$  increases due to catalyst poisoning by carbon deposition and the depletion of  $CaCO_3$ .

	H <sub>2</sub> chemisorption	N₂ physisorption <sup>b</sup>		
Catalyst	Ni active siteª [µmol <sub>Ni</sub> /g <sub>cat</sub> ]	S <sub>BET</sub> [m²/g <sub>cat</sub> ]	V <sub>p</sub> [cm³/gcat]	D <sub>p</sub> [nm]
Freshly reduced	262	163	0.91	5.2
1 <sup>st</sup> post-breakthrough	10	142	0.75	5.9
2 <sup>nd</sup> carbonation	255	158	0.88	5.7
10 <sup>th</sup> carbonation	210	155	0.87	5.9
10 <sup>th</sup> post-breakthrough	8	133	0.72	5.9

Table S1. Physicochemical properties of reacted Ni/MgO-Al<sub>2</sub>O<sub>3</sub> DRM catalyst

<sup>a</sup> Ni active sites quantified by  $H_2$  chemisorption using a stoichiometry factor of H/Ni = 1.0. <sup>b</sup>The specific surface area, pore volume, and pore radius were calculated using BET and BJH models.



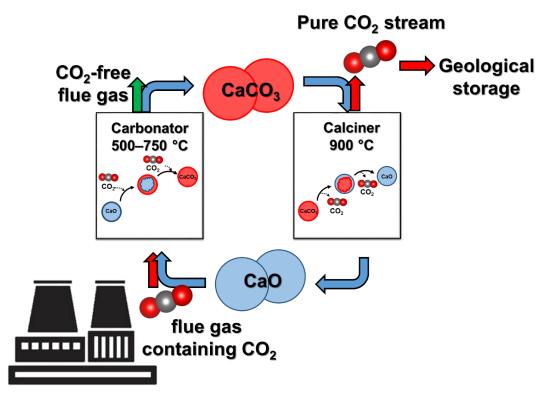


Figure S1. Schematic diagram of a conventional calcium looping based CO<sub>2</sub> capture process.

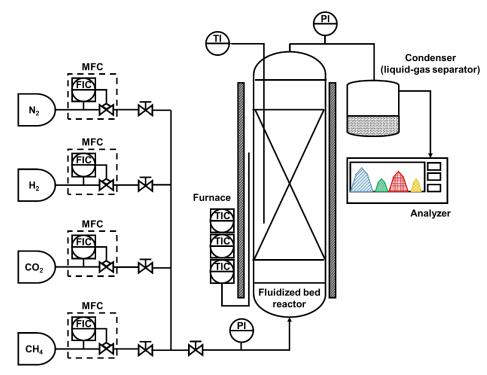
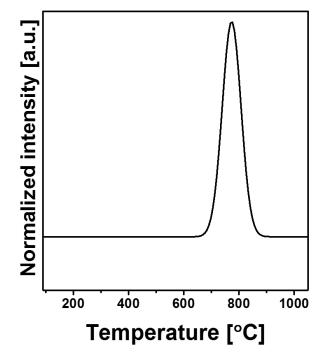


Figure S2. Schematic diagram of the fluidized bed setup.



**Figure S3.**  $H_2$ -TPR profile of Ni/MgO-Al<sub>2</sub>O<sub>3</sub>

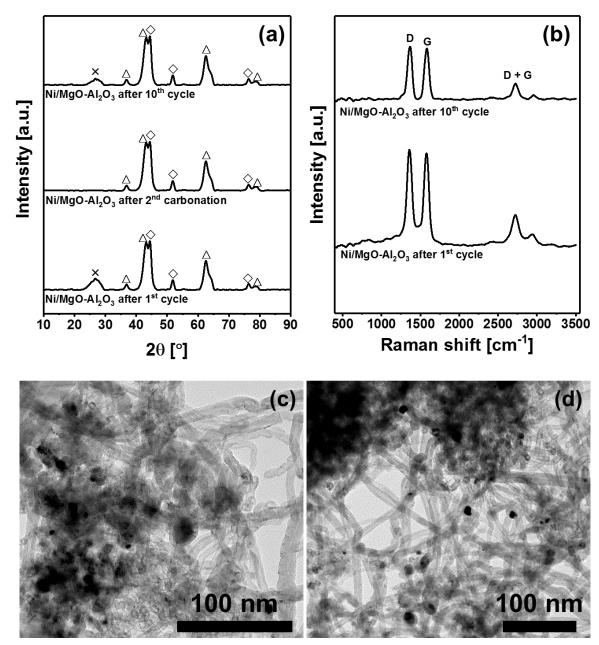
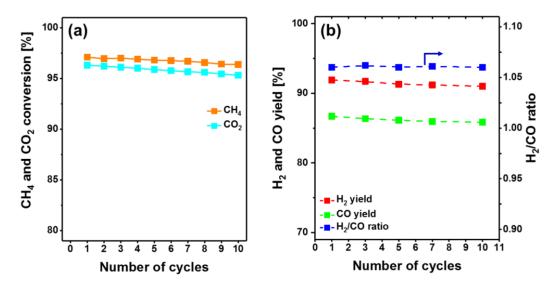
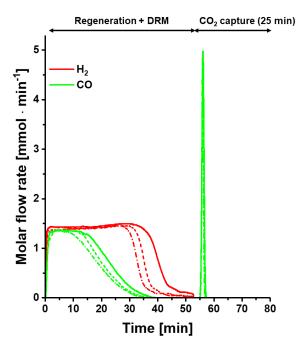


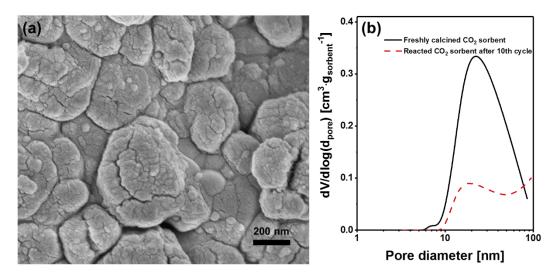
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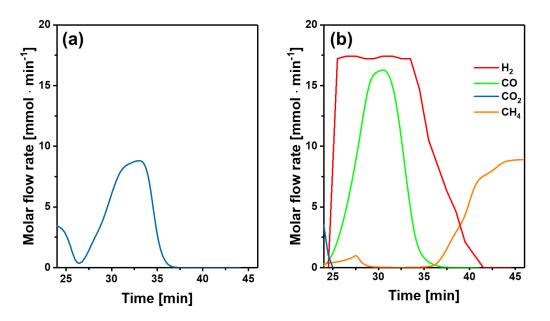
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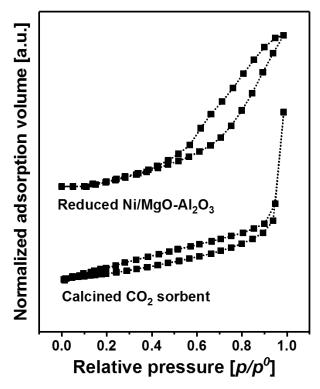
**Figure S6.** Molar flow rate of  $H_2$  and CO during  $CO_2$  conversion (DRM) and subsequent  $CO_2$  capture at different cycle numbers: (----)  $1^{st}$ , (---)  $5^{th}$  and (---)  $10^{th}$  cycle



**Figure S7.** Characterization of the reacted CO<sub>2</sub> sorbent: HR-SEM images of (a) reacted limestone after the 10<sup>th</sup> cycle (calcined form), and (b) BJH pore size distribution of the freshly calcined and reacted limestone.



**Figure S8.** (a)  $CO_2$  release profile for 3 g of limestone at 900 °C and (b) regeneration of limestone coupled with DRM reaction at 900 °C.



**Figure S9.** N<sub>2</sub> physisorption isotherms of calcined limestone and reduced Ni/MgO-Al<sub>2</sub>O<sub>3</sub>.

### References

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