## Supporting Information

# Reliable Manipulation of Gas Bubble Size on Superaerophilic Cones in Aqueous Media 

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## S1 The reasons why superhydrophobic $\mathrm{SiO}_{2}$ nanoparticles were chosen to modify the

## SCCs

There are many superhydrophilicity and superoleophobicity materials in aqueous media. In our manuscript, we have chosen a simple method by dip coating the mixture of hydrophobic fumed silica nanoparticles and poly(methyl methacrylate) (PMMA)/alcohol solution on SCCs. SCCs did not need any pre-or post-treatment. The hydrophobic $\mathrm{SiO}_{2}$ nanoparticles create both microscale and nanoscale roughness, and provide low surface energy. PMMA acts as the binder to adhesive $\mathrm{SiO}_{2}$ nanoparticles together. This method requires no further surface modification and can be applied to a variety of substrates over large areas. Furthermore, the proximity of roughness and thickness values is smaller than the 100 nm threshold. It will not change the shapes of SCCs.

## S2 The wettability of SCC interface

On the smooth silicon wafer with superhydrophobic $\mathrm{SiO}_{2}$ nanoparticle modification the water contact angle is $160.5 \pm 2.5^{\circ}$ and the gas contact angle approaches $0^{\circ}$. Only if the gas bubble radium $\left(\mathrm{R}_{\mathrm{b}}\right)$ is larger than $2 R_{s c c}\left(R_{s c c}\right.$, the curvature radius of the liquid-gas interface on SCCs), the gas bubble can be absorbed by the gas film on the SCC interface. That is to say, the gas bubble only can completely spread at the position where $\mathrm{R}_{\mathrm{b}}<2 R_{s c c}$. If the $\mathrm{R}_{\mathrm{b}}<2 R_{s c c}$, the gas bubble can sustain stability as a spherical crown shape on the SCC interface and then they are driven to the base side of SCCs under the gradient of Laplace pressure.


Figure S1. Wettability characterization of smooth silicon wafer with superhydrophobic $\mathrm{SiO}_{2}$ nanoparticle modification and SCCs: (a) the water contact angle is $160.5 \pm 2.5^{\circ}$ and (b) the
gas contact angle approaches $0^{\circ}$ on smooth silicon wafer with superhydrophobic $\mathrm{SiO}_{2}$ nanoparticle modification; (c) The wettability of air bubbles with the diameter much larger than that of a SCC.

## S3 The calculation of gas bubble volume



Figure S2. A gas bubble attached to the SCC interface can be regarded as an ellipsoid. Its volume can be calculated as: $V=4 / 3 \pi a^{2} b$.

## S4 The effect of SCC roughness on the gas bubble manipulation

We regulated the surface roughness by changed the quantity and diameters of $\mathrm{SiO}_{2}$ nanoparticles. Surface height maps and sample surface profiles of SCCs with different roughness are illustrated in Figure S 3 . The roughness of the SCC without $\mathrm{SiO}_{2}$ nanoparticle modification is 17.11 nm . If the SCCs modified with $\mathrm{SiO}_{2}$ nanoparticles, the type of surface texturing/particle aggregation created by the assembly of the mixed nanoparticle multilayers: submicrometer-sized aggregated nanoparticles with a raspberry-like nanometer-sized outer surface. The RMS roughness of the SCCs modified with different quantity and diameters of $\mathrm{SiO}_{2}$ nanoparticles is shown in Table S1. The RMS roughness on SCCs modified with [PMMA/(20 nm) $\left.\mathrm{SiO}_{2}(2.0)\right]$ chosen for gas bubble manipulation in our original manuscript is the largest ( 65.58 nm ).


Figure S3. AFM images of surfaces of multilayers consisting of: a) FAS, b) [PMMA/(20 $\left.\left.\mathrm{nm}) \mathrm{SiO}_{2}(2.0)\right] ; \mathrm{c}\right)\left[\mathrm{PMMA} /(20 \mathrm{~nm}) \mathrm{SiO}_{2}(3.0)\right] ;$ d) $\left[\mathrm{PHAC} /(20 \mathrm{~nm}) \mathrm{SiO}_{2}(1.0)\right]$.

When a gas bubble was injected to the copper cone that modified by fluoroalkylsilane $(1 \mathrm{H}, 1 \mathrm{H}$, $2 \mathrm{H}, 2 \mathrm{H}$-heptadecafluorodecyl trimethoxy silane, FAS), the gas bubble just adhered to its interface as a sphere shape. With coalescing with more bubbles, the gas bubble grew. If its buoyance force exceeds the Laplace pressure and the axis-direction component of hysteresis resistance force impeding the movement of bubbles, the gas bubble move upwards along the CC. If the gas bubble is large enough, it finally left the CC (Figure S4).

The surfaces roughness significantly influences the contact state between the SCCs and the aqueous media. The contact state summarizes not only the thickness and distribution of the trapped gas layer, but also the axis-direction component of hysteresis resistance force impeding the movement of bubbles $\left(\mathrm{F}_{\mathrm{H}}\right)$.

After investigating gas bubble behaviors on the SCCs with different roughness, we found that the SCC roughness can affect the movement of gas bubbles. With the decrease of SCC roughness, $\mathrm{F}_{\mathrm{H}}$ increased and it is difficult for gas bubble to move. At the same $\mathrm{L}_{\mathrm{b}}$ (the bubble's
balance position), the gas bubble volume at the SCC with small roughness is larger than that at SCC with large roughness. Correspondingly, the maximum volume $\mathrm{V}_{\text {max }}$ achieved at the SCC with small roughness is larger than that achieved at SCC with large roughness (Figure S5). The $\mathrm{SiO}_{2}$ nanoparticles on the SCC modified with $\mathrm{PMMA} /(20 \mathrm{~nm}) \mathrm{SiO}_{2}(3.0)$ are asymmetry. Thus, the gas bubble with small volumes can reach the middles part of the SCC. The maximum volume ( $V_{\max }$ ) achieved on the SCC (S-3) is smaller than that on SCCs (S-1 and S-2)

Table S1 The RMS roughness of the SCCs modified with FAS and different quantity and diameters of $\mathrm{SiO}_{2}$ nanoparticles

| No. | Nano Particle | Size/Diam eter (nm) | $\begin{gathered} \text { Quantity } \\ \left(\times 10^{-2} \mathrm{~g} / \mathrm{ml}\right) \end{gathered}$ | Polymer binder | RMS <br> Roughness(nm) |
| :---: | :---: | :---: | :---: | :---: | :---: |
| N-1 |  | - | - | - | 17.11 |
| Smooth |  |  |  |  |  |
| $\begin{gathered} \mathrm{S}-1 \\ {[\mathrm{PMMA} /(20} \\ \left.\mathrm{nm}) \mathrm{SiO}_{2}(2.0)\right] \end{gathered}$ | $\mathrm{SiO}_{2}$ (hydrophobic) <br> Aerosil R202 | 20 nm | 2 | PMMA | 65.577 |
| $\begin{gathered} \mathrm{S}-2 \\ {\left[\mathrm{PMMA}^{2} /(20\right.} \\ \left.\mathrm{nm}) \mathrm{SiO}_{2}(3.0)\right] \end{gathered}$ | $\mathrm{SiO}_{2}$ (hydrophobic) <br> Aerosil R202 | 20 nm | 3 | PMMA | 35.261 |
| $\begin{gathered} \mathrm{S}-3 \\ {\left[\mathrm{PHAC}^{2}(20\right.} \\ \left.\mathrm{nm}) \mathrm{SiO}_{2}(1.0)\right] \end{gathered}$ | $\mathrm{SiO}_{2}$ (hydrophobic) <br> Aerosil R202 | 20nm | 1 | PHAC | 31.28 |



Figure S4. Dynamic balance of gas bubbles on FAS-CC interface.


Figure S5. Variation of gas bubble volume at different balance position ( $\mathbf{L}_{b}$ ) on the SCCs with different roughness

## S5 The calculation of the relation between $L_{b}$ and $V$



Figure S6. Schematic illustration of the relationship between the apex angle of cone ( $2 \alpha$ ), the balance position $\left(\mathrm{L}_{\mathrm{b}}\right)$, and the local radii at the two opposite sides of the gas bubble ( $R_{1}$ and $R_{2}$ ).

The part of the SCC encapsulated by the gas bubble can be considered as a truncated cone. $R_{2}$ is radius of base circle; $R_{l}$ is radius of top circle; $x$ is height or distance between the centers of
the base and the top circles; $l$ is apothem or distance between any two closest points on the base and the top circles; $L_{b}+1 / 2 x$ is distance between the center of the base circle and the imaginary point that connects all apothems.

$$
\begin{aligned}
& \square \tan \alpha=\frac{R_{1}}{L_{b}-\frac{1}{2} x}=\frac{R_{2}}{L_{b}+\frac{1}{2} x} \\
& \therefore R_{1}\left(L_{b}+\frac{1}{2} x\right)=R_{2}\left(L_{b}-\frac{1}{2} x\right) \\
& R_{1} L_{b}+\frac{1}{2} R_{1} x=R_{1} L_{b}+\frac{1}{2} R_{1} x \\
& \frac{1}{2} x\left(R_{1}+R_{2}\right)=\left(R_{2}-R_{1}\right) L_{b} \\
& \therefore x=\frac{2\left(R_{2}-R_{1}\right) L_{b}}{\left(R_{1}+R_{2}\right)} \\
& I=\sqrt{\left(L_{b}+\frac{1}{2} x\right)^{2}+R_{2}^{2}}-\sqrt{\left(L_{b}-\frac{1}{2} x\right)^{2}+R_{1}^{2}} \\
& =\sqrt{\left[L_{b}+\frac{\left(R_{2}-R_{1}\right) L_{b}}{R_{1}+R_{2}}\right]^{2}}+R_{2}^{2}-\sqrt{\left[L_{b}-\frac{\left(R_{2}-R_{1}\right) L_{B}}{R_{1}+R_{2}}\right]^{2}+R_{1}^{2}} \\
& =\sqrt{L_{b}^{2}\left(\frac{R_{1}+R_{2}+R_{2}-R_{1}}{R_{1}+R_{2}}\right)^{2}+R_{2}^{2}-\sqrt{L_{b}^{2}\left(\frac{R_{1}+R_{2}-R_{2}+R_{1}}{R_{1}+R_{2}}\right)^{2}}+R_{1}^{2}} \\
& =\sqrt{L_{b}^{2}\left(\frac{2 R_{2}}{R_{1}+R_{2}}\right)^{2}+R_{2}^{2}}-\sqrt{L_{b}^{2}\left(\frac{2 R_{1}}{R_{1}+R_{2}}\right)^{2}+R_{1}^{2}} \\
& =R_{2} \sqrt{\frac{4 L_{b}^{2}}{\left(R_{1}+R_{2}\right)^{2}+1}-R_{1}} \sqrt{\frac{4 L_{b}^{2}}{\left(R_{1}+R_{2}\right)^{2}}+1} \\
& =\left(R_{2}-R_{1}\right) \sqrt{4 L_{b}^{2}}\left(R_{1}+R_{2}\right)^{2} \\
& S=\pi I\left(R_{1}+R_{2}\right)
\end{aligned}
$$

$$
\begin{aligned}
& F_{L}=2 \gamma\left(\frac{1}{R_{\mathrm{T}}}-\frac{1}{R_{2}}\right) S \sin \alpha \\
& =\frac{2 \gamma\left(R_{2}-R_{1}\right)}{R_{1} R_{2}} \pi l\left(R_{2}+R_{1}\right) \sin \alpha \\
& =\frac{2 \gamma\left(R_{2}-R_{1}\right)}{R_{1} R_{2}} \pi\left(R_{2}-R_{1}\right) \sqrt{\frac{4 L_{b}{ }^{2}}{\left(R_{1}+R_{2}\right)^{2}}+1}\left(R_{2}+R_{1}\right) \sin \alpha \\
& =\frac{2 \pi \gamma\left(R_{2}-R_{1}\right)^{2}}{R_{1} R_{2}} \sin \alpha \sqrt{4 L_{b}{ }^{2}+\left(R_{1}+R_{2}\right)^{2}} \\
& =\rho V g \sin \beta-\pi \gamma\left(\cos \theta_{r}-\cos \theta_{a}\right) \cos \alpha\left(\frac{3 V}{4 \pi}\right)^{\frac{1}{3}} \\
& =F_{B}-F_{H} \\
& \therefore \sqrt{4 L_{b}^{2}+\left(R_{1}+R_{2}\right)^{2}}=\frac{-\rho V \sin \beta R_{1} R_{2}}{2 \pi \gamma \sin \alpha\left(R_{2}-R_{1}\right)^{2}} \\
& 4 L_{b}{ }^{2}=\left(\frac{\rho V g \sin \beta-\pi \gamma\left(\cos \theta_{r}-\cos \theta_{a}\right) \cos \alpha\left(\frac{3 V}{4 \pi}\right)^{\frac{1}{3}}}{2 \pi \lambda \sin \alpha\left(R_{2}-R_{1}\right)^{2}}\right)^{2} R_{1}^{2} R_{2}^{2}-\left(R_{1}+R_{2}\right)^{2} \\
& L_{b}^{2}=\left[\frac{\rho V g \sin \beta-\pi \lambda\left(\cos \theta_{r}-\cos \theta_{a}\right) \cos \alpha\left(\frac{3 V}{4 \pi}\right)^{\frac{1}{3}}}{4 \pi \lambda \sin \alpha\left(R_{2}-R_{1}\right)^{2}}\right]^{2} R_{1}^{2} R_{2}^{2}-\frac{1}{4}\left(R_{1}+R_{2}\right)^{2}
\end{aligned}
$$

## S6 The effect of salt on the gas bubble manipulation

The salt in the aqueous media will significantly change the surface tension. We have investigated the contribution of the salt in the bubble size in the NaCl solution with two concentrations ( 2.7 and $5.4 \mathrm{~mol} / \mathrm{L}$ ). According to the excess pressure formula on free gas bubbles, the bubble size in the NaCl solution is smaller than that in water resulting from their increased surface tension. Furthermore, the surfaces tension significantly influences the contact state between the SCCs and the aqueous media. The contact state summarizes not only the thickness and distribution of the trapped gas layer, but also $\mathrm{F}_{\mathrm{H}}$ and $\mathrm{F}_{\mathrm{L}}$.

In order to investigate the contribution of the salt in the bubble manuscript, we used the SCC with apex angles of $3^{\circ}$, which are the most sensitive to the change of gas bubble volume, as shown in Figure S 7 . With increasing of surface tension, $\mathrm{F}_{\mathrm{H}}$ increased a bit. It impeded the
movement of gas bubble. Thus, at high $\mathrm{L}_{\mathrm{b}}$ (the position closed to the base side of the SCC), V in NaCl solution with concentration of $5.4 \mathrm{~mol} / \mathrm{L}$ is larger than that in the water and in NaCl solution with concentration of $2.7 \mathrm{~mol} / \mathrm{L}$. With the decrease of $\mathrm{L}_{\mathrm{b}}$ (the position closed to the top side of the SCC ), V is similar in water and NaCl solution.


Figure S7. Variation of gas bubble volume at different balance position $\left(\mathrm{L}_{\mathrm{b}}\right)$ in water and NaCl solutions.

S7 The relationship between $L_{b}$ and outside pressure when the pressure were cycled multiple times in water and NaCl solution

When the pressure were cycled (i.e., decreasing and increasing) multiple times in water, $\mathrm{L}_{\mathrm{b}}$ varies with increasing and decreasing of outside pressure; however, it is not same at the same outside pressure in each cycle (Figure S8 ). At first cycle, $\mathrm{L}_{\mathrm{b}}$ decreased with the decrease of $\mathrm{P}_{\text {out }}$ due to the increase of the gas bubble volume. When the Pout decreased to $-7.5 \mathrm{psi}, \mathrm{L}_{\mathrm{b}}$ reached minimum value. Increasing the Pout, the volume of gas bubble decreased and the gas bubble started to move downwards only if the gas bubble is small enough, and $L_{b}$ increased. When the first cycle finished, i.e., the outside pressure turned back to initial pressure (the atmospheric pressure), $\mathrm{L}_{\mathrm{b}}$ reached the maximum value $\left(\mathrm{L}_{\mathrm{b} 1}\right)$ in the first cycle, and it cannot come back to the original position $\left(\mathrm{L}_{\mathrm{b} 0}\right)$. At second cycle, $\mathrm{L}_{\mathrm{b}}$ changed from the starting point Lb 1 , the variation of $\mathrm{L}_{\mathrm{b}}$ is similar as the first one. Furthermore, at the fifth cycle, the gas bubble cannot move
downwards with the increasing of Pout.
When the outside pressure decreased, water started to evaporate at water-air interfaces. With decreasing of the outside pressure, the volume of water vapor increased. Water vapor entered into not only the gas bubble but also the gas layer. When the Pout increased, water vapor in the gas bubble cannot completely condense to water. Thus, after the first cycle, the volume of gas bubble grew a bit larger. Furthermore, when the water vapor that entered into gas layer, the hysteresis resistance force increased to impede the movement of gas bubble. Correspondingly, after the first cycle, $\mathrm{L}_{\mathrm{b}}$ cannot come back to the original position ( $\mathrm{L}_{\mathrm{b} 0}$ ). Similarly, if we repeated the decreasing and increasing Pout, the volume of gas bubble increased a bit, and $\mathrm{F}_{\mathrm{H}}$ increased a lot. At the fifth cycle, the gas bubble cannot move downwards with the increasing of $\mathrm{P}_{\text {out }}$ and $\mathrm{L}_{\mathrm{b}}$ did not changed.

In order to eliminate the effect of water vapor on gas bubble volumes, we investigated the dynamic balance cycles of single gas bubble on SCC interface in $5.4 \mathrm{~mol} / \mathrm{L} \mathrm{NaCl}$ solution. At the first cycle, $\mathrm{L}_{\mathrm{b}}$ decreased with the decrease of $\mathrm{P}_{\text {out }}$ due to the increase of the gas bubble volume. When the $\mathrm{P}_{\text {out }}$ decreased to $-6.0 \mathrm{psi}, \mathrm{L}_{\mathrm{b}}$ reached the first local minimum value. Increasing the $\mathrm{P}_{\text {out }}$, the volume of gas bubble decreased, however, the gas bubble didn't move downwards. When the first cycle finished, i.e., the outside pressure turned back to initial pressure (the atmospheric pressure), $\mathrm{L}_{\mathrm{b}}$ still kept at the same position $\left(\mathrm{L}_{\mathrm{b} 1}\right)$. At the second cycle, $\mathrm{L}_{\mathrm{b}}$ changed from the starting point $\mathrm{L}_{\mathrm{b} 1} . \mathrm{Lb}$ decreased with the decreasing of Pout. After $\mathrm{L}_{\mathrm{b}}$ dropped to the second local minimum value $\left(\mathrm{L}_{\mathrm{b} 2}\right), \mathrm{Lb}$ increased with the increasing of Pout. Similarly, $\mathrm{L}_{\mathrm{b}}$ cannot reach the original position of the second cycle $\left(\mathrm{L}_{\mathrm{b} 2}<\mathrm{L}_{\mathrm{b} 1}\right)$. At the third and fourth cycles, the gas bubble moved downwards little with the increasing of $\mathrm{P}_{\text {out }}$.


Figure S8. Dynamic balance cycles of single gas bubble on SCC interface in water and in NaCl solution with concentration of $5.4 \mathrm{~mol} / \mathrm{L}$. Cycle $1,2,3,4$ and 5 : decreasing processes of $\mathrm{P}_{\text {out }}$; Cycle $1^{\prime}, 2^{\prime}, 3^{\prime}, 4^{\prime}$ and $5^{\prime}$ : increasing processes of $\mathrm{P}_{\text {out }}$.

Video 1: Dynamic balance process of one gas bubble released at tip side of SCC.
Video 2: Dynamic balance process of one gas bubble released at base side of SCC.
Video 3: Dynamic balance process of one gas bubble merging with another gas bubble on SCC interface.

Video 4: Maximum volume of gas bubble held on the tip side of SCC.

Video 5: The change of gas bubble's position on SCC interface when decreasing system pressure.

